

224

-270116

62 308

-27

01

8960

→ -038

-120

(7.62 + 1098 + 0.70 C) ?

951 + 0.61 + 10.085 (1)

S. 021-52

228.000\*

0.000\*

32.500\*

-27.000\*

-1.000\*

-0.035\*

-0.120\*

4.500\*

79.433

0.000

-0.436

-0.051

-34.617

-0.401

0.040

-31.883

50.006

-0.998

0.492

224

250205

00

22.5

-24

42

20FS

Y + 191 + 2014

①

9.62 + 0.43 - 0.135

535 Oct 1914

229.000\*  
0.000\*  
32.500\*  
-24.000\*  
-42.000\*  
0.190\*  
0.020\*  
5.350\*  
117.490  
0.000  
0.819  
-0.030  
96.195  
-0.383  
0.074  
-45.033  
-0.053  
-0.997  
-6.223



266-135

00 32.7 -17

35

15.0 0 : 61 30

230

268-5

15.2 0 . 59 58

15.2 15.1 6-1.192-89

14.94 + 0.235 - 0.585 (1)

561  
+10  
+10

230.000\*  
0.000\*  
32.700\*  
-17.000\*  
-35.000\*  
0.600\*  
0.010\*  
1.950\*  
24.547  
0.000  
2.454  
0.035  
60.248  
-1.427  
0.179  
-35.036  
-0.171  
-0.983  
-4.206

232

46485

60 32.7 -22 54 126 126 175

11.84 18475 + 0.095 D

+10 -125 7.25

232.000\*

0.000\*

32.700\*

-22.000\*

-54.000\*

0.010\*

-0.125\*

7.250\*

6.5  
200 263

281.838

0.000

-0.267

-0.013

-54 -70 -75.341

-0.529

0.101

-106 -139 -148.961

-0.050

-0.995

-14.091

46437

00 228

-29

11

13-9

109

67

233

13.06 + 10.84 + 10.45 (2)

1-9 Oct 2017

233.000\*

0.000\*

32.800\*

-29.000\*

-11.000\*

0.100\*

0.040\*

6.100\*

165.959

0.000

0.503

-0.069

83.412

-0.082

0.007

-13.640

-0.035

-0.998

-5.878

234

825-458

DD: 32.4 -28 34 146 15.4 h. 200143

(+)

~~1395 #006110015~~

1481 + 0.725 + 0.275 (1)

JCS Soc SS14

234.000\*

0.000\*

32.600\*

-23.000\*

-34.000\*

0.155\*

-0.205\*

9.250\*

144 8.5  
501

707.946

0.000

0.123

-0.019

+62

87.265

(+2)

-1.207

0.091

-604.4

249

-854.283

-0.112

-0.996

-79.634



235

46440

SD

33.3

-21

50

14.4

105

108

13.93

+0.68

+0.03

①

45

0.03

235.000\*

0.000\*

33.300\*

-21.000\*

-50.000\*

0.100\*

-0.030\*

705 7.300\*

257 288.403

0.000

0.331

-0.001

485 95.380

-0.366

0.115

-94 -105.454

-0.043

-0.993

-12.318

4105 -30 7.3

236

765-73

60

33.3

-20

11

11.7 12.5

g-h

.158

59

12.29 1096 1090 ①

79

4170 4100 5.7

236.000\*

0.000\*

33.300\*

-20.000\*

-11.000\*

0.170\*

0.100\*

5.700\*

138.038

0.000

0.935

0.014

129.021

-0.016

0.139

-2.238

0.011

-0.990

1.506

240

-220181

OD 33.4

-21

54

9.8

F5

Y +054 -106

10.61 +0.71 +0.155 (2)

574 465  
501-55+

240.000\*  
0.000\*  
33.400\*  
-21.000\*  
-54.000\*  
0.055\*  
-0.105\*  
4.650\*  
85.114  
0.000  
-0.037  
-0.001  
-3.110  
-0.557  
0.114  
-47.409  
-0.064  
-0.993  
-5.433

+0286 +017 M

241

21070

070 33.6 -21 02 8.0 F=0

4 +105 +009

①

7.85 10.425 -204

4.0  
511 + 2011  
+100

241.000\*  
0.000\*  
33.600\*  
-21.000\*  
-2.000\*  
0.100\*  
0.015\*  
4.000\*  
63.096  
0.000  
0.442  
0.007  
27.866  
-0.185  
0.126  
-11.680  
-0.020  
-0.992  
-1.282



243

-240169

00

340

-24

33

9.165

4 +108 -025

10.43 +0715 +0.265

①

110-30 495

242.000\*  
0.000\*  
34.000\*  
-29.000\*  
-33.000\*  
0.110\*  
-0.030\*  
4.950\*  
97.724  
0.000  
0.371  
-0.069  
36.293  
-0.392  
-0.001  
-38.290  
-0.025  
-0.998  
-2.451

