

4.12 - 045 055 568 2.658 ⑤ 1520,23

2657

4.11	-712	810	-	2.191	26775
4.17	-709	818	-247	2.135	25"
4.12	-716	810	-239	2.203	28"
4.18	-735	795	-245	2.183	2920075

3.57 +547 237 387 2554 ③ 1523

1030 3.62 -191 1057 -421 2.093 26Jan75

3.60 -192 1036 -423 2.094 27 " "

3.60 -193 1062 -409 2.099 28 " "

3.63 -174 1057 -408 2.100 19 Aug 75

3.59 -175 1058 -400 — 28 " "

3.58 -177 1061 -402 2.096 31 Oct 75

3.62 -174 1054 -417 2.095 23 Nov 75

3.60 -199 1105 -433 2.092 27 " "

8727 22 547 -5 05 966

630 +95 +72 C

4874 23 172 + 48 22 120 MY

215945

5.43 + 1.04 + 0.81

5.63 + 0.36 > A

2014  
39051

5 42.6 14 25 9122 +27c

5.94 + 1.36 + 1.57 c

AC

+350 1451

682 +144.0

10.22 +0.73 +0.21 2 Sunday

-D<sup>o</sup> 1520  
405754

G 56.1 - 0 24

-92.0 to 1.1 B  
-91.6 ± 0.4

12 Y 10

24 V 14

39 C 9

24 ± 5

9.01 ± 0.49 ± 0.03 120"

9712

22

51.9

440

87

120

111

216646



7560

5.13	-248	875	-272	2.123	17 Aug 75
5.10	356	887	345	2.142	18 "
5.11	-362	913	364	2.124	19 "
5.10	341	856	362	—	
5.10	<del>324</del>	855	-374	2.142	20 Sept 75
5.10	355	923	377	2.144	25 "
5.11	347	850	343	2.152	26 "
5.11	-366	892	377	2.144	18 Oct 75
5.10	362	887	362	2.142	19 "
5.09	-361	848	362	2.141	1 Nov 75
5.09	350	873	-377	2.144	31 Oct 75

ms HD Ca 20-217  
G 78-26 = G 95-20 = LFT 268 = W 1324

85 0 1450  
100 30 20

$\mu = 1.20$

$\alpha_{1961} = 3^h 13^m 54^s$  }  $12.2$   $\Delta \alpha = +3.90$   
 $\delta_{1961} = +37^{\circ} 58.0'$  }  $+2$   $\Delta \delta = +13.3$

60" Feb. 23/24, 1963 W 1800  $\mu = 1.36$   $\alpha_{1965} + 167.3$   
10.66 1.20 1.01 (1.15)

85 M (10)  
30 V (20) 10.69  $+1.22$   $+0.97$  3 844-60"

4

G90-37

$\Delta 1961 = 7^h 58^m 36^s$  }  $+1$  }  $13.0$  }  $\Delta \alpha = +3.84$   
 $\Delta 1961 = +32^\circ 52.6'$  }  $\Delta \delta = -9.19$   
(1950)  $0^h 57^m 54^s$  }  $\Delta \alpha = +3.84$   
(1950)  $+32^\circ 54.4'$  }  $\Delta \delta = -9.19$

$\mu = 0.27$

60" Mar. 23/24, 1962      12.17      0.52      -0.18      .23  
 60" Oct. 28/29, 1962      12.12      0.52      -0.17      .22

322

Carbon +

W-142-03

17 22 05

-29 12.5

V E  
Pd 6.0

9.56 +4.57 = 2 1/2  
9.38 +4.63 = 3 1/2  
9.40 +4.53 = 3 1/2

5

(1)

7.10 +1.29 2-1/2  
2-1/2

8711 22 52.1 -16 32 122 17H

S.60 + 1.11 + 1.08

S.14 + 0.375 @ 102.65

8716  
~~8714~~

22

524

-5

15

947

8719 22 53.1 -31 54 120

6.09 + 1.36

2049

5 51.5

+10 34

69 II

+1336

39632

6.12.1149

+1.43 A

82



2044  
39640

5 49.5 -52 88 89 III +13e

5.16 + 0.59 + 0.73 C + 00089 - 07801 = 114

+

2051 5 516 +8 14 100 -42  
39695

6.30 + 1.25 + 1.46 L

5.66 + 0.465 (2) . GC

2053  
29721

5 50.9 -87 35 120

ac

+32/144

2093

5

553

+1

14

102

+3676

46352

6.22 + 1.47 + 183 C

CC

mm

Smithson

2097 5 55.6 -1 00 120 160.7

40397

6.22 + 1.14 + 1.20 C

CL

2059

5

56.1

212

48

9.49

41154

651145

40369

6073.5

-0011 4013

144?

