

125184

Node

14 15.3

-719

GFE

Year

$$6.48 + 0.73 + 0.29 \text{ (2)}$$

$$6.13 + 0.25 \text{ (3)}$$

$$\Delta(R-v) = -0.15$$

$$\Delta N-v = -0.1$$

M V

W

$$-12.5 + 3.3 = -27.3$$

$$-13 \quad 0 \quad -10$$

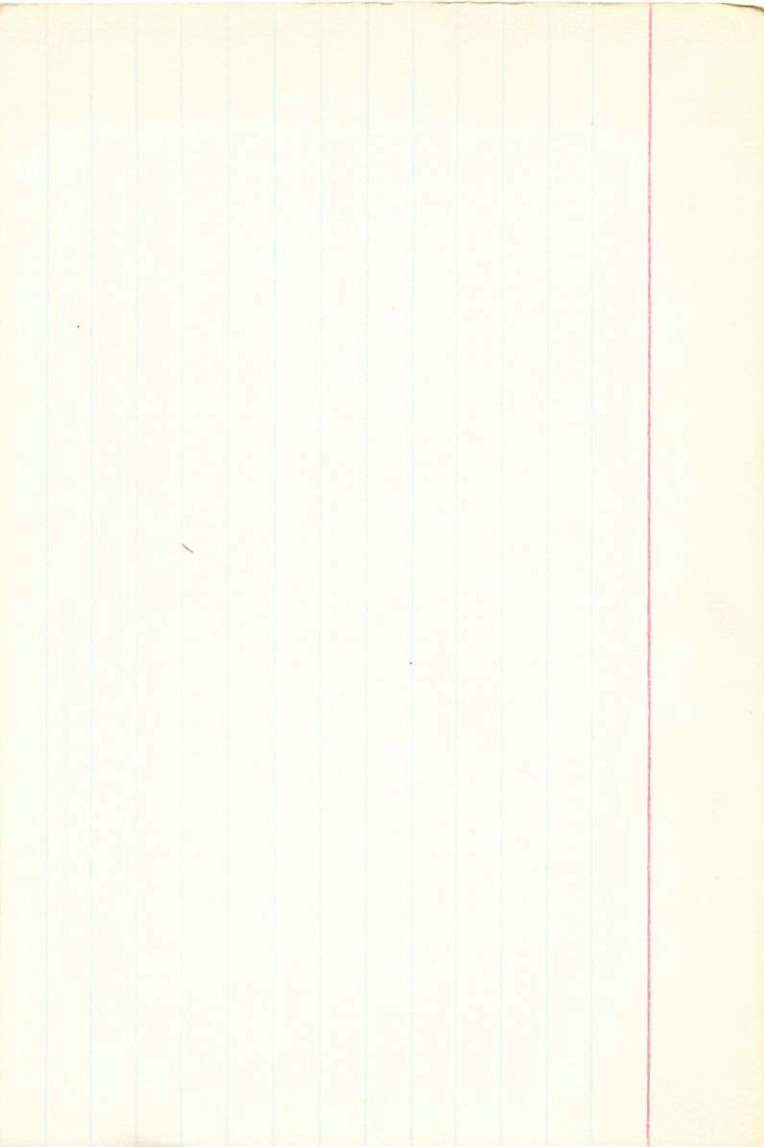
$$-14.1 + 0.257 = -0.237$$

MLI) 11(100)

+425 1000

568 5.18 070

~~588~~



used

125455

17 17.0

-4 55

100  $\overline{11}$

43055

57666)

4714(20)

5621(6)

464(12)

50

7.55 + 0.85 + 0.52 (2)

7.17 + 0.30 (3)

$\Delta(B-v) + 0.2$

$\Delta(n-b) + 0.2$

$$\begin{array}{r}
 \text{M(LI)} \quad \pi(105) \\
 + 5.00 \quad \cdot 0.465 \\
 \underline{6.87} \quad \quad 0.42 \\
 18.7
 \end{array}$$

n ✓ W

+43.5 - 52.2 + 8.3

+18 - 25 + 7

14.5 15"

-8.0 20.655 - 0.144



Old

125595 14 18.3 -40 10

Y 3257

9.58 +0.195 +1.14 (2)

$m(I)$   $\pi(\mu)$

+6.43 .040

8.41

7.98

347(16)

8.98 +0.47 (4)

566(6)

$$D(B-U) = -0.05$$

39

$$\Delta(N-B) = -0.01$$

+43.4 -49.6 +16.1

+18 -19 +6

+3.1 -0.565 -0.073



Old

127871 14 31.1 + 9 34 102V

Y3295

18 D(3)

27 A(29)

-1 M(6)

107 (10)

19

8.90 + 0.92 + 0.68 (7)

8.38 + 0.33 (5)

A(B-V) + 0.4

A(M-B) + 0.5

6.66-6

14.60 + 1.85 + 1.65 (1)

12.78 + 1.135 (2)

M(I)

+ 5.45  
8.10  
5.24  
60.5

2.18

2.45

+27.6 + 0.154 - 0.518

~~77.8~~ - 45.4 - 12.4

-19 -13 -10

563  
338





202  
241  
461

128774 14 364 -56 41 G5D

43311

436(11)

247(10)

31

7.42 + 0.66 + 0.15 (3)  $\Delta(B-V) = 0.1$   
9.24 + 0.225  $\Delta(M-V) = 0.25$

11.30 + 1.425 + 1.17 (4)

10.31 + 0.675 (2)  $\Delta(B-V) = 0.35$   
 $\Delta(M-V) = 0.095$

41(I)1  
+ 7.22

963  
471

$\pi(M)$   
0.033

u v w  
-45.6 -22.6 -61.5  
-9 +8 -21

431.8 + 0.404 - 0.303



Old

130871

14 47.9 +7 01 R2P

73351.1

9.08 + 0.965 + 0.70 ②

8.60 + 0.36 ⑤

464(10)

$\pi (M)$

$M(I)$

10.23

0.28

+5.49

8.22

2.73

$D(10-1) + 0.35$

$D(7-0) + 10.5$

W V W

+66.3 -66.8 +10.1

+16 -22 +12

" "

-31.3 -0.525 -0.067

5.89  
5.81

46



131977/6 14 54.5 -21 11

4335

A 5.80 +1.00 +1.06 (5)

200M (12)

5.22 10.40

(stk)

0(10-0) -035

105 (12)

