

410045

CC16

(89)

14.4

+40 40

8.7 dmo +12

2w

146

M 20 (7)

SF 25 (4)

5594 +09435
+556 +0922w

6050

0409

+556

M L R

07350

R D M

60554

069w ←

0420

+524

+090

S F R
Cin 20

146

8.12 +0.61

~~560 +092~~

5

8.12 +6.1

(635)

557 +095

7.51 -

114
1/3

9947

9947

5672

5633

5632

+108 0587

0985

1282

6156

0120

013

+108 0587

0245

1282

H.S.

H.S.

0597

116

0591 114

1.116

146 00 144 490 40 40 dno 4122 sw

+40045 405
Yad 45 536
.060510 3W

-2.5 3 W/dm
+7.0 100/1500

+2

Upper
+1.556
+1.574
St R
Mc R
4122



571 ✓ $P=20$
0215 0595
+1.7 1.12

+0.540 40.050 435.1 -16.8 +0.8
0.0 +23 -11 0

944 9985
0442 1114
571 ✓
022 ✓
+1.78
0595
Pc = 410
1112

.050 Cn

-19.111

0 37.3 -19 44

88

0 420 2.1 -19 12.79

+27C 2W
dm2

w-105

MC - AL +255 +0.11

10.6 10 +8.3

+0.255 +0.011

9993 9912 } 2542
0364 1326 } 0229
-7.1

0 413 24.648 1902.3
 +0250510.6
 +0244
 -42 10 52.97 1897.2
 -07378.7 6-
 -073

$\frac{-1.168}{23.480}$

$\frac{3.85}{49.12}$

42 13.066
 1 11.248
 43 24.314
 $\frac{-0.343}{2.71}$
 1172

18 63.77
 8 12.68
 1924.39

10 51.12
 $\frac{+0.6}{5.104}$
 2.81
 26.42

24.935

40.3

10 53.77
 $\frac{-0.8}{1955.81}$

-034

42.6

$\frac{24.901}{.586}$

$\frac{53.85}{52.45}$

45.4

$\frac{1.106}{7}$

$\frac{3.33}{3.33}$

4378

0 43.4 -42 11

-26.3 ± 0.6 C₃(u)
-22.6 ± 1.1 C₃(u)

POW way

-25.5 ± 0.7

GC919
-4202-09

8.4 7.88 + 1.26 (+232)

A

Y146 E
8.4 } "
8.9 }

8.9

R5V
R7V

R6V } way
R6V }

+262 -082 Case
+278 -073 GC

78
+207
+278
-08
566 GC
GC

78 ± 12 C(17)

+71 532

00 52.6 +70 54

314,272
48

364⁺

W577

00 58.957.5 +71 24.72

CC66

59.0³

only the day 7 m d w

Green. Ad.

+1.735 -0.395

11113

10.2 M2 19.7

11113
10.4 M2
11113

1.783 -42.1 W

5.484

0.108

1.734 -41.0

-42.5
-0.570
0.0

Not at end of table

* erroneously called 80.700⁰6 in Yale Newsletter Conf.

(X)
M

Spinn AOS 433-440 5⁰ dust cut

AOS 440 1950 00 293 +66.59 20.160 3.1

150W 26.3 +66.42

10.06 8.79 +1.055 (2)
8.77 +1.08 R

1922.25-94 2.27 40.40 9-1.2

1958.15 140 3.40 3.8

1.31

R.A. : 1.000
DEC. : 71.400
PM. R.A. : 5436.000
PM. DEC. : -422.000
DISTANCE : -0.500
MODULUS : 8
RAD. VEL. : 0.000

q1 (U) : 0.826
q2 (U) : -0.121
q3 (U) : 0.551
dU : 7028.296
U : 55.828

q1 (V) : -0.563
q2 (V) : -0.103
q3 (V) : 0.820
dV : % -4416.83
V : -35.084

q1 (W) : 0.043
q2 (W) : 0.987
q3 (W) : 0.153
dW : % -1624.76
W : -12.906

+160120

1 06.0

+16 59

dir 6

-36-2 (12)

