

1796 5 23.6 +3314 Ag -8.76

3521

CC

7.11 415

1759

5

227

~10

22

505

+56.68

35536

①

5.67 + 1.48 + 1.85

①

5.81 + 4.95

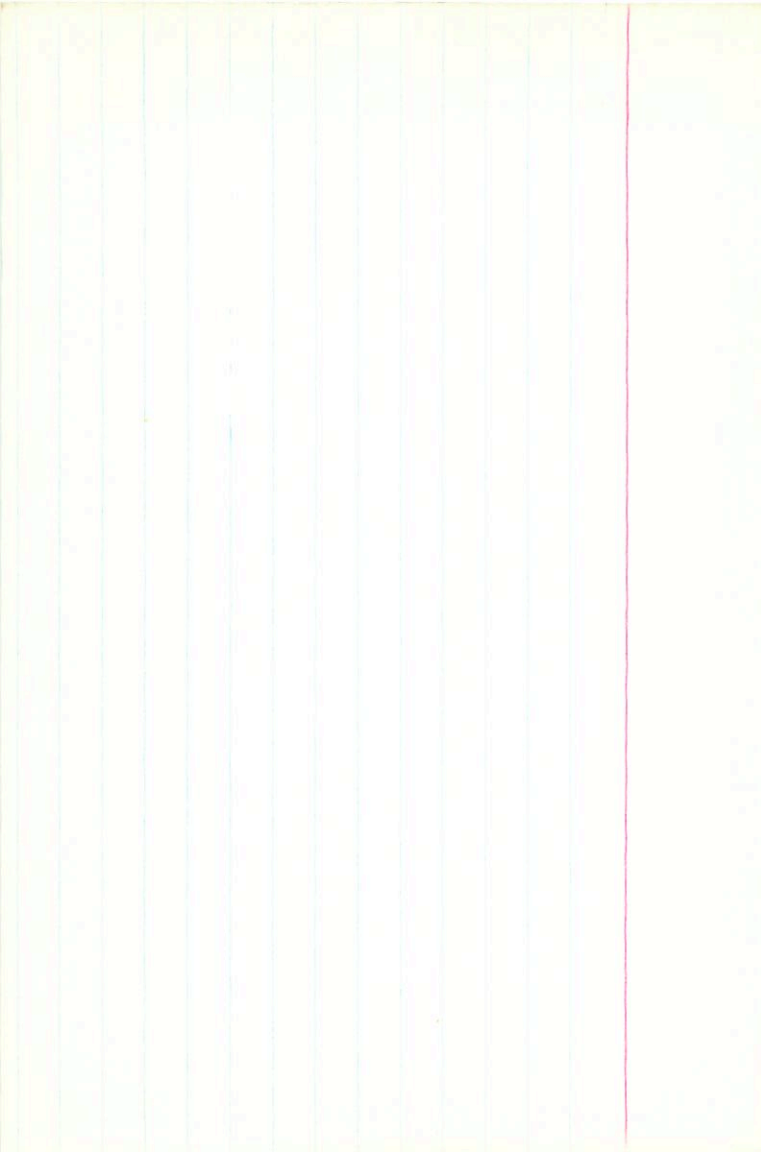
5.60 + 1.54 + 1.89

②

66 ± 2.0

-60075 - 6185

4.83 + 0.635 (2)



17km

302 22

1802 5 2T4 +63 01 gml -18.5 f

35593

5.44 +170 +2.02 (2)

4.16 +0.935 (3)

4.45 +0.90 (1)

-00048-0024 FHY

Q Am

1905

5 243

35620

5.10

+1.39

+1.64

(3)

544 ± 20

4.43

70.50

2A

-0002 -0472

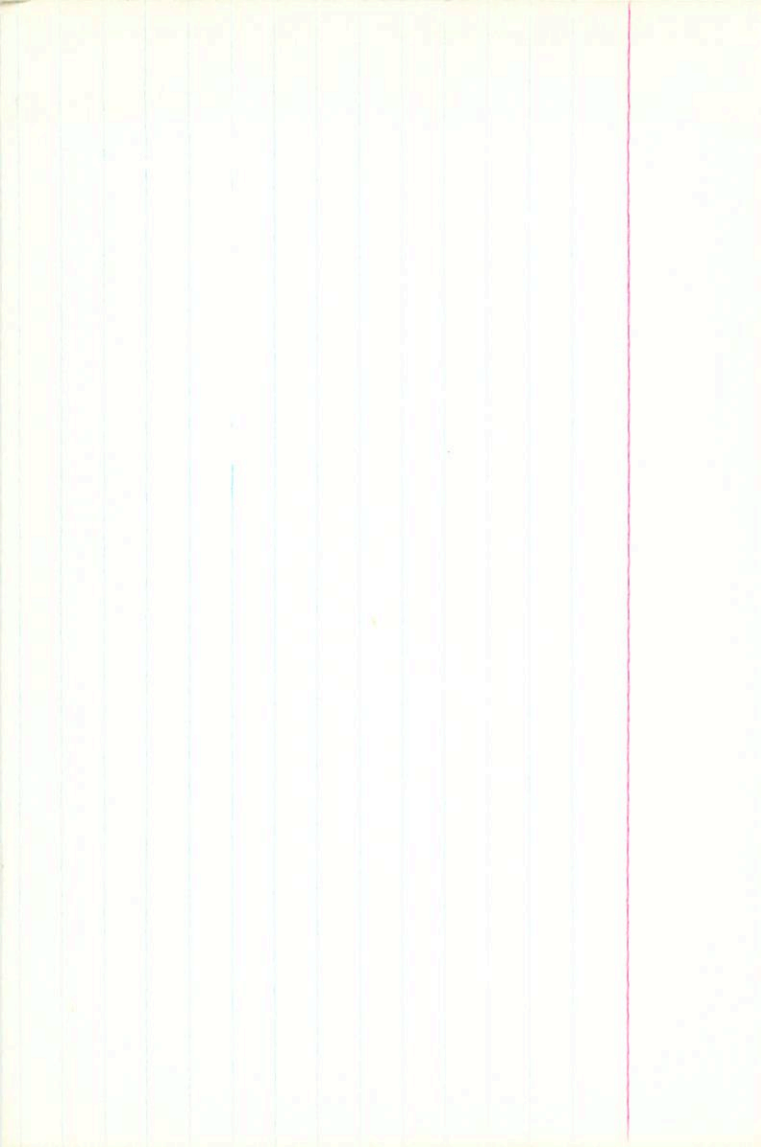
+31.0

734 26 103 p

Age used
Standard of Thompson

1813 5 23.5 -44 17 100 -

35265 6.08 7.20 (2.24) 6 02



394 710 -
3.44
10-0

1816 5 25.1 417 12 gm1 -2334

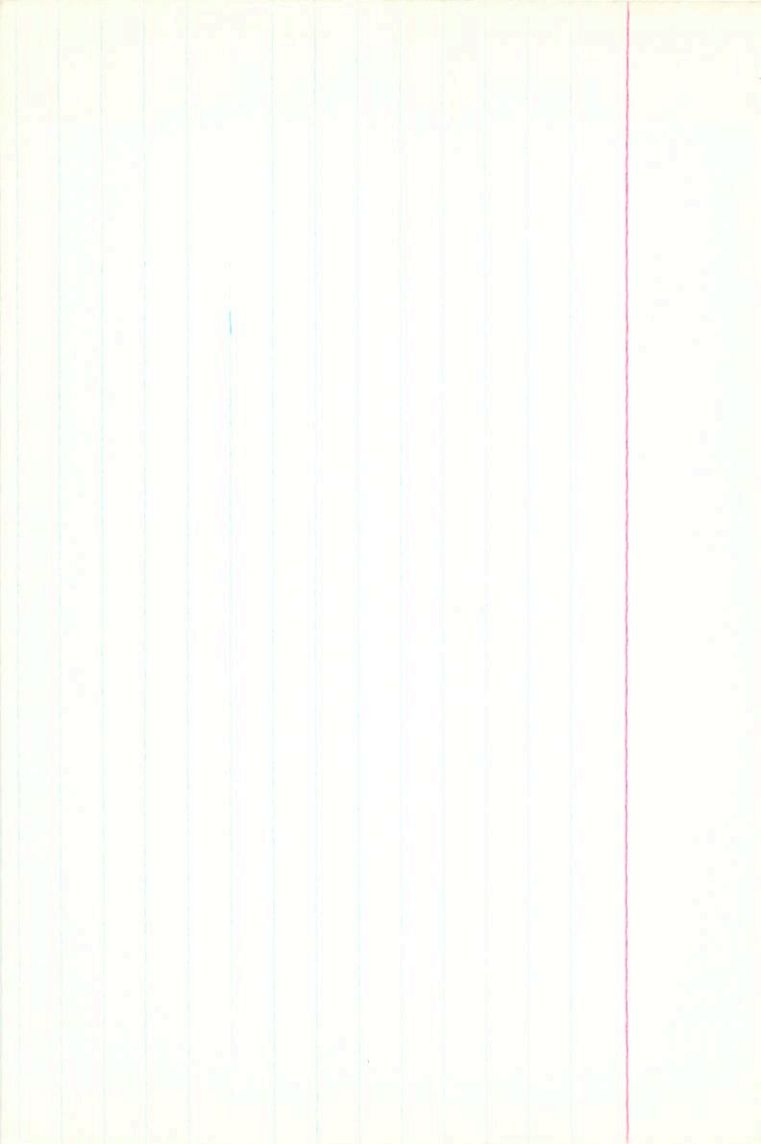
35562

5.78 + 1.58 + 2.00 (4)

4.74 + 0.80 (3)

~~4.74~~ + 0.74 (2)

