

2 line 8.3 + 1.55 + 1.10 - 5.3 - 2.1 - 1.8 - 6.8 - 6 + 3.9 100? E=110!
 6.55 + 1.90: 9.9 - 3 - 1.2 - 7 - 30 + 2.90 A=110!

2 line 8 14.6 + 15 09 13.9 8

$\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$

795 pa
 -0003 -0.031
 -0.6 +0.7
 +0.9 -0.5
 +0.9 +0.7

-0004 -0030

-556 242 779 +0852 -0425 -0377 -246 +3.0 -71.6
 -145 888 -1137 +0013 -1305 -1292 -49.8 -1.7 -109.0
 +819 356 -451 -0078 -01523 -0601 -51.5 +1.8 -50.7
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 $\frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001} \frac{+1}{-0001}$
 6.57 + 2.10 +0156 -0413 -0255 1000T
 +0041 -1263 -1224 -347
 -0232 -0506 -0738 -131
 -59

+3101940

-0011

-035

RS line 9 07.6 131 10 1444

12051 174 0948 1896

37770

1409.1

-0009 ±38

-0005 ±33

501 1409.8 9.5

-020 -040 CL

(164)

2.82
15.7

37796 29.13

1.25
4.55

466 1530.53

1929.53

230

-0010 +033

-16 -017

-0.3 -0.8

127 111

~~6009 -0300~~

-682 131 718

+04503 -0217

+09306 +9.2

+10.3

-012 982 -188

~~10011~~ -1629

-1629 -40.6

-2.7

730 134 670

-0484 -0222

-0700 -21.9

+9.7

-130 -30

+0348 -0156

+0202 +3.4 +10.3

+13.7

282

2

+ 7 -1346

1350 -23.0 -2.7

-25.7

2426

-0415 -0140

-0605 -10.0 +5.4

-0.4

0.6

RS Inc 9 07.6 +31 10 +14.44

HR3639

-138 -336 LR
~~10~~ -1
 -13 -33

-682	131	718		+0420	-0205		+0215	+5.4 =	+15.8	+10.3
-012	982	-198		+0007	-1536		-1529	-39.2 =	-40.9	-2.7
730	134	670		-0450	-0210		-0660	-16.5 =	-6.9	+9.6

250µ.

RS Inc 5.2 +1.60 +1.24 -5.6 +16 -41 -7 -13 +14.4 120± E=00
 HR3639 3.2 +1.90 7.0 +2 -15 -7 -33 +42°

~~096~~ ⁰⁹¹⁵ 5.36 +1.57 +1.14 → ~~3.45 +1.03~~
097 ~~118~~ 5.20 +1.60 +1.24

2439 131 3.19 +1.90

134 3.24 +1.90

144 3.18 +1.91

165 5.61 +1.62 +1.05

176 5.88 +1.53 +0.96

177 5.89 +1.54 +0.96

202 5.84 +1.57 +1.01

212 5.72 +1.57 +0.98

230 5.55 +1.58 +0.97

241 5.47 +1.60 +1.14

243 3.75 +2.08

252 3.81 +2.08

267 5.84 +1.51 +0.96

273 3.61 +2.03
282 3.09 +1.90
283 3.24 +1.90

MCS MEAT-IT(B)

RS line 9 67.6 +31 10 120^d

6.2-22

(over)

