

2529 648.6 +2150 $A=2\bar{1}$

44508

8965

522-02

+374

0

-0003

-0365 - 1.15

-0004

-025

-0063

-006-034

Ans 1

601 150 1162 2940 $\frac{1}{2} \text{ of } 60$

605 140 1.1725

603 145 1.1675

141 138

282 $a=022$

1.171 $a=109$

1.153 $a=117$

1.462

2866 56

2856 59

1457 $a=211$

1410 $a=117$

-0.4

5.5

2540

6 45.5 +34 62

A3 VII

50019

8989

0

3.59 +10 +10 J

^{11.8}
060 178 1.163

2 SP2

196

2.834 JG

282

a=111

1.1534

+22.4 Wpward

0

-66009

-05089

FIRY

-

0011

2L

~~5000~~
5000

-001-050

2539 6 44.6 / +38.56 A7

56018

8993

6.11 + 40 +

2540.000*

6.000*

49.500*

34.000*

2.000*

-0.001*

-0.050*

3.600*

52.481

22.400

0.017

0.965

22.533

-0.217

-0.035

-12.167

-0.094

0.259

0.854

2574 6 513 -43 54 189

Bring

Now

648 -32 105 621 2762 -25

95

627

190

817

2529.000*

6.000*

48.600*

21.000*

50.000*

-0.006*

-0.034*

5.500*

125.893

34.400

-0.015

0.959

31.098

-0.133

-0.228

-24.586

-0.094

0.170

-6.020

4.10 401

625 2 06.4 -18 01 M1 —

13215

6.10 + 1.61 + 2.02 ①

4.95 + 10.945 ②

626
13222

2 057 173 47 966 -32.04

GC 525
+0124 -0295

12013

619

2

05.4

444

13

28 III

424.46-

G-L

2447-71

~~10.23~~

10.53

908

370

067

20mas)

611
12642

2 01.8 -Y 21 CNS +24.5

GL 75.0

561 +1.88 +1.96 L +0010 -0595

472 +0.76 (3)

923 921

614

12472

2 03.5 +8 00 NY -26.46

6.2-6.4

+1.91

(13)

GL F.S.S

6.3V +1.63 +1.82

6.0

-0005 -032

~~5.3V +1.09 (1)~~ ?

5.0V +1.015 (10)

376

7754

1 1512 447 10 100

1.36

R-L

396 1 20.9 133 59 68 IV 12.86

8375

GL 13.5

6.28 +0.83 +0.48 A +0.174 +1.185

5.94 +0.295 2 A

347

1 20.7

+20

12

125

-11.38

8394

5.96 +1.70 +2.05 /

G-L

±4.5

-00125 -008

4.25 4.10

SE 4

4.60

1 21.2 -31 13 195 III -16.0

8448

584 +16.1 (0.58) C

584 +158 +2.05 (1)

-00074 -0413 FIVY

4.90

+0.745 (3)

437

420 1 23,4 -64 88 MO III +23.0 ^{cut}

4810

592 +1.56 +1.41 C +60383 -0152 Field

507 +0.645 (2)

R Sel

4/23

430
9057

1 22.1 + 42 44 64 $\overline{11}$ -11.3a

S. 27 ~~4099~~ + 0.82 (3)

5c

435
9184

1 224 - 47 01 gmy —

430 + 1.66 + 1.86 C

5.12 + 1.13 (2)

cc

439

1 30.2

+58 04 2.121

-0.68

9352

570 +1.52 +1.15 A

RL

450 1 32.1 + 18 12 gm2 -26.18
9640

5.94 + 1.48 + 1.86 2 GC 52.0
+ 00205 - 068

4.91 + 0.975 - 0

452

1 32.9

+40 49

181 III

+65.2 6

9712

6.40 +1.12 +0.99 (3)

454
9746

1 334 +49 25 9101 -43.26-

1000720
-00185-0135-

410 bar

456 10 345 +72 47 88 II-III -4.08

9774

525 +0.96 +0.72 (2) -00241 -0089 FIV

4/6/1
9900

1 34.9 + 57 43 G5 II -816

5.56 + 138 + 1.43 45

22

4.97 + 0.57 25

4.02

468 1 349 - 58 32 M1 —

15852

6.2V +1.61 +1.89 (3)
5.08 +1.08 (3)