6-6 = 30
+ 6013 - 050



1823

5 255

-21

26

g 67

+33.9 f

35991

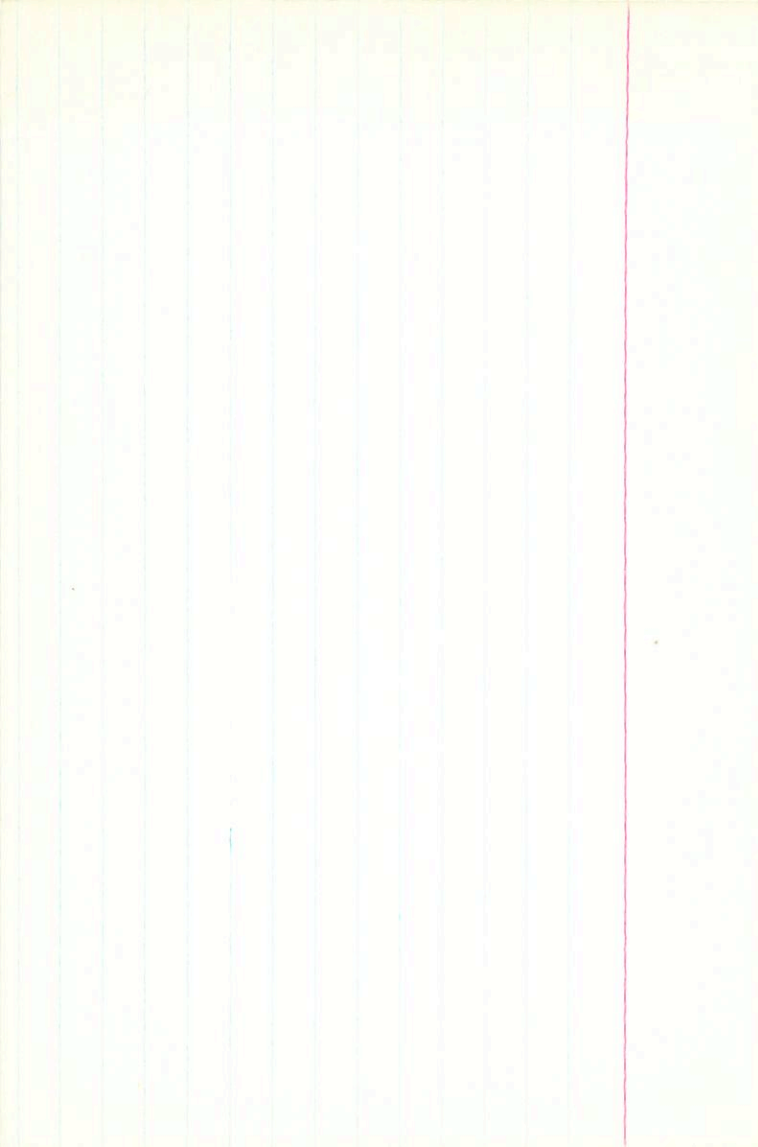
6.06 + 1.04 ~ C

6.10 + 1.03 + 0.86 ①

5.64 + 0.35 ①

N30 ± 6.0

+0009 + 0.315



24150*

1824

5 27.4 44 25 144

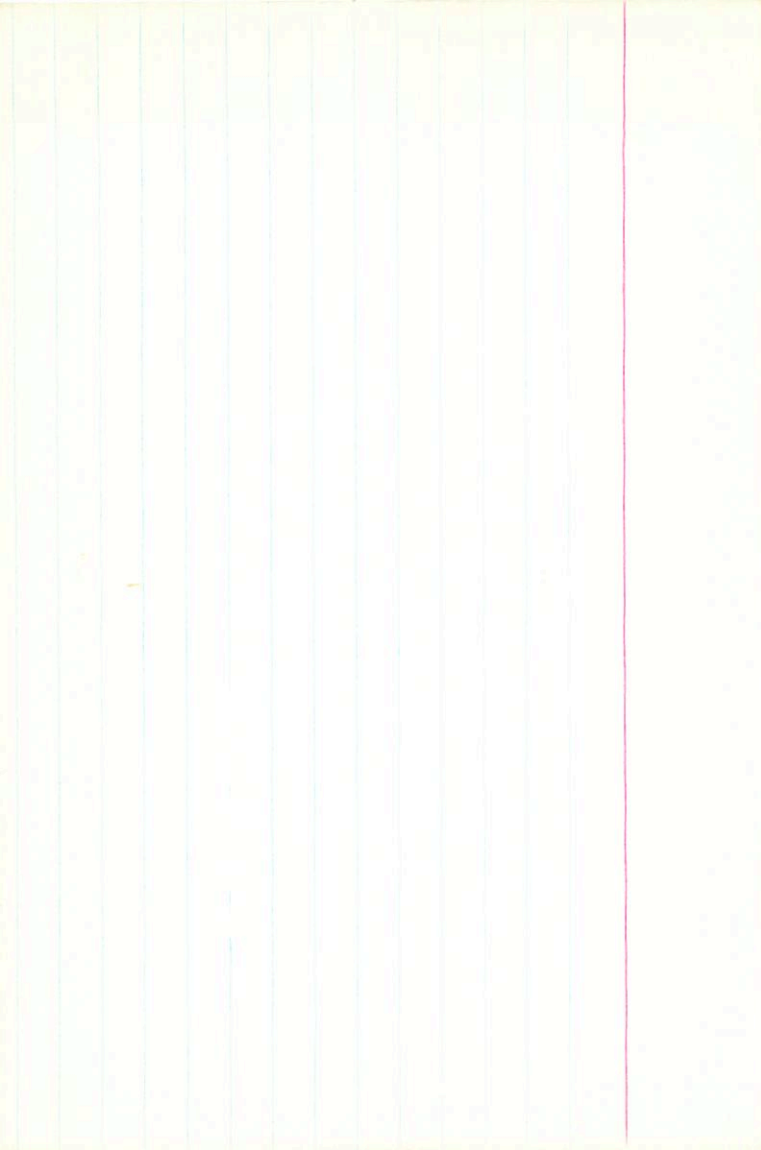
120P +1414

36040

5.54+110+1.110

New position

$\frac{5.54}{5.54} = 3.5$
0000-0372



1830 5 26.9 -J 30 g 68 +23.16

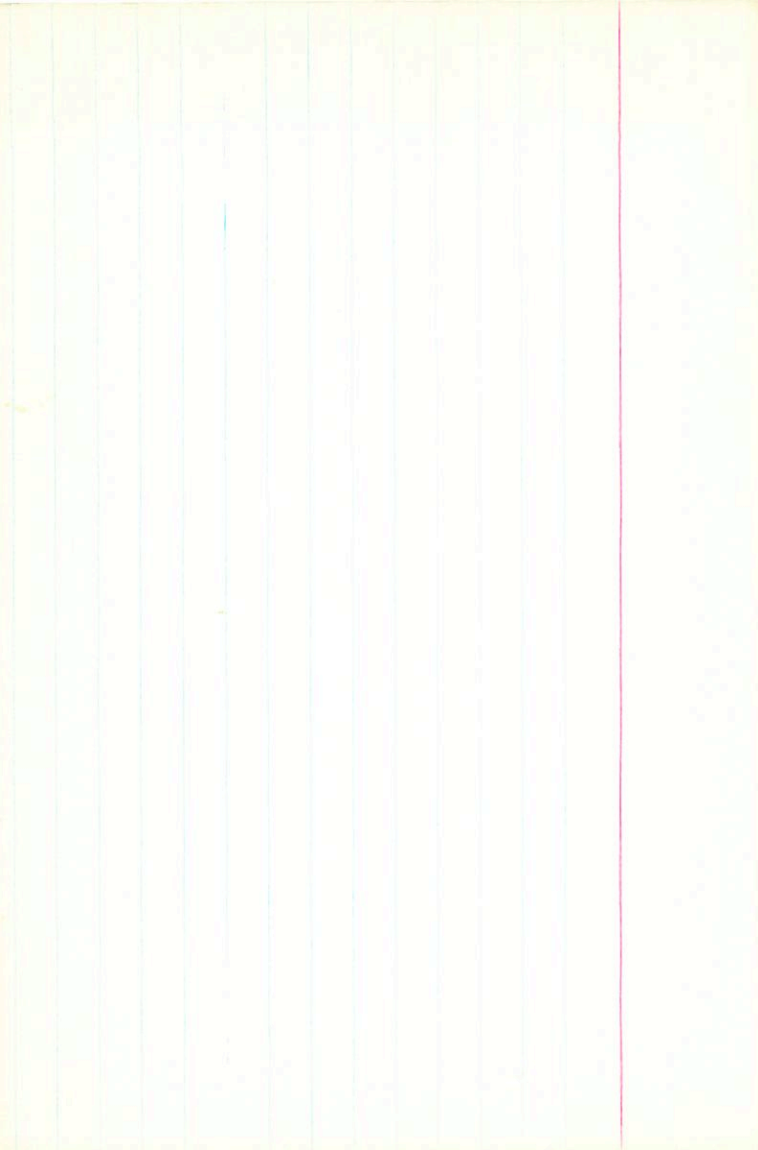
36134

590 +11.5 +1.07C

GC ±6.0

- 0021 -0075

Neurospora?



1831

5

277

+22 25

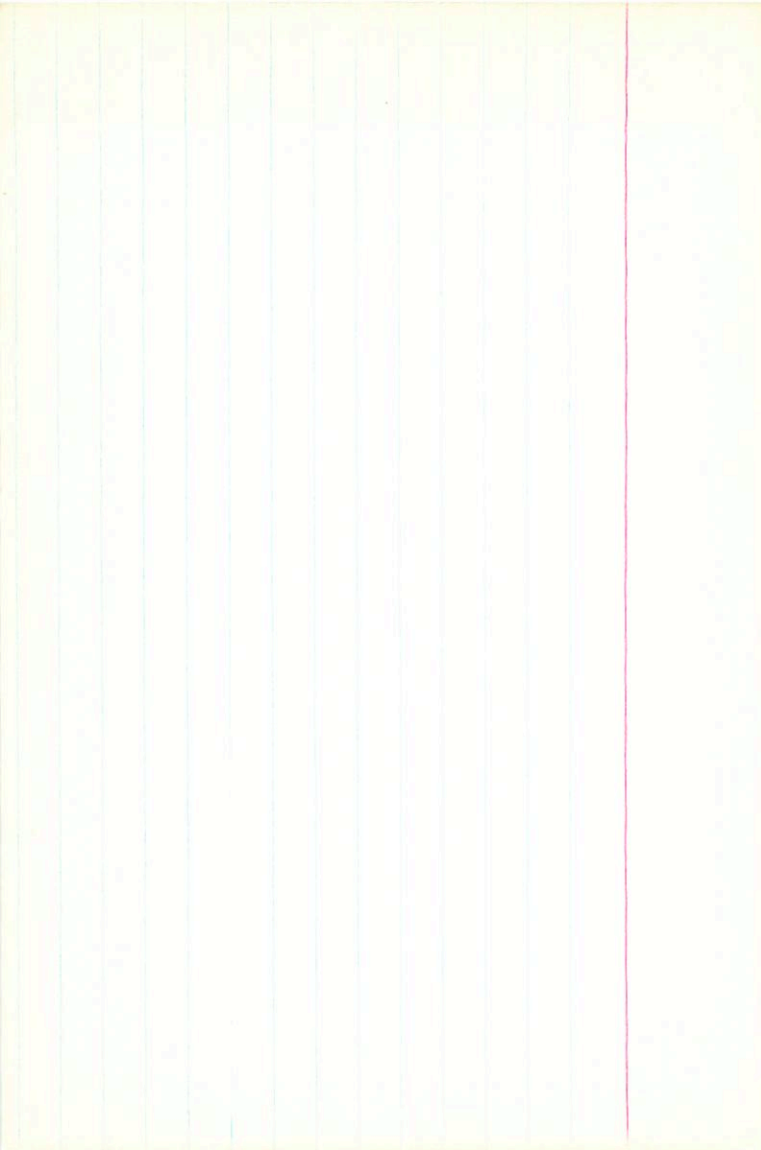
150

+1.77

36160

6.200-118-615

BL



7 Jan

1836

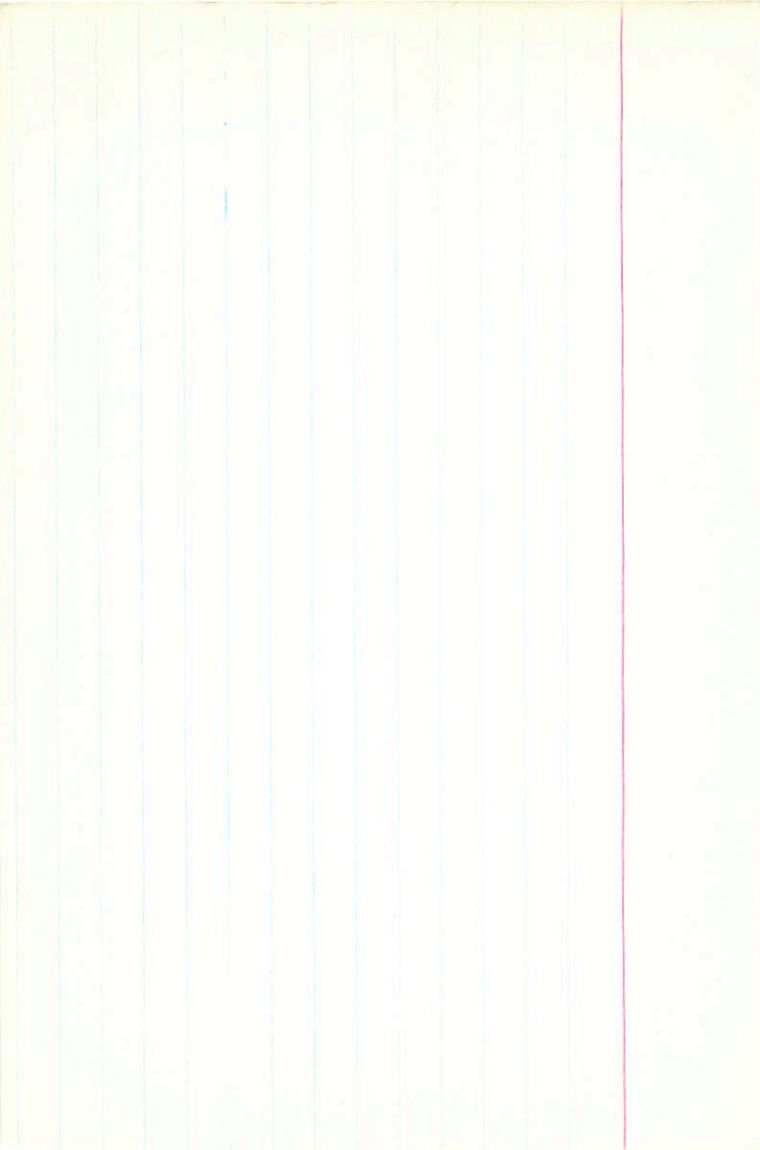
5 25/6 -58 58 G5 +10.00

26149

5.13 +0.99 - C

G2 ± 5.0

-00155 +034



CIR Di Motion

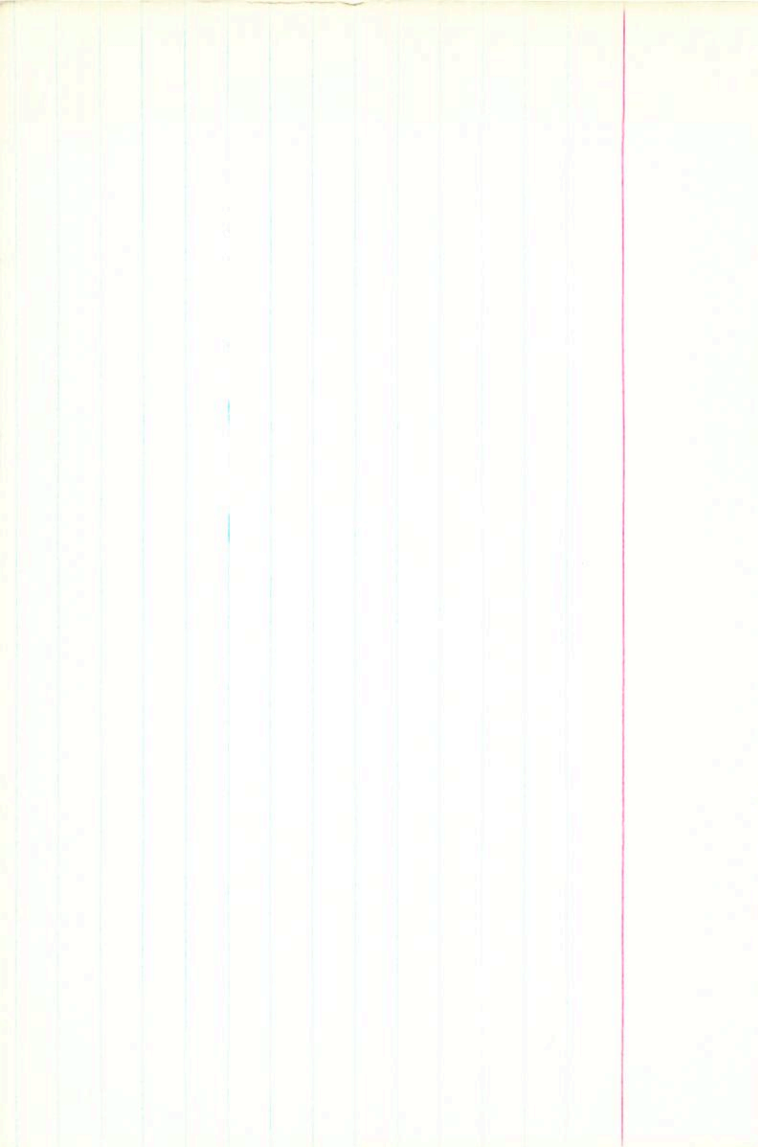
1837 5 27.7 +5 20 R277 +15.0

CIR Di

36217

6.21 +127 +1.35 C

GC



1844

5

33.0

+75.01

gms

-3.2

36344

6.14 + 1.595 + 19.55 (2)

2.2

5.16 + 0.80 (1)

201 384

1866 5 32.5 +54 24 gmo +0.58

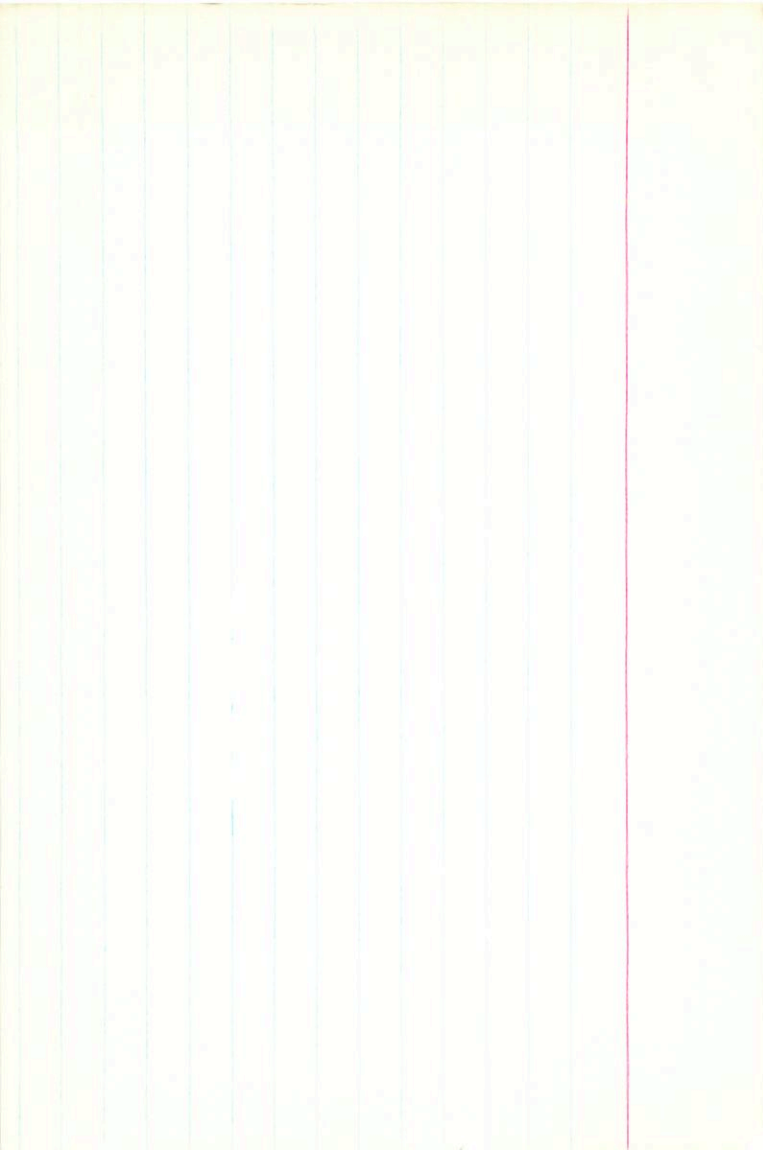
3667A

5.64 + 16.3 + 158 (2)

