

2476

22

10.2

+58

57

100

210505

6.30 +1.12 +1.07

(28)

7-2-1941

20 28 43 -4 51

R: -24°

5
.

E 2-M

154939 6.12-86-17 89 102 5.1

144126 6.20-08-39 88 105 6.15

144126 6.21-10-41 105 6.55

VH 18 km 14 18 57 - 64 06.5 87-95

marks

BV RV



212 + 125 + 187 15 Jan 71

25

HT 8521

547

T' Gm

22 29.6 -4L R

-18.0

2440070	R	0.56	π -I	+2.25
0094		3.89		+2.41
0111		3.80		+2.37
0133		3.67		+2.32
0134		3.66		+2.30

1.26
4.21
5.21
6.36

243658		3.49		+2.11
2439700		3.55		+1.45
1021		3.52		+2.04
2707		3.58		+2.04
2703		3.54		+2.05

3.16
2.67
0.57
6.7
26.2
1.50
1.9
6.8

.69 ✓

-18.0

+0026 -013 Slay 1570

+9
+0035
+2
-011

+1036
+1339 +37
-0844 -16.8
-0816 -3
+14.0
+1.9
+14.0

919 114 -562
-200 975 -043
-537 -189 -822
+1098 -0059
-0341 -0508
-0916 +0098

279 μ

6.70 Hypothesis

25

3.12
2559
0.5
6.7 15

2.72
1.72

3x

3.12

2559

0.5

6.7

15

P Riv

13913

2

13.3 + 24

50

+0023-012

+0032-019 CL

+0025-010 new

+0023-010 MC →

+0024-010

+0033-010

1967

23.16
-0.58
21.4 + 38 18
5.03
1.8
1.9
1.7
1.7
1.535.3
52 -11.32

214
GC472

-0213 440 -026+3.6
-019
+2

RAnd

0 22 23.001 1960.2 + 38 18 2.20 1988.8

+055
.053

- 3 -44
1.07
3.27
26.5

070 -26.4

072 58

4.40
143
0.579

loss -0.56
-04 -0.035 MC

265/1940
1.85
1.54
1.70
1.25
13.25

25
24
25
32
52
60

-3 -0.016 Foluid
-15 -24

25
3.25
3.13
3.47

25
24
25
32
52
60

-007 -037
046

125
3.13
3.47

25
24
25
32
52
60

-4 -043

070 -2.6
-3 -46

070

-2 -39

367

230M

-7 -37

-113

230M

+863	+288	+414
-494	+306	+814
-107	+507	-406

-0286	-6505
+0144	-0587
+0036	-1591

-0791	-18.2
-0323	-8.6
-1555	-35.8

-22.9
-17.8
-10.4

-4.7
-9.2

4.0
-4.0

-4 -43

267M

-29.0

267
12
-83.7

0 -47

-0163	#0587	-0750	-27.5	-32.2
+0044	-0024	-0580	-19.4	-28.6
+0020	-1844	-1824	-67.1	-71.7

-13.7

-22.4
-0662

-0662

-57.1
-61.7
-2020

T Cup

P 8

E n-m

T Cup 105° +13.8

201886 101 +104 6.58 -0.11 -0.47 +05 6.95

1933

E = +07

T Cup 5.6 - -5.75 -79 +8 0 -41 -12 388

HR8113 3.5 +8.00 7.25 -27 +7 +1 -43

+14
+14⁰

~~###~~

40202012

HR 8113

GC29611

02

7-20 107

T Cep

21 08.9

+68 17

Phase	V	R	R-I	Phase	V	R	R-I	TB
C.005	9.07	5.96	2.94 58.5	523	5.38	3.20	1.95	260.6
061	9.27	5.98	2.95 90.7	688	6.91	4.24	2.13	324.9
156	8.59	5.48	2.79 117.8	855	8.65	5.39	2.80	389.8
182	8.27	5.16	2.71 127.7	924	9.44	5.96	2.57	416.7
215	7.82	4.78	2.63 140.8	1019	9.60	6.03	2.85	453.8
367	5.92	3.64	2.13 199.8	1083	9.41	5.86	2.75	478.6
384	6.11	3.91	2.17 206.6	1.135	9.65	5.36	2.80	498.8
421	6.07	3.75	2.15 220.7	1.202	7.86	4.81	2.60	524.8
461	5.90	3.62	2.07 236.5	1.356	6.08	3.91	2.27	544.8
474	5.81	3.55	2.03 244.4	1.409	5.96	3.66	2.18	605.6
518	5.64	3.44	1.98 258.5	1.444	6.01	3.72	2.08	638.6
				1.543	5.96	3.61	2.02	687.5
				1.592	6.73	4.08	2.27	684.8
1679	7.38	4.46	2.27 710.7 ←	1.613	6.53	3.92	2.27	207