46449

BD 340

-24

54

140

116

146

243

13.44 + 0.855 + 0.44<sup>4</sup> ①

465-45 7.0

243.000\*

0.000\*

34.000\*

-24.000\*

-54.000\*

0.065\*

-0.095\*

7.000\*

204 240 251.189

0.000

0.028

-0.026

5 7 5 7.128

-0.544

0.068

-97

-87 -130 -136.536

-0.038

-0.997

-9.519

2011

46451 07 342 -23 18 12.0 138 210

months

2 10.26 +0.70 +0.04 ①

7

-70 -120 395

244.000\*

0.000\*

34.200\*

-23.000\*

-18.000\*

-0.070\*

-0.120\*

3.950\*

61.660

0.000

-0.580

-0.011

-35.748

-0.311

0.092

-19.205

-0.022

-0.996

-1.361

765-50

00 34.3

-19

07

17.1 14.8 g .154 117

246

14.42 +0.685-0.20(2)

6.0 58-5714

246.000\*  
0.000\*  
34.000\*  
-19.000\*  
-7.000\*  
0.165\*  
-0.085\*  
0.400\*  
12.023  
0.000  
0.457  
0.027  
5.496  
-0.745  
0.153  
-8.952  
-0.103  
-0.988  
-1.236



LTT 027

247

46453

070

344

-24

46

16.7

223 168

266-138

070

344

-24

46

8.4 + 2.25 = 10.65

268-8

10.1 + 3.26 = 13.36

25022

8.078 50.240 170

8.20 + 0.65 = 8.85 (1)

440-240 2-6

247.000\*

0.000\*

34.400\*

-24.000\*

-46.000\*

0.040\*

-0.240\*

2.600\*

33.113

0.000

-0.432

-0.024

-14.289

-1.068

0.069

-35.352

-0.064

-0.997

-2.114

256

46454 . CD 345 -25 14 125 103 96

12.6

-250224

$m_1$   $m_2$   
+100 -95

1175+075 +024 (1)

mc (II) plate

+100-50 5-9

250.000\*

0.000\*

34.500\*

-25.000\*

-14.000\*

0.100\*

-0.050\*

5.900\*

151.356

0.000

0.281

-0.028

42.481

-0.448

0.062

-67.822

-0.036

-0.998

-5.411

251

46456

00 34.7

-14 44

148

165 115

268-10

00 34.7

-14 44

12.4 +3

21 117

-20° 5'

10.92 +0.805 +0.315-①

445  
+160-80  
0914

251.000\*

0.000\*

34.700\*

-19.000\*

-44.000\*

0.160\*

-0.000\*

4.450\*

77.625

0.000

0.449

0.023

34.834

-0.713

0.143

-55.380

-0.093

-0.989

-7.204

ADD 528

10225 - 10

252

1331 32

46457

00 347 -25 02 5.5 6.7 1.0 1.37650

-250228

5.59 +0.715 +0.20 (4)

5.25 +0.27 (4)

634

+1390 -15 0.55

252.000\*

0.000\*

34.700\*

-25.000\*

-2.000\*

1.390\*

-0.015\*

0.550\*

12.882

0.000

5.581

-0.025

71.895

-3.483

0.065

-44.875

10.368

-0.998

-4.738



44 454 00 348 -32 14 131 115 125

255

12.74 10.95 10.64 (1)

58.5  
59-564

0.163  
-0.995  
0.001  
-73.498  
-0.043  
-0.497  
33.330  
-0.091  
0.225  
0.000  
147.911  
5.850\*  
-0.065\*  
0.095\*  
-16.000\*  
-32.000\*  
34.800\*  
0.000\*  
255.000\*

4+1824

WYLD

254

142 .315 230

00 34.9

-21 10

15.7 +1 .35 224

14.9 +1 .35 227

13.7 146 9 .36 224

0.0 2.1 2.0

266-141  
269-12  
825-554

14.50 +0.465 -0.54 (4)

-250-220 1.0

256.000\*

0.000\*

34.900\*

-21.000\*

-10.000\*

-0.250\*

-0.220\*

1.000\*

15.849

0.000

-1.555

0.011

-24.648

-0.266

0.122

-4.211

-0.049

-0.993

-0.779

254

46464 80 35.1 -34 22 124088 70

12.68 + 0.865 + 0.52 <sup>(2)</sup>

529  
+85 6.25  
+90

259.000\*  
0.000\*  
35.100\*  
-34.000\*  
-22.000\*  
0.090\*  
0.035\*  
6.250\*  
177.828  
0.000  
0.448  
-0.108  
79.753  
-0.081  
-0.075  
-14.868  
-0.043  
-0.991  
-7.634

4445

4445

00 352

21

16

138 OSC CS

260

①

12.73 + 0.65 - 0.075

+90 +05 6.6

260.000\*

0.000\*

35.200\*

-21.000\*

-16.000\*

0.090\*

0.035\*

6.600\*

240 208.930

0.000

0.450

0.011

+108 94.089

-0.082

0.119

-19. -17.078

-0.005

-0.993

-1.039



266

4644 80 354 -22 47 13.3 134 130

G-D 630 80 354 -22 44 14.06 .18 138

1340 + 0.65 - 0.04 (1)