46.4 + 0.805 (2) 10265

66

4.23 + 0.74 (1) (4)



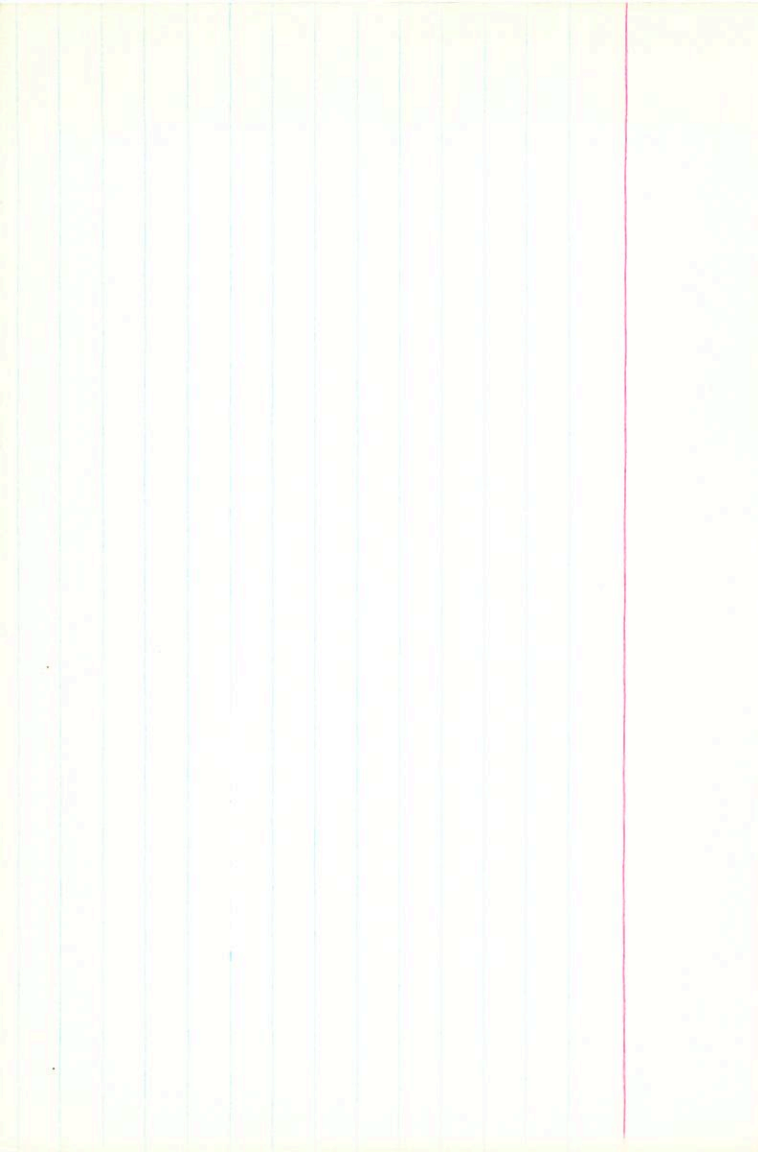
5.04 476
20

1870 5 30.2 -45 59 102 -

36734

5.85 + 1.35 - C AC

5.27 + 0.515 ⊕



1874 5 31.5 -1 30 120 +9148.15t

h281

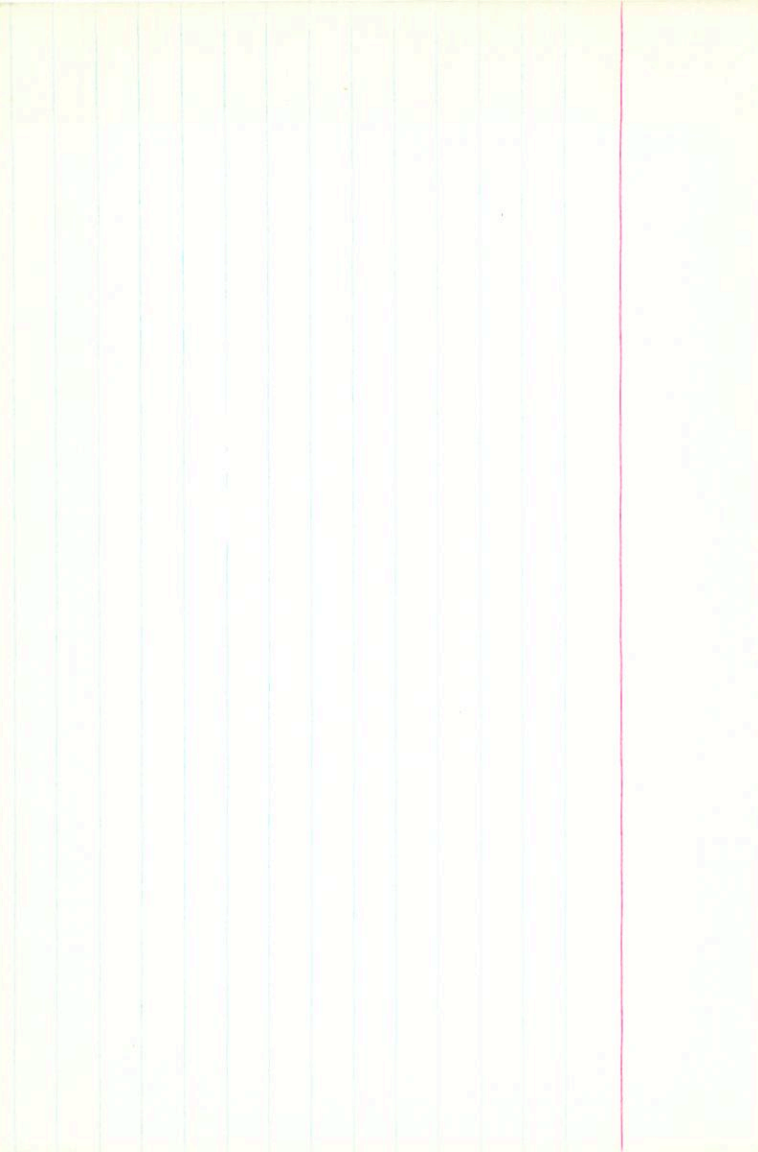
26292

5-52+1.54+1.876

5.56+1.60+1.520 slabs

0-6

5.01+0.665 (2)