HR3639

1-412.0

-6010 -0332.0

+14.44

13P1546

+ 2 -1

AD7491 ✓

-0008 -0347 →

5.5 of 15.44m. Mould

250 Pa. 7.00

-682 131 718

+0388 -0211

+0177

+130

+10.3

+15

-012 982 -158

+0007 -1583

-1576

-270

-2.7

-42

730 134 670

-0415 -0216

-0631

0.0

+96

-7

Handwritten box containing: 250 Pa. 7.00, +15, -42, -7

Handwritten notes at bottom left: 220, 191.0, 13.95, 13.20, 130, 10.7, 6.97

2439092 534+156+1.14

95 532+157+1.14

96 530+157+1.14

115 520+160+1.21

131

3.19

+1.90

134

3.24

+1.90

144

3.18

+1.92

165 561+162+105

267 584+151+0.96

176 598+153+0.96

273

3.59 +2.03

177 599+154+0.96

202 584+157+1.01

212 572+157+0.98

230 555+158+0.97

241 547+160+1.14

373 +2.07

373

252

+1.99

TMLVM 12 52.7 + 47 29 5.83 -17

447702003

34.750 18973

+ 40
~~81~~0

-000733 -012 42.5
⁻⁰¹²
⁻⁰¹⁴

2.88 19964
+63
3.51

39.704

39.704
39.685

3L

-0020 -010

-020

-44

2.95
+16
2.92

1531.41
1554.42

q/m →

-030 -015

.699
141

141

-77

2.74
1.1

260M

-935 520 177

550 791 294

-013 -343 934

+1167 -0370
~~-0702~~ -0555

+0817

+18.2

-3.0

-438450

-5.0

+5016 +0244

+0172

-9 259
709

-16.0

-0022281 -01454.9
-0040 -022

29.794 1916.60
023
1867

-0030
1080 -015
3.31 1908.18
+58
88

34.699
-168

-020 2.74 1555.42
-1.15

S Cami Box
HD 59980 5.25-4.77
-5.0
8.55
+1
-5
-13
-21
+13

S Cami
07 30.0
+08
26
70-13.2 Vm
E = +05

$\frac{-0.10}{+1}$ -0.18
 $\frac{-0.11}{-0.17}$
 $\frac{-0.11}{-0.16}$ -0.17
f = +13.0
-0.16
 $\frac{-0.17}{-0.14}$ -0.08
 $\frac{-0.17}{-0.25}$ -0.12
From 332.2

V R N-I Above 2440710
-0.0015
-0.02p
V

7.37 5.40 +1.83 0.43 199.9

7.32 5.35 +1.77 0.455 208.9

7.22 5.27 +1.81 0.50 223.8

7.47 5.37 +1.87 0.51 236.8

7.20 5.51 +1.89 0.555 241.7

8.38 5.89 +2.15 0.62 262.7

5.15 4.13
4.13
4.13
4.13
E = 2 + 0.10
R2
330
330
N-I
4170
R2
4170
-0.18 -0.12
+1.8
+58
-47
-18
5.15
8.59
7.14
2.15
1.92
7.15
E = 8.30 m
+58
-57
-41
+38
-40
-48

720
656

				E	$n-m$
HD 60000	8.85	+0.01	-0.04	B8 +0.05	7.6
60109	8.65	-0.01	-0.09	AU +0.05	7.75
60355	7.39	-0.035	-0.16	B8 +0.05	6.55
60502	7.20	-0.04	-0.11	B9 +0.02	6.25

New calculation

$E = +0.5$

7.2 - 5.3

- +1.77

-396

$$\begin{array}{r}
 5.20 \quad 2.17 \\
 1.735 \\
 \hline
 4.82 \\
 2.23 \\
 \hline
 2.6 \\
 6.5 \\
 \hline
 9.1
 \end{array}$$

Observer:

652 115

+22 10

660 18

STATION

MAGN

TIME

600 18

650 10

620 18

626 59

640 10

610 10

600 10

660 10

*601 16

*610 10

*610 10

*600 18

*600 10

*600 10

*600 10

*600 10

*600 10

*600 10

on Vmp

3rd class re
also with specimens

3 Mr Mr

Comments:

SC Mi
59950
• 10095

7

30.0

-0014 ± 3.4 -002 ± 3.0 $1=3389$ w_2
 -0014 -030
+08 26 69 g M72 +68 C

5025

0.313 1899.0 +8 25 35.33 1895.4

$\begin{array}{r} 21 \\ 3 \overline{) 84} \end{array}$

$\begin{array}{r} 66 \\ 35.99 \end{array}$

$-00014 -021$
 $-1 +1$
 $\hline -0015 -020$

$\begin{array}{r} 1323 \\ 25 \\ 348 \end{array}$

$\begin{array}{r} 34.87 \\ 18 \\ 35.02 \end{array}$

$\begin{array}{r} 0.288 \\ 25 \\ 316 \end{array}$

$\begin{array}{r} 332 \\ -052 \end{array}$

$\begin{array}{r} 34.45 \\ 955 \\ 34.53 \end{array}$

~~$\begin{array}{r} 0.288 \\ 25 \\ 316 \end{array}$~~

~~$\begin{array}{r} 1936.64 \\ 24.45 \\ 54.53 \end{array}$~~

$\begin{array}{r} 34.53 \\ 34.78 \\ -1.22 \end{array}$

$\begin{array}{r} 36.4 \\ \hline 41.0 \end{array}$

-0010
0.867 19/6.06

$\frac{84}{90} - 0017$

$\frac{0.882}{\cancel{0.878}} - 0014 - 023$
 $\frac{0.035}{\cancel{0.015}} - 021$

