

B -015 151 899 2891

1945

5-

38.2

+29 27

BF

05

6.43-10-39

7.17-05-14

+29

-043 124 599 2.764

111 607

222

829

(B) -015 151 899 2.891

7.17

147 892
294
1186

$m_v + 1.25$
7.05

(38) x
Hindan

(2.1) x
6.1

$m_v = -0.1$

VO $\frac{6.4}{6.8} x$

+19.0

+0042 -02692L

+0009 -02586L

+00051 -0240 F124

+0067

+006-024

B

8712 0772 } 0244
0071
4909 -9970 } +7.25 004
6.43

1945.000*

5.000*

38.200*

29.000*

27.000*

0.006*

-0.024*

6.100*

165.959 195

19.000

0.002

1.000

19.248 19

-0.111

0.016

-18.172 -13

-0.037

-0.009

-6.246

-2027.000*

5.000*

50.500*

59.000*

52.000*

0.000*

-0.020*

6.300*

181.970

-2.900

0.049

0.857

6.378

-0.071

0.428

-14.099

-0.040

0.285

-8.158

47.06
8
46.98

66.40

28.968
34
4
00
24.

31 km 30. +6005 ± 1.8 -0.20 E 1.4
 39220 5 50.5 +0608 -0.21
 +59 5-3 5.3 40 -2.9a

3653

+0004

-018

7462 29.006 1900.3 +59 5-2 47.14 1891.6

0.25

28.981

29.004 (blurred) 46.46

48.31

14.67

24.0

1927.6

14.015

25.70

28.985

49.70

29.010

-2.45

47.31

0.33

0.12
 +.031

(34.5)

47.33

1.00

28.985

47.55

47.31

1944.84 11947

39.8

29.001

47.04
 -14
 33

47.13

1947.01

(48.2)

6.62-06-39

5 57.1 -1 27 RS III

2109
40524

-012 094 648 2703

090 650

180
830

V^0
 w^1

$M_V = -1.35$

2111 5 52.9 +27 34 608 B&Dob

H66

~~20800~~ 593 2.058

~~158~~
293

∴

2130

60.5

415 42

104

515 11-12

5.16 - 0.42 109 602 2.722 0.85

56 610

$\frac{192}{802}$

$M_v = -0.9$

$V_0 = 5.90$

$\frac{5.95}{75}$

+24.3

PL15

spread spec

12:00 All line

T0002 - 020

T0013 - 0154

T0015

8177 6.5

5767

7000

018

T0020

018

T00042 - 0170 20

T00079 - 0164 32

T00062 - 0148 32

T00058

~~T0009-015~~

T002 - 018

- 11

0034

2.73

7.33

29674 34.1

25.76

20

305

2975

980

1000

35.64

961-084

1000±23
+1002

-0.14±18

-0.21

31.8

1005

1.02
32.71

29684

66.57

35.29

1005

1002

-5

1.24

106.6E

+1002

29696

66.57

35.718

-0.6

1005

1002

35.82

+0.90

29675

35.12

35.82

+0.90

1005

1002

35.82

+0.90

1 Glen over me 1st L 011 +23 16 565

2134 Apr 5 13 FWD 4.15 +0.87 +0.52 25

41116 3.81 +0.31 25
510.9.5

17 +10 WSD 456 295 10.4 402 E 1
452 4.7 3.6 4.1

-0.00062 -0.1017 HWD 120.24 1566

-0.00064 -0.1022

-0.0008 423 13.3

-0.0058 13.3 13.3
13.3
13.3

-0.006 -102

446 -
m₂ / m₁ = 0.587

Hank's K.S. (110)

Robert Atwood

18 years?
5m 2.0

3.7 7.2 2.6

-17 -19.794

-0.264
0.013

-33.047 *25*

-0.403
-0.122

16.549 *17*

-0.046
0.992

20.200

75.858 *558*

4.400* *3.75*

-0.102*

-0.006*

16.000*

23.000*

1.100*

6.000*

2134.000*

Handwritten notes:
2.2
2.2
2.2

Handwritten: 0125



Handwritten:
A
B
444
325

Handwritten: 272

used (Kru)

1 stem 01.1 +23 14 +20.2a

HNR2134

4.14" +0.71"