4.85 452

1977 5 312 -38 83 102 -0.6a

2698

$$5.47 + 1.22 = C$$

$$5.46 + 1.23 (1.33) C$$

$$5.56 + 1.19 + 1.05 (1)$$

$$\underline{5.49 + 1.22 + 1.84 (2)}$$

$$7.94 + 0.425 (2)$$

0.6

step 1

1881

5

31.4

-

3

5

10

120

+15.4

5.31 497

36874

5.80

+1.06

+0.58

①

6.76

+1.06

+1.02

6

5.37 +0.39

②

5.78

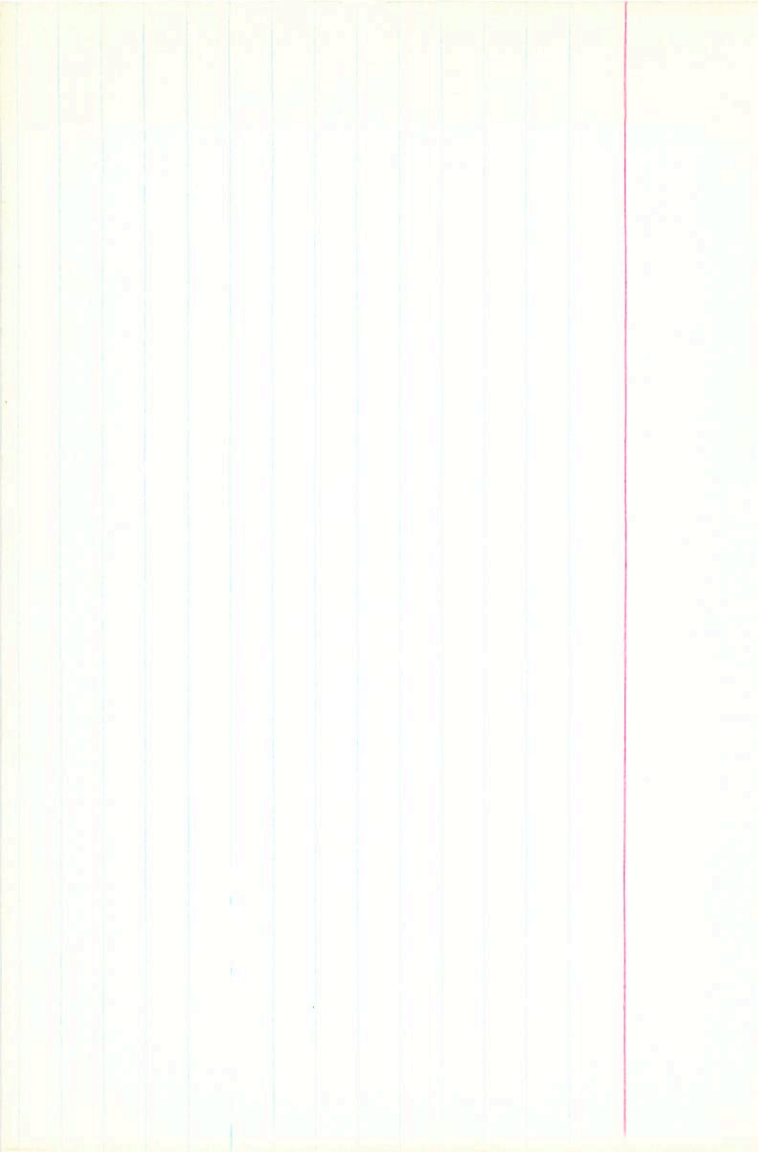
+1.01

+1.00

②

240

Strong



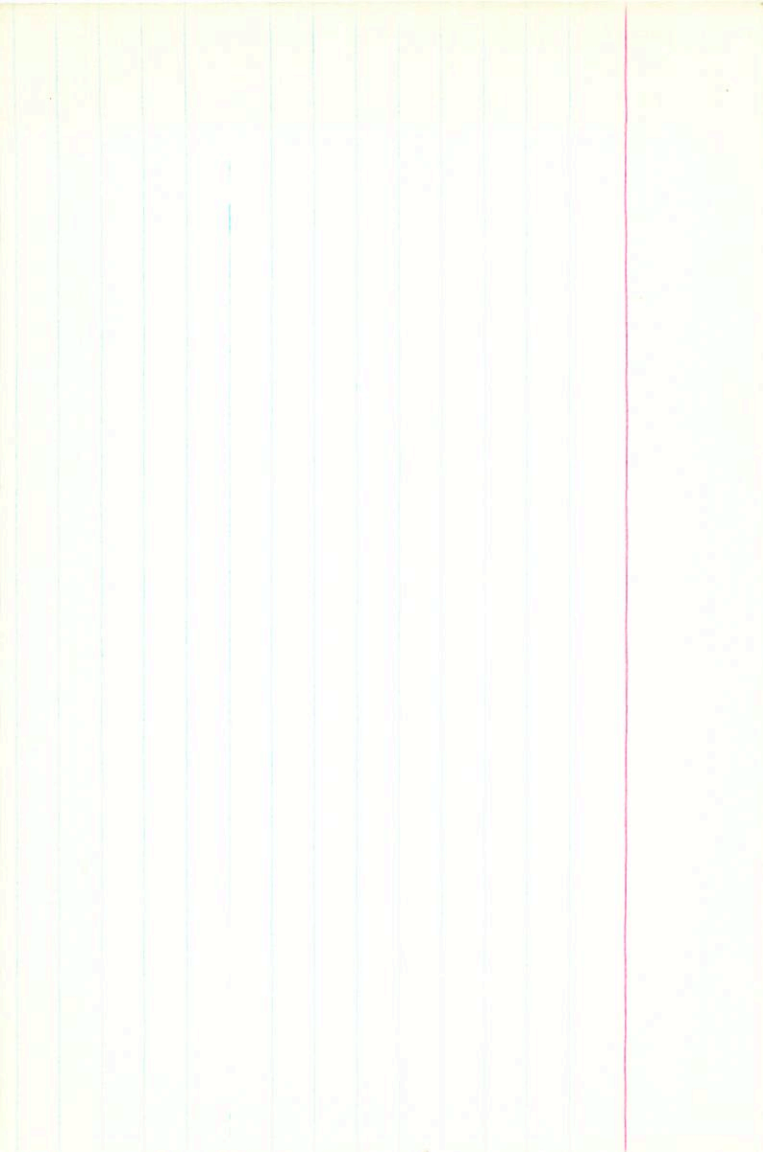
1884

5 33.4 +40 09 63IF -18.26

36841

6.08+103+0.69 A

66



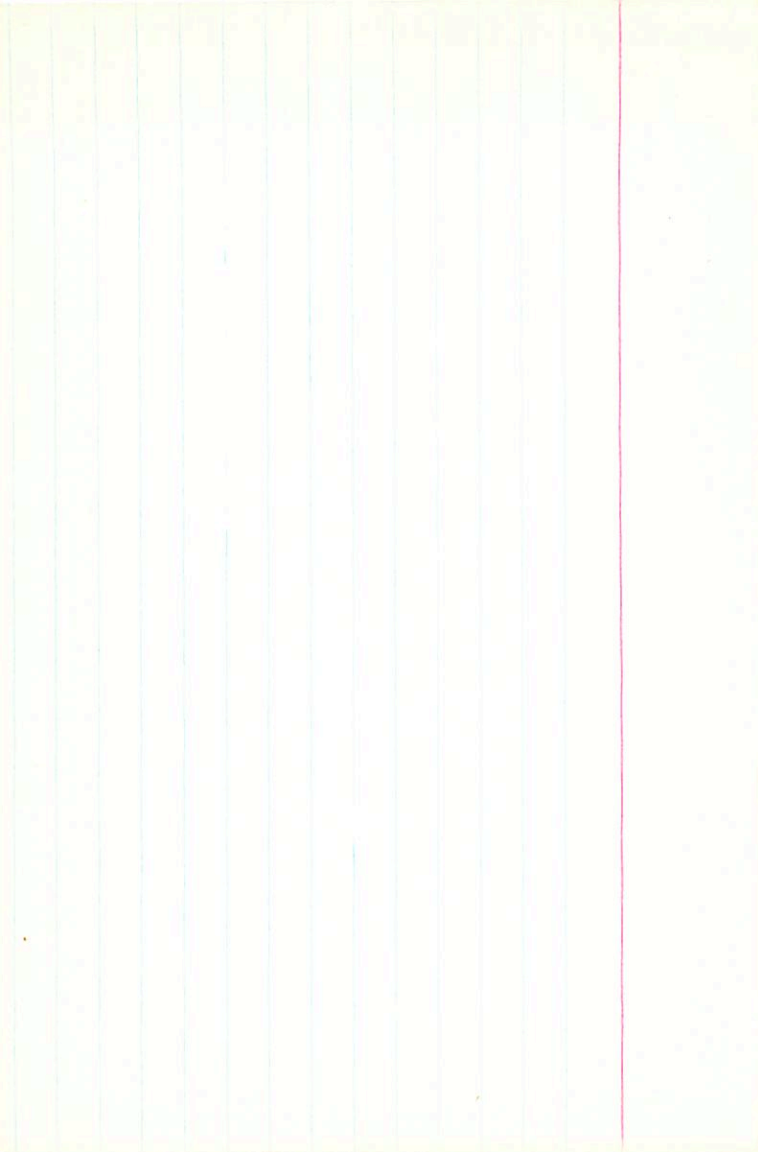
1888

S 45.6 + 85 10 gmo - 45.56 -

36905

6.10 + 1.565 + 1.500 \rightarrow + 0.1266 + 0.04 Fx4

5.14 + 0.6550



1908

5 343

+11 60

125

III

-110

342

~~6~~

3701

6.05

+1.60

+1.81

①

5.90

+1.60

+1.93

2A

N80 ± 6.0

5.01 + 0.645 ①

+00315 -011

17000
1900
82160

5 342 + 9 16 6817

1909

5

33.4

-33

7

100

+440

37192

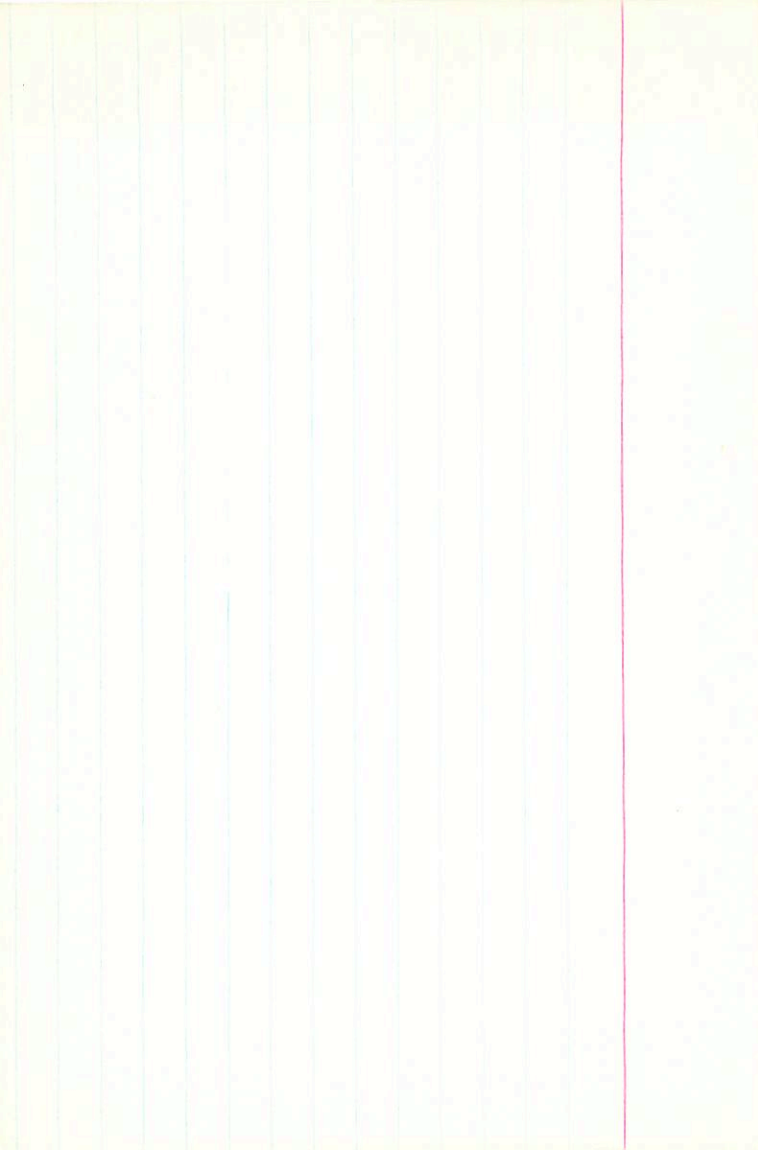
5.77 + 1.12 (2.20) 6

5.77 + 1.11 + 1.015 ①

5.28 + 0.345 ⑤

stay

+0023 +110



26 Aug

1914

5 354 +80 28 +1.76

37269

G-L ± 2.5

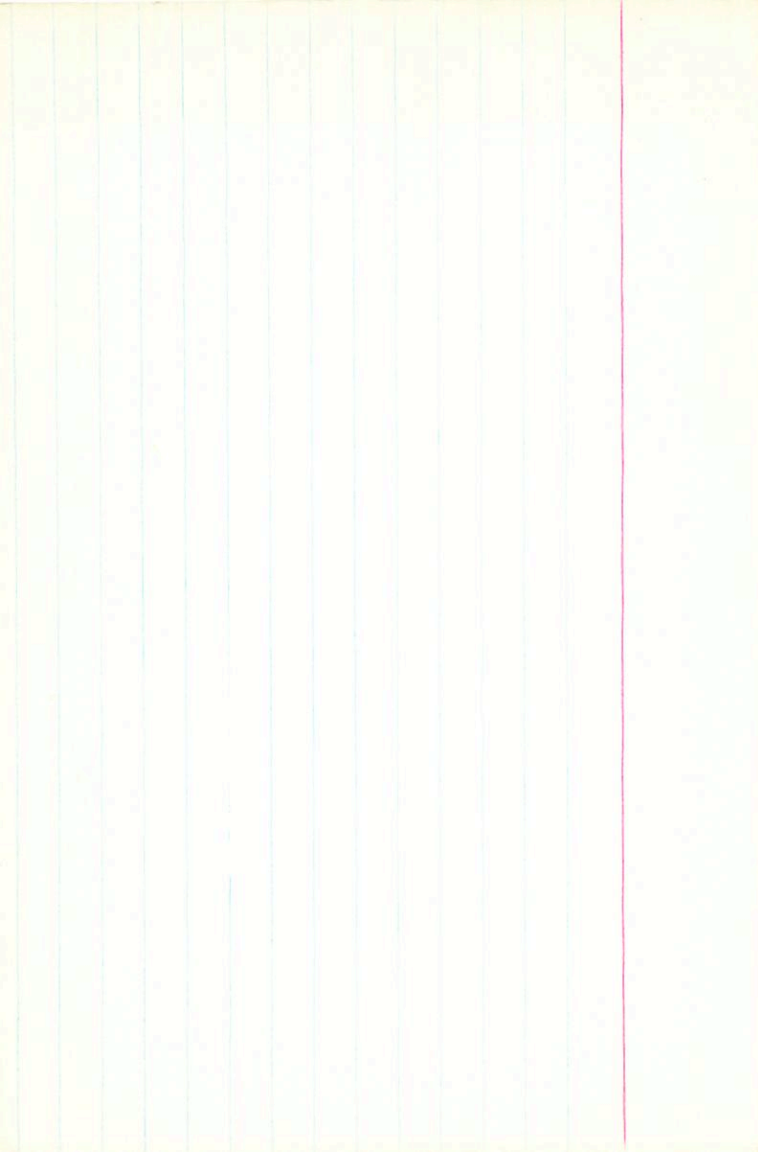
40 5.40 +0.45 +0.25 E -0012 -008