75

+120-100

266.000\*

0.000\*

35.400\*

-22.000\*

-47.000\*

0.120\*

-0.100\*

6.6

12.900\*

209 288

3801.894

0.000

0.237

-0.002

48

67

899.308

-0.698

0.097

145 -202 <sup>2452</sup> -2654.745

-0.068

-0.995

-260.015

267

4690 60 355 -20 37 13.9 124 229

$13.67 + 0.715 + 0.08$  ①

95-80 235

267.000\*

0.000\*

35.500\*

-20.000\*

-37.000\*

-0.095\*

-0.080\*

7.350\*

295.121

0.000

-0.582

0.018

-171.783

-0.085

0.128

-25.204

-0.021

-0.992

-6.332

19-

131

224 209  
66  
2

268

41072 00 355 -21 00 145 106 147

13.65 70.995 10.620  
13.31 70.385 ①

455-90 6.65

268.000\*

0.000\*

35.500\*

-21.000\*

-8.000\*

0.055\*

-0.090\*

6.650\*

213.796

0.000

-0.001

0.013

-0.253

-0.496

0.121

-106.104

-0.060

-0.993

-12.920

270

46476 00 35.5 -02 05 14.5 III 154

13.01 +0.675' +0.025' (2)

1-6 001-054  
+50-100 7/

270.000\*

0.000\*

35.500\*

-32.000\*

-8.000\*

0.050\*

-0.100\*

7.100\*

263.027

0.000

-0.043

-0.087

-11.259 -10

-0.528

-0.043

-138.763 -124

0.026

-0.995

6.927

284  
685



-370211

10.7 120

271

-6046 -168

46477

9.5

.130 2.13

267472

80

35.5

-36

42

11.971

220 208

10.19 + 0.77 + 0.225 (1)

65 851-024  
+70 -155 39

271.000\*  
0.000\*  
35.500\*  
-36.000\*  
-42.000\*  
0.070\*  
-0.155\*  
3.900\*  
60.256  
0.000  
-0.090  
-0.128  
-5.443  
-0.295  
-0.110  
-47.886  
0.101  
-0.986  
6.068

272

46478      00 35.6      -24 28 13.0 120 74

---

Published 16.54 454 00 3.11.1948

12.55 4880 10.36 ①

115 + 35 6.25

272.000\*

0.000\*

35.600\*

-26.000\*

-38.000\*

0.115\*

0.035\*

6.250\*

177.828

0.000

0.551

-0.037

97.989

-0.143

0.039

-25.365

-0.026

-0.999

-4.615

825-576

00

358-2119

121 140 1200

125

274

13 12.25 + 0.315 ①

37

1212

$$\begin{array}{r}
 1196 \\
 49 \overline{) 1196} \\
 \underline{490} \phantom{0} \\
 706 \\
 \underline{706} \\
 0
 \end{array}$$

465-115 205

274.000\*

0.000\*

35.800\*

-21.000\*

-19.000\*

0.165\*

-0.115\*

6.1 7.050\*

166 257.040

0.000

0.381

0.012

62 97.819

-0.869

0.117

-143 -223.251

-0.098

-0.993

-25.198

45535

20281

266-144

246-16

265-74

00

358

-18

59

275

12.4

.405

113

10.2

+3

.40

93

13.2

+3

.45

93

11812.9 m

.397

101

11.71 + 109 + 0.81 (1)

11.17 + 0.44 (2)

10.99

10.14

5.9

4

+400-75 4.4

275.000\*

0.000\*

35.800\*

-18.000\*

-59.000\*

0.400\*

-0.075\*

3.7

4.400\*

549

75.858

0.000

1.429

0.034

+78

108.396

-1.287

0.152

-70

-97.650

-0.149

-0.988

-11.311



276

46481 60 35.9 -26 41 170 096 133

13.24 to 50-050 (2)

470-65-0.25

276.000\*

0.000\*

35.900\*

-26.000\*

-41.000\*

0.070\*

-0.065\*

-0.250\*

8.913

0.000

0.121

-0.036

1.083

-0.436

0.038

-3.883

-0.021

-0.999

-0.186

277

-220107

825-604 <sup>2060</sup> <sub>362</sub> "

010 36.8

-21

34

8.5

90 g

1.250

126

14.5 16.0 m  
unfilled

3

9.57 1025 (1)

9.27

9.9

9.4

1.5



45  
55-155  
+155

277.000\*

0.000\*

36.000\*

-21.000\*

-34.000\*

0.195\*

-0.155\*

4.500\*

79.433

0.000

0.402

0.011

31.928

-1.104

0.113

-87.656

-0.122

-0.993

-9.658

895-615

280

00 362 - 25

18 13.5 14.7 h-m 240

102

191 Street 246-1103

1333 46.915 <sup>575</sup> 70~~45~~ ①

NO 1071 + 0.11 + 1.015 ①

9-7 05-1824

-13.379

-0.998  
-0.064

-163.670 -121

0.058  
-0.783

172.182 +127

-0.023  
0.824

0.000  
208.930

6.600\*  
-0.050\*  
0.235\*  
-18.000\*  
-25.000\*  
36.200\*  
0.000\*

280.000\*

154.5

273

220187

DN 36.3 -27 27

281  
9.8 60

4 +050-052

9.34 +0.61 +0.04 (1)

