

2457

431

-30 32

85 15

-052 114 483 2.716

154 103 453

204
699

$M_V = -1.0$

2502

6 44.3 -10 03 A07A

$\bar{x} = 00$ 5.65 - 06 - 10

-017 125 1.053 2.924

120 1056

$\frac{240}{1296}$

Vandm

$m_v = 10.1$
 $v_v = 5.65$
5.55

2471

408 + 3609 A22

48272

628 + 06

8785

∠

857

132

1193

2858

at at

-151

148 1181
396

149
298
116
60
1571

A=95
A2121

-04

43
28

4.00
4.22

2415 L 327 -32 40 05 II

561-09

115

-035 102 893 2.766 8th

92 850

189

1079

$$M_V = -0.55$$

10

$$\frac{5.55}{6.10}$$

~~1953~~
Vauvey

2360

6 276

-63 48

BCI

45736

6.25 - 14 1.32

Perman

-865 123 535 2722

104 548

2086
986

10 6.25

-09

MV 7.15

-1:

-0029 ± 7.1 4021 ± 5.9

37-113 1900.6

53.23 1898.7

2309

6 2 2.0

-12 57

188

Prüfung

6.11-09-64

6.11-10-58 3 299

10.52 + 10.42 + 10.87 3695

= (14-4) + 07

10.31 25 102

614-11 81 358 2688 ②

58 360

$\frac{156}{516}$

H8 1 photo

-3.2

5.75

8.41

2304 6 22.5 423 22 A0E

44427
8290

6.08 +0.02 0.00 3.44

FG

016 152 1.083 2.842
018 136 1.103 2.831
017 140 1.093 2.836

total

31
-32 111
25 111
21 111

-266 w/p

148
298
1090

025 = 4
160 = 138
141

166
187

-6003
-0227
1384
1415

+6.45

a=27

1163

-6004
-0223

5.10

1375
1336

1411

-605

000 142 1099 3321

-9.829

0.088
-0.071

-4.676

-0.160
-0.085

-26.936

0.983
-0.008

-26.600
104.713

5.100+
-0.023*
-0.005*
22.000*
23.000*
22.500*
6.000*

2304.000*

2304

6 22.5 733 21

AVD

6.08 + 0.200 3.45

2

19 136 1103 2.93 1

2

141 1099

~~292~~
1381

-0.4

2224 6 116 -29 23 BF

Spring

Windy

6.54 -46 ¹³⁸ 118 629 2.760 23

104 638

$\frac{208}{846}$

-0.2

PT logs
Horse



42.2 48 39 42.2

-1162

-0.5002 ac 415
-0.0006 + 49 new
0.0000 + 23 Me
-0.0005 + 15 fed me

RT C₁₀ 19 42.2 +18 39

V R R-E JD

0.76 2.01 6.05 0.82 206.1

1.08 10.02 7.95 1.73 213.0

1.1 10.34 8.25 1.87 209.9

1.44 12.17 9.42 2.10 332.0

1.71 9.46 8.01 1.69 342.8

1.884 8.82 7.33 1.50 411.8

1.445 9.65 7.83 1.73 486.4

2.108 10.51 9.56 2.17 454.8

2.12 10.63 8.75 2.10 410.6

3.35

RT C₁₀

HD 86686 6.0 to 7.0

7.00 +1.70 +1.30 -3.4; +53 -114 -8 -4; -16.0 140 8.105

9.0 +6 0 +5 +16; +120

555 ✓

COO +23 ML

+3
+23

RT \log 81.9 + 12.2

186.882 78.7 + 10.2 2.87 - 0.04 - 0.09 0.00 5.00^m

76.0 + 10 5.20 - 0.09 - 0.21 + 0.2 5.00

RT 644
186686

19 42.2

+600.1 ± 14.4 +010 ± 10.6 2W
+0011
+48 39 6.25 g M2 -1162

12104

12.642 19183

+48 39 25.49 1917.7

- 3

639

- 32

25.17

12.64
10

650

25.0 1929.6
- 28

25.02

-2 +10
+5

-3 +15
+15

+0011
+011

380 pa.