5155. -022 -024 +65

-10018
35.44 1912.77

$\frac{-0025 67}{86.111}$

$\frac{34.78}{\cancel{1.33}} - 66$
19 36.25

-396 363 943

-283 826 -487

674 432 224

+0413 -0361

+0245 -0422

-0911 -0430

+0052

-0527

-1341

+2.7

-27.0

-68.6

+573

-33.1

+15.2

45502560

V Lan

23 09.5 +59 26 6.72 gM62 -30.56

218997

14560

111

14054300

6.2 + 8.6

7 66.0 + 10 06

(S) - Cap

R C Mi

15

V

R

R-I

Phone

244000

498.06

337.91

7.4 - 11.6 via

7.71 6.40 +0889 0.73

303.6

7.79 6.40 +0892 0.79

323.6

7.89 6.51 +0895 0.815

331.6

7.83 6.66 +0.85 1.64

610.8

7.27 6.26 +0.83 1.70

631.8 ←

785 = m - m
-0007 0003
↓
Inches
mm

7.48 6.22 +0.96 1.82

673.7

8.12 6.52 +1.05 1.87

698.7

8.22 6.57 +1.09 1.91

703.6

8.48 6.74 +1.14 1.94

713.6

8.67 6.58 +1.17 1.975

724.6

+45 - 21 - 6

T let MS
19.3 - 20 20 66-77 5
msc II

H 201760 159d (162)

GC437 S-shun Canyon 92-1291

(59m as low cut sep) 10056 } BL
-D020 }

Apus Aug. 2018 Vol 22, 289 1998
also 1969 m v w

1970 0.1 m length in V 0.05 ^{from in V.8} M(I) 425-29-36
0.1 " " " R ^{Same as I} 4.05

T let

H 201760 5.1 H 62+1.70-905 +33-35 -36 +56 2291 160^d E=102

345 H 44 625 +18-21 -4 -20 0150 II -80

-0706 ± 1.0
-0002
-232 ± 1.2
-234
Σ mlyga

0 Cf 2 16.8-03 12 g m l e + 63.8a

14386 49 044 1898.0 -3 12 13.34 1901.8 +64.22(16)
G-2296 031 +11.41 +66.67(14)
W1301 080 1.93 +63.04(15)

7477 33.321 18 65.13 +66.18(13)
-30853 15.720 12 9.13 +63.94(13)
49.061 +64.72(14)
14051005 081 +3 9.57 2058 +65.14(12)

-5-47-85 .015 072
-008
±1 ±1
-009 -232 Gc

49.062
-1
061
10.24
8.36
1375
11.34 1939.15
+35 21 A2E
11.01 10M(7)
-52(12)
36 365
35.7

562 827 -059 998 -009 232 +63.8 014 -4 -1.099

005 -008 -007 012 -033 -071 +63.7 +53 +36

+51 +31 -77 015

+52 +33 -58

+6 -34 -77

02

+52 +34 -40

03

+14 -20 -69

M2I2

21 42.0 455 23 415.3

Map
HRLG316

1/2
41lep #101443

2.4

18655 100 +3.6 6.95 +0.205 -0.81 80 ± +0.80 9.8
 239758 101 +4.4 9.50 +0.26 0.54 10.8 10.0
 207506 102 +4.6 7.38 +0.32 -0.44 80 ± +0.60 9.5
 WGC 7160 104 +4.5 +0.2 9.6

Map 4.1 +7.25 +2.3 -8.1 44 +1.8 +1 0 419.3
 HRLG316 2.4 +1.36 8.8 +1 0 +1 +3 0122a 44.0
 B = +0.88 44.5

hot Cap 002 (See S.C. Swinson Aug. 5, 1949, 923, 1948)

P 2+19.3 DN2 (P = -16) also shown 082 in 9.5 giving $M_{bol} = -8.7$
 marking it very similar to HRLG16 ($M_{bol} = -8.5$, 399 m 15. very old!)
 in LMC

V0 B-V Exp E m-A

208501 3.30 -09 0878 +89 9.9

211971 410 +06 A2IR +83 9.7

267260 2.9 +06 A2FA +46 9.8

+001 +005² 4.8 + 19.3

$\frac{-1}{000} - \frac{2}{+003}$

533

763 617 193 | 0 +0098 +84 +3.7

-101 -1820 978 | 0 -0026 +17.5 +19.9

-629 766 077 | 0 +0109 +71 +1.4

+3102725
 0620662
 SUB

15 19.4 781 33 -1.0

-009 ± 6.1 -009 ± 6.1

21.559 1907.9 46.12 1908.1

" -012 " -016 -7 -21 *Latin*

-2 +5
 -9 -16

			250Mn	
-510 802 -313	+0240 -0608	-0818	-8.5	+0.3
667 548 445	-0379 -0454	-0833	-24.0	-0.4
-544 -018 839	+0309 0	+0309	-8.0	-0.8