RL

X and

469 1 36.4 +44 08 68 111 1668

10072

4.97 +0.89 +0.55 A

5.01 +0.89 +0.56 2E

QC

470 / 370 + 53 37 125 III - 61.48
10116

GC 73.5
-0016 -001

495

1 40.2

45 03

09 102

+12.28

1048b

6.38 +102+095

101335 + 007

GC

53.5

5.89 + 0.325 3A

Sp. 3 78.01^d

1 41.0 731 56 G8 III - $\overline{12}$ - 4.6e

10581

503

Ac

+

504
10597

1 41.4 + 45 54 9115 - 1846
6.30 + 1.41 + 1.71 (1)

RL

Residuals ?

567

10659

1 41.4 - 5 01

RSD +19.7

6.20 +1.53 +1.88 C

5.35 +0.635 (2)

417 335

513 1 43.5 -5. 59 8104 110.86

10924

5.34 +1.51 +1.87 C -0011 -0273 5.44 ~~12.8~~

4.58 +0.635 (2)

315
346

S19

1 44.2 - 51 04 gmy - 200a

10934

5.48 + 1.62 - c

4.40 + 0.94 (2)

GC # 40

+0032 - 020

521
10975

1 45.7 +37 42 100 II +36.5 f

5.94 + 0.97 1071 A
5.92 + 0.99 1074 1A
5.92 + 0.98 1072 (F)

~~10975~~ 5A4
+0095 -0259 7.15

1 Am

530

1 47.4

+22

02

150 III

+1.38

11155

$DM = 1''$

3"

5.52

+0.34

3 J

S. 86 +0.78 +0.50 $\sqrt{5}$

-0012 -007

G-L ±0.5

73 H6 I

Bm = 1.06

543

1 50.3

+40 29

9 101 -2.18

11428

5.40 + 1.32 + 1.41 42

5.40 7.20

-0007 + 0009

RE

551

1 51.9 + 40 26 122

+ 316 8

11613

~~160 45 - 64 266 8~~ 7 3.0

544 + 0047 - 0643 7 2.5

11624
55m

1 52.0 + 36 52 120 -1.68

RL

556

1

530

+37

01

gmd

HLTB

11727

S.91 +1.59 +1.59 (1)

GC

557
1749

1 53.2 + 37 01

120 III
~~977~~

75-8.58

Answers

557

✓

1911

$$5.70 + 1.16 + 0.92 \text{ (P)}$$

$$5.22 + 0.38 \text{ (Q)}$$

$$11.93 + 1.10 + 0.90 \text{ (R)}$$

$$11.20 + 0.57 \text{ (D)}$$

$$11.16 + 0.42 \text{ (D)}$$

$$R-C \quad F.15 \\ + 0152 + 00115$$

SLV
11928

1 54.9 +27 82 9M2 -2.56
5.85 +1.57 +1.81 (3)

AC

3 Nov

568 1 554 448 57 267 -0.46
11949

OL

572
12005

1 57.9 +77 40

100 -2.66

20

379 364

583

157.4 -21.05 gmi -15.08

12255

5.91 + 1.62 - 2.00 = 5.53

GL 230

4.45 + 0.81 (2)

+0.0085 + 0.205

223 206

587

1

580

-8

46

945

+638

12292

5.5V4151 +135C

3.60 +154 (2)

49 W00

542

2

00.2

+25-

52

68 $\overline{11}$

0.02

12339

5.17 +0.95 +0.75

(18)

-0037 -0168

564 +2.2

6.01
1200g

1 59.9 + 13 14 g m 2 - 2.38

5.99 + 1.60 + 1.83

(3)

+ 0035 - 609

6.2 7.55

347 345

602

1 59.7 - 44 58

9105

-30.6E

12524

5.13 + 1.49 (2.52)C

1230

± 25

4.30 + 0.65 (3)

-60275 - 2415

375- 1 16.1 + 27 19 G-5 III -73.8 6-
7782

New York

42.64

385

4036

1 17.3 -0 46 88.14 +142

5.86 +64 +32

RL

$\Delta m = 1^m$

1.5

v

OC 80.90

A7E

374 1 14.6 431 29 150 ~33.76
9724

Q.C

1148

3

45.0

+71 10

A2 TV

8 Cam

23401

4557

4.66 +0.03 +0.07 J

~~+02487-0354~~
O

St?