584 05-054

-1.952

-0.999

-0.021

-39.650

0.026

-0.425

22.322

-0.042

0.239

0.000

93.325

4.850\*

-0.050\*

0.090\*

-27.000\*

-27.000\*

36.300\*

0.000\*

281.000\*



825-617

07

864-25

33

1741534, 2007

282 ✓

101

14.06 + 0875 + 10.44

①

4150-130 7.3

282.000\*

0.000\*

36.400\*

-25.000\*

-33.000\*

0.150\*

-0.130\*

6.6 7.300\*

209 288.403

0.000

0.282

-0.024

59 81.360

-0.896

0.054

-197 -258.378

~~-0.055~~

~~-0.998~~

-15.845

BD

-220 109

OD 34.5

-21 33

9.0 6.5

283

7 +067 +023

9.21 +0.605 +0.021 ①

1.7 Set 541

283.000\*

0.000\*

36.500\*

-21.000\*

-33.000\*

0.095\*

0.025\*

4.100\*

66.069

0.000

0.445

0.013

29.430

-0.135

0.113

-8.938

-0.010

-0.994

-0.638

46455

00 36.9 -26 32 149 102 163

286

1408 + 101 + 072 (2)

130-95 6.85

286.000\*

0.000\*

36.900\*

-26.000\*

-32.000\*

0.030\*

-0.095\*

6.850\*

245 234.423

0.000

-0.115

-0.032

-28 -27.023

-0.458

0.038

-112 -107.302

-0.014

-0.999

-3.217

46507

07 37.3

-20 07

12.4 14 85

243

① 10.98 + 07.15 + 0.21 ①

+140 +10 5.15

293.000\*

0.000\*

37.300\*

-20.000\*

-8.000\*

0.140\*

0.010\*

5.150\*

107.152

0.000

0.589

0.028

63.135

-0.308

0.132

-33.003

-0.024

-0.991

-2.577



4/6508

00 07.3

-24 53

134 100

25

294

12.22 11.01 10.18 (1)

195 + 25 5.15  
504 54

294.000\*  
0.000\*  
37.300\*  
-24.000\*  
-53.000\*  
0.095\*  
0.025\*  
5.150\*  
107.152  
0.000  
0.445  
-0.015  
47.709  
-0.135  
0.062  
-14.510  
-0.015  
-0.998  
-1.622

-250245

245

18

8.7 60

46514

00

37.4

-25

19

11.5 156

217

Y +022 -162

BPM -094 -125

205 13

8.76 +0.71 +0.125 (4)

8.77 +0.71 +0.125 (1)

8.76 +0.71 +0.125 (2)

-35-140 2-65

0.000\*

37.400\*

-25.000\*

-19.000\*

-0.035\*

-0.140\*

2.650\*

33.884

0.000

-0.490

-0.019

-16.607

-0.427

0.055

-16.158

-0.017

-0.998

-0.526

U-

18-

263

296.000\*

LTT 350

297

46515

0

13.5 1372 109

266-150

00 37.5 -28 18

13.5 + 1.37 109

267-152

13.6 + 2.38 115

269-11

14.0 + 1.38 113

881-269

12.413.4 R 253 111

12.70 + 0.68 - 0.015 (3)

12.59 + 0.26 (1)

+350 -135 6.45

297.000\*

0.000\*

37.500\*

-28.000\*

-18.000\*

0.350\*

-0.135\*

5.7

6.450\*

138

194.984

0.000

1.075

-0.046

149

209.579

-1.415

0.010

-157

-275.910

-0.064

-0.999

-12.513

---

299

46517 00 32.8 -27 32 146 100 220

13.02 + 0.695 - 0.03 (2)

65-25 4.55

299.000\*

0.000\*

37.500\*

-27.000\*

-32.000\*

-0.065\*

-0.075\*

6.550\*

204.174

0.000

-0.449

-0.039

-91.592

-0.141

0.022

-28.775

0.014

-0.999

2.933



MT 25)

46518

$\frac{300}{178}$

264 131

267-150

00

37.4

-33

28

12.3

+

29

124

269-10

12.5

+

2

131

132

10.96 + 0.425 - 0.19 ①

11.00 + 0.195 ①

!

5.9 081-5ct

300.000\*

0.000\*

37.400\*

-33.000\*

-20.000\*

0.225\*

-0.180\*

6.500\*

5.95  
1545

199.526

0.000

0.465

-0.092

72

92.714

-1.284

-0.064

-198

-256.131

0.040

-0.994

3 2

7.932

46519  
~~267-133~~

2501

301

9.0 224 139

9.0 +1 .31 103

269-13

00

37.8

-34

14

86+2 .31 106

6.7.2

6.70+51-02 ①

6.68 52 -02

✓ 2.2 90-1031

301.000\*  
0.000\*  
37.500\*  
-34.000\*  
-14.000\*  
0.310\*  
-0.090\*  
2.200\*  
27.542  
0.000  
1.029  
-0.100  
28.334  
-1.133  
-0.078  
-31.192  
-0.015  
-0.992  
-0.412

20297

302

00 37.7 -19 42 120 137 235

12.06 +0.935 +0.55<sup>60</sup> ①

4110-80 5-1

302.000\*

0.000\*

37.700\*

-19.000\*

-42.000\*

0.110\*

-0.080\*

5.100\*

112.5 104.713

0.000

0.244

0.034

27 25.534

-0.592

0.137

-67 -62.015

-0.074

-0.990

-7.724

↔

Old

19467

3 04.9 -13 57 65 BNot <sup>July</sup> ~~July~~

6.94 +0.64 +0.12 (2)

m(1)

+3.97

6.78 +0.20 (2)