.v11

-30

8
-25.0

R Cuyg

19 35.5 +50 05

-000613.0 -00972.8

44603064

38 28.692 1902.9 11.34 1898.9

154

5.40 1.23

5.02

1.54

3.24

-29

-5
-3
-8

-9
+5
-4

down
-008-004

2869

stop

9

413 9000-126 -0157 -0171

270 011 963 -0162 -0002

-870 431 939 +0330 -0082

248

-0328
-0104
+0248

-9 +3.8 +3.5
-28 -29.0 -29.0
+3 -7.2 -6.0

-10
-33
B

408

$$82.7 + 13.8$$

Play

964

506

160

~~44~~

32

45

6

1.24

35

Play

19 35.5

+50

05034

1719

877
11042
5534
1111
1110

426.35

TD

243-3248

4264
2132
2396

RE RE

.54 9.26 6.58 1.44 2854 .84

.58 5.40 1.46 303.9 .72 .935

.63 7.77 5.44 1.29 324.9 .77 .94

.65 7.76 5.44 1.27 331.9 00

244332

.76 8.32 5.84 1.51 392.9 .12

.84 9.11 6.33 1.78 415.7 .20

.84 9.87 6.85 1.53 436.8 .215

11.23 8.14 2.38 263

.84

53.9

16

512

145

349

5469
500

-28

-0005 - 009

Rupp

124284

-14643.0 -00/728

185456

19 35.5

750 05

540-50-255

27152

12027

28692

1462.9

750 5

11.34

18489

033

64

4774

1774

729

-0010 -002

1190

44.7 122.5

098

48.25
40.225
28.705

21.42

11.12

316

M 130

25

250

11.78
11.81

316

413 902-126 -0195 -0086

-0281 -19.0 +3.2 -11

-5.7 -5

270 010 663 -0126 0

-0128 -13.4 -24.1 -30

-4.1 -28

-870 431 239 -10411 -0041

+0370 18.4 -6.2 +2

+11.5 +5

956
-
058
45
419
803

608

762
38
530

535
88
93

27
296

X_{lyg}

19 48.6 732 46

	R	R-I	JD
0.06	5.14	2.83	79.8
0.075	5.39	2.94	84.6
0.11	6.73	3.63	113.7
0.15	6.85	3.79	117.7
0.175	7.34	4.12	127.6
0.365	9.93	6.33	206.6
0.50	10.09	5.82	392.9
0.55	9.35	5.22	415.8
0.935	7.68	4.34	436.8
0.975	5.34	2.99	454.8
1.03	4.29	2.26	475.7
1.355	9.93	5.93	406.51

Rhosu
mendaya

57, 2

16.

182
170
-12

68. +33

64	+2.9	+29°3438	8.52	+0.01	-0.70	82 ¹⁰	+25	10.00
67	+2.5	186777	2.87	-0.3	-39	85	+14	7.75
66	+2.8	187461	7.62	-0.9	-38	89	+05	7.80

AGVD P=4139

-0026 ± 41 -042 ± 3.7

(-012)
-051
-059

X Cgg

19 48.6 + 32 47

947.2 -1.94

HR7564

18796 38.485 - 19045 + 3247 11.5 -4 1899.5

-033 -042 6-c

27451

118

13.66

1325.48

12201

1603

-0023 -056

2744 1528.4

10.60

43203543

4091

46.55

-05
+12

57.680

12.28

38.594

-030

12.20

394

38.524
1808

586

38.9

12.19

11.09
-057

11.34

38.551
544

-017
544

38.524
069

10.907
10.96

153689
-12

-12
11.22

38.523
244

10.96

1940.89

$$\boxed{-0.030 - 0.052}$$

$$\boxed{-0.026 - 0.050}$$

1.00
1.35
1.70
+0.5
3

200 NA

$$\begin{array}{r|l}
 458 & 810 - 365 \\
 233 & 287 \quad 929 \\
 -858 & 510 \quad 057 \\
 \hline
 & -0637 \quad -1996 \quad -2633 \\
 & -0331 \quad -0707 \quad -1038 \\
 & 41220 \quad -1257 \quad -0037 \\
 \hline
 & -52 \quad \quad \quad +0.7 \\
 & -22 \quad \quad \quad -1.8 \\
 & -1 \quad \quad \quad 0
 \end{array}$$