-116

597
5.05
4.47
775.45
96792

"-1004 + 016

448	4887	-140	-0083	10073	+0590	+224	+39	+162
250	480	4947	-0047	+0022	-0025	-1.0	-113	-1120
463	448	4206	+0163	+0347	+0510	+193	-5	-24.1

0.000*
19.000*
42.200*
48.000*
39.000*
0.000*
0.023*
9.000*
638.957
-116.000
0.097
-0.138
77.166
0.003
0.968
-110.379
0.050
0.211
7.038

CHCys

13 246

+5008

C4 449
182919

-0005±3.2 -020±2.6
-0006 -007
19 23.2 +50 08 6.6v
S/R 1079
gml6-53.78

22820

11865
14.191 150.11 +50 8 30.70 1894.3

mod 6.6 11.2 +104 044
235

-0011 -010

1.11
31.81

X

7.5 (1000) 36442
14.1 92

35.3

34.4 1425.7
54.6 8

7276

-11.5 -54
-544 -10
-12.5 +4

200
-019

31.74 1.06
+3

36.9
42.1

14.216

31.57 1947.06
31.57

220

31.29
31.53
28

3543
41

407

4.10

1.20

Nov 22 1967 15:01 +0.52 -0.04 1 2439817

Jan 1 1968 15:01 +0.88 -0.12 2 56

Feb 1 1968 15:03 +0.52 -0.14 2 88

Dec 25 1968 14:77 +0.725 -0.265 2 2440216

Jan 20 1969 14:62 +0.65 -0.35 1 42

Feb 14 1969 13:56 +1.64 -0.48 1 67

Apr 22 1969 14:10 +0.64 - 2 334

May 6 1969 14:21 - - 2 348

May 17 1969 14:52 +0.74 -0.31 1 451

Sept 12 14:28 +0.73 -0.43 1 477

Nov 4 14:42 +6.71 -8.31 2 530

Nov 17 14:56 +0.72 -0.28 1 543

Nov 21 14:37 +0.72 -0.40 1 547

1444 +72 = 34

41604351

Sold 20 40.5 +16 54

884 6.53 +1.71 7.98

882 6.88 +1.64 8.67

881 6.87 +1.63 8.5

9.97 7.04 +1.64 8.28

5.24 2.03 +1.65 4.88

Sold 8.8

-4.45 +1.03 +3.7 -2.4 +2.2 -1.3.0

277 5=+10

6.85 +1.63

9.7 +11 +6 -3 +14

-15.5

957

-13.02

70015 +3.20 +016 = 3.4
Lubrication

70015
+3
70019

(40 > 2)

612	453	-457	+0638	+0480	+1118	+103	+5.9
088	519	850	+0092	+0467	+0559	+37	-11.2
-786	561	-261	-0820	+0505	-0315	-24	+3.4

L 1

F

Sdel 61.8-153

19890 55.4-166 4.04 -13 -48 +03 4.45

196724 64.6 -12.1 4.80 -02 -08 +03 3.70

196867 60.3 -15.3 3.77 -06 -22 +04 3.15

R Dia 16 32.5 tll 52

149880 V R¹¹ P.I. 50

.025 9.15 7.03 +1.79 637 -0039 -017 det

.055 8.42 6.64 +1.55 70.7

.055 7.64 6.28 +1.37 806

.11 7.48 6.16 +1.32 846

.17 7.76 6.28 +1.39 986

.23 8.4 6.46 +1.52 113.7

.285 9.68 6.81 +1.75 1226

1.085 7.60 6.10 +1.33 333.8

1.12 7.35 6.01 +1.24 331.8

1.285 8.57 6.66 +1.41 3726 85

R Dia 7.3 +1.35 +0.85 -3.55 -40 -142 -17 -24 -132.8 246 E=405°

HD14980 6.1 +1.30 8.55 -4 -8 +10 -15 +36°

R 98.5 + 39.7 = 5.08-03-16

97 41 14+ 5.53-6-16 404 4.50

R Dia 4070950
 145580 16 32.5 20032
 766 51 6.3 9M7e-132.86
 22297
 -0052573
 2036511.0
 7017
 -0041 224 010

9536

31.322 1904.1 466 51 28.30 1907.0
 234
 1.555
 -45 -4
 -41 -33
 -47 -14

$$\begin{array}{r} 234 \\ \underline{1361} \end{array}$$

$$\begin{array}{r} 10053 \\ \underline{2760} \\ -15 \end{array}$$

$$\begin{array}{r} 1.555 \\ \underline{29.85} \end{array}$$

03
 5124
 891

3043

$$\begin{array}{r} -34 -17 \\ \underline{-8} \\ -14 \end{array}$$

30.4 1930.3 -50 -7
 -21
 -49 -14
 -6 +3
 -41 -15

$$\begin{array}{r} 470000 \\ \underline{178} \\ 48 \\ \underline{08} \\ 1660 \\ \underline{44} \end{array}$$