CC82

10.6

run

W654

Y1231

-43 -51 -17 .050

-09 -61
Li
As

run

43511 (12)

G772-23

01 32.4 +31 32

481-008

9971 9977 / 480

3209 -0625 / 024

12.2

0528

1.84

G-72-23

1 3714 431 32

6487 91

481 -008

1351

1.57

12.33

11.29

11.10

11.34

189

9.95

9971

9977

480

028

321

-0675

423

0528

184

21

10607 | 35.8 - 67 55 60 II

Y 363.2

8.31 + 0.58 - 0.12 (2)

MLF) 21/101

8.16 + 0.225 (4)

$\frac{2.16}{7.99} = .016$
 $\frac{3.99}{3.99}$

$\Delta(B-v) = +0.07$

$\Delta(n-Q) = +0.32$

-5 Y (12)

+17 C (8)

$\sqrt{5}$ →

Haha → probably not

L1159-16

1 5-20~~5~~ +12 50

G-3-33

12.30 +1.80 +1.38 0.211 ~1.77

10.48 +1.38 1,2 12 +10.95

+1.064 - 1.785

~~4.1.0.1.1~~

4.04 p.m.

726 362 553
-633 678 370
260 639 723

3688 - 3.0628
- 3.2074 - 5.7865
13174 - 5.4068

+1.6260
-89468
-40811

+3

-42

-19

CC144 2 03.F +44 57 9.9 dmo H220 24
1150

+240 -410 Ca

F.S. 307

10091

2² 0.8.37
2² 13.3.47.3
+ 6⁰⁹ 22.53

221

4102.1 (9M + 8)

410M (8)

9.07 + 1.17 M

~~116-045~~

1.18 -057
1.7

5² 15⁵
31² 15⁹
21² 7³

9.048 + 7;

ES due -141 -045

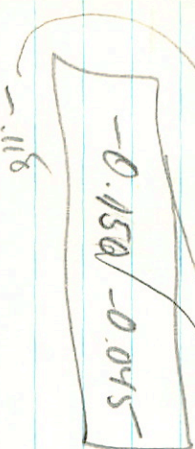
→ Van der

-5079 1 -057

-116 -045 mcr

118 -057

99 (1000 - 9836)
222 (1000 - 6212)
74 (8394 - 3.4)
2.22



-100 20 -057

9.000 8.34 + 0.42 (2)

-119

1000

-9836 1149



0.0028

-642 -021

9991 0244 -7050 -6282 1294 -0260

0340 2.33

(671) Pine 2 10.2 = 238 CFS
 900 7850
 4884 1476

HR650 45
 43
 GC2652 3.67
 3.
 6665
 5.67 + 5.6 + 0.7 3.9
 356.196.402 2.556 B 34.64
 3.59

[m] 250 + 8
 7.24 6.68 + 22 3.9
 GC+

[c1] 331
~~+144 +52~~
 +365
 1.5
 -14 -11
 +02489 -0.645
 515

0294-071
 2.14 + 2.7 - 3.8 + 1.4

+11 -14 +7

364-71

(2.0)

3.52
 3692
 +371 0.64

13.084 431

0.404
-0.853

35.181 - 268 100-

0.139
-1.380

2.925 1.90 3.01

1.064
3.503

3.800
23.119

2.000*
-3.069*

4.311*
-23.000*

-2.000*
19.200*

2.000*
613.000*

20180

225

-2601207

2 12 20 -26 31

1970

15092

9.18 +1.20 +1.10 B

8.50 +0.49 C

80
2.7
1/2

1450
216.25
81146

97946

1234

AD51733

74001

24000

-0045577.8
-0047
13.4
-18 28
-18156.4
-132

After 4538 (2)