5.22  
123

0(10-0) -11

11 (11)

155 (8)

B 7.95 +1.51

+1.22 (4)

+6.05

176

7.03 +0.895 (stk)

0(10-0) +04

11 (11)

4.13  
123

0(10-0) -085

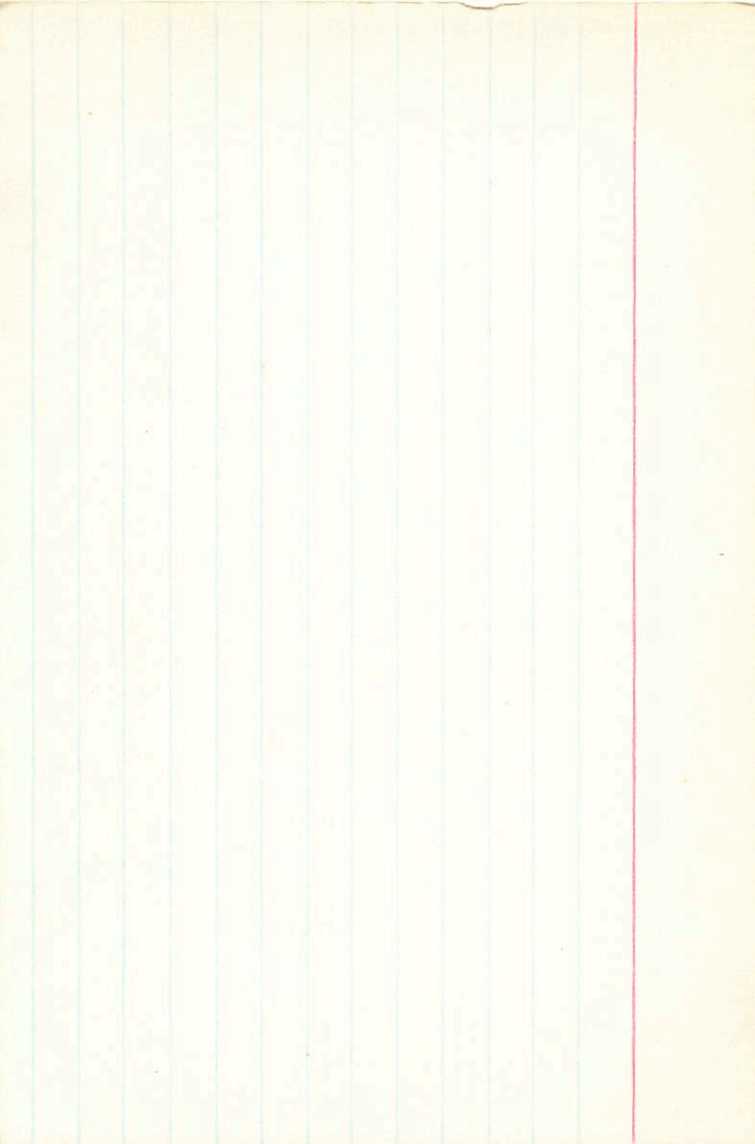
(7.36)

0(10-0) -1740

-43.9 -20.0 -34.8

-47 -23 -81

Flight 110000



dd

132683 14 58.0 -80 56 mo

$\pi(\mu)$   
 .068  
~~10535~~ ←  
8

$m(I)$   
 +7.15  
 758  
8

43386 9.49 +138 +129 ①  
 45M(N) 8.62 +0.645 ④  
 547(12)  $\frac{6.4}{798}$   $\Delta(B-V)$  00  
 35(N)  $\frac{134}{6.62}$   $\Delta(N-B)$  00  
46

5.01-8.9e-5.1e-  
 41- 71- 8-  
 -21.9 -26.8-10.5

+14.0 0.000 -0.474

16.62 -241.330 -16.1  
 1





old

133612 15 03.8 -47 48 100%

Not good

$M(I)$	$\pi(IV)$
+5.86	<del>0.28</del>
<u>60</u>	
22.9	0.35

$$8.91 + 0.94 + 0.535 \text{ (2)}$$

$$8.42 + 0.39 \text{ (3)}$$

$$\Delta(D-V) + 105$$

$$\Delta(U-S) + 40$$

24	V	W
-465.3	+27.5	-24.2
+3	-5	-5

$$-70.5 - 0.697 - 0.070$$



old

-303746 15 11.5 -3 37 1245

713439

58M(10)

20 Y(10)

33 Y(7)

356(7)

9.82 +1.125 +0.99 (3)

9.12 +0.48 (2)

A(13-1) +075

B(11-13) +106

M(I)

+6.54  
860

-2.77

711(A)

036

037

m v m

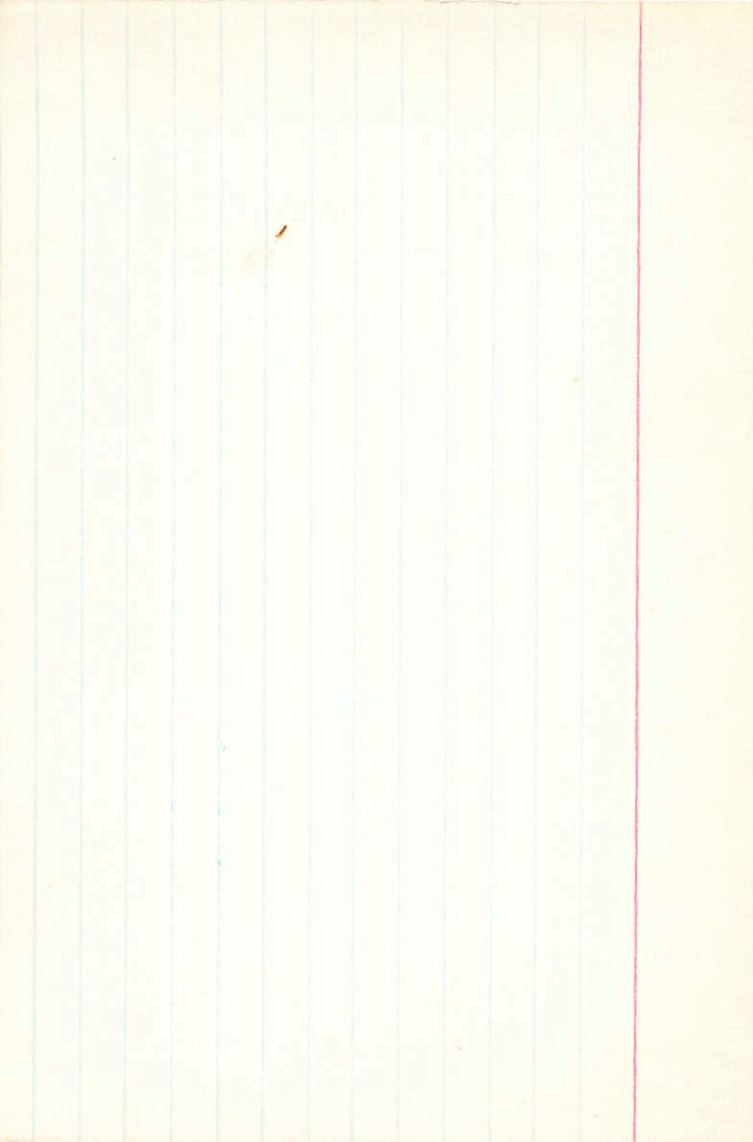
+141.2 -45.3 -11.5

+22 -18 +22

" 2910

" 245

-1056



Colcl

136834 15 20.2 +1 36 123  $\bar{E}$

13473

31m(5)  
34Y(12)  
36

8.27 + 0.555 + 0.865 (2)  
7.92 + 0.325 (4)

$\Delta(B-N) - 0.75$   
 $\Delta(N-B) - 2.05$

M(I) 71(M)  
+ 520 10205  
7.50  
280 345

2 2 4 4  
+213 244 -12.2

" " 365 - 369

0 -24 +2

15.350  
1.600  
-365.000  
-369.000  
1.700  
22  
-30.400

-0.507  
0.503  
-0.700  
-4.194  
21.190

0.667  
0.743  
0.052  
-2453.477  
-55.255

-0.547  
0.440  
0.712  
174.049  
-17.825

old

Varian of NISU in ROB no 120  
1960  
an economy.

137763/78

15 25.5 -9 11 d125

Y 3491

d125

$$6.90 + 0.835 + 0.42 \textcircled{3}$$

n(I)

$$6.59 + 0.225 \textcircled{5}$$

+ 403

61M(7)

631

66C(8)

1.68

$$\Delta(B-V) = 0.35$$

$$\Delta(R-B) = -0.7$$

474(12)

$$7.59 + 0.93 + 0.65 \textcircled{3}$$

$$7.20 + 0.295 \textcircled{4}$$

$$\Delta(B-V) = 0.75$$

$$\Delta(R-B) = -1.35$$

$$\begin{array}{r} 4.93 \\ - 4.91 \\ \hline 0.02 \\ 1.98 \\ \hline 1.98 \end{array}$$

~~137763/78~~

043

$$6.151-61 \quad 13.72 + 1.355 \textcircled{2}$$

red

137626 15 25.7 -49 47 65  $\bar{V}$

M(I)	17 (pt)
+5.02	.048
<u>0.50</u>	
1.52	0.04

43487 7.65 + 0.78 + 30 (1)

526(7) 7.21 + 0.315 (2)

$\Delta(B-V) + 12$

$\Delta(U-B) + 3$

u ✓ w

" -0.218 -0.091

+48.2 +4.5 +07  
+6 -9 +2





old

137628 15 27.5 -74 11 125  $\sqrt{2}$

Not good

9.01 + 1.01 + 0.83 (2)  
8.31 + 0.355 (3) +

$\Delta(B-U) + 0.45$   
 $\Delta(U-D) + 1.05$

M(I)  $\pi$  (nt)  
+ 5.95 .0405  
 $\frac{2520}{1.47}$   
581  
792 / 1.1  
2

u v w  
-19.9 -47.0 -26.9  
+4 -7 +4

+53.2 -0.053 -0.147



old

8  
138648

15 31.1 -16 50 dG9

var  
var

8.14 + 0.845 + 0.455 (2)  
7.77 + 0.315 (4)

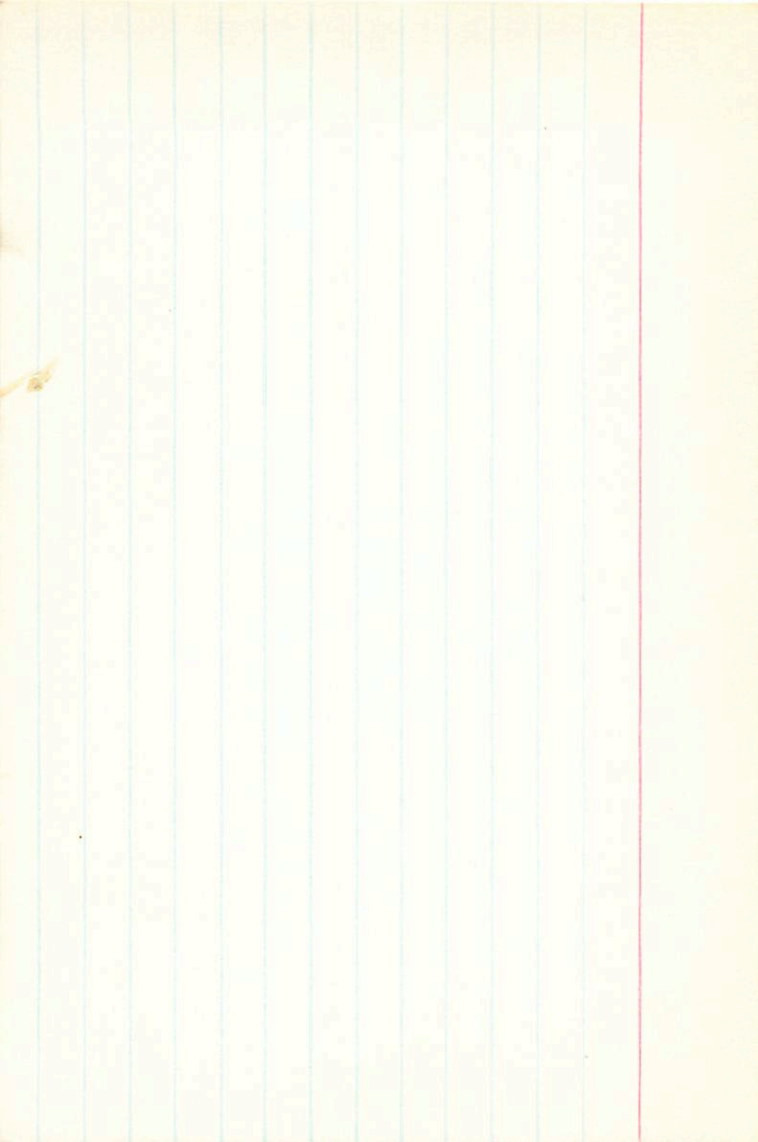
m(I)    π/pt)  
+5.135    .038  
745  
2.33    034