036	149	1.216	2.822
028	156	1320	2.836
<u>032</u>	<u>153</u>	<u>1.216</u>	<u>2.830</u>

FG
at out
85
71

-1.0

-E

+0441 -0374
3
4

Fire

120306	462
151958	42078
1585	2 189

143
1212
326
38

+0213

+018-040

+0047
22
20
+023

~~-038~~

515

-0.85
-1.75 5.50

1148.000*

3.000*

45.000*

71.000*

11.000*

0.018*

-0.040*

5.150*

107.152

~~1.000~~

+10

0.144

0.704

L 14 ~~14.722~~

-0.120

0.672

13⁴

-12 -13.521

-0.090

0.230

-9 ~~-9.888~~

60 (BV) km

2197

6 69.3 +22 56 MICA

42543

$+0037 + 027$
 $\underline{-16}$
 $+0021$
 $+021$
 238.5
 -64
 31
 89

$6.55 - 036$
 131
 120
 868
 270
 1105
 2.807
 Stu
 Eg

Spem 762?

D: Van

$$E(1-y) = 1.505$$

$$M_y = 0.00$$

$$V_0 = \frac{6.5}{6.1}$$

+0030 + 019 GC

10036 ± 5.7 1015 ± 4.2
10043

26.944 15975

46.57 18943

$$\begin{array}{r} 47.41 \\ - 84 \\ \hline \end{array}$$

$$\begin{array}{r} 26.944 \\ - 10043 \\ \hline 26.788 \end{array}$$

5-4.755

32.050

26.835

$$\begin{array}{r} 26.835 \\ - 0.53 \\ \hline 26.305 \end{array}$$

26.7

26.852

72.46

38.68

$$\begin{array}{r} 38.68 \\ - 34.28 \\ \hline 4.40 \end{array}$$

$$\begin{array}{r} 47.41 \\ - 34.28 \\ \hline 13.13 \end{array}$$

54.55

1929.40

257
249
11

109

020

260

440

12

9145

132.32

2760

5.42 2156 (2.58) C

5.42 41.54 41.90 1

4.51 49.225 (3)

GC

43.0

101130 - 040 34₂ 1528

422
412

117

00 27.5

-4

15-

MOTIV

447

2637

5.72 41.55 41.84 C

40.00 051 -0074 FK4

4.34 40.715 (3)

1872

4 17.1

-63 23

89

Q. 18.1

Spring

576 → 27⁹¹

137 730 2576

129 735

$\frac{258}{993}$

55

110
2567

00 26.3 +36 27 965 4102

60563

531 1 48 26 -10 48

466 -502 +922 -178 2.244 (19)

41939 188

468 -505 +921 -184 2.235 71 Dec 75 (4)

469 -494 +914 -174 2.239 12 Dec 75 (4)

467 -495 +928 -199 2.236 22 Dec 75

463 -496 +904 -210 2.233 3 Jan 76

465 -800 914 -172 2.239 4 Jan 76

466 498 +916 -188 2.236 (5)

464 -500 +919 -183 2.240 (16)

647

1381

4 21.2 + 9 21 A2

27820

5325

5344

5-12 + 0.07 + 0.10 533

Sum = 0

Bud 51

(15)

024 126

1153 358

179

a = 0797

1.126

D38

172

1.156

2.877

(2) 512

1.506

1.576

1.148

02040

201 183

-0014 -007

-0016 -006

-0037

-0023 -008

(4.70)

1148

143

266

1514

045

514

-021 -006

-35

647 2 10.8 +47 15
13554
2668 pdwt1504r 6.06 +0.40 -0.07 J
• AOS1709
Δm = 0.9?