41116

Sp. B. P = 9.6^d

-007-1056c
-009 -102N3D

3801

7B

-0007 -102 N3D
-0007 ± 1.2 -104 ± 1.0 GC → N3D

9676

9.89669 31.7
Aufpas

(Obs: 96,188)

8116-0138
5892-9999
1021
-0574
-24

0201
3351

0156
347

2207

1224

$\begin{matrix} 528 \\ 206 \\ \hline 106 \\ 106 \\ \hline 212 \\ 212 \\ \hline 424 \\ 424 \\ \hline 848 \\ 848 \\ \hline 1696 \\ 1696 \\ \hline 3392 \end{matrix}$

$\begin{matrix} 124 \\ 124 \\ \hline 248 \\ 248 \\ \hline 496 \\ 496 \\ \hline 992 \end{matrix}$

111

114

$\begin{matrix} 564 \\ 228 \\ \hline 792 \end{matrix}$

$\begin{matrix} 103105 \\ + 01032 \\ \hline 104137 \\ - 0184 \\ \hline 103953 \\ - 0168 \\ \hline 103785 \end{matrix}$

1213

$\begin{matrix} 10022 \\ 10022 \\ \hline 20044 \\ 20044 \\ \hline 40088 \\ 40088 \\ \hline 80176 \\ 80176 \\ \hline 160352 \end{matrix}$

2207.000*

6.000*

10.600*

18.000*

42.000*

0.002*

-0.017*

7.300*

7.2

278

288.403 3000

21.300

-0.015

0.978

+16

16.365

-0.074

-0.209

-25

-25.652

-0.031

0.007

-8

8.685

13201236

2134

Si

6 022

132

36

41264

-031 122 759 2.768 6 12496

~~414 132 904 2.748 6 4466~~

70010 510.0 -016 59.5

15889 1505.7

75051 1505.2

98651

85451 1549.8

1414 5111

ADSV7749

42111 6 06.4 1000 +62 31 5.6 A0 +34.26

3871

7817

21.271 1904.1 +2 30 32.75 1895.4

$$\begin{array}{r} 262 \\ -9 \\ \hline \end{array}$$

$$\begin{array}{r} +0005 \\ -015 \\ \hline \end{array}$$

$$\begin{array}{r} +1.08 \\ \hline \end{array}$$

$$\begin{array}{r} +0002 \\ -018 \\ \hline \end{array}$$

5m 118'

$$\begin{array}{r} 21.253 \\ 317 \\ \hline \end{array}$$

$$\begin{array}{r} 276 \\ +004 \\ \hline \end{array}$$

$$\begin{array}{r} 33.00 \\ \hline \end{array}$$

$$\begin{array}{r} 1933.2 \\ -0006 \\ \hline \end{array}$$

$$\begin{array}{r} 287 \\ \hline \end{array}$$

$$\begin{array}{r} 276 \\ \hline \end{array}$$

$$\begin{array}{r} 53.18 \\ \hline \end{array}$$

$$\begin{array}{r} 21.249 \\ +27 \\ \hline \end{array}$$

$$\begin{array}{r} +.014 \\ \hline \end{array}$$

$$\begin{array}{r} 32.6 \\ \hline \end{array}$$

$$\begin{array}{r} 32.84 \\ +22 \\ \hline \end{array}$$

$$\begin{array}{r} 1938.88 \\ \hline \end{array}$$

$$\begin{array}{r} .276 \\ \hline \end{array}$$

$$\begin{array}{r} 21.248 \\ 276 \\ \hline \end{array}$$

$$\begin{array}{r} 33.06 \\ \hline \end{array}$$

$$\begin{array}{r} 33.12 \\ \hline \end{array}$$

$$\begin{array}{r} 36.2 \\ \hline \end{array}$$

$$\begin{array}{r} 40.3 \\ \hline \end{array}$$

B +1 A6W

$$\begin{array}{r} 21.248 \\ 276 \\ \hline \end{array}$$

$$\begin{array}{r} 2.48 \\ \hline \end{array}$$

$$\begin{array}{r} 1.44 \\ \hline \end{array}$$

$$\begin{array}{r} 55.24 \\ 332 \\ \hline \end{array}$$

$$\begin{array}{r} +0001 \\ -015 \\ \hline \end{array}$$

24 204

6.100
2.500
9.000
-19.000
6.900
240
240
34.200

-0.090
0.445
0.891
-43.913
19.937

-0.481
0.764
-0.430
-89.303
-86.134

0.872
0.467
-0.145
-4.883
-6.143

6.100
2.500
9.000
-19.000
6.000
150
150
34.200

-0.090
0.445
0.891
-43.913
23.511

-0.481
0.764
-0.430
-89.303
-28.865

0.872
0.467
-0.145
-4.883
-5.746

2174

A 5.71 053 130 1.228 2.822
 B 6.99 019 148 981 2.574
 66.4 12 30 AD

4211

7817

+0003-019

+0005
+0007

Bud 51

+0002-019

X3117

+0003-019 ±2

+0005-019

+0005

+0002-019

5.25 +008 +0.14 5.49 ~

065 160 1.153 2.816 IG

0532190 1.328 2.804 4.604

0588148 1.212 2.810

1.1804 256

1.5271 2.516

1.1691 2.034

6.54 +004 -0.02 A02 5.5 ~

6.90 +017 163 969 2.874 (3) 404

40.8 Q=105

n=

144 1218
334 1218
944 1218
643 1209

-09

SPR

(-27)

647
577
90

2174.000*

2174.000*

6.000*

6.000*

6.400*

6.400*

2.000*

2.000*

30.000*

30.000*

0.002*

0.002*

5.75^r -0.019*

-0.019*

6.000*

6.050*

140 158.489

162.181

34.200

34.200

-0.041

-0.041

0.891

0.891

124 23.975

23.824

-0.073

-0.073

-0.431

-0.431

-25 -26.368

-26.639

-0.034

-0.034

-0.144

-0.144

-10 -10.273

-10.398

2 Car

22.8 - 52 40

F016

2326

45348

S.S

-0.75 +0.155 +0.22 *Green*

+02

-0.67 10.11 5

~~-0.24~~ -1.08
19

+100290¹⁴¹⁵
435

+0222 FRY +20.5a
4

-5.45

+0263
+ 415
+0308

1031 1023

+11
+04

2326.000*

6.000*

22.800*

-52.000*

-40.000*

0.031*

0.023*

5.800*

5.25

1125 144.544

20.500

0.084

0.138

+12 14.994

-0.059

-0.893

-25 -26.892

0.151

-0.427

+8 13.102

13 Mon

6 30.2 407 22

412.82
HR.32

HR23FS

+2 -5

-DD13 -DD06 W₂ SD

-041

AOIT8

+001-005⁸⁻

-007 -002400

-002 -002F

-003 -007

-DD11 -DD14

974
158
1134

-DD16

Edde

50 W4 984 2647

0.000 -001

15mm
5mm

2456

NC 2269

38.2 49 56 67

Finch's low limit

47839

87220

466 -0.24 -1.07 95
465 -0.25 -1.08 3 62

8.8873"

dundell 2204

-059 +035 -111 ② 2.589 ③

2600

$\frac{20}{-0.11}$

$\frac{11}{11}$

+8
-7
-00045
-0003
-0006
±1.0

E=405

-0006

-003-006

$V_0 = 450$

8.45

-006-004

96

33.2
X 211

M -445

634880-028659

47887 6 38 24.839 1899.6 49 30 49.7 11507

6.000*
 38.200*
 9.000*
 56.000*
 -0.003*
 -0.006*
 9.600*
 831.764
 21.000
 -0.006
 0.920
 14.019
 -0.018
 -0.390
 -22.812
 -0.026
 0.038
 -20.581

WLC
2244

2450.000*

3 Mem

2473

48324

6 40.9 +25 11

+8.82
9.0

W₈ 8D

2232

(+14)

-005 -014030

000 -01660

-005 -01512

-004 -015

700 21 -0164
-00015 -0156

664

273 3427 4142

1.349 910

-0020

+26.2

8.43 47322-47224

-002-015

892-5403 8032

-2
-15

8.85 5748 4212

1.377 985

+9.0

9.12 6446 5523
906 630-56 5434
912 62-14 5244
915 915

1.414 1017 445 W17

938

-1621

0005 0016

573

-4525

+24 904

6 40 51.373 1931.4 425 10 56.95 1931.7

6.650
25.200
-2.000
-15.000
7.000
251
9.000

-0.214
0.076
0.974
-3.578
7.867

-0.409
0.898
-0.160
-60.353
-16.601

0.887
0.433
0.161
-38.387
-8.194