4.27 6107

2065 5 52.4 -11 48 125 141 +8746

39853

5-66 +1.53 +1.84  $\pi$  GC  $\pm$  5.0  
+0047+039

467 +0.655 (2)

2105

5

579

448

56

120

11026

240486

Q-C



Udu

2063

5 529 + 20 88

g m r e

39816

2082

5

55.3 -39 58

9126

—

40091

5.551.50 ✓

GO

2081

5

55.5

+49

56

964

-416

40084

60

2090

5

557 + 54 34 100

- 564

40003

06

2006 5 540 -1130 05 +21.06

40000

230 ± 6.0

+0071 -051

5.50 + 1.13 + 1.11 ①

2026  
39385

5 y.g. -22 5-7 120 -

G.16 + 102 on (2.10) C R C

2220

6 13.3 +23 59 85 III -20.96

43261

609 +090 +1042

-5010 -015

8c ± 2.5

2225 ~~6~~ 11.7

42184



2235  
43335

6 13.5 +17 11 150 +37.9

AL

2242

U 136

-20

16

IPD

→

43346

5.91 + 1.32 (2.43) C

5.89 + 1.36 + 1.37 (1)

PL

5.24 + 0.49 (2)

504

43 00 11.2 -24 35 125 -

943

6.40 41.99 +1.65 1

541 40.605 (2)

66250

+

462 57 151 1129 2.837 B 15.11.73

3131

4.61	-628	+408	261	2.341	26.10.75
4.67	-639	<del>926</del>	<del>279</del>	<del>2.329</del>	27
4.63	-639	907	286	2.339	29
4.63	-639	896	271	2.329	11.11.75
4.63	<del>639</del>	897	255	2.348	12 "
4.67	-641	895	277	2.343	3 Jan 76
4.66	-639	896	283	2.342	"
4.67	-657	903	279	2.344	15 Jan
4.63	-652	905	270	2.339	18 "

11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31

(R) T Apr

20

48

14  
22

-5

7.2-14.2

2024

~~16~~ 16.5  
16.5

W Run

S 235 +36 52

-132 C

453.8 10.23 2.15 +1.74

457.7 11.33 8.56 +2.23

472.6 9.73 7.66 +1.23

488.6 8.95 2.16 +1.45

703.6 8.50 2.14 +1.43

712.6 9.17 2.29 +1.52

727.6 9.34 2.17 +1.56

(over)

70003 -0.12  
-2 0  
0 -0.12

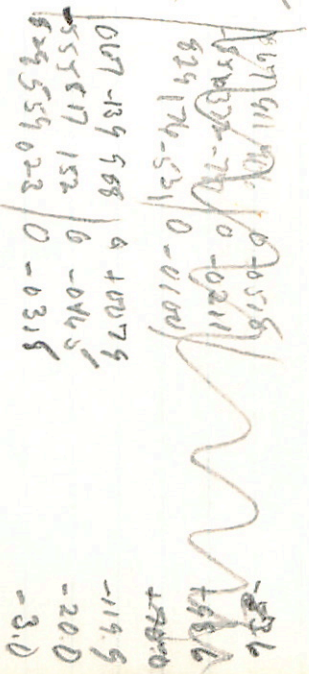
W Run 8.9

2.15 +1.42

W Run 8.9

7.15 +1.42

E = 10.35'



-3.3 -114 -46 0 -132.0 274' E=10.35'

8.8 +1 -3 -12 +1°

n v w

W Am

171.2 +1.0

35433

173.2 -0.2

8.04 +0.32 -0.46 +50±

35453

173.7 -0.5

2.44 +0.12 -0.75 0.56 +0.35 8.40

E





+4.72e

MOI ad

4' Run L 21.0 +49 19

H172289

<sup>5</sup>  
+0.0001 -0.0004 N30

+49 01488

4.91 + 1.96 + 2.14

+0.0003 -0.0007 GC →

H1D44537

4.75 1.42 2.18

-0.00012 -0.0007 FRY

FL8325

3.73 +0.86

+0.0001 -0.0003 FRY →

W4058

+0.0001 -0.0004

RW Bot 850

-000774.9 -015 453

129355

14 39.1 +31 47 7.67 gms -11c

8540 to RV

-0015 +002 6.177 1918.8 +31 47 5.89 1919.4

$$\frac{-0017 + 002}{-022 + 002}$$

-425 734 -263

642 678 320

-413 -026 910

+0563 -0070 +0493

-0596 -0064 -0660

+0372 0 +0372

-019 10000 -0026 430

+52.2 +12.9

-65.5 -3.5

-27.2 -10.0 452 MS

A R-I

500 +1.48

1/4 1/2

+0652 -0570 +0582 +22.1  
-0690 -0064 -0754 -28.6  
+0437 0 +0431 +14.4

724 +12.9 349  
-32 -3.5 435  
+6 -10.0 98

$$2 \sim \frac{1}{3} \frac{1}{9} = 3000$$

1174

712

2

245

+31

34

g 121

-34.37

15172

62

4.53 4.37

735

2

283

-22

46

g m 1 -18.66

15652

6.10 +1.58 +2.02 C

GC 73.0  
+0005 -0285

5.16 +0.74 @

926

2

273

+33

36

121 III

+746

15464

6.31 + 1.08 to 59

①

new position?