6.58

$$\Delta(B-v) = -0.5$$

$$\Delta(u-B) = 0.00$$

$$\pi(\text{pt}) = 0.30 \text{ sq}$$

$$n-m = 261$$

|                 | u     | v     | w     |
|-----------------|-------|-------|-------|
| <u>194630yr</u> | -19.5 | -32.7 | -21.2 |
|                 | -8    | -9    | -3    |

e

+12.3  
~~100~~

" 0.000 -0.264

.030

+3.97

-19.8 -33.0 -21.3

-5° 3063

10 24.2

-6 15

108

X 2447

9.79 +0.95 +0.645 (2)

m(I) n(II)

310(16)

9.22 +0.415 (2)

15.88

0285

84(10)

$\Delta(B-V) +135$

551

027

17

$\Delta(U-B) +345$

282

+279 -0.008 -0.655

u v w

-47.9 -93.1 -40.4

674

164

-16 -21 -17

→ -51.7 -97.3 -43.7



18143 A 2 52.7 +26 40 DR2

603.0

A 7.62 +0.93 +0.71 ③

7.18 +0.32 ③

+1  
+2

G-36-43 13.86 +1.575 +1.16 ⑤

12.51 +1.24 ①

+36.4 -16.8 -15.2

+6 -14 -1

0226  
0227  
+300.0

(X)

4747      00 47.0 - 03 29

1420

716 10.27 10.30 (4)

654 10.24 (3)

5-8<sup>4</sup>(10)

8(13-1) 108

522(1)

8(11-0) 119

Not Merged

R Pal

941 3 06.1 444 40 NO III

19474 (I) 3.81 +0.48 +0.83 J

I R-I 4(L)

342 302 +0.35 +0.95

338 306 +0.324

206 +0.34 +0.44

1030 430 -16.8 -12.1  
211-41 260 46 -10 -2

6-11.4

Σ An

951

3 08.8 +19 32

102 III

1977

J

4.37 +1.03 +0.86 J

~~II~~ R-I u(I)

3.60 +0.36 +0.35

392 3.57 +0.35

6 = 32.1 +0.355

.022 +37.6 -16.8 +2.2

2-M 3.27 +4 -5 +3

191345

3 02.5 +25 03

$\Delta m = 00$  1"  
5.46 -0.03 -0.35 J B7 E

20150

3 12.0 +20 51

4.89 -0.02 -0.01 J 140 E -E

1'

10 m L v

16753

3

17.3

-21

56

gms

20728

3.76+162 1.87

5

C?

F R-I 4(LI)

1.38 +1.125 5

1.26 +1.12 10<sup>2</sup>6<sup>5</sup>

1.32 +1.12 -3.3

f = -56.0

21531

3 26.3 -19 5-7 dm8

8.42 + 1.32 + 1.24 (2)

7.63 + 0.55 (4)

2/18-1) + 2  
24

077 + 47.6 - 14.5 - 5.3

0.57 + 23 - 5 + 17

+ 561 1341  
+ 340

x News

1949

4 33.0 +16.24 125.17

29139

086 +155 +1.55 5

-0.07

-0.75 +0.685 (1) 4

-0.68 +0.655 (5) 4(1)

-0.80 +0.735 102.65

0.74 +0.705

-2.0

.056

+186

-16.8

-23.7

2.41 125

-1

-9

-3

$\frac{0}{-20.3}$

4 Nov  
1805

S 243 +34 25 fR3p

cnstr  
H lin work

35620

R R-I M(I)

5.06 +140 +1.66 A

3.93 ± 0.50 A -1.37

6 0.0

.0087

+330 -16.8 -16.7

m-m 5.30

0 -2 -1

redlined?

~~35619 S 243 +34 42 9.55-10.24-0.71 07 J~~

35621



$n^{\circ} 50V \pm 6cm$  2yd

+108

2742

7 20.6 +82.30

SS56 I R-I

read 485 +1.63 +1.80 2g

0.62.36 +120 R2,45

11(I) -4.10

$b = +28.2$

-0051 +37.2 -168 +7.5

mu-16.43 +1 -1 0

55075

7 15.9 +11 21 612 -0.04 -0.10 (new) <sup>85</sup>

2993

7 41.5 -28 17

62576  
HOTOY

<sup>610</sup> 282 H.715 295 -

4.58 +163 +198 2595 -

295 +0.725 5

4.58 +163 +201 9155

M(2) 5

4.58 +164 +192 (C)

f = -2.3

Pos M

W/O?

Pos?

630 636 +1 +1 0

61487 7 29 30 -27 53 88 6.55 -0.18 -0.91 Crew

62445 7 41 34 -25 41.4 89 8.35 H.0.025 -0.215 (9) 49

62500 7 41 43 -28 24 85 10.16 0.00 -0.525 (5)

62640 7 42 43 -28 21 89 8.08 -0.135 -0.575 (2) 49

65273

7

53.8

-5-7

18

914

5272

Answer

3323

8 26.1 +60 53

→ G-5 II-III

71364

2.72 +0.285 J  
3.36

3.36 +0.95 +0.53 J

M(E) = +16

about ?

