

3461 ✓ 08 43 25 18 14 406 120711

223 02 64 12^m 46 4

344-065 1235 -404 (H) 15248(30)

341-100 1245 -453 15425 12 4

342-058 1222 -437 (H) 127m 51 (3)

342-074 1234 -455 (3)

342 1600

the 373 211
346 373

11111111

(H)



Again
34774
24775

34774 $\sqrt{0.5}$ 20 +28 51 661 A3731
24775 $\sqrt{0.5}$ 20

3499 -127 1142 -493 15 Apr 25 16" 3.59+335(A)

409 -96 1130 -460 2 Apr 25 24" 0"

397 -148 1173 -477 19 Apr 25 16" X=245 -13
402 -134 1148 -460 -0.10

583 407 449

579 333

657 -664 910 +121 2.377 25 Dec 29 60" N, -1.35

659 -670 912 +209 2.386 12 Dec 29 40"

663 -646 899 +188

2 Apr 25 6.55

446 172 1064 244

Ey 1017

41.5

→ 0.00 105 1014 2.916

+385 A

337

6D

99h

220

18h

heh

573

544

533

534

~~Do not~~
~~scribble~~
p. 9

670

88

3477 ✓ ✓ 08 43 35 -42 34 405 + 87

10^m 42^m cont

4.09 - 180 1033 - 436 30 Apr 78
4.05 - 184 1033 - 430 29 " " 24^m
4.07 - 182 1033 - 433 (2)

3.75 10350's
3.72 210 Cmp

3428 ✓ 08 44 50 -01 58 5.64 + 1.10

✓

5.70 -55 1258 -475 25man 75 076

55 55 1257 -471 2.6 " 760

55 55 1258 1257

21

872 840

524 335 140 77

5.81 + 354 17man 75

5.29 + 365

527 - 40.338 9 June 71

527 + 40354 7 June 71

526 + 40346

(195) ✓

(21)

752 - 40323 9 June 71

743 - 40405 15 June 71

→

3484 ✓ 08 45 15 - 13 25 431 + 090

13th 22nd "

4.34 - 158 1050 - 443 15 Apr 55 " 16 "
4.33 - 170 021 - 840 19 " " 19 "
4.34 - 164 491 - 1049 444

24c 318 618 1360 1360
318 1360 1360
318

3491 ✓
7544 ✓ 8 43 45 -68 09 60 103 II

6.33 +191 1511 -485 29 2880
~~6.33~~³³ +187 1510 -485 2 2250 547
6.30 +189 1510 -486 537
6.33 8.53

4112 ✓

7.95 +0.547 12080
7.56 +0.532 14148
7.86 +0.542

✓
3493 08 46 55 -06 28 6.08 +1.28

6.09 +54 1355 -490 25man 75
6.10 75 1400 509 26 "
6.09 75 1398 -500
5cc
779

R
5.59 444 13man 74
LC 1000 141 55 15

5.57 444 17man 75
5.55 4450
1111 ✓
5.73 +0.934
535
+10
1000

(RF) ✓

5-28-77 Du-0

76.8 -46.25
46 370 40

3497 8 76 36 41 38 638 757

376 95289 6.24 300 191 405 26.5

88 585 268 50

6-24 340 202 388 2.607 23 Mar 71

6.33 346 181 398 2.629 9 Apr

6.33 382 202 379 2.614 23 Jun 73

195 388 2617

609 +0.18 136.28 63 3341 895 -406 2.153 4 Feb 73

6.29 +0.185 21 Mar 76 369 636 638 -325 894 -393 13 Mar 77

6.07 +0.215 17 Mar 76 636 -338 986 -402 16 Mar 76

105 +0.19 3 637 -331 992 -391

5255L

the length of

3510 7 49 89 115 265 6.5 6.5 6.5

6.36 307 939 437 2.185 18mm 82 0-5.5

6.36 -312 919 -425 2 Jan 77
6.32 -307 914 -425 6 11"