GC2723

8.00 + 1.03 + 2.69 = 555 (2) the same

WC254

24.953 1595.3 -15.2788.99 -0645C -18156.4

9232
923
24.12

25.095

+10.15
58.84

41.5

35 3.89
7

103430

14.207
10.642
24.842

3.89
-72

901
921

4.07
+23
4.3

41.64
-5.80

7566
378
43.9

56.624
25.276
24.9

4.00
24.930
-195

144.36

24.9
131.9
18.9

52.63
41.9
4.12
-20/4.90

550 835 -317 948 -064 -181 +5.3 057 -2 -8.5 ✓

035 -031 -053 048 -062 -398 +5.0 +4 +3 061

+3 -4 -15

-11	-8	-10
-----	----	-----

14039 2 14.9 +56 20 8.6 dir 0 +3.27 3w
 +0409 + 9.5 -232.48.0
 +0408 -221

2758

1276 52.222 1905.5 +56.19 57.15 19047

$$\begin{array}{r} -1.820 \\ \hline 50.402 \end{array}$$

(33.1)

$$\begin{array}{r} 10.51 \\ \hline 7.66 \end{array}$$

7686
 38.4
 (33.7)

51.38
 29

2.1 1925.8
 (33.7)

$$\begin{array}{r} 409 \\ \hline 505 \\ 515 \\ 52 \\ \hline 1152 \end{array}$$

52.132

$$\begin{array}{r} 11.3 \\ \hline 130 \end{array}$$

$$\begin{array}{r} -36 \\ \hline 096 \end{array}$$

58.57 1947.06

$$\begin{array}{r} -14 \\ \hline 19 \end{array}$$

58.3
~~1947.06~~

$$\begin{array}{r} 2.05 \\ \hline 3.64 \\ 3.91 \\ \hline 0.21 \\ \hline 7.45 \end{array}$$

-540487

2 15.7 -54 14

LFT 203

475.1

1.49 + 1.39 + 0.59 0.064 0.81 441 - 6 0
10.46 + 0.75 1, 1 7 + 9.3 + 25 - 4 0

} ?

+47 +.35

688	922	-023	1.5327	1.3005	2.8332	+41
-648	507	-509	-1.4434	1.0213	-4223	-6
325	-398	-855	9240	-7169	+6071	0

-540487 2 15.8 -54 13

475.1

Buq (17)

NO

11.49+139 +0.99

10.46 +0.75 1,1

+0.47 +0.35

688	721	-673	+1.5327	+1.2986	2.8313	+41
-648	567	-509	-1.4436	+1.0213	-4233	-6
328	-348	-858	+1.7240	-7169	+ .0071	0

+31 434

2 20.1

+31 36

393

2 25.7

+32 1.57

+31 ~~44~~ VV

9.35
10.1

3.16
2.6
2.9

84 1
1200 2
2000

+0.455 +0.104

McC-AC +0.455 +0.104

9.4 MOP +8.2

13.0
11.5
2.9

WOR 2

13.0
11.5
10.4
11.9
11.9
11.9

0.21 = 0.2

1959.72 105 0.26 5 WOR

1960.84 115 0.15 4 WOR

393.000*

2.000*

25.700*

32.000*

2.000*

0.445*

0.115*

2.900*

38.019

~~13.000~~

-11.5

1.455

0.741

46.80

~~45.695~~

-1.075

0.504

46.60

~~47.415~~

1.214

-0.443

52.56

~~51.898~~

0857

0594

1175

16.83

+8.6

+11.0

-18.4

-23.9

+20.7

+16.8

24.5
30.2

12.6

$\frac{7}{2289}$

151	07	051
139	01	681
148	16	841
148	(12)	121

15967

02 26.7

20

12

4303

434 236

610

442

4230

188

1285

4303

853

02 257 +82 02

+310434

9.58 +136 +1.22①

+064①

+0.455 +0.105 ML-AL

-18.0

R.A. : 2.450
DEC. : -20.200
PM. R.A. : 692.000
PM. DEC. : 230.000
DISTANCE : 1.850
MODULUS : 23
AD. VEL. : 30.300

q1 (U) : 0.659
q2 (U) : 0.653
q3 (U) : 0.373
dU : 2740.815
U : 75.568

q1 (V) : -0.656
q2 (V) : 0.742
q3 (V) : -0.139
dV : % -1209.294
V : -32.574

q1 (W) : 0.368
q2 (W) : 0.153
q3 (W) : -0.917
dW : 1300.068
W : 2.400

16157 2 32.5 -44 01 N7E

(equal) 400

M(I) T(100)