.017

+449

-16.8 -110

135.4

9m-m 3.58

+5

-4

-4

75732 8 yq.b + 28 31 dro

5.97 + 0.87 + 0.63 (2)

13.15 + 1.65 + 1.15 (2)

11.52 + 1.30 (3)

3777

9 26.6 -71 23

9102

82350

~~I P-I~~  
4.64 +0.36

5.46 +1.08 +0.99 C

5.48 +1.08 +0.96 (2) 99-

$n(I) (-0.05)$

5.07 +0.385 (2)

6 -14.8

0.011 +48.8 -14.8 -9.2  
4.80 +5 -2 -1

1970

E m-m

83979

9 34.32 -90.49

5.10 -0.15 -0.56 C

+03

6.0

79764

9 05.35 -90.26

4.71 -0.17 -0.76 C

+06

6.15

80950

5.86 -0.02 -0.04 A C 0

4246 10 50.6 +54 51 103 17

94247

4.00 +0.49 A

5.09 +1.36 +1.52 A nyne

35.1

→ ~~107~~

1077

+339

-16.8

-14.3

6 +55.1

m-m 5.57

+3

-1

-1

4409

11 23.0 -35 47

g 100

99322

5.27 + 0.995 + 0.745  $\textcircled{2}$  5.22 + 0.99 - cap

4.90 + 0.31  $\textcircled{2}$

6 + 23.6

.0127 +38.0 -16.8 -5.2

2 - m 4.47 +5 -2 -1



99322

11 23.1 -35 47

6967

5.27 +0.995 +0.745' ⊕

4.90 +0.31 ⊕

<sup>0.13</sup>  
0.0128

4.46

+38.2 -16.8 -5.2

+5 -2 -1

+23.6

4450

11 30.5 -31 34

G-7 III

100407 2.85 +0.34 5

3.54 + 0.94 + 0.71 J  
3.53 + 0.95 + 0.71 C

335  
- .50

6 + 28.1

10215 +36.0 -16.8 -23.8  
25-11 335 +8 -4 -5

101431

11 38 45 <sup>15-20</sup> -34 34 09 4.70 -0.08 -0.21 C

E

105671

12 07.3 -45 56

15 2

2802

440(6)

A

7.97 + 0

7.97 + 0.40 (3) (2)

B

11.90 + 1.16 (3)

Rudo  
2  
Budo

-4.2 <sup>4</sup>/<sub>372</sub> <sup>4</sup>/<sub>069</sub>

Ufanta

4682

12 16.5 -54 51 9 m3

107079

3.24 + 0.79 (102,65)

3.24 + 0.795 1895

5.00 + 1.59 + 1.95 C

5.00 + 1.61 + 1.94 4 Eggs

$\delta + 7.5$   
 $-2.5$   
 $\uparrow + 0.1 F 06$   
 $E_{OR-I} = 04$

10071      +424    -16.8    -14.7  
 m-m 5.75    +3        -2       -1

106490      12 13 34    -58 35 82E    2.79 - 0.24 - 0.89 C    E on-m  
 107250      12 18 26    -56 33 7.9 89    7.88 + 0.03 - 0.155 ③ + 13    7.0

4707

12 18.7 -60 15 gics

107446

225 40.54 7h.14<sup>m</sup>

2.28 +0.53 (10<sup>2</sup>, 151)

2.26 +0.55 1345-

355

-128

3.58 +1.45 +1.63 @ 5.55 -  
358 +1.41 +1.63 Copy

4220

0195 +406 -14.8 +15.7  
2h-M=3.55 +7 -4 +3

106563

12 16 50 -63 50

Q312 4.05 -0.18 -0.17 C +0.2 5.25'

107377

12 19 16-60 23 Q689

9.54 +0.135 -0.13 @ +0.25' 8.65'

107395

12 19 20 -61 52 9.085

8.99 +0.04 -0.48 @ +0.23' 9.35'

E 2h-M

109217

12 30.5 +10 34

7552

6.30 +0.965 +0.705 (3)

5.77 +0.345 (2)

+726

.0068

+33.2 -16.8 -13

6.00

+2 -1 0

4831

12

39.8

-4.7

32

8101

110458

3.91

3.51

+0.405 J

4.66

+1.09

+1.02

C

~~1.08~~

~~3.37~~

~~10.37~~

~~1102.64~~

~~1102.64~~

3.64

"012

+431

-16.8

-15.7

8 + 14.0

n-m 462

+4

-3

-1

4973

13 08.8

-43.06

grid

11474

5.27 +10.15 +0.915

(2)

5.25 +1.05 - 9m C

4.85 +0.365 (2)

.014

+37.1

-16.8

-6.5

8 119.3

M-A = 4.25

44

-3

0



5068

13 24.8 -15 42

101 17

116976

4.75 + 0.10 + 1006 J

3.55 + 0.305 J + PHS

4.75 + 1.09 + 107 C

$$\frac{+12}{-17}$$

6 + 46.0

$$\frac{E = +03}{B-V}$$

.015 -49.1 -16.8 +2.8

m-m 4.12 +5 -3 +1

↓ van

116658

19 23 36 -11 00

0.98 -0.23 -0.92 C B I

E

m-m

+02

3.0

0.96 -0.25 -0.93 J

R Rlypa

5050

new d  
375

12 27.0

-28 01

911722

117287

R

+181

5.65 +1.52 +0.53 399 new

May 8<sup>th</sup> 3.11 4935

4.98 +1.52 +0.79 g.

new 4.10 +2.17

6 1397

00055

1444

-16.8 +6.7

2h-m 6.31

+2

-1

+1

Gp 12.78 +1.045 +0.975 (3)

375  
380  
385

34081  
40860  
5679

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735  
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736  
399  
349  
737  
400  
350  
738

5297

14 Oct

-53 13

~~986~~ B5111

123569

474 +0.94 +0.72 C

454 +0.315 (2)

+26

.018

+388

-14.8

-140

$n-1 = 3.44$

+5

-5

-2

out?

5370

~~14~~ 174

+ 16 33

173 04

125560

485 + 123 4141 5

391 + 0.43 5

485 + 124 4137 4

$\frac{4.26}{5}$

$\frac{4.26}{5}$

8 + 6.9

014

+ 48.4

- 16.8

+ 12.8

28.11 = 4.26

+ 6

- 2

+ 3

131023

14 49

32

109 51

24 dls - 14 pds

up brackets



15 mag 20 2.60 10.25 10.375

-0.217 10.051

2035

+41.5

-16.8

-14.4

+8

-5

+5

135.6

131117

HR 5542

14 50 46 -30 27 6.25 G1

3354.0

✓ Red Hydrogen

317112  
136m)

6.46 + 0.59 + 0.10  
6.18 + 0.19

6.10 + 0.205 Mg<sup>70</sup>

1.070 444.4 -16.8 + 2.5  
202 + 9 -11 + 6

RRUM

5589

14 56.8

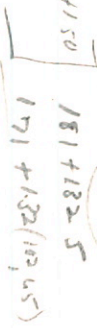
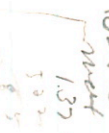
tbl 08

gas

1328 N3

~~1770~~ + 150 min

4.58 + 159 + 160 J



$\delta = 146.5$

$\cdot 009$   
 $-1350$   
 $-16.8$   
 $+16.2$   
 $+3$   
 $-2$   
 $+1$

I R-I

1.53 + 132

149 + 137

147 + 142

145 + 150



5705

15 18.6

-36 05

125 151

136422

2.10 + 0.645 J

2.03 + 0.63 10<sup>2</sup> 652.06 + 0.635

377

-191

6 + 124

0.175

+37.7 -16.8 -14.1

m-m 3.77

+2

-5

-1

E (12.2) + 0.3

1470

E m-m

136664

.15 21 14 -36 45

4.53 -0.15 -0.61 B5C C 104 5.45

137058

15 23 14 -24 38

4.60 0.00 -0.06 A0W C 103 3.50

5969

16 003

-25 43

g 105

143787

3.77 + 0.465 (2) S<sub>99</sub>

437

-62

501 + 1.24 + 1.23 2 E<sub>99</sub>

+19.7

 $E(A-v) \sim 0.10$ 

0135

+43.3

-16.8

-7.3

m-m = 439

+1

-3

+1

144334

16 04 20 -23 31 5.92 -0.08 -0.56 +0.11 6.75

144661

16 06 04 -24 22 6.32 -0.00 -0.52 +0.12 6.95

~~143275~~  
14333

15 58 29 -22 32 2.31 -0.11 -0.90 C

order  
number  
total

E

m-m

6072

16 16.0

-50 02

RU II-IV  
G 8 III

MUS 3<sup>u</sup> 3.22 +0.415 5

3.44

7.01 +108 +1.17 C  
4.02 +108 +1.17 5

f 6.0 = (R.I.) = N.09  
3.44  
N.10

.020 44.1 -16.8 +16.9  
3.44 +3 -6 +3

6103 20.1  
16 ~~15.3~~ + 8.1 00 120 17

147677

4.14 +0.32 5

4.85 +0.97 +0.80 5

4.86 +0.99 +0.79 4

6 1443

run straight

6.147

16 28.3 -16 30

68 IV

148786

3.65 + 0.3055

4.27 + 0.92 + 0.71 J

4.28 + 0.92 + 0.72 C

6 + 2.5

Neubau?

Amey  
absonderlich  
im Hintergrund

.0165

+33.6 -16.8 -8.6

3.89 (m-m)

0 -3 +1

6477

17 51.7

+40

02

123 III

163219

$9.5^m 2''$

S. 16 11.19 + 11.2 A

6 + 27.7

$(-1.10) + 0.44$  2005

21-11 = 5.35

+41.2

-16.8 -14.1

.0085

+2

+1

0

6482 18 37 11 -71 29 102 III

17159

3.00 + 0.40 @ 5% = 4.01 + 1.13 + 1.02 C

840

-11

1 - 25.0 E = +0.1 0.205 + 36.2 - 16.8 - 0.8

m-n 3.41 +5 -5 -2

169976

4.44 - 0.12 - 0.39 89 III C + 61

Rdgs

7157

18 53.8

+43 50 m5m

175865

070 + 149 (10245)

3.9 1.55 1500 E

087 + 148 5

075

6 + 178

0105

+445 -16.8 -3.4

9m-m 4.94

+4 +1 +1



183275 19 26.8 -27 05 113 11

5.5-1 +1.15 +1.14 (2)

5.15 +0.36 (3)

4.79

~~8.80~~

<sup>0</sup>  
-14.8

011 +335 -14.8 -8.0

-4.80 +1 -1 -2

cut?

7635

14 56.5 +19 21 125.5

184314

1.97 +0.685 J

2.06 +0.675 A

3.477 +15.7 +1.64 J

2.02 +0.68

3.47 +1.55 +1.92 A

6-5.2

.0105

+37.4

-16.8

-15.7

(m-n) = 460

+2

+1

-2

E = +05

7679 20 62.9 +19 50 122.18

140608

4.26 +0.37 A(1) 5.09 +1.06 +0.98 A

4.2-1

$\delta = -8.2$

$E = 2.05 \times 10^{-35}$

0.013 +47.3 -16.8 +11.2  
20-21 4.24 +3 +2 +1

E

140229

5.67 -0.08 +4.8 E 380-11 +0.06 6.40

144040

5.33 -0.04 -0.19 0.42 +0.05 5.20

8128

21 13.0

-15 22

gms

202364

3.30 +0.99 (102, 65)

5.24 +1.43 +1.86 ③

610

-2.50

↓ -38.7

E = +0.4 + 2.7 = 3.1

m-m = 6.10

Tou de tlow

202671 21 14 14 -15 09

5.43 -0.105 -0.50 E +07 6.05

2021519 21 12 39 -10 44

6.50 -0.08 -0.32 c/m 70.045 6.30

200761 21 04 10 -17 21

4.06 -0.01 +0.02 A/C 00 2.50  
4.07 -0.01 -0.015

204771

13514

21

22.6

+46

19

NO. 11

5.23 + 0.97 + 0.80

4.82 + 0.325 4

Grouped N

W. L. L. L.

8262

21 34.1

445 09

2044 1

311  
1653  
79

205738

1.73 + 1.68<sup>797</sup> 5

5.44 + 1.62 + 1.26 5

1.58 + 1.84 (1.82, 1.5)

5.37 + 1.60 + 1.27 5

1-5.0

20-21 = 6.4'

near SS layer  
unconformity  
understand well known

Benjamin

2047110

1

205905

21 36.2 -27 32 64  $\overline{10-11}$

52140

6.76 + 0.62 + 0.11 (3)

324(12)

6.58 + 0.205 (2)

496(17)

$\delta(10-1) - 1.5$

$\delta(10-1) + 0.3$

045

+38.7

-16.8 -14.5

1.73

+2

-6 -12

E 93-40/41

207451                      21 46.7    +05    29    dir

5271.0

36M(8)

42 Y(10)

66X(4)

8.68 +1.02 +0.83 (3)

8.02 +0.405 Y

14.93 +1.73 +1.15

13.28 +1.285 (2)

N of Wpdy



8636

22 29.7

- 47 09

m3 II

214952

-0.80 + 1.365 J

2.10 + 1.64 + 1.60 C

out

$$\begin{array}{r} 4.49 \\ \hline -5.29 \end{array}$$

✓

 $-58.0 = \beta$ 

.0125

+446

-16.8

-26.5

 $m - M = 4.49$ 

+6

-2

-3

8748

22 549 +84 05 124 17

217382

472

3.48 +0.535 5 4.72 +1.43 +1.70 5

6 = 122.2

2. - 21 = 4.80

+4.6 -16.8 -7.7

" .0105

+4 -2 -1

220572

23

22.5

-57

08

8112

14688

5.64 + 105 + 0.57 (2)

5.08 + 0.37 (2)

-56.6

.011

443.5 - 16.8 + 6.8

4.76

+4 -3 -1

222443

23

386

-1157

909

14839

588 + 098

92

5.42 + 0.335 (2)

BD9

+36.5 -14.8 +2.9

5.2

+3 -1 -3

223252

23 45.4 -03 02 R-8 III

5.48 +0.54 +0.70

5.07 +0.33 (2)

4.67

.0125

+34.3 -16.8 -1.9

4.52

+4 -2 -1

12/14/16 13 53.2 46 21 110 12

43178

18C17)

5.78 + 1.12 + 1.08 (1)

5.16 + 0.425 (2)

(24)

18 (13-1) - 0.2

0 (12-3) - 0.65

8.08  
- 1.0

9.40

0.011

4.50

248.9 - 53.0 - 20.0

+ 5 - 6 - 2

↔

old

6378

1 02.0 -25 52 145  $\bar{E}$ 

7215

9.82 +1.16 +1.14 (3)

M(I) H(pt)

46.40 0.035

9.14 +0.48 (4)

868 0.36 ←

39C(8)

866

 $\Delta(B-v) = +0.04$ 

|               | u     | v     | w    |
|---------------|-------|-------|------|
| $\Delta(B-v)$ | -27.7 | -33.7 | -5.2 |
| $\Delta(u-s)$ | -10   | -12   | 0    |

 $\Delta(u-s) = +0.04$ 

way 630

+3.7 -0.037 -0.334

|       |    |
|-------|----|
| 44    | 44 |
| +6.38 |    |

-27.2 -33.0 -5.2

→ 6660

01 049 422 42 42 d116

group

7224

41M18)

8.40 +1.12 +1.06 (2)

8.72 +0.435 (2)

m(F)

7(12)

+630

.0605

725

.064

988

.046 ←

14<sup>am</sup>  
10

Δ(B-V) 02

Δ(U-V) -02

.0

2 V W

+16 +.095 -0.488

-5.8 -22.9 -28.8

-4 -15 -17

→ +5.59 -4.2 -33.0 -32.5