$$\begin{array}{r} 30.19 \\ \underline{0.34} \\ 30.53 \end{array}$$

-31 -15 5000

-263	+558	+114	+0386	-0681
+628	+277	+277	-0918	-0055
-735	-277	+619	+1080	+0157

+0255	-142
-0573	-486
+1277	+038

5000	-132.8
-256	-15.4
-152	-103.1
-18.4	-92.2

SB -24 -15

+0259	-0681
-0711	-0055
+0836	+0147

-0382	-40
-0764	-142
1033	-17

TXRue
 15-0077 16 34.3 +60 34 6.85 SR 79.4 SR(79)
 -0068±5.0 +015±3.8 SR 79.4 SR(79)
 +0080 +003
 34 6.85 SR 79.4 SR(79)
 8
 9M4e 45-2.0

22330

9546 17.495 1906.1 +60 34 9.43 1801.8 8.50

299

begin end cut

74
 8.69

465 -39 +126
 /000 +13 -16 +15

7.13 +1.71 +1.75

17. 994

12.3 1925.9 45 -15

55.97
 21.618
 175.50
 63.8

29.7

8.150
 38
 8.108
 8.74

63.8
 647 1114

7151
 35.8

17.437
 30
 967
 557
 237

34.8

906 1045.61
 -22
 884
 8.81
 +.12

$$\begin{array}{r} -0084 + 013 \\ + 1 \\ \hline + 2 \end{array}$$

$$\begin{array}{r} -0082 \\ + 012 \\ \hline \end{array} \quad \boxed{-060}$$

AT Wa 16.4 +59 53

33~

AT Wa 535 +1.63 +1.35 -3.55 421 -17 -35 +4 -35.7 ?
+1.16051 3.75 +1.20 6.2 +11 +6 -6 +25 gms +420

us

AT Run

16

16.4

+59

52

174
564
23

147232

By

2433976 5.43 +1.64 +1.62

275

389

+128

9a15

398 +1.23

284

3.90

+1.28

216 5.35 +1.63 +1.70

298

3.53

+1.30

217

3.87 +1.26

230 5.47 +1.60 +1.65

244 5.35 +1.62 +1.70

385 +1.26

246

3.84 +1.26

251

3.91 +1.25

261

3.98 +1.31

266

3.50 +1.37

267

5.50 +1.61 +1.66

147232 16 16.4 $+59$ 53 5.6 $gM4$ -35.76
 $+0010 \pm 2.8$ $+020 \pm 2.1$
 $+0014$ $+023$

21943

9392 24.940 1889.7 $+59$ $5-2$ 32.27 1889.5

340
 348

$\frac{060}{930}$

-1.21

31.06

1.28
 154

0.00
 24.945
 $\frac{24.945}{50}$

71.2 1926.1

39.68

31.52

42

31.94

9
 31.85

1.88
 458
 638

999
 9

9985

45.8

25.004

4992

24.951
 $\frac{30}{981}$

+ 062

32.08 1944.81

-34

32.34

7091
 35.5

46.0

32.10
 $+ 1.04$

R Gem

04.3

+22 47

Se

003-003

ml

-40.8

-0003-008 Lubin

-0004-005 ✓

-005-005

R Mem

53791

7 04.3

+222

47

5.97

-40.86

370d

+005

-44.2

-005

-5385e

-90

4679

⁴²⁴
2844

-006

⁴⁷⁹
2370

9340

20.818

1894.2

+2246

56.68

1889.3

$\frac{-28}{790}$

-0004 -005 \rightarrow
¹⁵⁸⁰

$\frac{30}{56.98}$

20.724

$\frac{19}{743}$

$\frac{744}{-046}$

36.1

$\frac{56.34}{3}$

1932.4

$\frac{6044}{30.3}$

20.715

$\frac{30}{745}$

$\frac{744}{-046}$

56.471928.04

411.0

$\frac{250}{56.50}$

$\frac{56.58}{-1.40}$

-308

125

943

10087 -0080

10057 +13

-38.5

$\frac{56.58}{-1.40}$

-347

908

-239

10099 -0214

-0115 -2.8

+9.6

886

899

237

-0250 -0095

-0345 -8.5

99.7

9398.000*

7.000*

4.300*

22.000*

47.000*

-0.005*

-0.005*

7.500*

316.228

-40.000

0.004

0.943

-37.156

-0.013

-0.236

5.463

-0.031

0.233

-19.146