$\Delta m = 0.4$
0.2

F0D

L 8.57 +0.275 +0.06 F0D E

56 years



1914

5

37.4 + 65

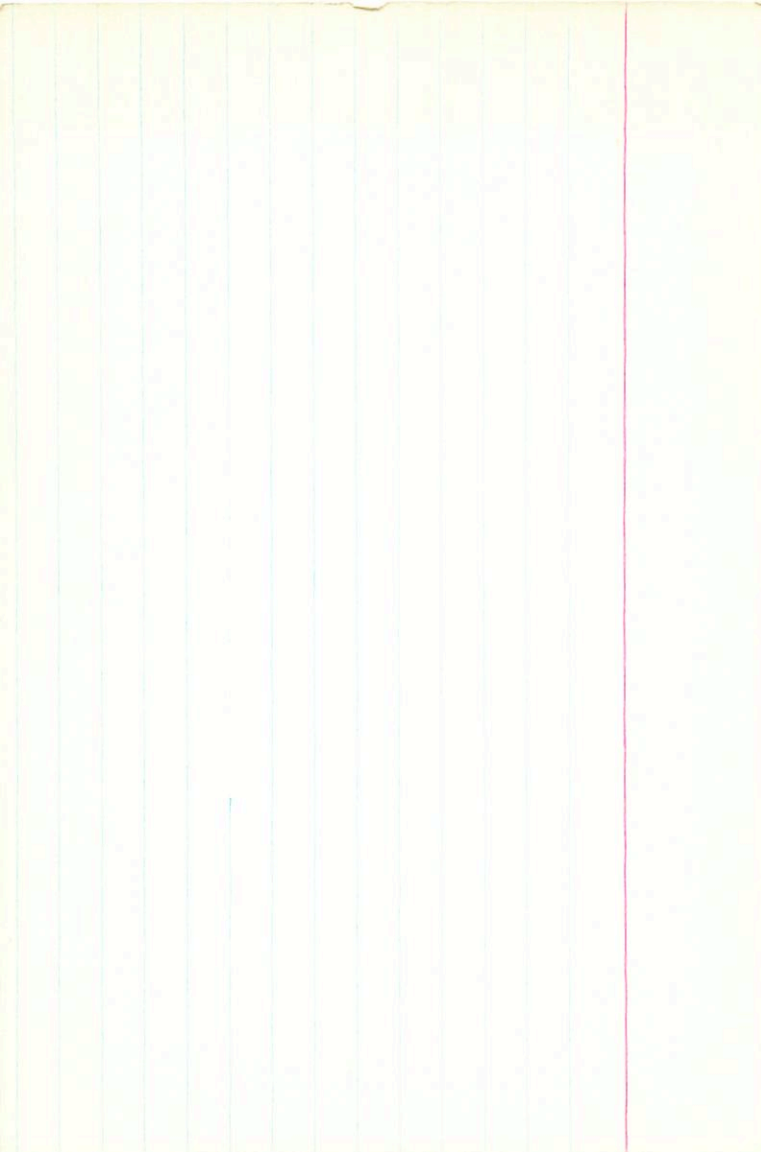
40

gives

-15.16

37289

62



SB 180.87^{of}

1417
37297

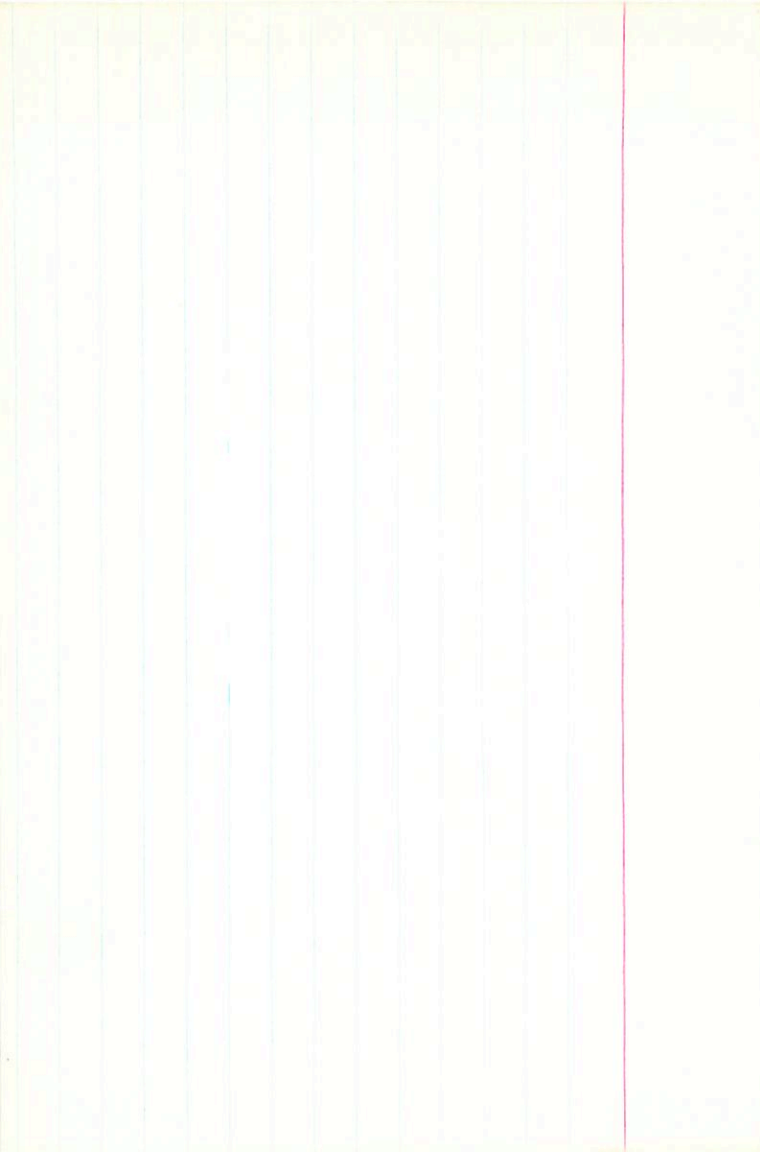
5 32.7 -64 16 987

+4.64

5 33 +1.04 +0.86 C

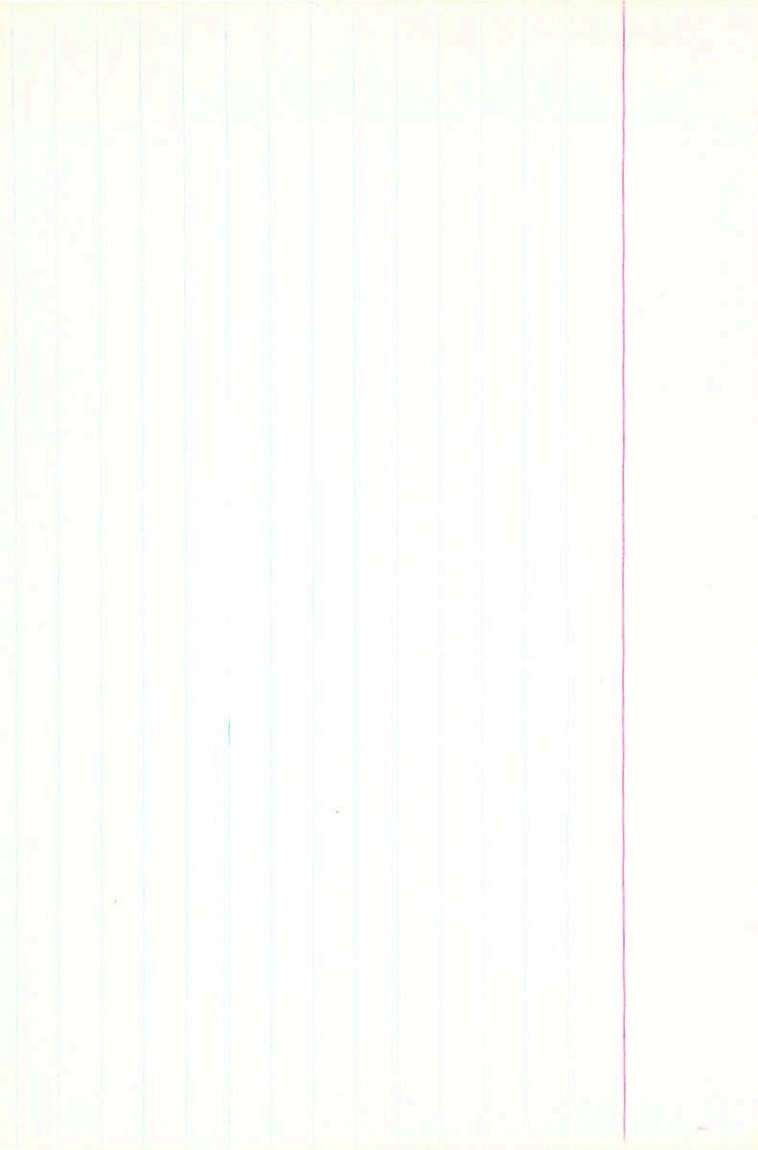
230 ± 3.5

+5058 -006



1527 5 347 -47 21 120 -

37434
6.10 + 1.14 (2.17) 120 BC



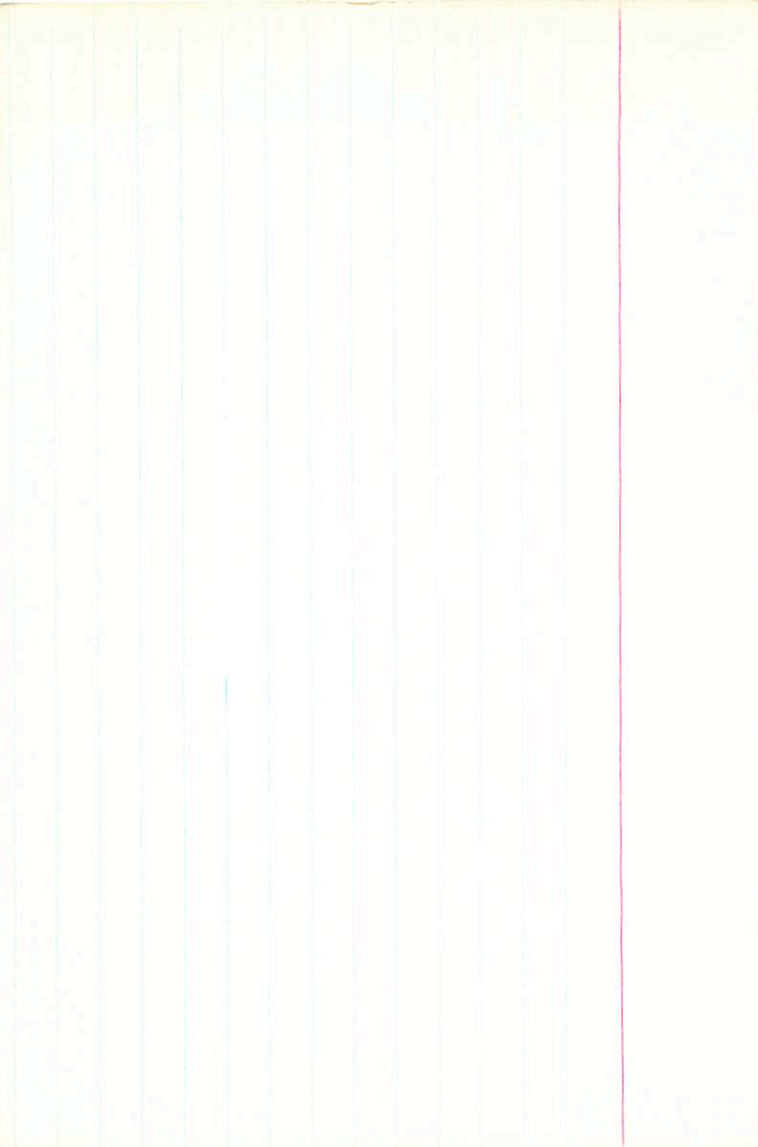
1430 5 34.3 -5.8 54 54 122 -

555
500
555

37462

6.75 + 1.45 + 1.80 ① 00

5.55 + 0.625 ②



3.54

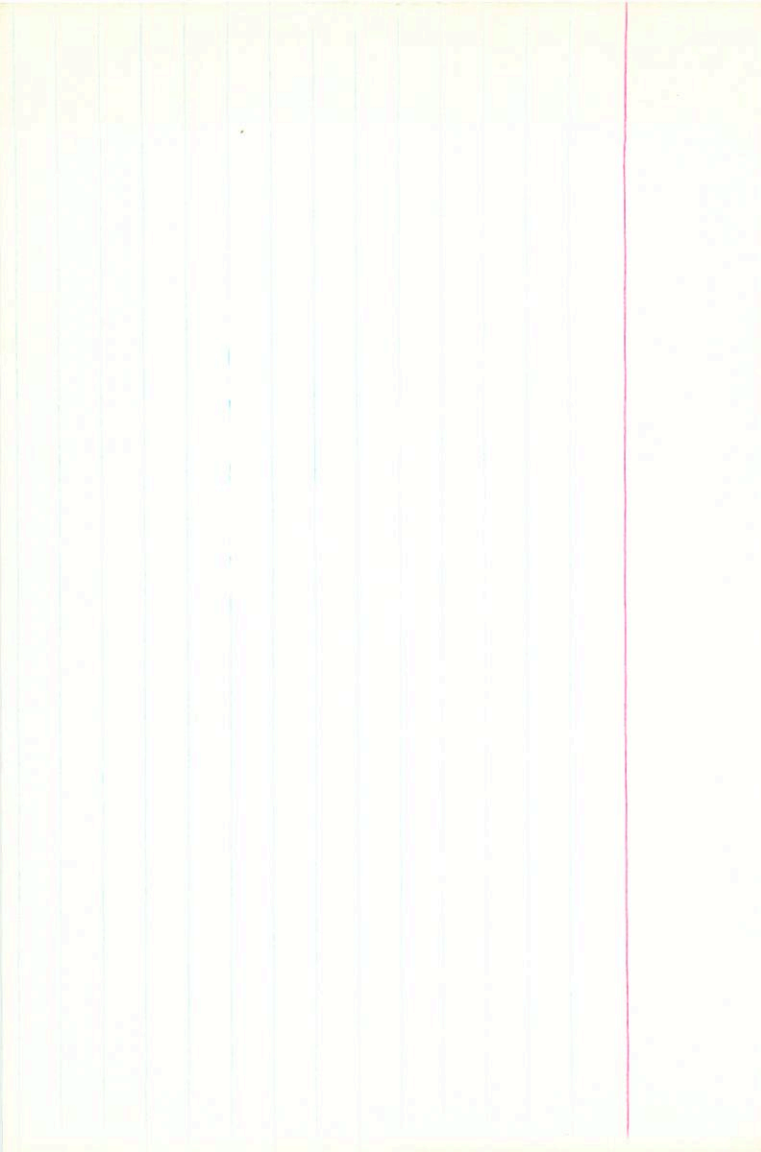
1924 5 37.5 431 54 m1 +4.88

87536

6.15-6.35 +2.075 +2.09(5)

4.73 +1.19 (2)

ac



24.6mm

1941

5

38.8

+56

34

ag

89

-28.4

f

37601

6.05

+0.95

+0.73

A

+0023

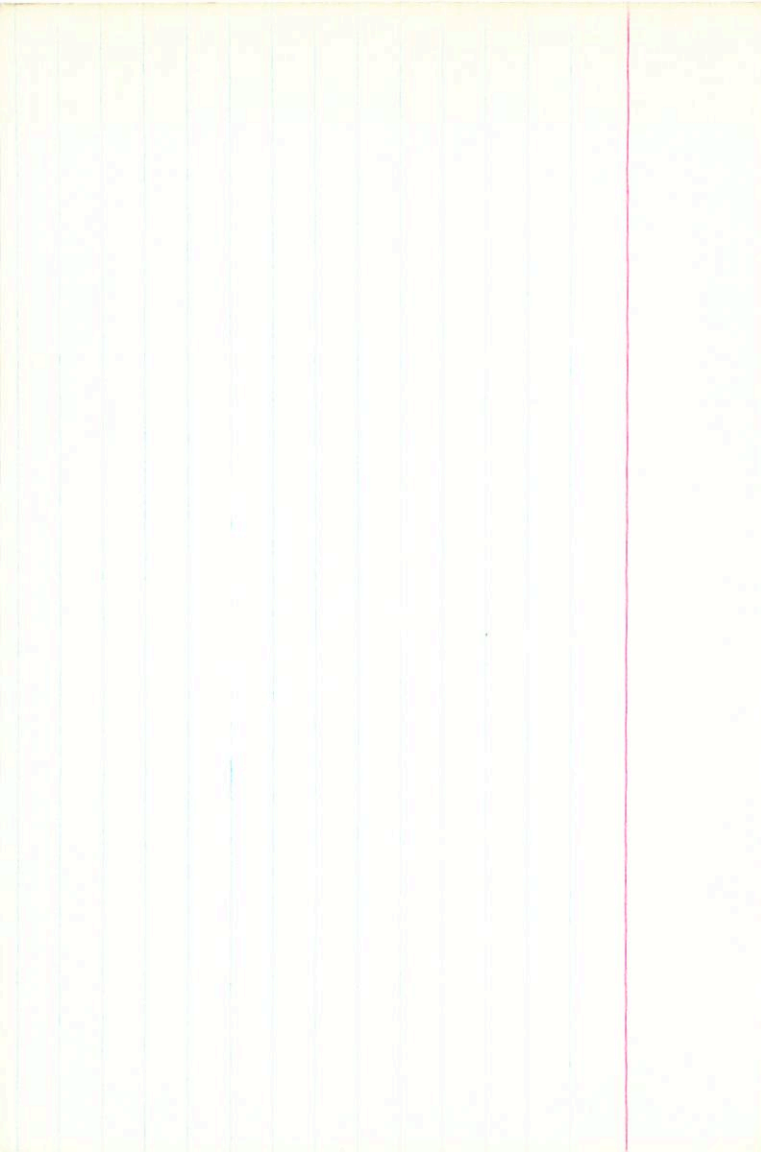
+0305

5.65

+0.335

3A

N30 ± 2.0



2 men

1953

5 33.9 -26 23 112 +56.7a

112477

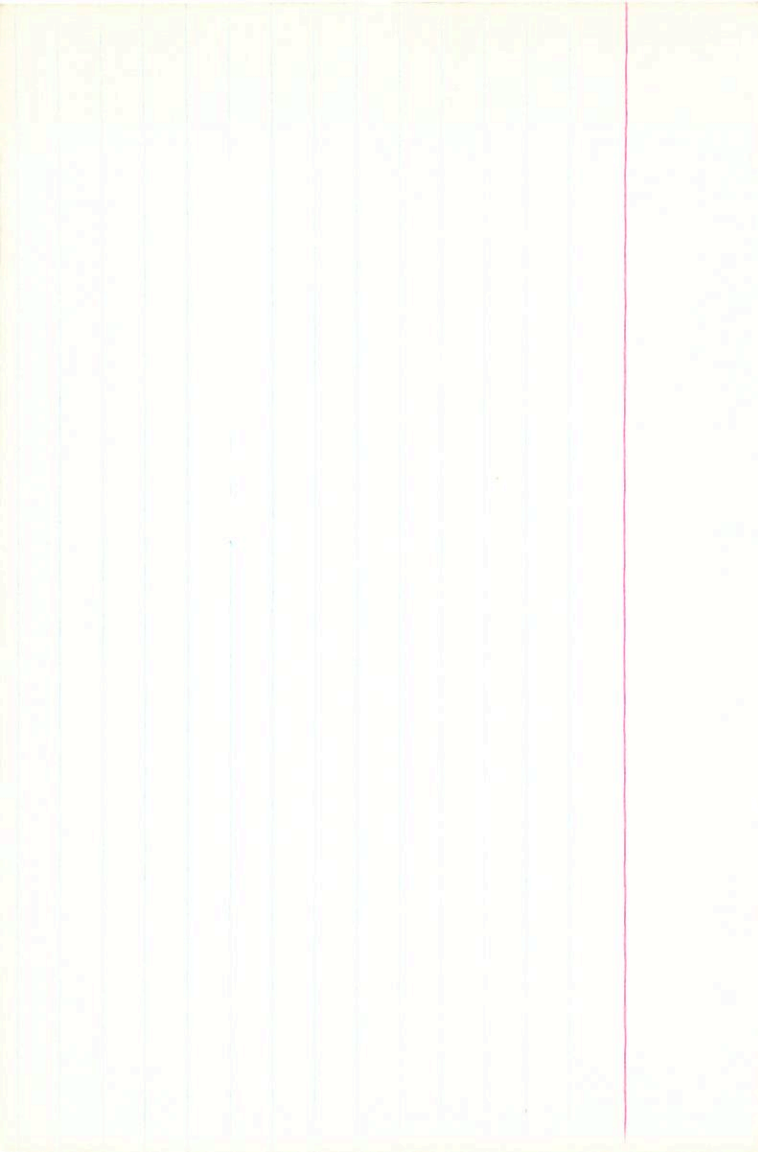
27763

5.18 +1.13 +1.15 C

5.19 +1.13 +1.14 \textcircled{D}

4.57 +0.39 $\textcircled{2}$

+03181 +2854 F124



1958

5

37.9

-82

40

9100

-8.38

37811

5.44 + 0.91 (2.00)