284 (16)  
190 (16)  
25

$\Delta(B-v) = +0.55$   
 $\Delta(u-B) = +1.55$

W    V    W  
-46.3   -44.2   +7.5  
-2    -14    -7

150.0   -0.096   -0.314



Old year

144253 16 02.7 -20 19 d N2

43641

$$7.45 + 1.045 + 0.88 \textcircled{2}$$

$$6.91 + 0.385 \textcircled{6}$$

526(15)

534(16)

53

$$10(1.0) + 1$$

$$10(1.0) + 2$$

$$11(1.12) \quad 11(1.0) \\ + 15.97 \quad .087$$

$$2241 - 340$$

$$6.23$$

$$6.12 \quad 0.83 \\ \frac{6.53}{4}$$

~~11~~

$$" \quad -0.343 \\ + 0.332$$

+34.0

$$11 \quad 11 \quad 11 \\ + 34.2 \quad -19.5 \quad -13.7$$

~~1000~~

$$+ 2 \quad - 9 \quad - 2.1$$

146800

16 16.6 -48 06 N3E

add

43697

8.95 + 0.95 + 0.615 (2)  
8.61 + 0.335 (4)

M(I) H (pt)  
+ 5.20 .025  
8.27  
3.80 0.25

457(12)

28 L(28)

33 C(15)

33

$\Delta(B-r) = 01$

$\Delta(u-b) + 095$

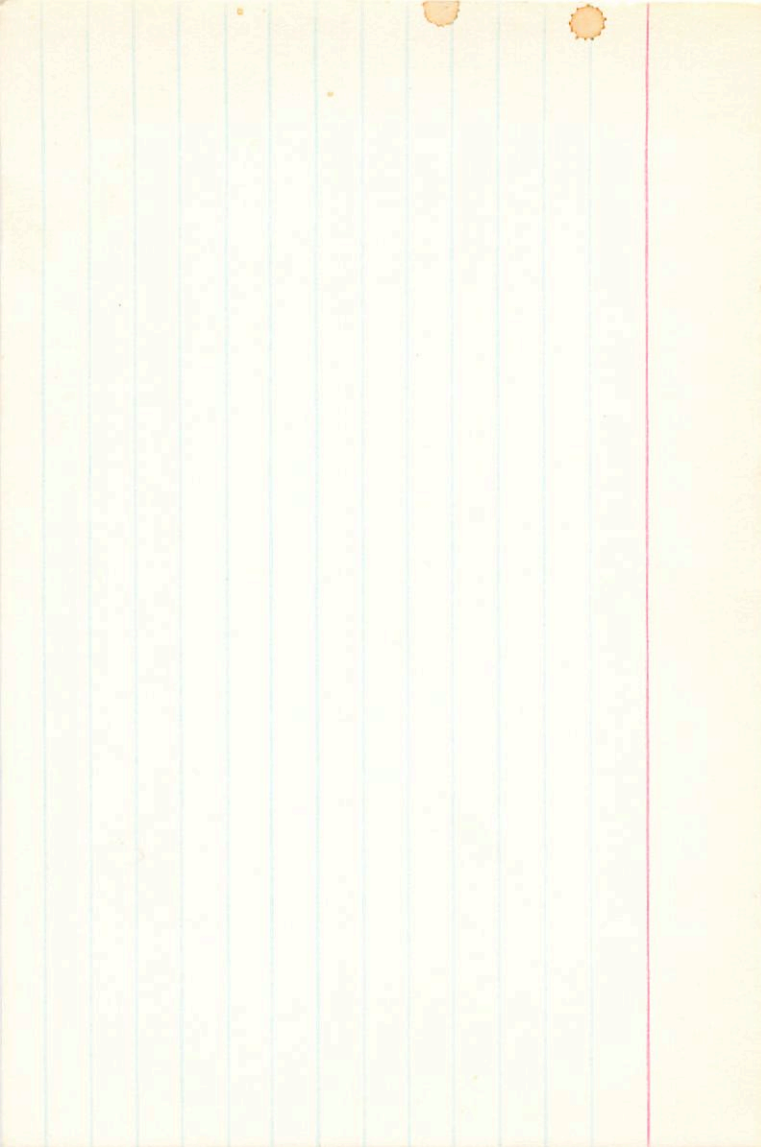
M V W

41.2 - 0.404 - 0.784

add

+61.1 -134.8 -48.0

+17 -36 -13





old

HJ 148530

16 26.1 +03 22 G5B

$n_1(I) 71 \text{ (pt)}$   
 $+4.58$   
 $\frac{817}{\cancel{22}} \cdot 0.22$   
 $362 \text{ 019}$

$73743$   
 $27M(5) \quad 8.81 +0.77 +0.38 \text{ (2)}$   
 $344(10) \quad 8.44 +0.27 \text{ (2)}$

$\Delta(B-V) +005$   
 $\delta(R-S) +005$

$2744(14)$   
 $\frac{30}{30}$

$\eta \quad \checkmark \quad W$

$-76.4 \quad -76.3 \quad -35.1$   
 $-13 \quad -18 \quad -10$

$4220 \quad -0.007 \quad -0.516$



149/62

16 30.4 +3 21

Y3762

35 n(10)

42 Y(110)

43 D(3)

07

8.85 +0.88 +0.55 (2)

8.41 +0.345 (2)

0(10-0) +0.9

0(n-0) +2.05

41(I)  $\pi$ (nA)

+5.86 .0325

9.06  
270  
270

0.24

M ✓ W  
+4.69 -6.97 -2.9

5+  
0 -17 +9

" " -0.374 -0.189

244  
308



old

1496.06

16 34.2 - 40 46

1128

43771

8.97 + 0.985 + 0.755 (2)

M(1)

$\pi$  (1/2)

316(18)

8.59 + 0.31 (4)