7522

8.80 +1.36 +1.055 (4)

+25
7.14
7.5
083

7.50 ~~4.8~~ +0.76 (10)

7.40
7.40
7.40

.072 ←

83C(7)

7.01

$\Delta(B-A) = +0.065$

21 V W

$\Delta(B-A) + 0.16$

-6.2 -31.1 -323

-8 -11 +4

+41.9 +0.061 -0.240

W 4/630 110

16157 2 32.5 -44 01

GL2097

410295 CPD

Get away 9.70 away +1.35

CEKE

Sp. B. wpt
n = 41.9

-440775

+0053 -290

~~Spring~~

D -8 -11 44

7522

+...2 + 3
+0055 -267 = 1.5 Ju.0 -33.0 -32.4

+057 -305 -GL

~~43 43 22 10 10~~

D.4

+068 -271 wpt

-4 -33 -26 .07

11067

+0047 -301 C.M. 151-301

174860

-2 27 27

+0055 -297 GL+

+0051 -295

+055 -

+058 -295

93 212 GL

13

(81)

+0053 = 13.0
+0053

28,124
- 254

170

-44
-305 = 13.0
-289
0 39.07 1403.6
+14.15
24.92

28445
- 27

46

296

39.96 1955.89
- 9

40.05

15.13

115.7

+0108 = 106
+0106

+062 = 8.3
+056

16591 2

36.3

-42 07

110E + 485.5 = 0.8
C175

3173

7.25 + 94

15.912

1500.6

-42 7

13.25

18973

Quilts

-539
378

-3.27

0120 052

17.888
57.810
13.697
630
661

12.0

16.5 = 2

44.71 142844

8511
42.6

134052

1645
822
444

45.3

14.31
14.68
14.99
14.13
14.86 + 2.52
799
14.00

15548

14
981

955
307

8813
143
017

13.14 1556.17
+1
13.13

804

2 40.7

+ 3

~~32~~

A34

Let

11970

Land

6097 2181

22416

2099 218

2094 250

(F)

1201

10301

15177

LSL 2181

299 218

9446

2878

2056

419

1809

12

18.7

1.70

6559

24480

11.85

R.A.	:	2.650
DEC.	:	2.550
. R.A.	:	0.000
. DEC.	:	0.000
STANCE	:	0.000
ODULUS	:	10
. VEL.	:	0.000
q1 (U)	:	0.628
q2 (U)	:	0.456
q3 (U)	:	0.630
dU	:	0.000
U	:	0.000
q1 (V)	:	-0.661
q2 (V)	:	0.740
q3 (V)	:	0.124
dV	:	0.000
V	:	0.000
1 (W)	:	0.410
2 (W)	:	0.495
3 (W)	:	-0.766
dW	:	0.000
W	:	0.000

Observer:

1

-32.498

STAR

MAGN

ME

-0.894

0.413

-30.782

-0.439

-1.032

-7.395

0.089

-0.927

41.900

12.023

0.400*

-0.301*

0.051*

-1.000*

-44.000*

32.500*

2.000*

16157.000*

Comments:

A052450

16970 2 40.7 +03 02 3.6 Adj -5.16

1535

3" C.S

Plot

(104)

8
-10467 -1138 W3 -0 347 012- 1123 9892880

-01475 1184

1.12

$m_v = 1.10$
and 2.39

-1160

-1144-1147

-1.0

2040
0271
+2.4
0536
1.35

9966 -7775
-0884 -1159

2040
0977
424
0839

2.66
+3
-144
-147
1.35
-1.0

	2.660
	0.800
	-144.000
#12	-147.800
	1.350
#2	1.800
	-1.800
	0.627
#14	0.451
	0.636
	-141.263
	14.439
	-0.662
	0.739
	0.128
	-62.923
	-1.313
	0.412
	0.501
	-0.751
	-62.723
	-10.965

862