(9)

$$\begin{array}{r|l}
 -0564 & -1920 \\
 -0287 & -0680 \\
 11057 & -1209 \\
 \hline
 & -2484 \quad -22 \\
 & -0967 \quad -11 \\
 & -0510 \quad -1 \\
 \hline
 & +0.7 \\
 & -1.8 \\
 & 0
 \end{array}$$

W cgy

21 34.1 445 03 gmye - mva - m. (144)

205730

6c30250

5.1-2.4

447

+187

~~HR~~ 68222

+34 -16.8 -24

-18

-16

-37

-152

4048 4006 6c

100

184

+061+007 LB

~~4058~~ 4006

+47 -17 -29 . 004

+22 68

1348
+41.5 -0.2

441.3

-0177

-08 -14.3

-19.0

-1654

-30.2 +1.2

-29.0

+742	+671	+ 15	+2070	+0150
- 69	+ 54	+ 996	-0192	+0015
-667	+740	- 87	-1885	+0210

21.000*
 34.200*
 45.000*
 9.000*
 0.062*
 0.003*
 5.900*
 151.356
 -14.000

 0.228
 0.015

 34.228

 -0.020
 0.996

 -16.920

 -0.185
 -0.087

 -26.808

8262.000*

 21.000*
 34.200*
 45.000*
 9.000*
 0.053*
 0.006*
 5.900*
 151.356
 -13.500

 0.223
 0.015

 33.550

 -0.018
 0.996

 -16.105

 -0.162
 -0.087

 -23.394

0.030*

 21.000*
 34.200*
 45.000*
 9.000*
 0.055*
 0.006*
 5.900*
 151.356
 -14.000

 0.230
 0.015

 34.555

 -0.018
 0.996

 -16.614

 -0.162
 -0.087

 -23.298

42
 3

Wagey
205730

21 34.1

+005P

+45

09

5.0 g m 42 - 144c

+00657.1

+00000

30250

13572

8.207

1906.4

+45 9 0.18 1909.6

-196

8.011

+58 +7

-0.2 -0.6

-1.0 +0.7

-1.6 -0.8

11.24

80.524

80.68

80.23

.09

0.90

80.175

3

1.47

toys

+0005

17.6 1925.8

41.78

59.38

60

98

59.13

0.11

0.11

0.10

17.4

59.7

59.94

154

27.7

213

1929.6

202
1.62
222
204
202
1.26

29 85.2 341 468 358. 165
 315 206
 212
 103
 35

W Cng 21 37.2 445 09

205730 061 7007 45 +061 7007 40

7064+004

1hr 45 M

Handy

PC +3
 4/2
 +3
 -4
 +3

System

The plant is not well defined in the water

of (NRI) which has an end on standard by

Smade (Apr. 29th 9, 141 (100.59) 1564) The (R, I) / 1/2
 in by 333 and (Apr. 5. 1935) and number

W copy 50 +1.66 +1138 -425 +34 -17 -24 +58 -144 1305

1485262 370 7750 5.9 +22 -2 -17 +6 -550 550

23 1165

5.9

135

W. C. Gray 80.8 -5.0

E M-M

~~205060 88.7 -6.4 7.22 +01 -40 86 +18 7.5~~
~~205601 89.6 -6.1 6.76 -12 -60 86.5 +08 7.7~~
206280 90.7 -6.1 6.72 -06 -210 95 +04 6.1

5.0 3.3 -45.5 +004 +58 +42 +223 +3
+16.8 +16.5 6.40 -5.0 +6 -16.8 -17 +150
+13.5 May 190 142 -13.5 -30 -162 +17

E = +0.4

SUB V R R2 00 15 19.4 +81 32

9.20 15.5
8.00
3.00
1.50
7.00
2.15

0.444 7.80 559 2.12 236.9

fanbelt

.57 5.97 433 1.59 268.1

0.435 6.26 446 1.65 285.9

.644 6.64 478 1.75 303.7

595

M5 Super 131

243552.9 707 1.36 96
L2.9 704 132 75
66.8 263 1.81 69

AD

SUB 5.95 +1.35 +0.75 -4.5 -9 -25 +8 -9 -10 360° P=103
HD 4.3 +1.88 7.35 -3 -8 +3 -16 457°

434
366
341
561
199
565

195
456

Observer:

069° 01' 01" x10

STA

040° 0' 0" MAGN

TIME

620° 0'

852° 40' -33

314° 0'

080° 0' -

822° 11' -11

855° 0' -

880° 0' -

888° 1' -

898° 10' 79 328

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

898° 0' 0'

Comments: