

1224 8 54 24 -48 55 11.7 08 2
? ?

①
12.42 + 0.605 = 13.025

269.2

-1.9

1228 8 59 37 -47 34 124 08^T 2

31.8

(1)

1337 10.66 -0.055 22/units

268.2

-1.0

• COB-4604657

Shell?

See sp. below 2, 53

HD

1179

8 49 35

-46 19.5

114 A17a

Boston shell

Check

$$f = 246.3$$

$$f = -116$$

118

62

7740702

9

59

42

28

15

100MT

948

+1.59

19 Jan 15

937

+1.63

12 Mar 15

7.42

+1.59

20 Jan 15

7.53

+1.61

23 Jan 15

97450

-5302050

9

00

00

-54 16 8.1 89

?

96569

11 04.3 -68 81

NSD

Part
NSD

$$7.35 + 1.67 + 2.03 \textcircled{2}$$

$$6.46 + 0.80 \textcircled{2}$$

$$-0.001 - 0.009 - 1.8$$

+	28 £	36	+28
x	16 £	36	+16
△	15	£	+06
o	15	£	-05
●	15	£	-06
△	20	£	-12

✓

9141025-

9

04

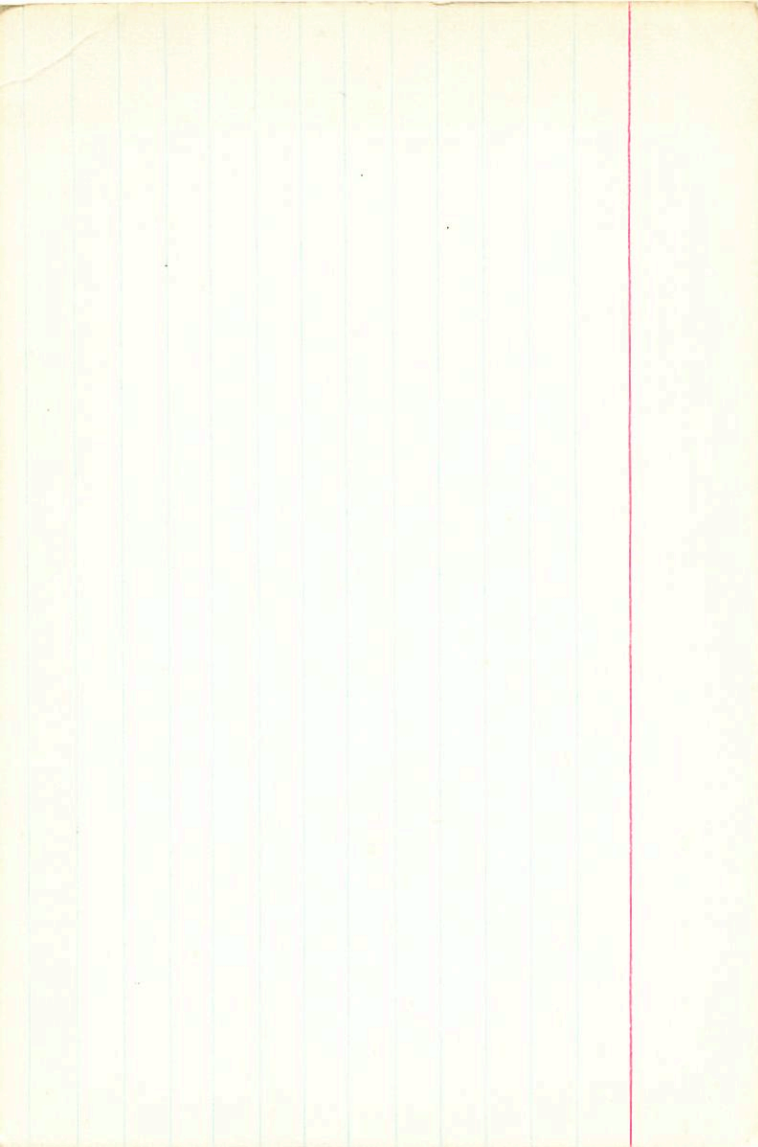
26

-53-

07

8605

Scipio 000-10104 548



R

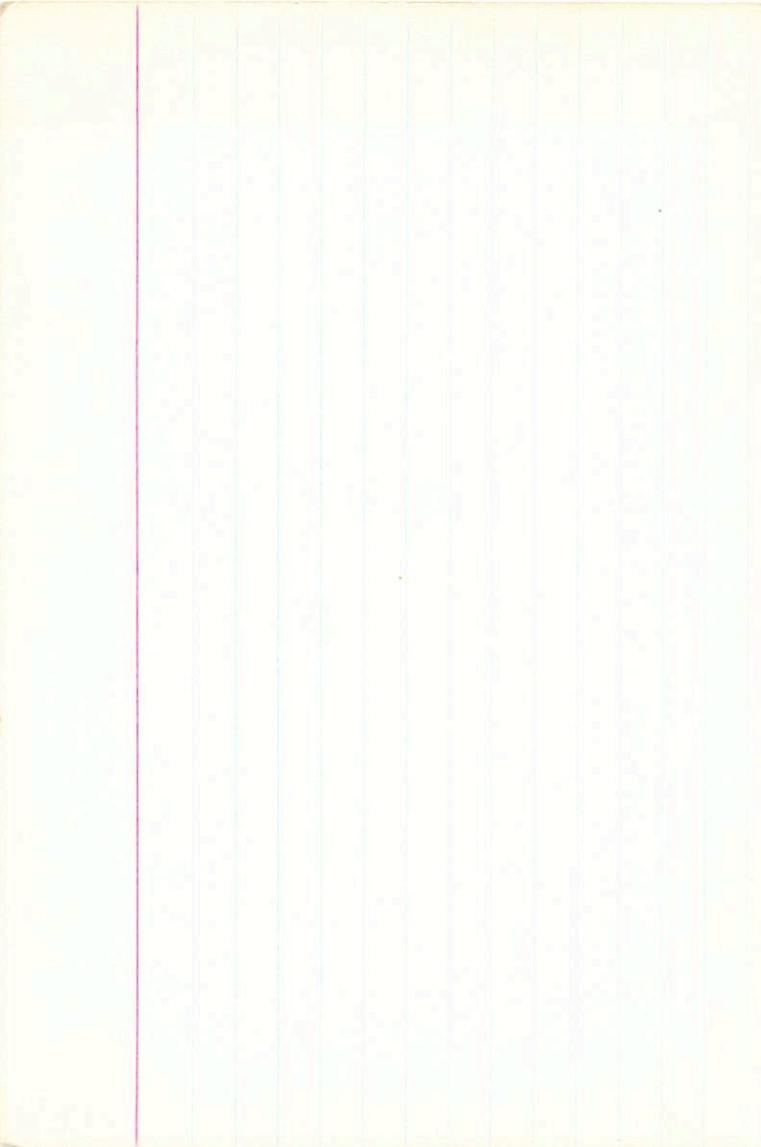
~~4502418~~

44 06

46 06.5

3.6 85

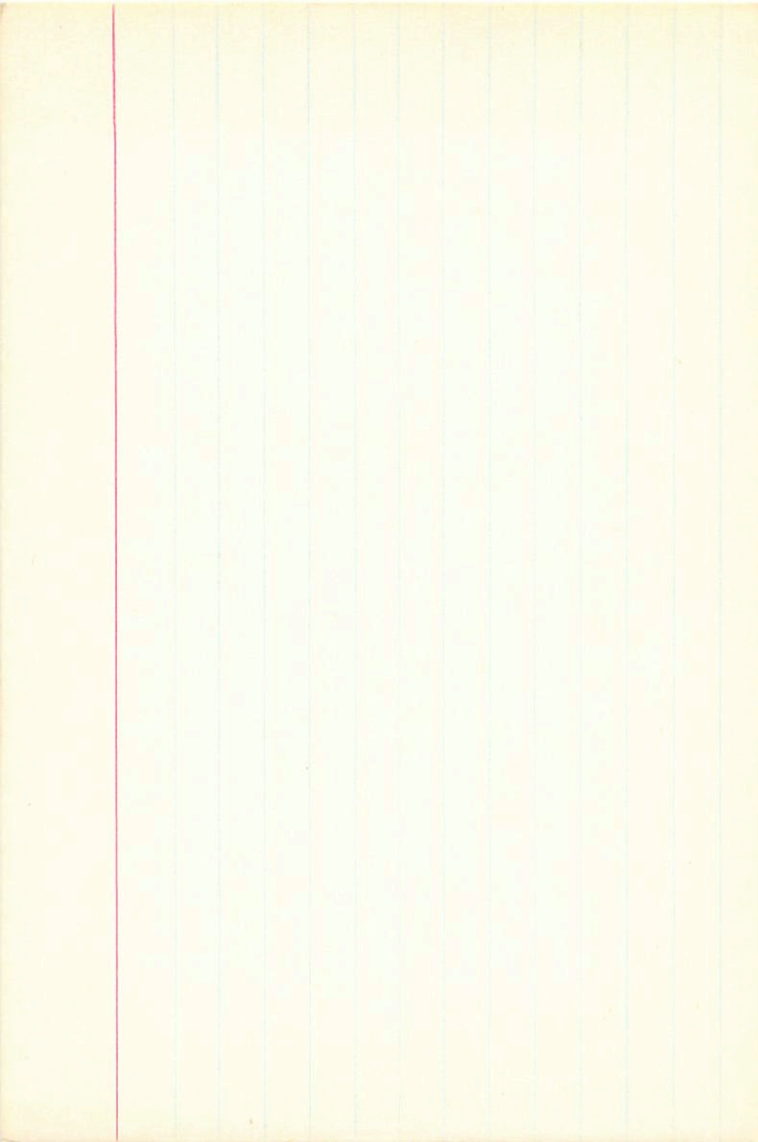
9.86 70.005 - 0.60 22 Jan 75



9464
-480 1503 08 44 26 04 14
-49 16 8.4 04

~~440~~

8.17 -0.095 -0.378 4pm 75



-4602938

✓

8

44

33

-46

855

98

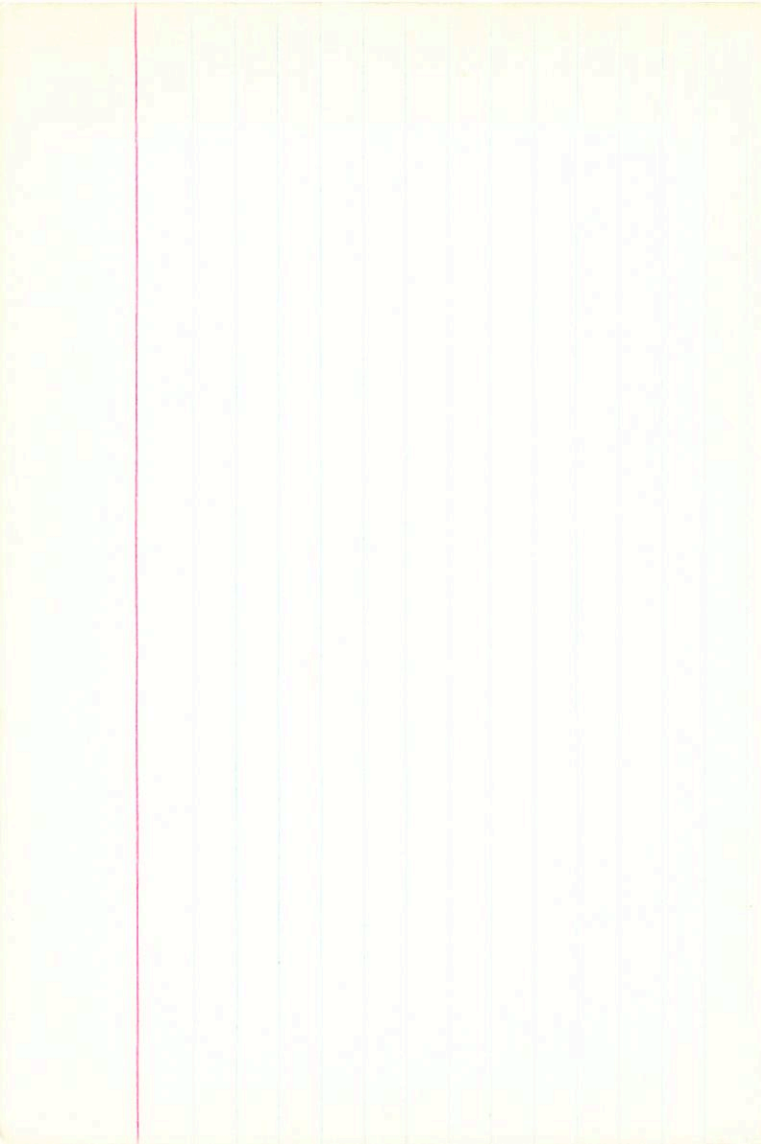
R4

9.53

^{-0.02} 1003

-105

20 Jan 75

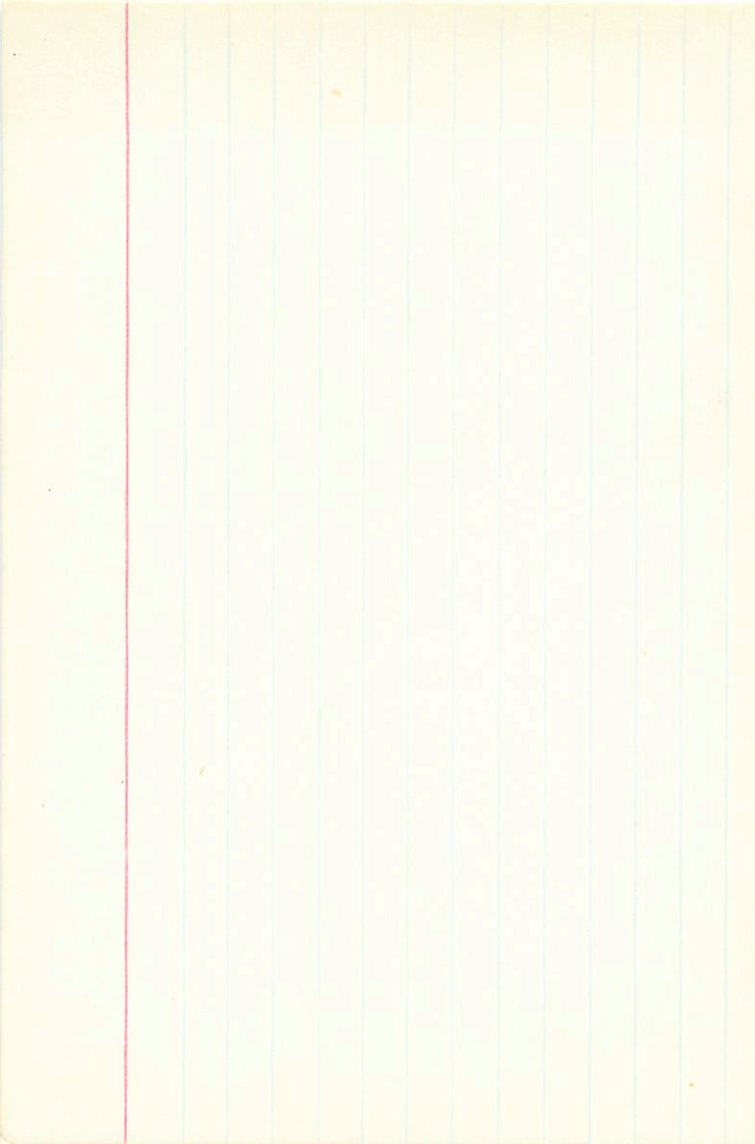


-4704332 ✓

95014 8 45 03 -47 29 96 89

-4702652

882 +0.08⁰³ -0.09 23 Jan 17



✓
-50° 1726 CPW 8 45 04 -50 52.5 10.3 B3

9.87 + 0.43 (1.40) B3 \bar{V}
9.86 + 0.425 - 0.325 4 Jan 74

9.86 + 0.43 - 0.325

269.2

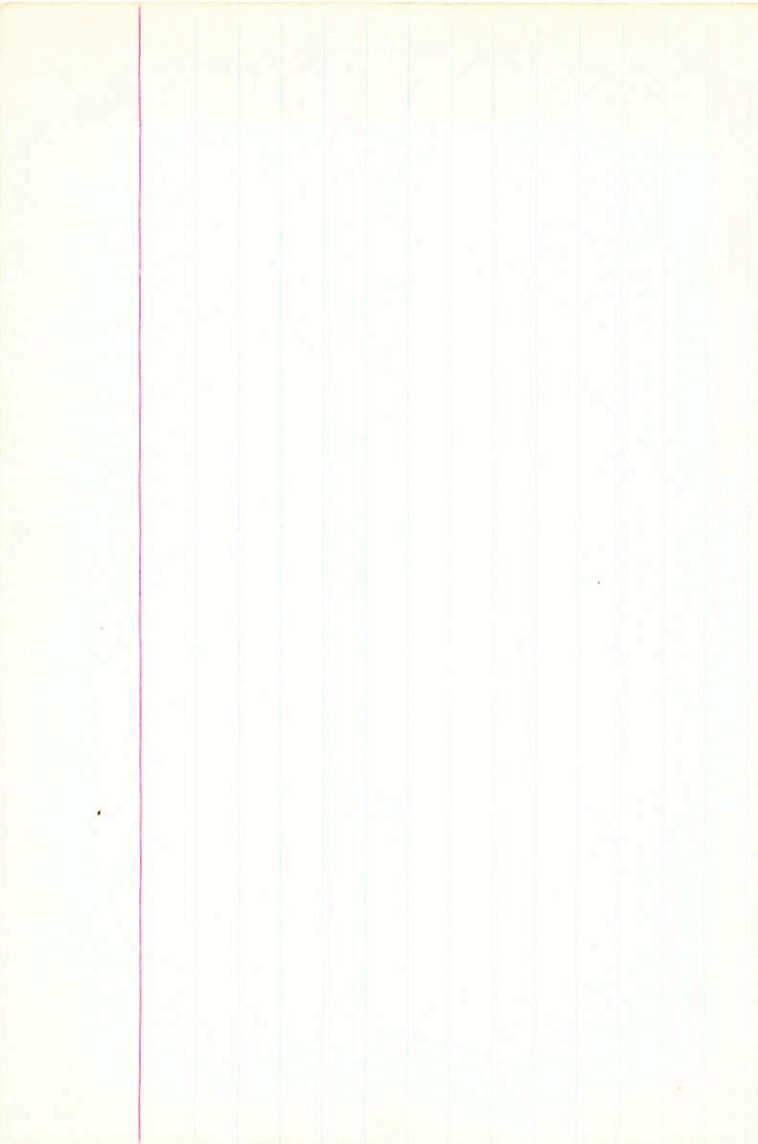
-4.9

2

4102968 8 45 27 46 28.8 2789

950 10.105 - 0.44 22 Jan 75

B

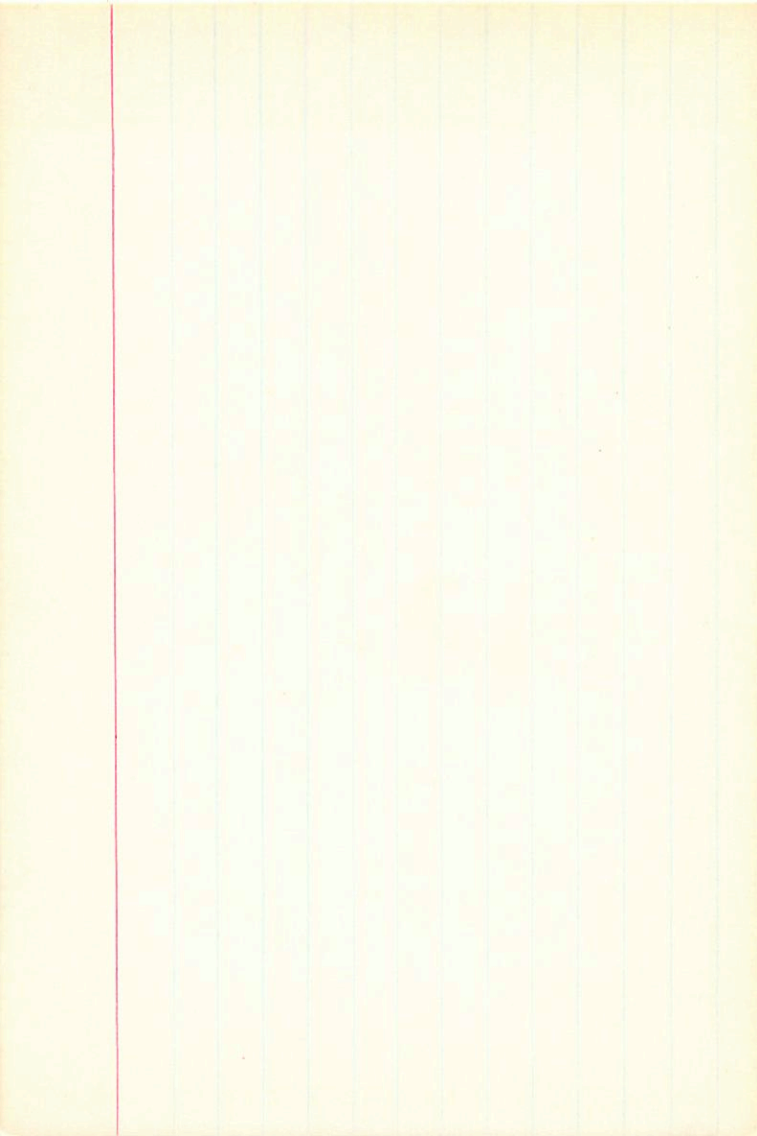


95129 GC

-4704339 08 45 30 47 275-6.805

-4702691

6.50 +0.22 -0.30 31 Dec 74



-49° 18' 65" N

8 40 35

-49 10 10.2 84

10.17 to ~~10.18~~ - 0.155 20 pms

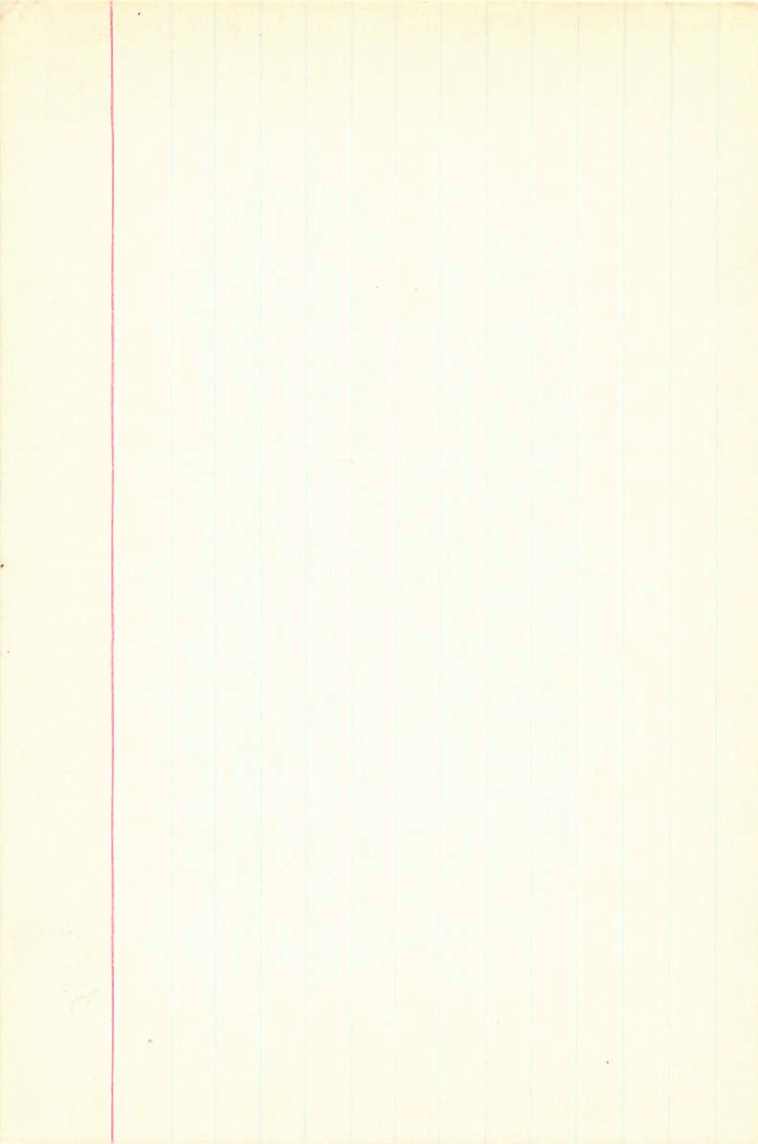
11-050
42 00 1-240 80 50 191-113

74456 R 8 41 27 -45 22 9.8 B9

CPD-4801572

" -0006-502 Y+L

913 -0065-0455 22 part



-4503039

5

46

00

-44

21.5

9585

R

941 10.04 - 0.57 22 Jan 75

06776044-

76259

-4901831

68

46

12

-58

04

92

89

-4903912

9.34

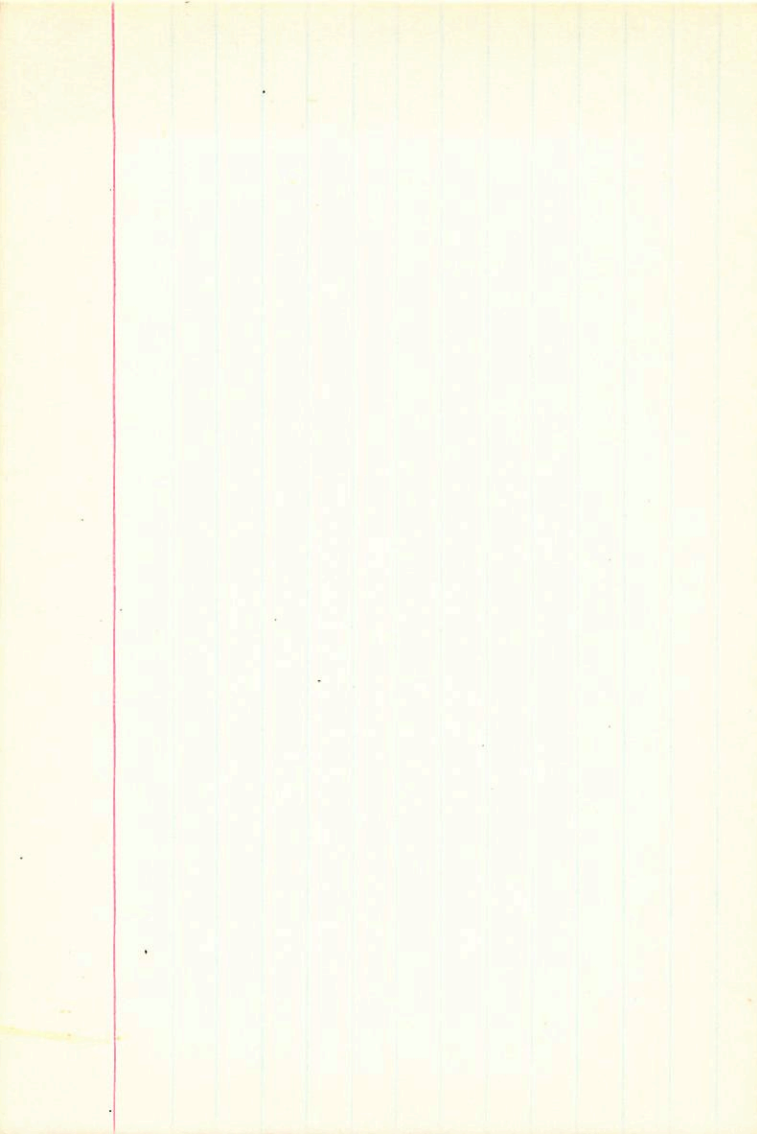
-0.13

-0.38

31

100

274



-4503046

8

46

16

-46

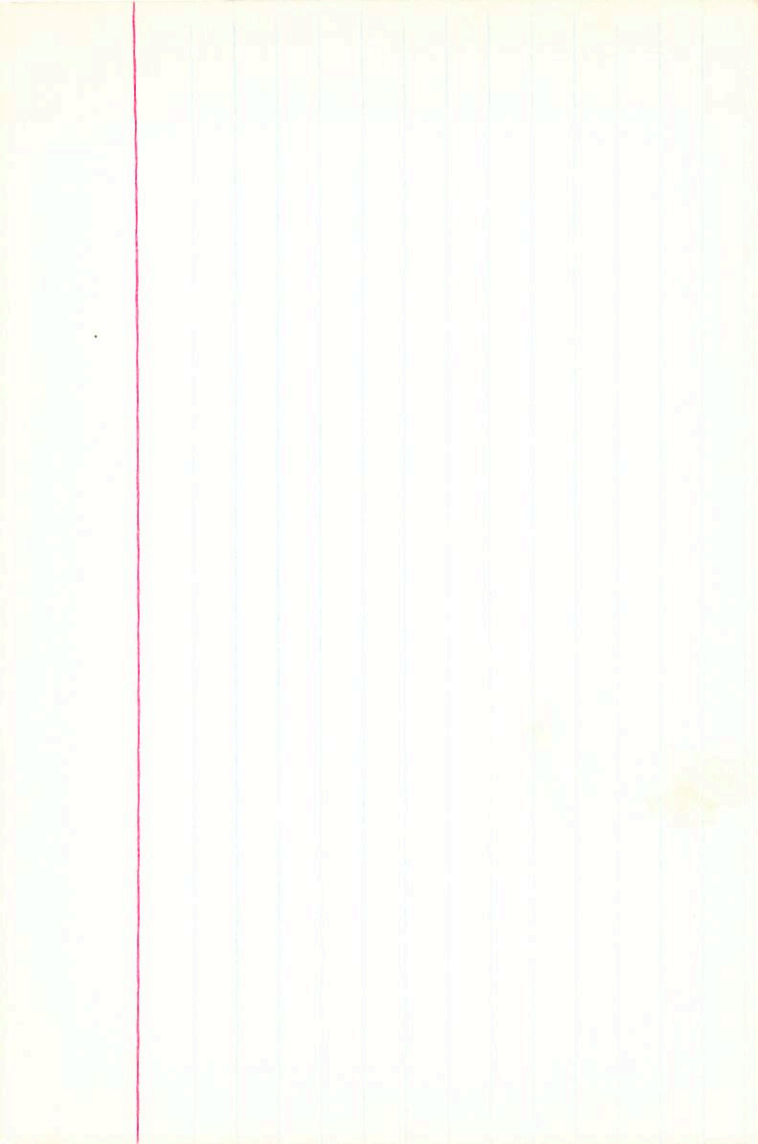
12.5

100

BS

6

10.03 TD.18-D.615 22 Jan 75



SS1156 F22 II

HQ8496

8 YL 28 -44 03.5 F2108

HQ85276

574 +0.56 +0.35 F22104 C

2656

-17

14075293

COO-4701558

Bird

(Si)

-4702729

08

46

29

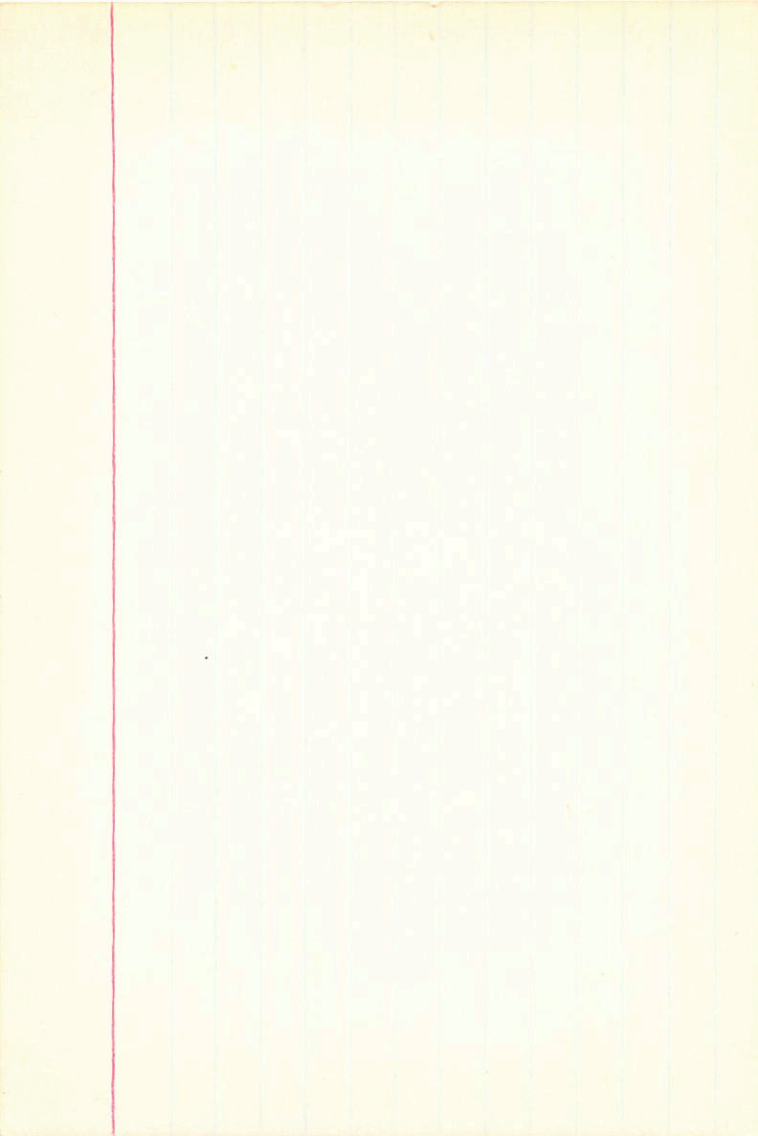
-47

48.5

54

89

9.29 -0.035 -0.20 31 Dec 74



62 581157 14075309

-4504549 64 46 35 -46 21.5 2682

-4503056

7.88 -0.025 -0.83 3110174

7.84 +0.02 -0.85 *Lenin*

7.86 0.00 -0.84

2659

-19

1158

8 44 39 -47 36.5 12.6 08

12.53 10.175 -0.51 4/Jan 25

Q

8.996.8

6 = 2.7

R

-4603016 8 96 43 -46 56.5 103 RF

10.50 +10.08 -0.55 22 Jan 75

④

100

—

95867

16

-4501839

08

~~40~~

41

-50

045

92

89

-4503819

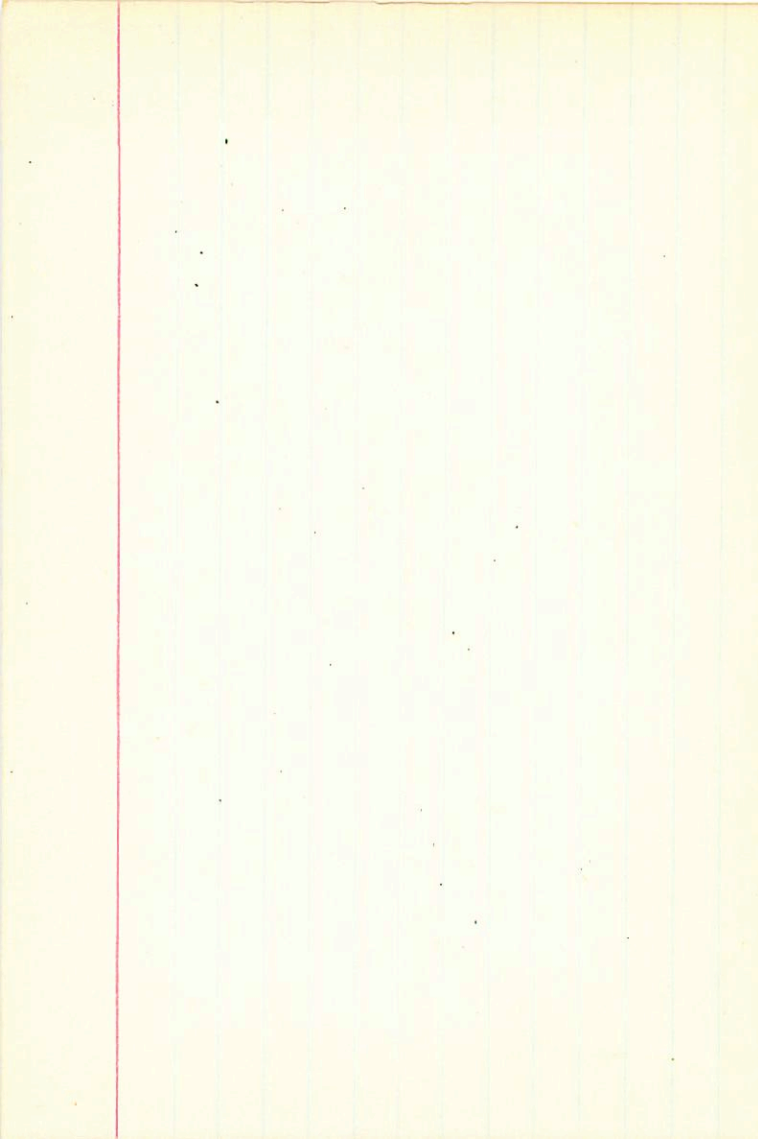
\$9.33

-0.11

-0.565

4 Jan 75

9.26 - 0.115 - 0.615 22 Jan 75



78344

-4603015

08 46 47 -47 06.5 92 R

-00107015

9.12-10.68-0205 22 Jan 75

-4603015

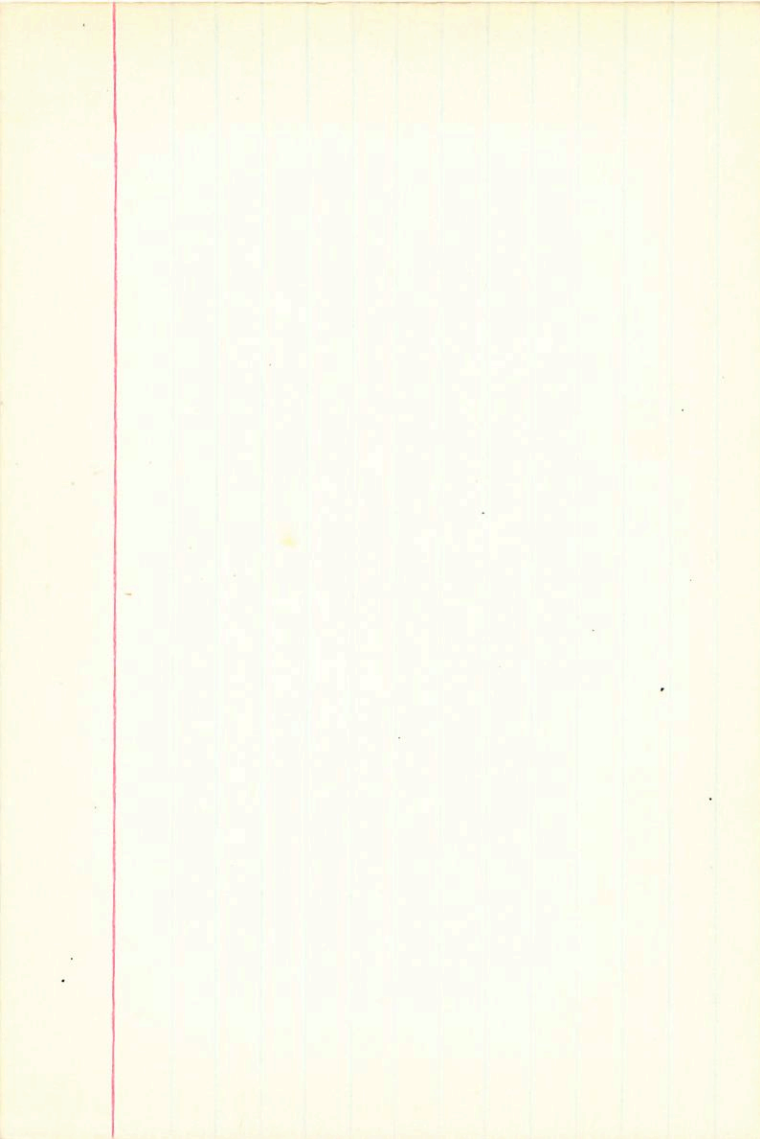
08 46 43 47 06.5 10.2 04

-00107015

16.46 10.18-0.05 22 Jan 75
(10.49 10.05-0.22 31 Dec 74)

3017

3015



75520

SS 116.2 · 88 47 46 -47 71 8.9 4778

-220274

9.17

+0.555

+0.525

31 Jan 74

8.20

+0.575

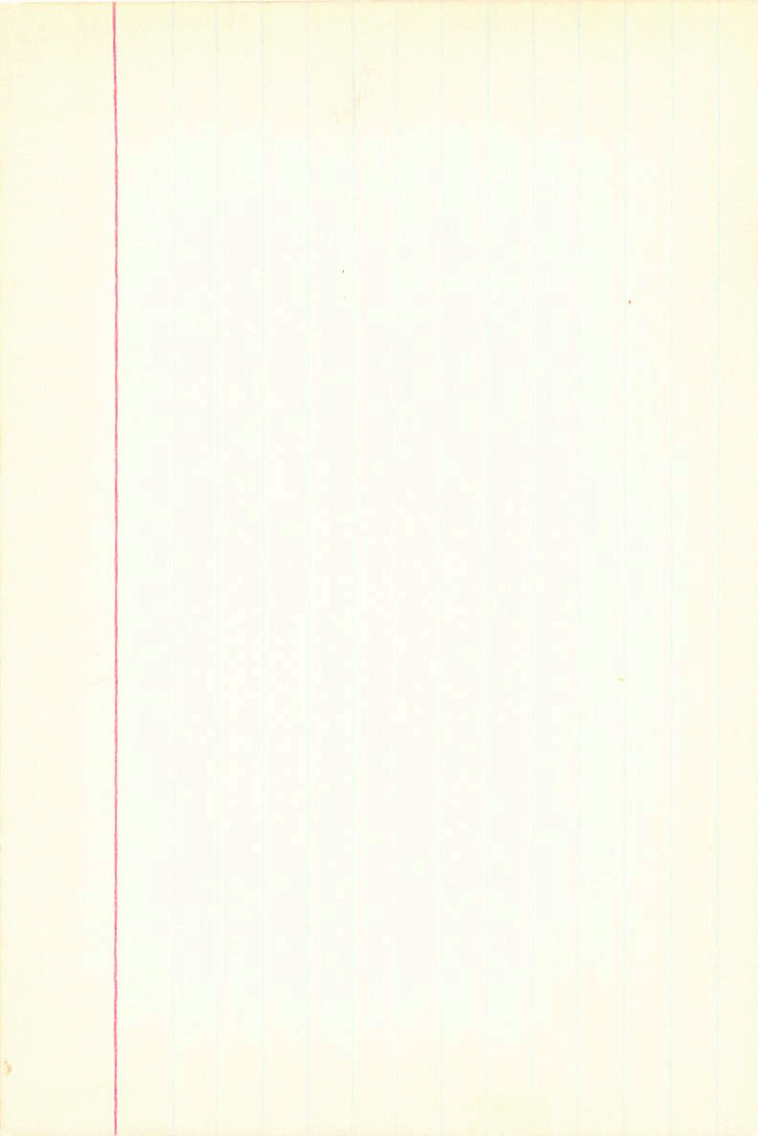
+0.50

4 Jan 74

8.15

+0.565

+0.515



95551 Not needed by SS

935 B

1164 / (-4903889) 8 47 500 -50 16.8 - 9500-1

-4901861

9.29 + 0.10 - 0.605 4 Jan 75

2690

-42

~~58#~~ 581165

-47 02750 08 47 55 47 40 8.0 B5

HD7553#

7.88 +0.325 -0.56 31 Dec 74

7.94 +0.37 -0.58 *Correct*

7.96 +0.345 -0.57

$$k = 267.0$$

$$f = -2.6$$

-463054 4 48 00 47 12 9.4 09

622" $\frac{3}{2}$ ft

960 + 0.08 ✓ - 0.66 25 pounds

19810561

75589

$n = 1026$

4503096

8

45 14

45

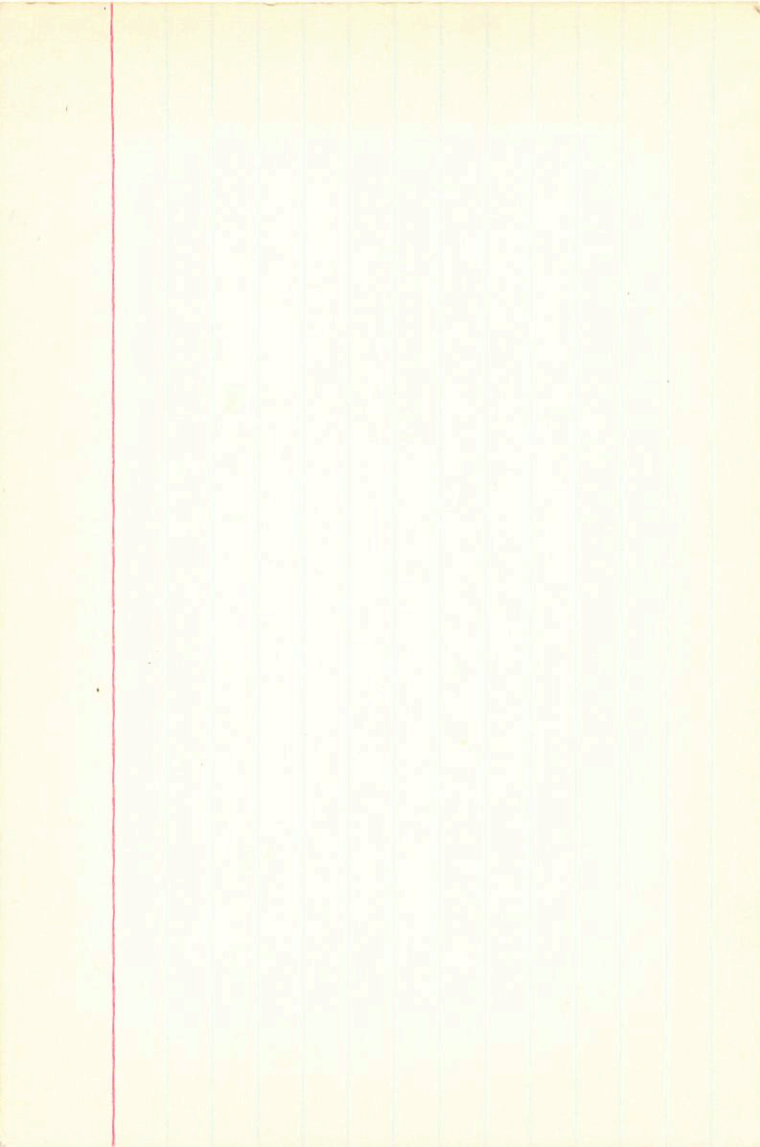
32.5

8.9 PD

-0049+038

8.35 + 0.265 + 0.05

4 years



1169

8

48 48

-46 455-

107

08

-4603053

1002 +0.095 -0.72

4/Jan 75

9.6

05

$h = 266.4$

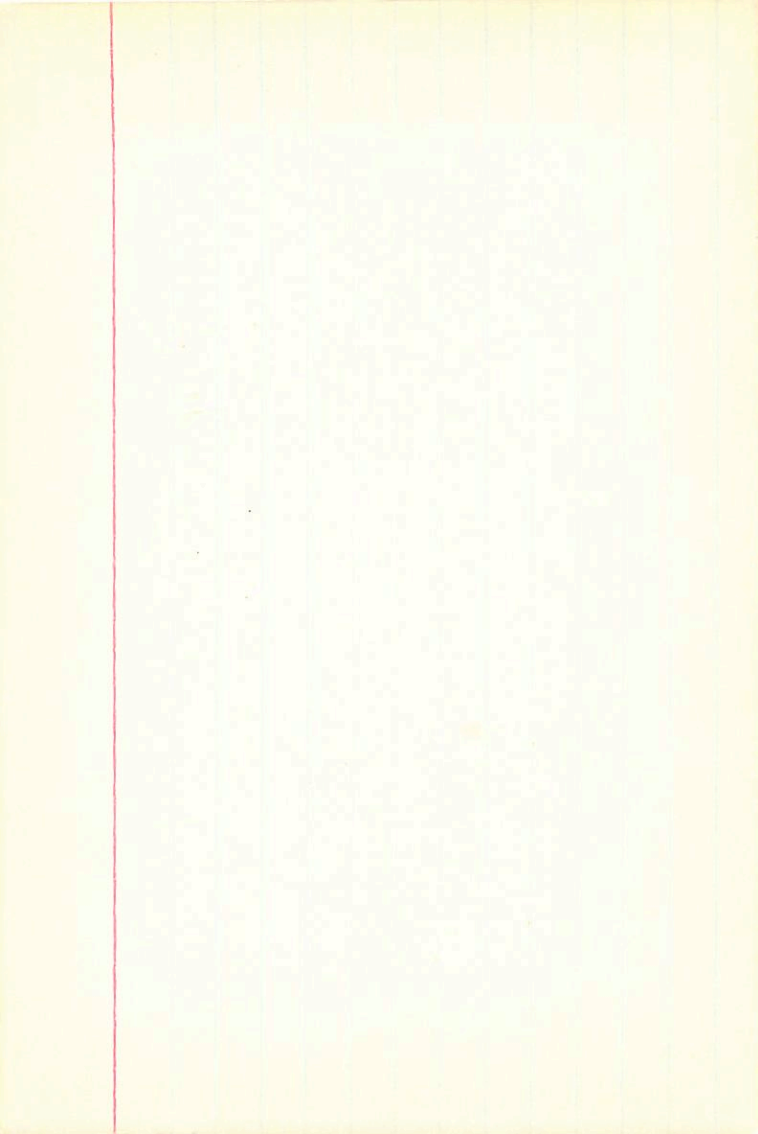
$b = -1.9$

28744
-4904411
-4702787

68 49 05 -47 82 102 BF

-0.05
9.59 -0.005 -0.548
9.55 -0.065 -0.52
9.57 -0.55 -0.50

312274
4/2/78



4504606

1177

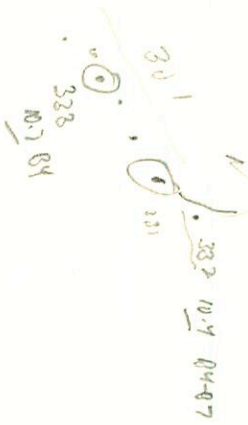
CDD-4403129

(3212)

8 44 22 45 25.5 26 08

8.44 +0.37 -0.62 BOSTY C

0.12 1.3



H

ZLCM

-10

APR 1962

8 49 23

48

57

106

89

10.19 +0.32 -0.45 20 Jan 75



912-514-216

2280

2100 11/10/10 11/10/10 11/10/10

4801443 8 44 25 -48 36.5 104 188

10.16 + 0.205 - 0.27 22 Jan 15

B
2.5"

R 13.33 + 0.56 - 0.045: 20 Jan 15

140934

140934

00 11 06

00 11 06

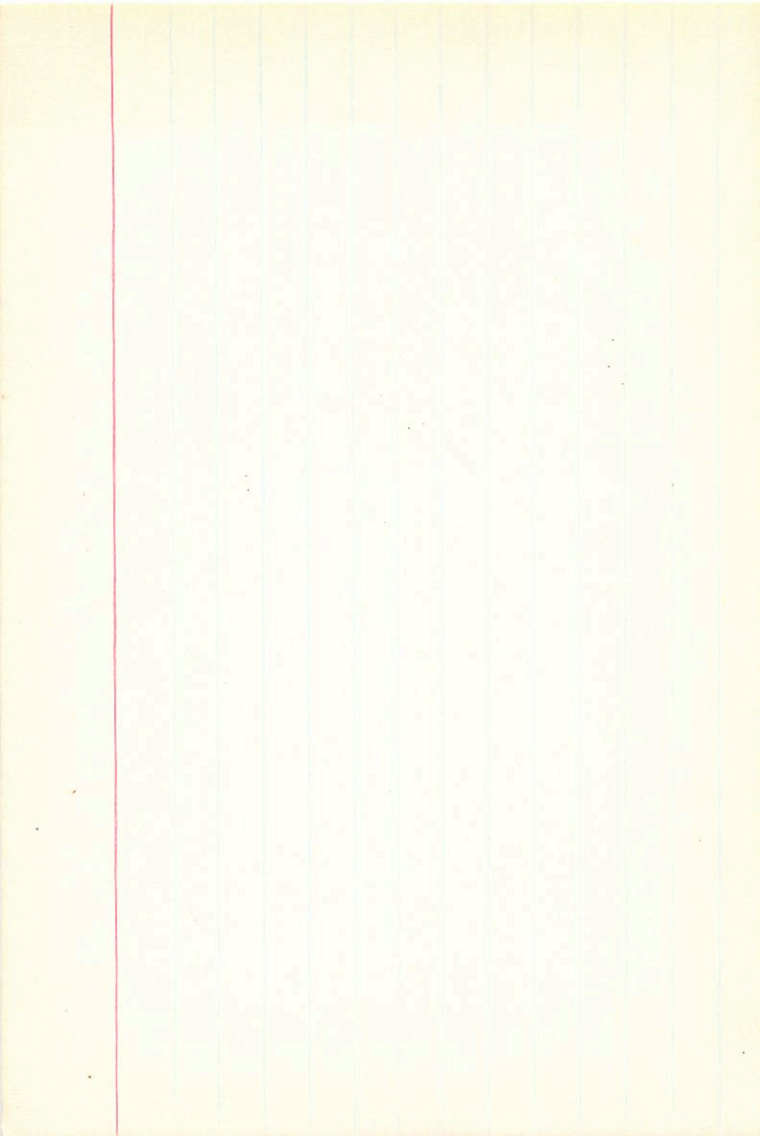
7

140934-00 11 06

789224

4702501 08 49 86 -47 41.5 96 85

9.10 -0.10 -0.59 31.12.74



SS 11T for HAD-20

-4602120
HR 3527

4 49 43 -44 25.5 R0711

ADN 5821

11m 3.5"

S.10-0.22-0.98 R0711 C

R0711
09.5 III

HR 3525

266.2

-1.6

-180 1571 B 5 44 45 -44 17 109 89

10.66 to 1.35 -0.42 -2 parts

1-2-56
976, 977-14

4901409

B

T 44 48 -44 52.5 10.5 84

1003 +0.12 -0.45 22 parts

10-11-37

10-24-37 10-24-37 10-24-37

1185

8 49 52

-46 325

110 ADI

9.76 + 0.65 + 0.125 4/25

$$f = 266.4$$

$$f = -1.6$$

1156 8 49 57 -46 17 110.08 -

994 1035 0.65 4 years

266.2

-1.4