+ 5.05  
728

~~0.25~~

390

0.23

$\delta(13-v) - 9.5$

$\delta(12-b) - 16.5$

-2.5 - 0.366 - 0.366

$\eta$	$v$	$w$
+32.4	-91.7	+4.4
+8	-23	+1

151090 16 42.6 +0.6 " dc6

73805

N3

M(I)

32A(16)  
334(110)  
1746(5)  
27

6.55 + 0.89 + 0.53  
6.16 + 0.32 ③ Δ(B-v) + 0.2  
Δ(N-B) + 135

+5.4  
5.53 (24)

10.30 + 1.04 + 0.91

9.74 + 0.41 Δ(0-v) + 10.8  
Δ(N-v) + 0.5

+5.93  
9.33  
3.40  
TT (M\*)  
'022  
021

-5.6 -0.212 -0.262

u v

-17.7 -70.0 +84  
-5 -15 +2



151337

16 45.3

-47

38

old  
140 5

Notice

9.38 + 0.91 + 0.59 (2)

7.08 + 0.32 (2)

M(I)

~~+5.48~~

6.74

1.60

# part 1

10585

048

 $\delta(B-v)$  00 $\delta(n-B)$  +045+2.9    "    "  
-0.088 -0.027

n	v	w
-24.9	-12.2	+31
+1	-3	+2



1541363

17 02.6 - 4 58

125D

3878 43880

98 A(2) 83M(8)

60M(6) 917(12)

874(12) 1256(16)

5076(14) 96

766(8)

93

M3.5D

m(I)

6.58

6.57

0.2 17 (cont)

A 7.76 + 1.15 + 1.05 (3)

7.05 + 0.485 Sta

D(B-v) + 0.6

D(N-B) + 1.15

B 10.08 + 1.44 + 1.06 (3)

9.00 + 0.905 Sta

D(B-v) + 0.9

D(N-B) + 0.65

15.1.134

u v w

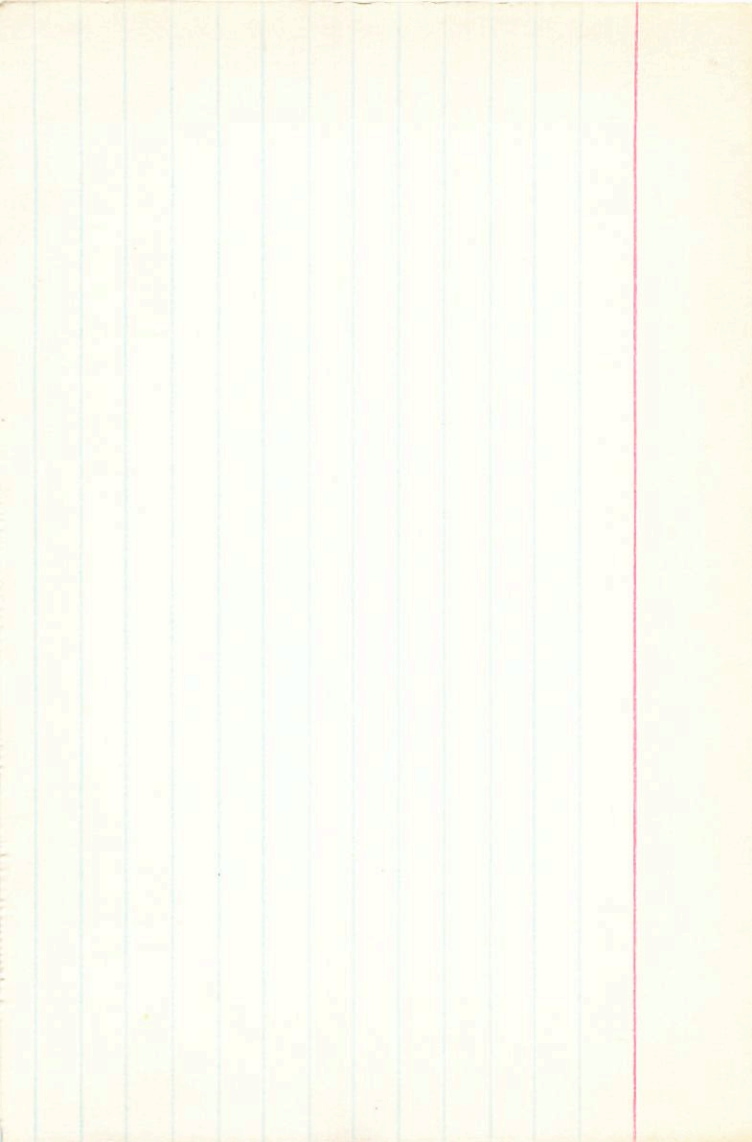
-46.2 -64.1 +21.3

-15 -68 +9

4333

7.91 .094  
918  
919 0955

old



4002

154590 17 04.6 -41 39 N5 E

43983

9.33 +1.055 +0.83 (2)

M(I)

+6.22

730

1.06

N (N<sup>th</sup>)

~~0.59~~

0.61

496171

6.80 +0.405 (2)