66 ± 4.0

-00175 -031

334

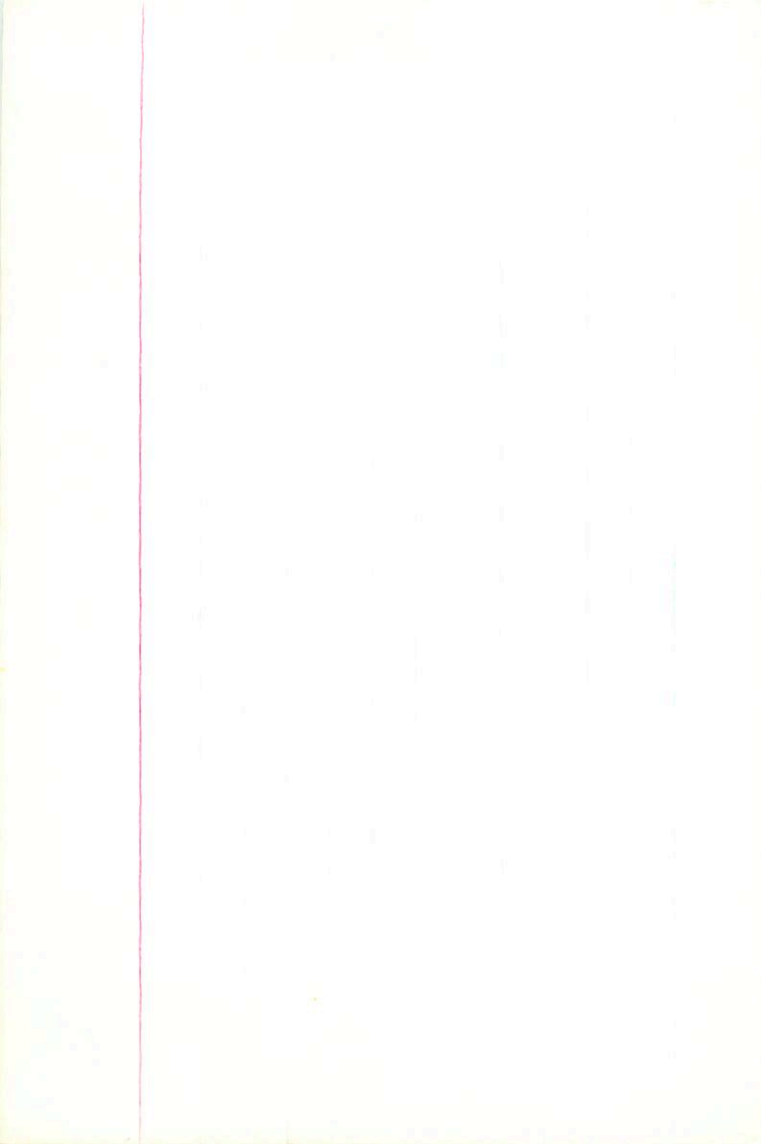
1964 5 36.0 -73 Y6 MY -11.1

37993 5.8V +172 +192 (1) CC ±5.0

455 +1.215 (2) -0028 +041

1554
~~32904~~

5
~~392~~ - 2
56
969

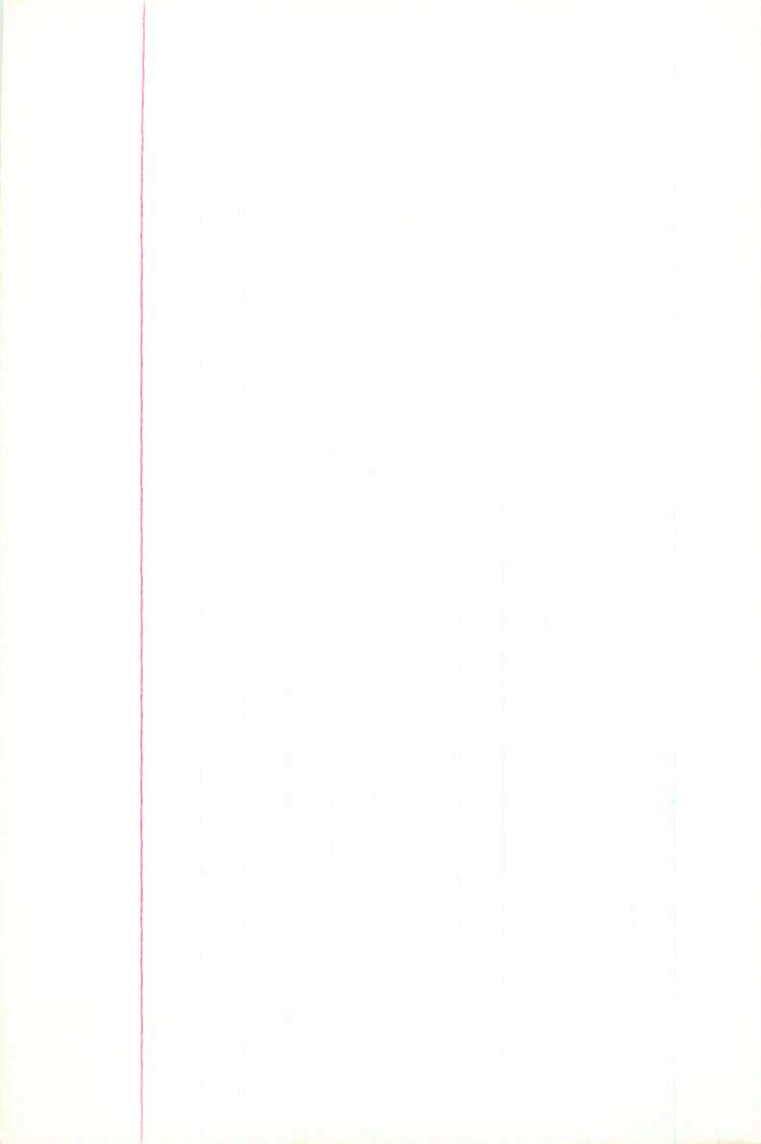


42 05 11.0 -26 19 122 -

942

5.94 +1.54 (2.56) C

66249



36

743

60 04.4

+47

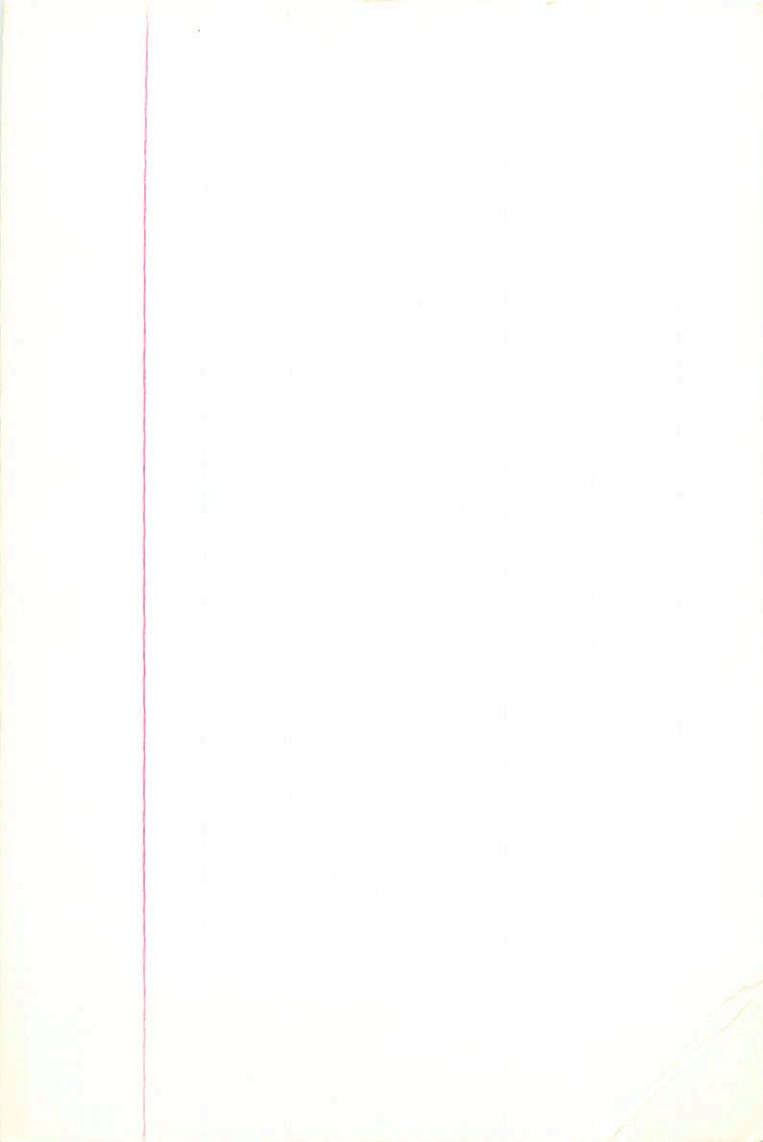
52

914

+15.76

6.15 +1.46 +1.75 /

CC 204



4.16

18

00 06.0

-12

52

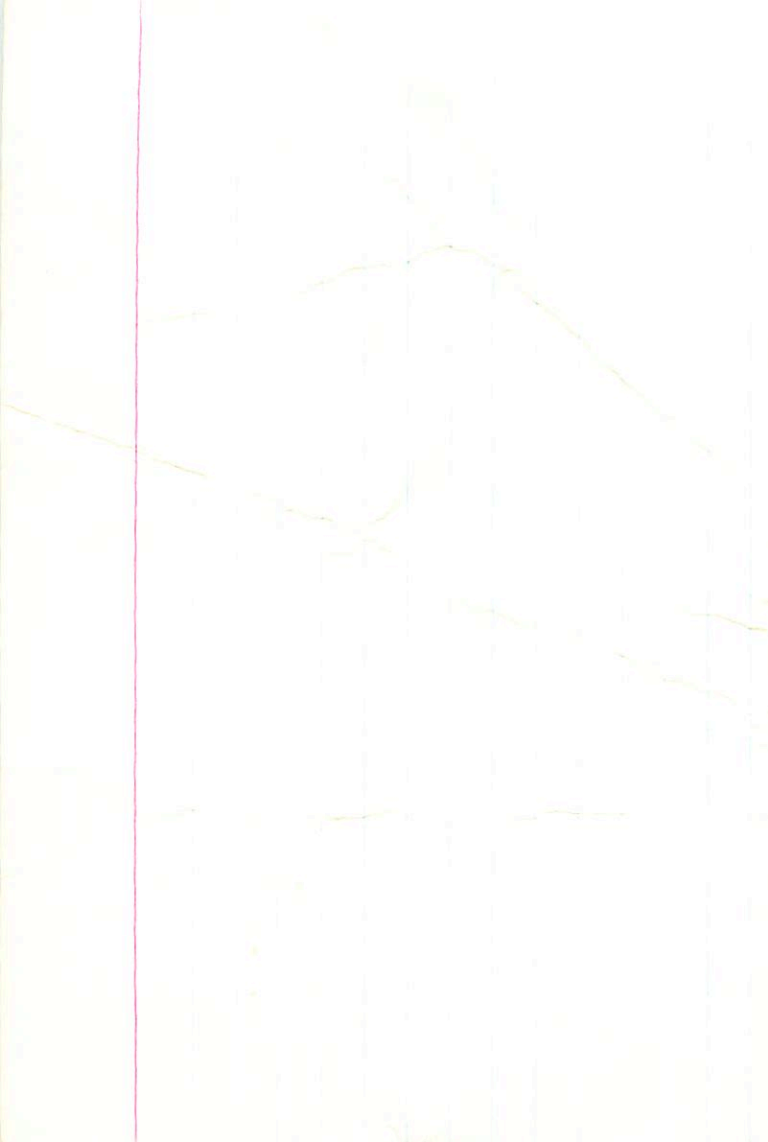
M1 III

402

6.05 +1.67 +1.97 C

5.11 +0.80 (4)

Ca 129



2966 7 396 +3 45- AD.