1.92

$$\begin{array}{r} 330 \\ 245 \\ \hline 85 \\ -465 \\ \hline 750 \end{array}$$

4479

22

10.4

+60

89

121 III

210939

8490

22

11.6

-21

19

140

177

5.35 + 82

8481

22

144

240

41

210967

Can

8482
211006

22 114 +28 22 8123

5.90 +115 +126

8483

22 10.8

H3

03

PM3

211029

571 + 1.56 + 1.93 G

4.49 + 1.04 D

8454

22 125

-44 43

969

6.08 + 1.02 + 0.82 ✓

8448

22

134

-41

52

905

631
13325

2 07.9 + 19 16 gms t/lr

5.70 + 1.64 + 1.91 (C) + 666.8 ~~Area~~
4.56 + 1.03 (3) + 1006.23 - 6344 FRY

621

2

06.9

+53 36

Gr III

+100 f

1387

N30

±3.0

+6028 -043

7956

20

45.2

134

11

113 III

138134

496 + 124 + 144

7962

20

449

+52

49

100

198181

7564

20

46.5

-19

13

gms

6.20 + 1.45 + 1.63 (1)

7968

20 47.9

-51

48

9101

$$5.06 + 1.16 + 0.555 \text{ ①}$$

7966 20 45.6 + 45 24 9 MO

640 + 1.61

7969

198345

20 46.2 + 417 39 125 III

5.57 + 117 + 1.78

9471

20

428

-85

06

120

552 + 1.42 + 158 ①

79975

20 47.5 + 5 21 120

6.21 10.55 + 0.80 C

7976 20 48.0 -12 44 9101

5.877 +111 +0.885 ①

9487 20 504 -40 22 9191

5.35 + 1.35 + 1.43 ①

7999

20

51.0

+29

28

122

198976

7997 20 51.1 = 28 06 g m²

~~5.44 1086~~

8000

20 520

-18 06 gms

① 5.28 + 115 + 0.54

1003

20

51.6

+45

100

88 III

149098

5.45 + 1.11 + 0.83

8005
199101

20 51.8 +33 15- 9145-

9505
199169

20 52.4 427 53

5.02 1.49 1.81

4.24 +0.555 A

Sto 10

20

53.2

+4

21

9 AS

6.05 +0.82 - 10.49 C

8011

20

53.3 + 13

32

120 III

194253

5.20 + 1.12 + 0.97

4.64 + 0.40 (4) A

8015

20

54.2

-9

58

9 115

154345

5.51 + 1.47 + 1.71 D

~~over~~

4.74 + 0.605 D 10265

8016
199437

2 44.9

150

22

9121

8015

20

55

33

-9

48

9105

13

5.5 + 1.47 + 1.71

474 + 10605

③

10265

8017

20 54.6 +00 16 122

6.05 +0.21 +134 C

8026

20

54 47

449

00

PT II - III

145612

5.50

£1.04

70.93

8030

20 56.0

+10 35

9 H

194655

8032
145697

20 56.0 +22 07 9.14

528 +145 +1645 ①

8035

20

56.5

+44

16

25

III

144870

5.54 10.58 10.84

8644 20 58.2 +19 08 gms

200044

570+113+100 0

5049

20

58.2

+59

15

9.124

seeds

5.51 + 1.40 + 1.69

8051

20

54.2

+35

50

945

209253

9055

21 01.6 -54 55 9122

8057

28

0.7

+14

32

DN1

260428

6.29 + 1.69 + 2.04 ①

5.25 + 10.835 ②

8062

200527

21 00.6

444

36

M378-II

8063

21 01.2

185

20

908

200577

8066 21 82.1 + 5 18 9125
200614

5.60 + 11.65 + 2.02 C

4110

9069

20

032

-41

35

912

5.53 105

1025-015

8067

21027

2 45

~~245 270~~

6.72 + 1.06 = 7.78

1070

21

030

-30

14

9 150

5.68 + 103

S072

21 01.8

+50 09

100

Chase