$\Delta(B-N)$  +0.2

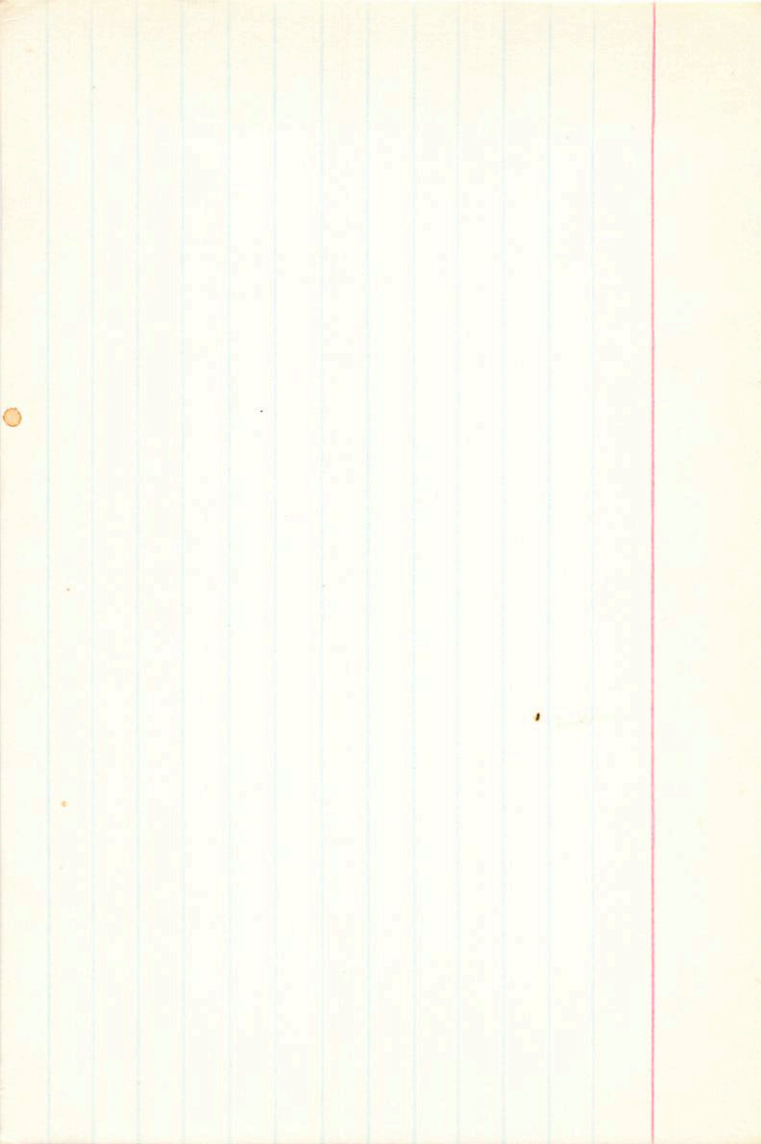
$\Delta(N-B)$  +1.35

N ✓ W

+26.2 -24.4 -1.4

+4 -17 -1

-19.1 -0.212 -0.314



155185

17

08.7 -46

29

1400

old

43497

277(12)

106(20)

186(17)

---

16

9.20 + 0.86 + 0.435 (2)

8.88 + 0.315 (2)

8.57

$\Delta (B-V) + 0.4$

$\Delta (U-B) + 1.75$

M(I)	7(100)
+ 5.12	10.23
<hr/>	
8.56	20.5
3.44	

2 V W

-0.30 -0.000 -0.680

+100.4 -94.3 -69.7

+9 -26 -17



end

97214 11 088 -10 42

Y2603

46617)

9.24 + 1.08 + 0.90 (4)

8.55 + 0.485 (2)

m(I)

H(1/2)

$\Delta(13-4) + 13$

$\Delta(11-3) + 265$

+655	048
<u>867</u>	<u>048</u>
152	050

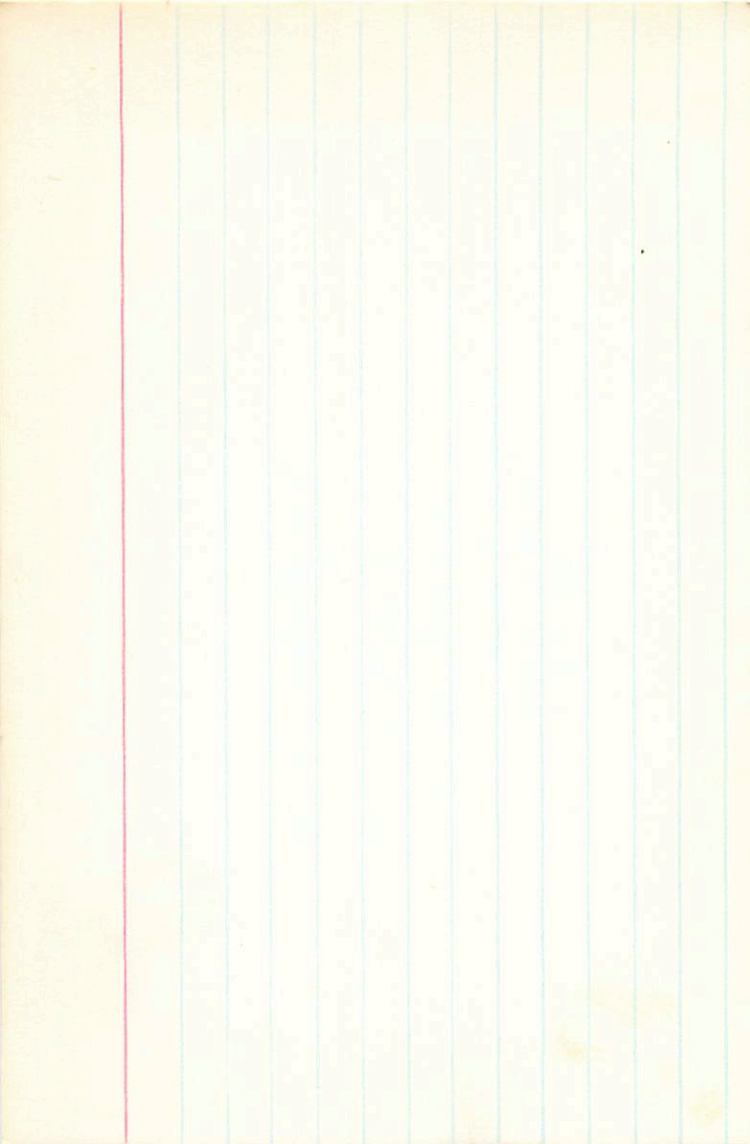
21 ✓ W

+112.8 - 22.2 + 28.6

+53 + 3 0

+400 450 + 600

→ +108.6 - 224 + 29.6





How

1502463 11 00.7 44 45 128

Net yield

8.70 +1.175 +1.125 (2) M(I) 7/107

8.18 +0.46 (2)

+6.45  
772  
1.27  
055  
056

$\Delta(13-4) -015$

$\Delta(14-3) -02$

M V W

+23.6 -20.3 +49

+11 -4 -6

-0.244 -034

48.2

→ +23.2 -20.1 +5.1

97233 ~~11 08.9 14 42 dmo~~

+2502393

11 33.2

+2452

4pm

128

not full

9.35 +1.00 + ~~0.755~~ (2)

8.79 +0.405 (2)

$\Delta(B-U) +07$

$\Delta(U-B) +21$

M(I)