599-03-08

2

2

-20.7 inches

-016 137 1072 2-814

132 1075

264

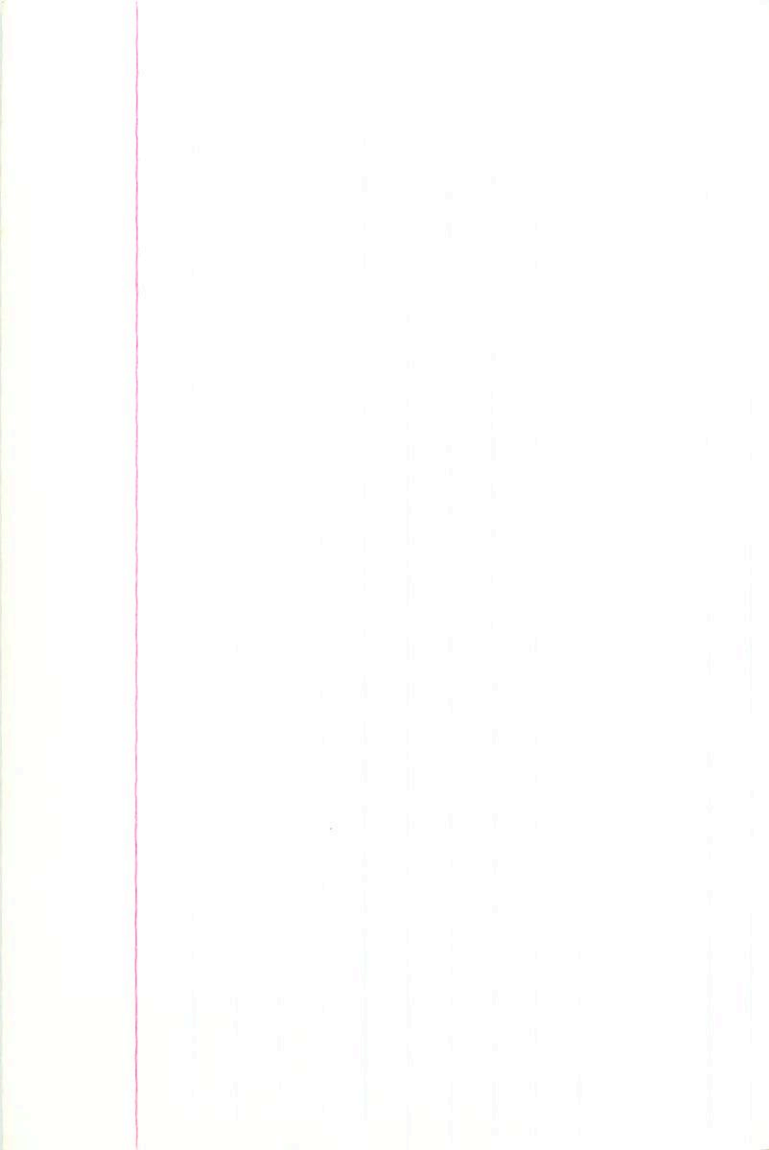
1339

SRM

+0001-0154

rem vcl

D



2956 7 324 -24 45 BF

Nov 1947

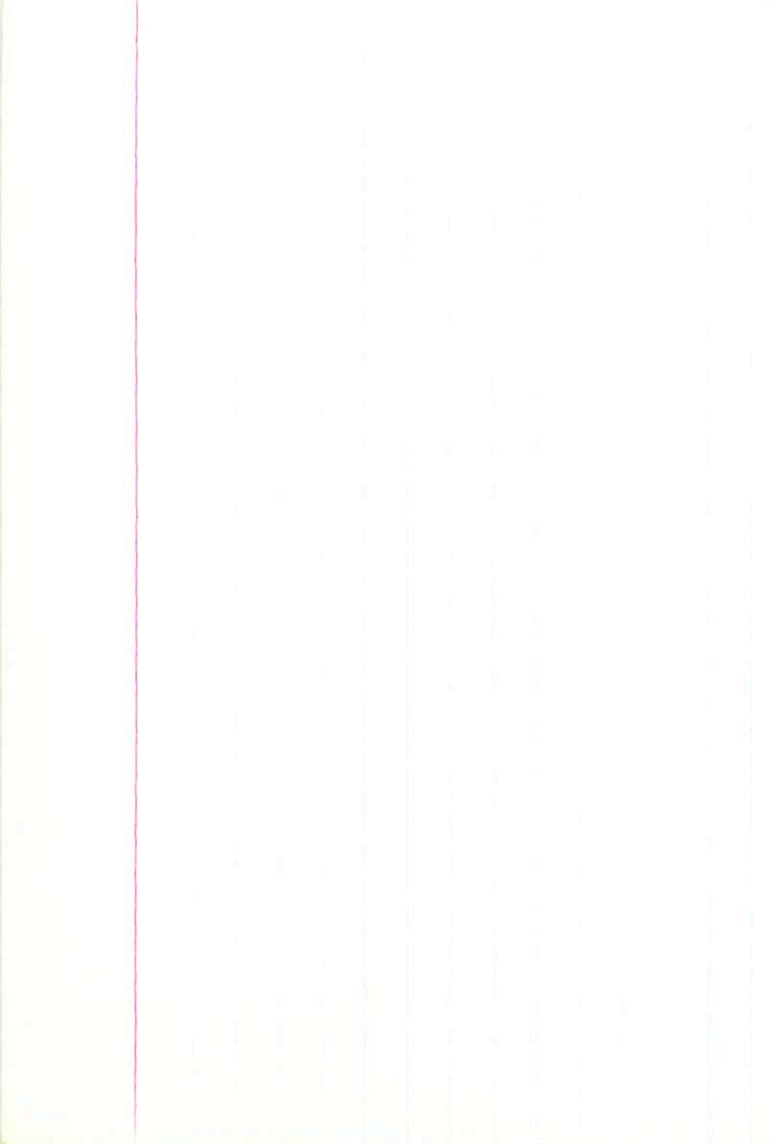
6.51 242 114 576 2.716

161 594

2025

786

39
②



2952 7 367 -39 52 AD

10000

661-18 146861 2825 (2) 3

141 865
282
1147

2946.000*

7.000*

38.800*

58.000*

50.000*

-0.039*

-0.050*

5.100*

104.713

8.700

0.174

0.810

25.314

-0.168

0.319

-14.827

-0.178

0.493

-14.340

2546 7 38.8 458 50 A3 IV

61447

10203

4.48 +08 +09 J

A3 IV

ⓐ

053 155 1.102

159

2.835

ⓑ SPC

11.15 +57 +67 599

↓ G ↓

f8.7 033141 1128

665

087=a

171

Bms 1

122=n

-0.2

342
1121
1663

-104113 -05171-144

330
1.121
1.457
1.548

-0364

-034-050

5.1

-7, 822

-0, 116

-0, 065

-18, 440

-0, 927

0, 049

16, 830

0, 356

0, 107

24, 000

77, 625

4, 450*

0, 015*

-0, 024*

-52, 000*

-34, 000*

35, 500*

7, 000*

2937, 000*

- 19 118

- 19 118

- 19 118

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- 19 118

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- 19 118

- 19 118

- 19 118

- 19 118

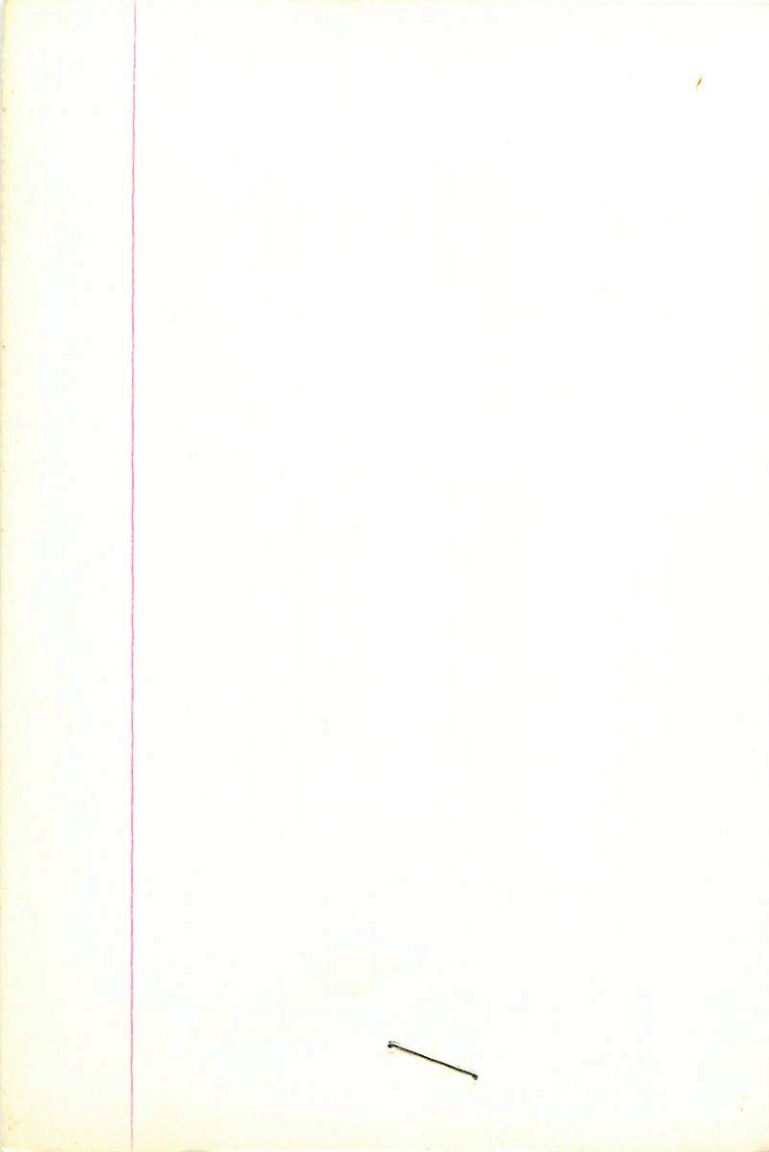
- 19 118

- 19 118

- 19 118

- 19 118

- 19 118



2437 7 35.5 -34 52 R8E

61330

10246

4.53 -09 -31 65

2854

4.53 -09 -30
4.53 -09 -30

-041 +120 +719

240

852

2.7344 (3)

415
03

959

60

113
-88226 +0133 F124

+27.06

E = +3

138
-0278

$V_0 = 4.44$

(4.44)

$N-V_0 = -12$

$2-130 = -325$

-024 +015

$MV = 0$

2667

20 015

-02

51

PM

150299

5.68 + ~~10.~~ 20 + 135 C

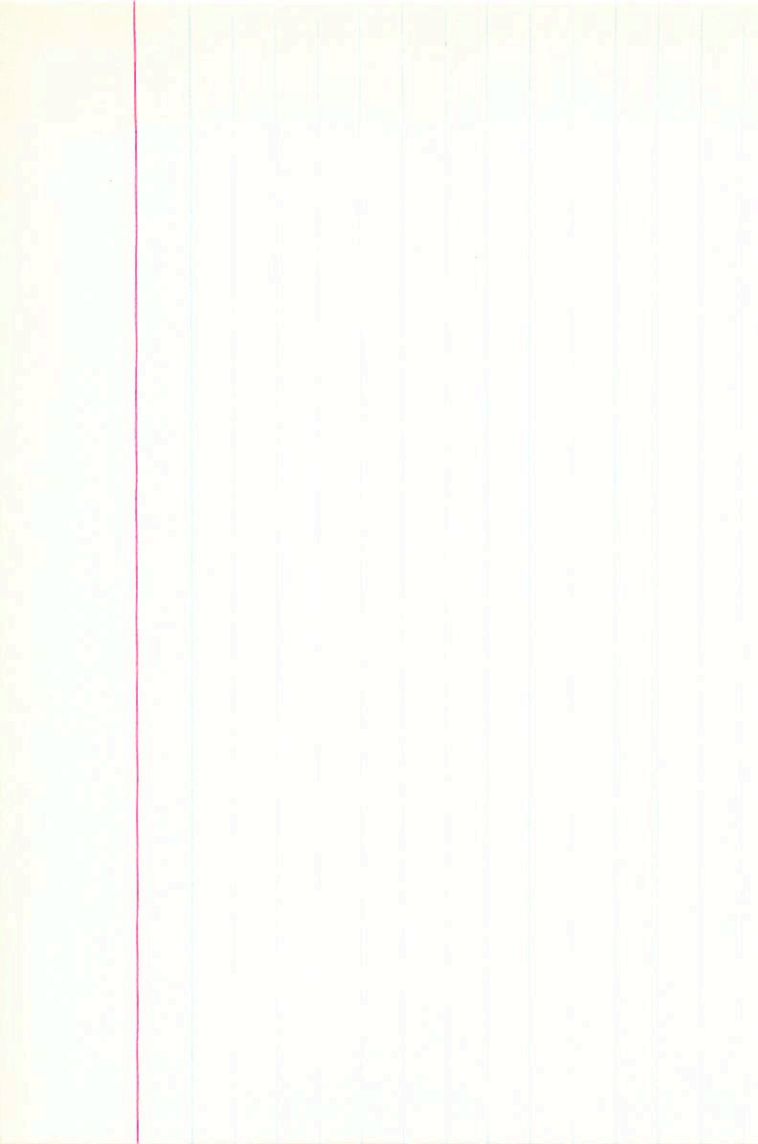
5.08 + 10.52 = 3 102,65

7663 ~~20 05 3F~~ 66 27 6

7664
140327

20 016 17 07 9100

S. 52 + 1.07 + 0.89 C



7676

20 01.0

+64 40

pm 1

5.27 +1.56 +1.81 (2)