Bird 51

Observ

-10.458

-8.759

-0.452

LS-2

-0.452

E

-0.098

-0.086

5.225

5.269

-0.080

01-

-0.080

0.040

0.041

-8.789

-7.921

0.889

16

0.889

-0.046

-0.040

-3.500

-3.500

123.027

120.226

5.450*

5.400*

-0.008*

-0.006*

-0.023*

-0.021*

21.000*

21.000*

9.000*

9.000*

21.200*

21.200*

4.000*

4.000*

1381.000*

1381.000*

Comments:

112

OD 82.7

+776 WY

18018

+1506

2589

621 +84 +55

(2)

70953

(4)

+0252

54.0

3607 9 010 -25 19 188

(2)

Novel

6.75 11 96 7572.728
99 755
148
953

406am

2201

6

11.2

+60

01

g 103

+12.1 f

40633

584

±2.0

40041

-0206

137 Jaw Side Pub
 Si Si Si Si 5 44.5' + 14 10

2633

29317

-027

049

1040

2.832

6 -5.3

81

044

1.048

286

0538

128

-15

+17

-00130 -0080 GC+ F20

1132

-0.05

-00145

-00983

+6

(54)

07

-0211

-020-008

141

287

1045

1329

2033.000*

5.000*

49.500*

14.000*

10.000*

-0.020*

-0.008*

5.650*

134.896

-5.300

5.15
107.5

-0.007

0.967

-6

-6.081

0.017

-0.232

13

3.560

-0.100

-0.108

-10

-12.967

260f 5 5-1.3 -33 48 B5E

2056

39744

7414

10015
27

487-15-5665
487-15-57C

228 12-1 408
-076 + ~~100~~ + 428 D

2.717 ⑩

-65009 + 035 Stamp 1571

048 423
136
619
030

2772
955

-0112
39

+300 8

-607 + 035

92
0.8
1

B-V 0 -18

E = +03
V₀ = 479 7115

M¹¹ 1
V₀ 5
1 2-13d -585

MV-235

2056.000*

5.000*

51.300*

-33.000*

-48.000*

-0.007*

0.035*

~~7.150*~~

269.153

30.000

0.149

0.458

138 134 53.706

0.080

-0.773

-12 -1.715

0.015

-0.440

-11 -9.291

2056

5

51.3

-23

48

85.2

39764

7416

487 - 0.15 - 0.71 65

2.717 10.00

1.0

(-74)

~~489~~

$M_w - 0.45$

-6056 + 0.321 + 1300.0 4.12

$w \frac{4.8}{5.25}$

-4056 + 1033

1954

37765

5

37.8

-34 07

87 IV

2.64-0.12-0.47 5

2653

855

0-48

400015

2035.000*

5.000*

51.000*

-23.000*

-40.000*

-0.000*

0.033*

5.250*

112.202

30.000

0.125

0.605

22.222

0.094

-0.695

-10.326

0.027

-0.388

-0.562

2127 5 597 41 42 AD

B + 08 6.58-04-27

-012 4120 720 2.720

126 720

2520

$\frac{2520}{974}$

$M_V = 0.25$

$V_0 = \frac{6.415}{6.65}$

10005 + 10035 64 + 131

10030 + 1003

-1045

-103 + 103

+0002 ±5.6 +007 ±5.6
000

41.429 1847.8 -0003 43.47 1846.3

-011
418

-011
418

42.93 1903.8

+17
43.10

41.370
+38
408

.01

-010

2127.000

5.000
59.700
1.000
42.000
-0.003
0.003
6.600
208.930
3.000

0.007
0.887

4.215

0.018
-0.427

2.434

-0.006
-0.176

-1.721

U for

2221

6

09.1 -68 50

1887

43107

5.05 -08 -20 C

Stalin

7886

^{1/16}
0006

-033 + 1344 + 7992 (2) 2820 (2)

^{1/17}
-18935 + 0185 FRY

124

899
²⁴⁸
1143

^{2.504}
577

1402

X 17.5K

E=00

505

^{1/17}
-0507

-0410 + 0119

V0 5.05
Mv = 10.25

4.8

-27.782

-0.485

-0.189

-6.090

-0.864

0.088

8.950

-0.137

0.111

17.500

102.329

~~5.050*~~

0.019*

-0.046*

-50.000*

-68.000*

9.100*

6.000*

2221.000*

34