14 Feb

736

2

29.0

+35

55

125 III

-35.96

15656

4.

5.16 +147 +1.77

(3)

700381

+0165 FIV

4.89 +0.595 2A

739  
15755

2 259 +34 19

9 111

-2.2

22

~~24~~

743

2

33.3

+72

36

68

III

-2.36

15920

5.15 + 8.99 + 0.58

34 - 00637

+ 02229 Fly

4.80 + 0.315

34



747

2

335

+65

32

125 14

4/14

16024

578

+154

+188

1

GL

F50

578

+156

+185

A

100825

-0085

578

+155

+190

(1)

14028

7218

2

326

+37

05

9124

4.38

RL

15 mi

3.09 203

250

2 32.8 + 34 28

gms -5.56

16058

5.39 + 1.64 + 1.93 (5)

15023 - 0465  
GL ± 2.0

$$\begin{array}{r}
 4.05 \\
 \underline{2.98} \\
 4.02
 \end{array}
 + 1.02
 \begin{array}{r}
 10.96 \\
 \underline{40.99} \\
 (3)
 \end{array}
 \begin{array}{l}
 (1) \\
 (2) \\
 (3)
 \end{array}
 15.95$$

16187

757

2

337

+81

23

110

+268

6.18.187

RL

P 7<sup>th</sup>

758

2

340

+84

03

+66.78

16210

+84

+0017-015

LG

80 wt

3.78

366  
52

759

2

335

-8

3

no III

114.16

16212

5.52 + 1.58 + 1.92 C

4.52 + 0.865

(2)

-00257 -0572 F144

(BaZ)

774 2 40.6 +81 13 10p 48c

16454

5.76 +1.30 +1.16

n30 7.15  
+0071-068

777  
KLL  
11/17/1

2 ~~349~~ 34 47



825  
19974

2 SL-5 +42 01 G-p +73a

5.47 +089 +061 (5)

5.06 +035534

G-c

886  
18492

2 56.4 +40 50 122

+31.98

GL

745

+6016 = 043

new print...

902

2 58

~~2 58~~

+10 41 126

+18.36  
~~+18.36~~

18200

5.98 +159 +145

(7)

+60525 -026

6c +45

5.02 +0755

(2)

7 EMI

904

2

58.3

-3

05

9

m

1

+81.1

L.1-6.3

GL 745

L.2V

+1.24 + 2.06

(7)

+ 6065 1013

504

+ 0.90 (5)

~~444~~

19760

4.24 415

920

3 019 +55 52 G9 III -1097

18991

+0012 -026

Morganite

923  
15066

3 021 440 24 120 III -3418-

27

+012 -016 MC  
 0 +1  
 S Box 14 212 +54 02 -015  
 -17.0

+0002 ~016 Ind. in  

$$\begin{array}{r} -3 \\ 0 \\ -012 \end{array}$$

85 8.75 7.20 +140  
 98 8.82 7.22 +143  
~~305~~ 9.33 7.46 +150  
 324 8.74 7.32 +133  
 332 8.41 7.21 +125  
 355 8.47 7.28 +112

~~Wood 630~~

1.50  
 7.20 +125  
 680  
 16  
 $\frac{5.2}{3.5}$   
 (97)

-676 734 065 0 -0417  
 652 555 517 6 -0310  
 -343, 392 854 0 +0293

-111  
 -8.8  
 -14.5

5 Box 9.6  
 7.2 +128  
 -3.55 -36 -35 +4 0 -170 271 d  
 965 -4 -3 +2 -12 +590

+03  
 E=103

0.000*	0.000*
14.000*	14.000*
21.200*	21.200*
54.000*	54.000*
2.000*	2.000*
0.000*	0.012*
-0.012*	-0.015*
3.700*	3.700*
549.541	549.541
-17.000	-17.000
-0.042	-0.091
0.063	0.063
-24.091	-50.900
-0.031	-0.002
0.519	0.519
-26.087	-10.014
0.022	0.000
0.852	0.852
-2.269	-12.080