+622

838

276

$\pi(1st)$

036

037

M

L

W

+4.6

+5.7

+7.0

etc

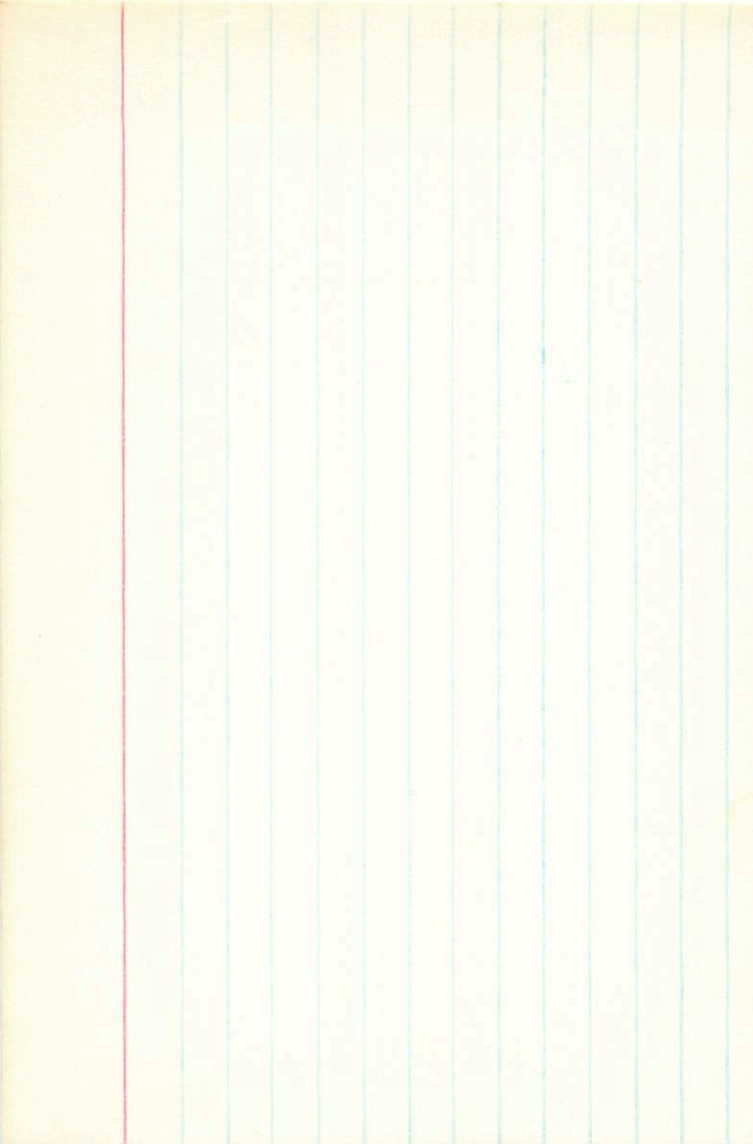
+1

+2

0

13.8

H<sub>2</sub>S +0.004 +0.056



year

+1702376      11 33.4      +17 15      128

not yet

9.57 +1.10 +0.575 (2)

8.54 +0.44 (2)

$\Delta(B-V) - 0.2$

$\Delta(M-R) + 0.8$

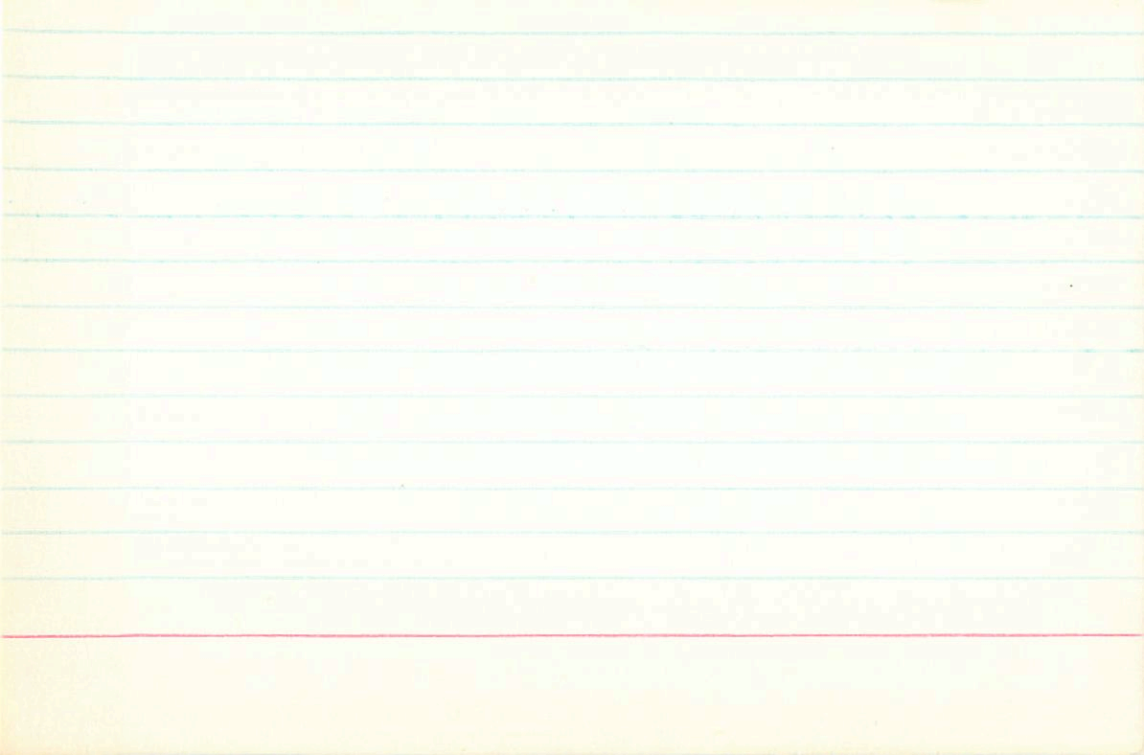
M(I)  
6.38  
9.50  
-----  
2.12

$\pi(\text{ref})$   
0.37  
0.375

M V W

OK  
-2.3 +5.5 +4.6  
-3 +2 +1

+1.3 +0.80 +0.20



101501

11 38.4 + 34 29

68W

42699

5.34 + 0.75 + 0.25 (3)