4.13 " +1.835 (2) 104,65



Ms
7624

20

02.9

+14 SD

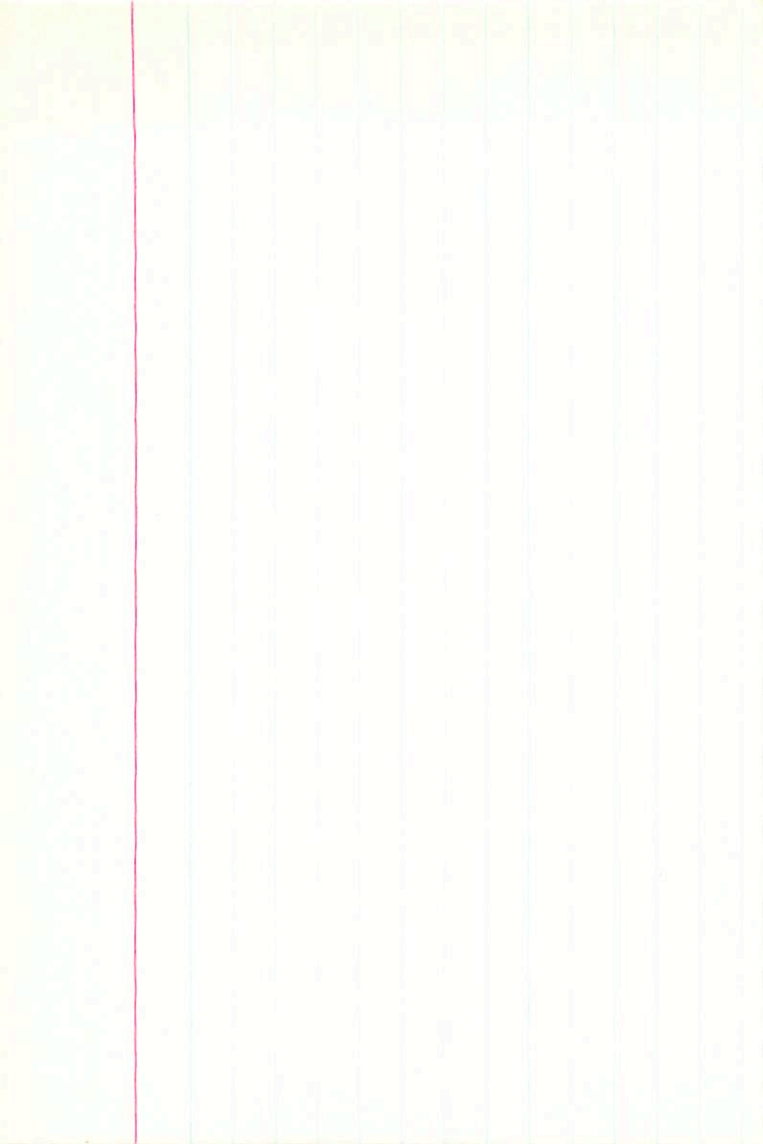
122 III

150608

5.08 +1.07 +0.95 3.12

4.60 +0.375 ①

4.63 +0.37 ① A



P2-112-

7650

20

03.1

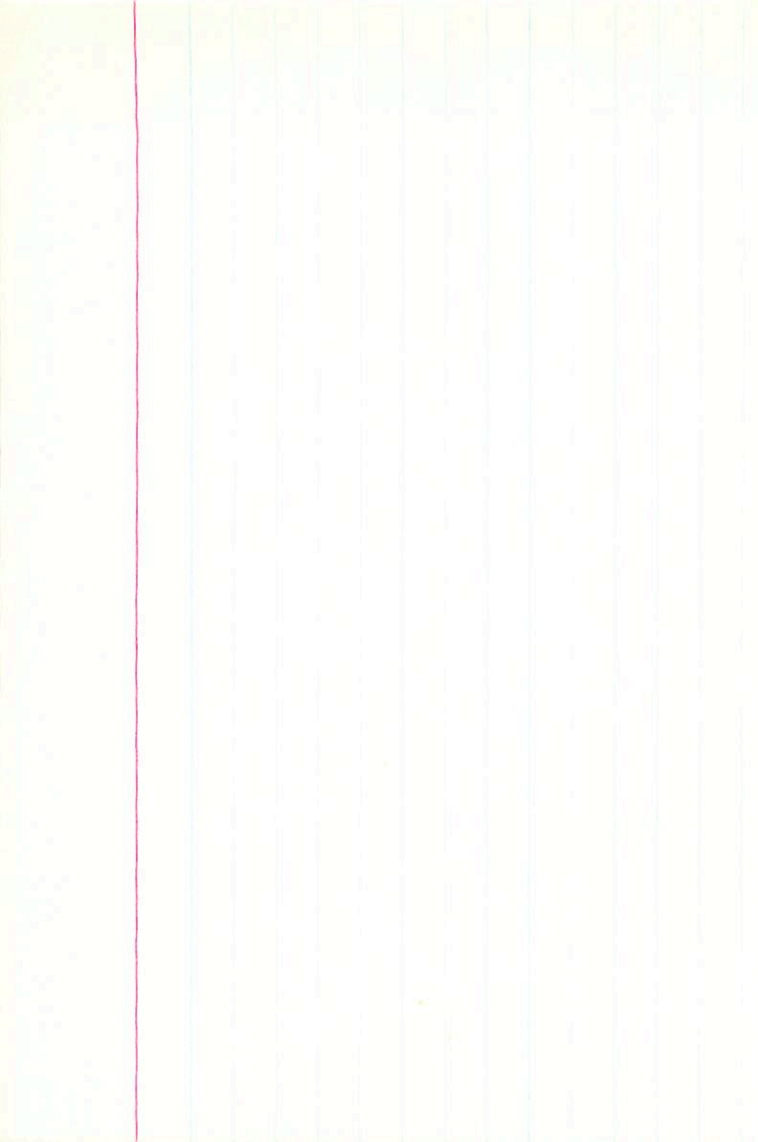
715

21

M2TH

150658

6.36



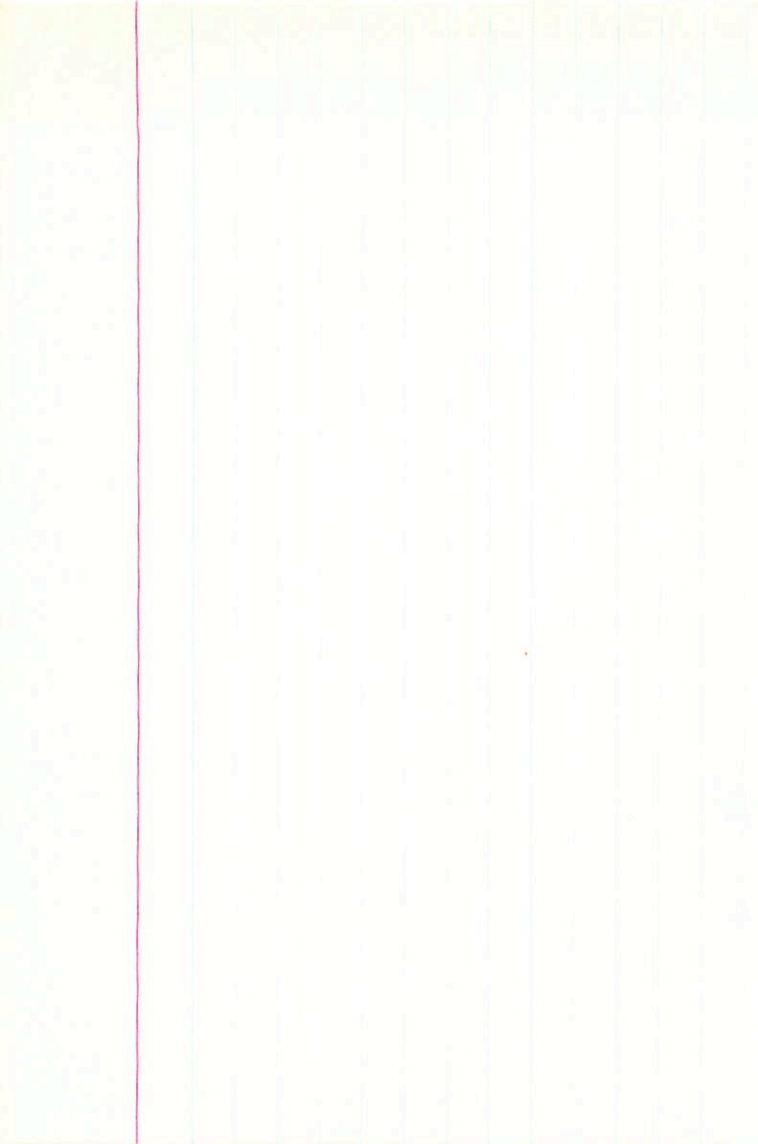
7686

20 01 01 + 26 20

M3 III

6.20 + 1.60 + 1.90 (2)

5.02 + 0.93 (1) 10, 65



2687

20

03.8

+51

41

M1

6.12 + 1.62 + 1.55 (D)

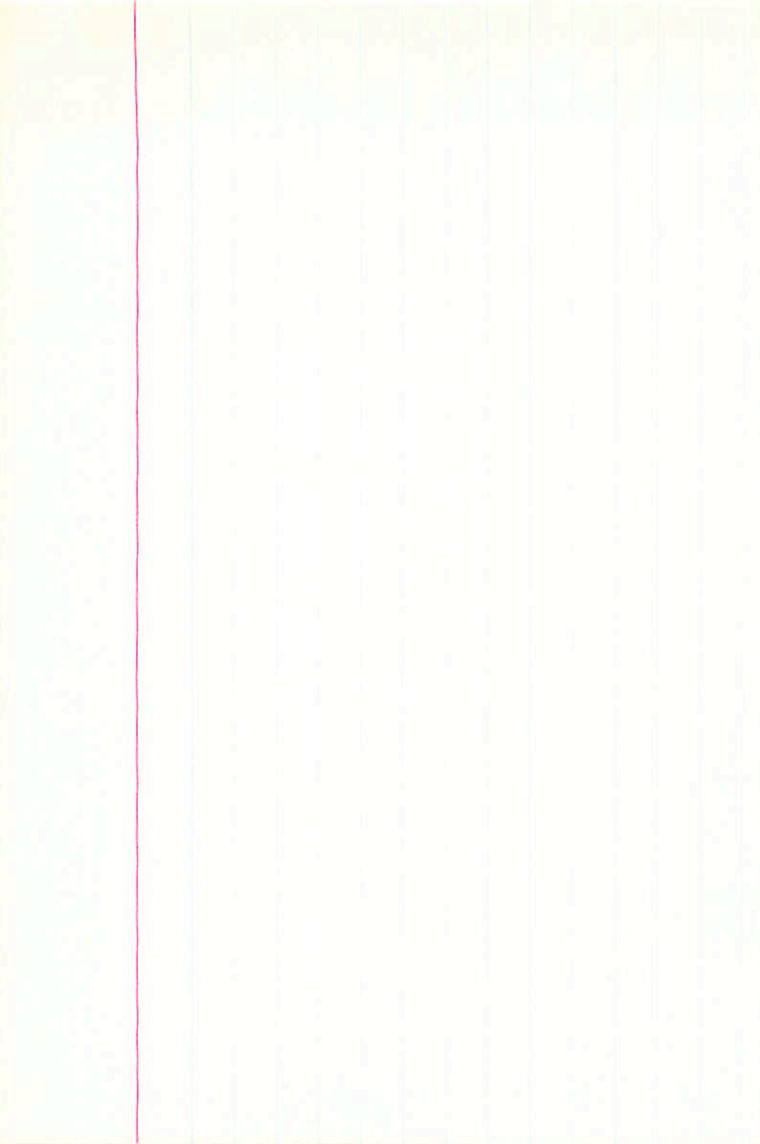
5.07

+ 0.80 (B) 10³ 65

7684 20 04.5- +85 50 100 IV
191026

3.86 +0.85-+0.56

5.02 +0.80 3.4



7690
191067

20 05.5 -00 5-0 9111
5-91 +101+091 C



9701
151277

20 04.7 461 50 128 111

5.39 41.18

4.89 40.42 2.5

7696 20 25.8 +16 30 gm3

6.42

7206 20 050 -42 55 122 III

6.25 +1.235 +1.33 1

5.65 +0.415 2

7204

941372

~~20047~~

+67

53

M1

7713

20

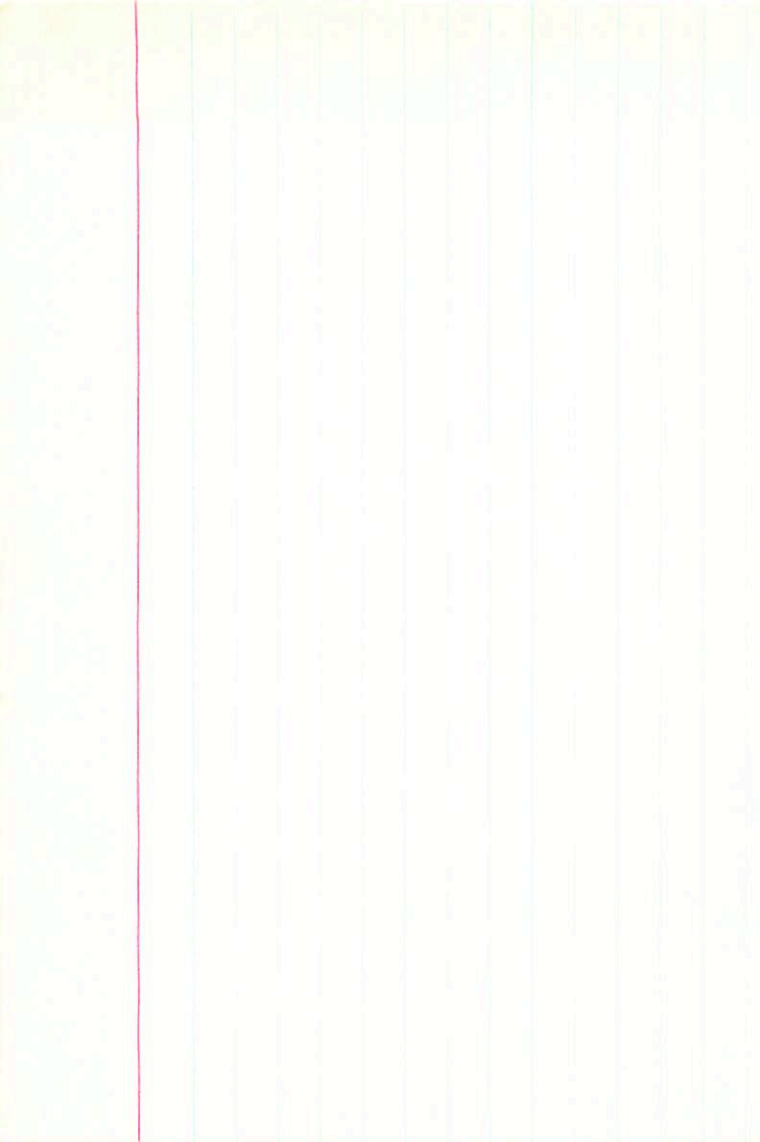
08.8

+20

30

120

191814



7714

20

10.5

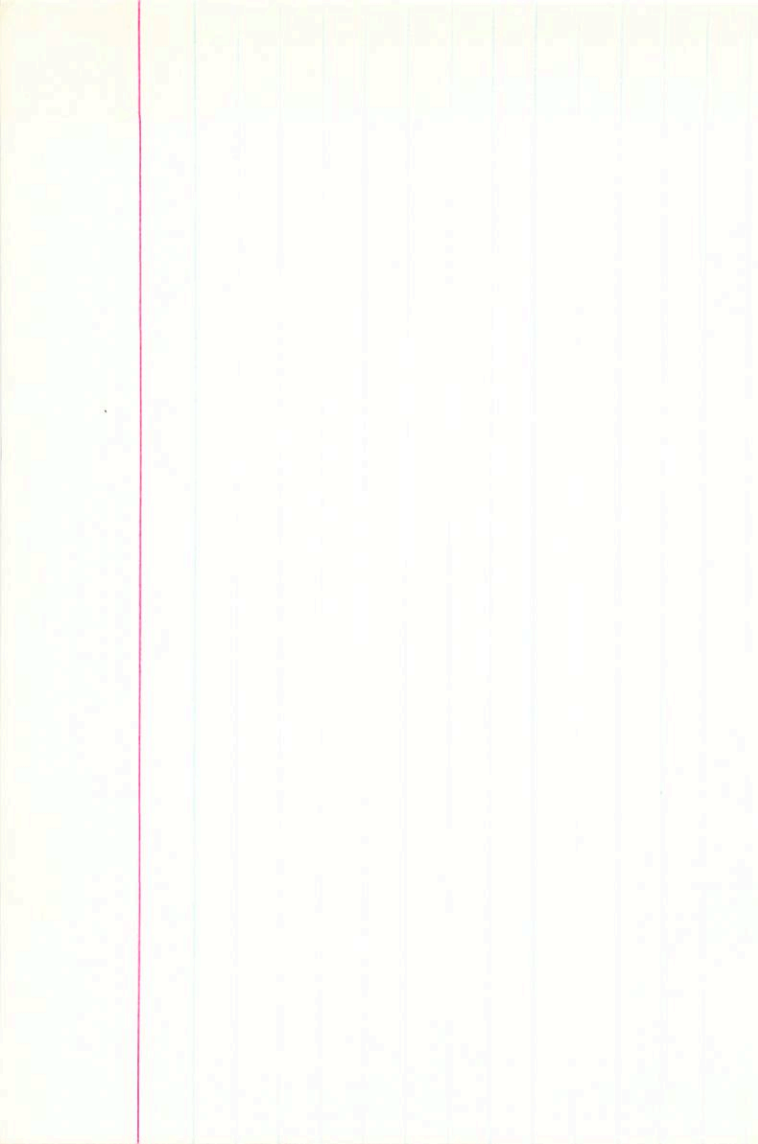
-52

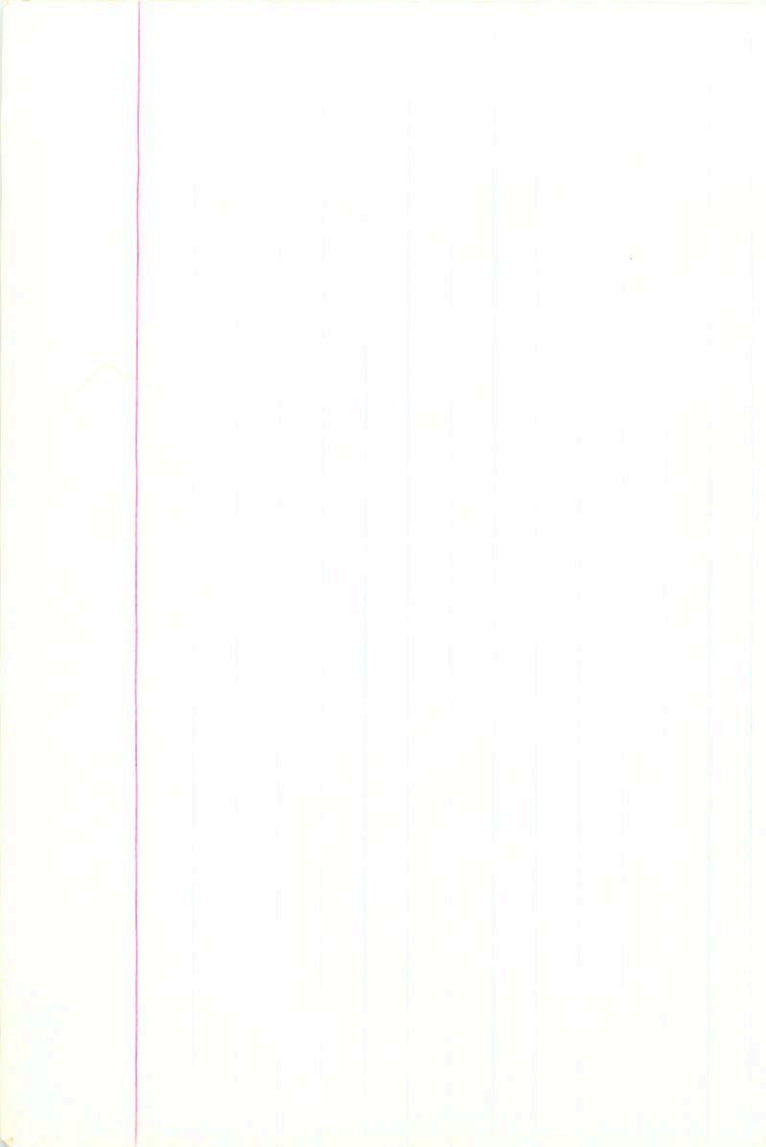
36

125

191829

5.70 +1.52 +1.51 ①





4.66 257 158 625 2.707 (5) 152073

2590 1

4.73 ~~473~~ ~~4820~~ ~~225~~ 2.154 27Jan75

4.70 -463 4905 -161 2.181 28Jan75

4.67 -463 4991 -179 ~~2~~ 25Aug75

4.65 -464 4887 -177 - 24Nov75

4.65 -458 4995 -174 - 1Dec75

4.67 -472 897 -172 - 4Jan76

4.65 -463 826 -181 2.191 16Jan76

77R

152004

10 09.7 +26 40

1B8 II-III

5.51 +1.40 +1.55



7720

20

10.6

-1

10

pp 105-

152107

S.477 4:43 + 1:24

4.69 + 0.655 + (3) 103.65