5.02 + 0.255 STD

M(LT) 7(1024)  
+5140  
477

$\Delta(13-0) - 0.2$

$\Delta(12-0) + 0.5$

$\frac{+39}{477}$  1025  
1195

110  $\Delta(14)$

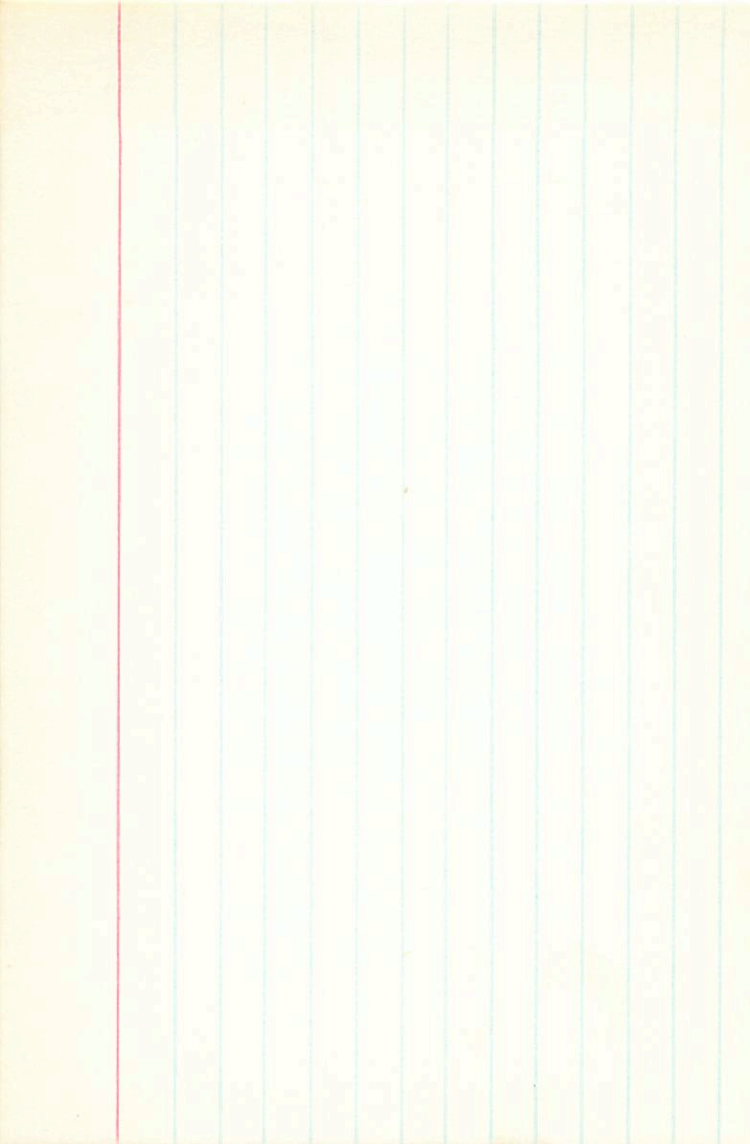
N ✓ W ✓

-7.9 - 15.7 - 3.6

-7 - 17 + 2

-7.2 - 13.0 - 3.8

→





+31<sup>0</sup>2290

11 42.1 +31 15

old

not good

8.98 +1.13 +1.055 (2)

8.36 +0.415 (2)

8(13-v) -0.45

8(12-g) -0.65

M(12) 7(12A)

+6.88

7.95

1.69

0.425

0.415

n v w

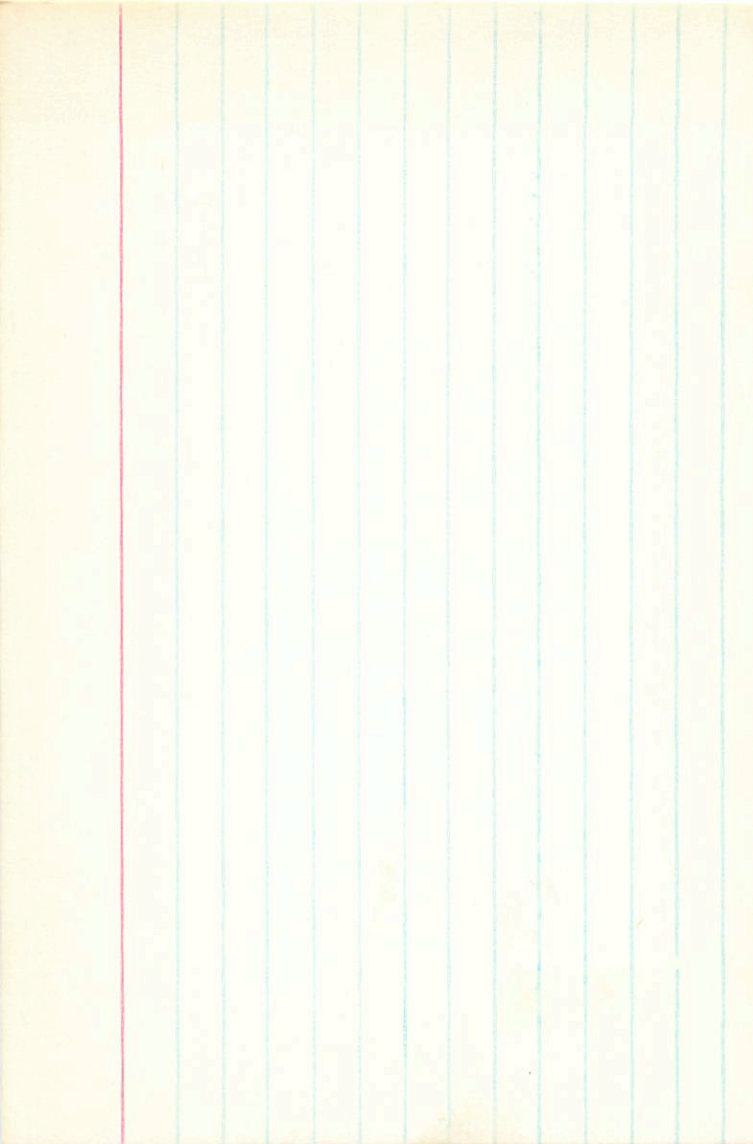
-5.0 -42.9 +25.3

-5 -18 0

+26.2

-0.060 -0.350

→ -4.0 -35.3 +25.3



4 hours

+720545      11 43.0    +72    21    128

multiply

8.94 +117 +1.12 (2)

8.35 +0.46 (2)

m(7)

+6.50

7(104)

B(13-4) -01

D(12-8) -015

789

.0505  
050

M V W

-11.6 -7.4 -19.8

D +3 -2

-23.1 +0.023 +0.066

→ -11.6 -7.7 -19.6