6.325 -309 924 429 (3) 2.138 7.52 +0.264 13
6.12 +0.225 3.277

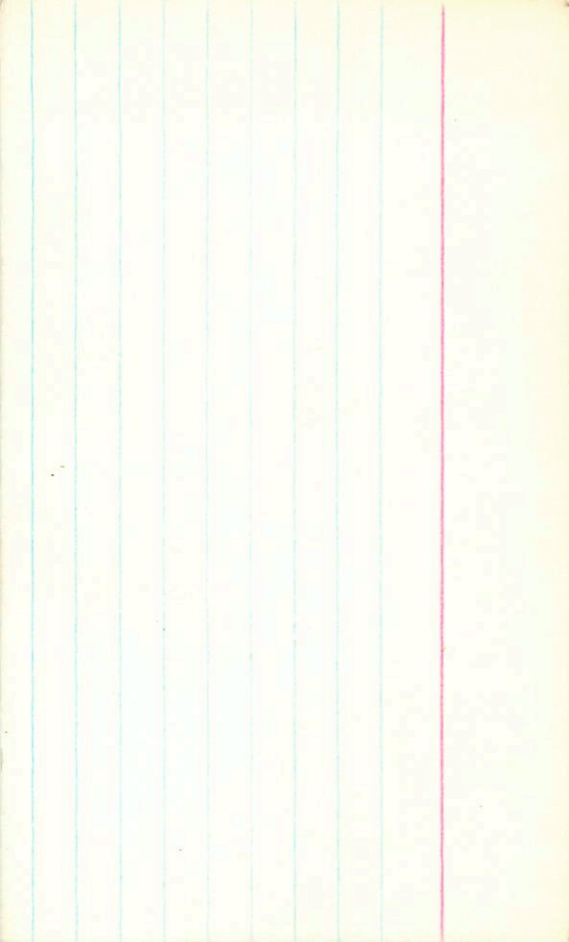
6.34 848 198 485 1612

4.42
105

~~4.42~~

~~4.42~~

583
55



3518 ✓ 8 44 35 -27 37 402 + 1.27

4.06 + 50 1364 - 467 15 Apr 25 16"
4.02 + 54 1370 - 467 17 Apr 25 16"
4.04 + 53 1370 = 467

~~7.74 601 442 + 135 + 0.5~~

790 602 442

✓ (40) ✓
✓ (40) ✓
✓ (40) ✓
LRF
SMHAR DEN

Integral

3513 ✓✓ 8 49 05 -29 22 5.98567

RR

(348)

5.98 124 1028 -488 25 m 7F

5.19 130 1033 -465 26 "

5.98 130 1030 -462

588

[280 + 400] 680

[2.28 + 400] 348

5.42 335 -326

5.40 334

(R) (X) (X)

5.47 +1348 17 m 7F

5.45 +0.355 18 m 7F

5.46 +348

5.54 206
5.57 1357
5.58 4158

Hydrus. Mill. P. 10

107 100

8522

2062

8

105

198

22

222
222
222

222

5.52-193

1110

-453

22mover

5.51-195

1114

-442

17mover

(589-202)

(1163)

-477

12mover

5.51-191

1107

-472

17mover

5.55-191

1103

-456

5.51

5.52-191

1108

-450

5.67

5.52-191

1104

-460

5.67

(585 515)

567

567

567

567

48

558

222

222

222

222

222

11mover

17mover

12mover

17mover

12mover

55 mc B 8 49.7 +28 30 1950
G-47-9

85" 1250

13.15 +1.64 +1.14 1 Jan 42
13.15 +1.66 +1.27 2 Jan 42

5.97 +0.87 +0.63 3 20"

7.92 +304 2820 51 → 5.54 236
7.94 +335 52102 5.57 257 265
5.55 246 → 253

55 line B 8 99.7 + 28 30 1850

G-47-4

10.1

9.45

13.28 11.48 + 1.30 10.46 43 1000

10.1

13.10 11.53 + 1.30 11 " " "

10.45

12.99 11.55 + 1.29 15 " " "

10.11

1.62

11.52
10.20
11.1.298

11.52 + 1.25

0.22

11.14

1.45

10.20
9.40
9.46
9.65
9.8

9.9

9.46 13.15 + 1.65 + 1.19 (2)

11.10 9.1

10.22

3529 ✓ ✓ 8 51 28 -13 08 6.25 120

6.13 -37 1294 -467 18210

6.12 -29 1288 -470 25m 78

6.13 -28 (1278 -454) 26

5.56 357

6.12 -32 1290 -468 (3)

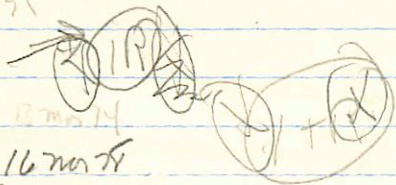
695

2

5.65 +395 13m 14

5.63 +381 16m 78

5.64 +388



[7.96 +0423] 19m 23

[7.43 +0409] 8m 23

5.64 +036 [15213]

3533

8 51 40 -32 26 6.45 1.46

$$\textcircled{A} \quad \begin{array}{r} 6.48 \\ +167 \\ \hline 1468 \end{array} \quad \begin{array}{r} -493 \\ \hline 4275 \end{array}$$

$$\textcircled{2} \quad \begin{array}{r} 6.55 \\ +160 \\ \hline 1471 \end{array} \quad \begin{array}{r} -487 \\ \hline 232887 \end{array}$$

$$\begin{array}{r} 6.50 \\ +164 \\ \hline 1455 \end{array} \quad \begin{array}{r} -460 \\ \hline 71148186 \end{array}$$

$$\textcircled{1} \quad \begin{array}{r} 6.51 \\ +163 \\ \hline 1470 \end{array} \quad \begin{array}{r} -485 \\ \hline \textcircled{2} \end{array}$$

(A)

(RT)

$$\begin{array}{r} 7.08 \\ +0.50 \\ \hline 8.08 \end{array} \quad \begin{array}{r} 10 \text{ MAR } 57 \end{array}$$

$$\begin{array}{r} 8.08 \\ +0.49 \\ \hline 8.57 \end{array} \quad \begin{array}{r} 11'' \end{array}$$

$$\begin{array}{r} 8.57 \\ +0.50 \\ \hline 9.07 \end{array}$$

7.151 → 9 more than 100 ~~6218~~

203

3534 53 06 -5 22 599 +65

6.04 307 947 -465 2.131 31 Jan 77

6.05 277 916 -448 18 Mar 77

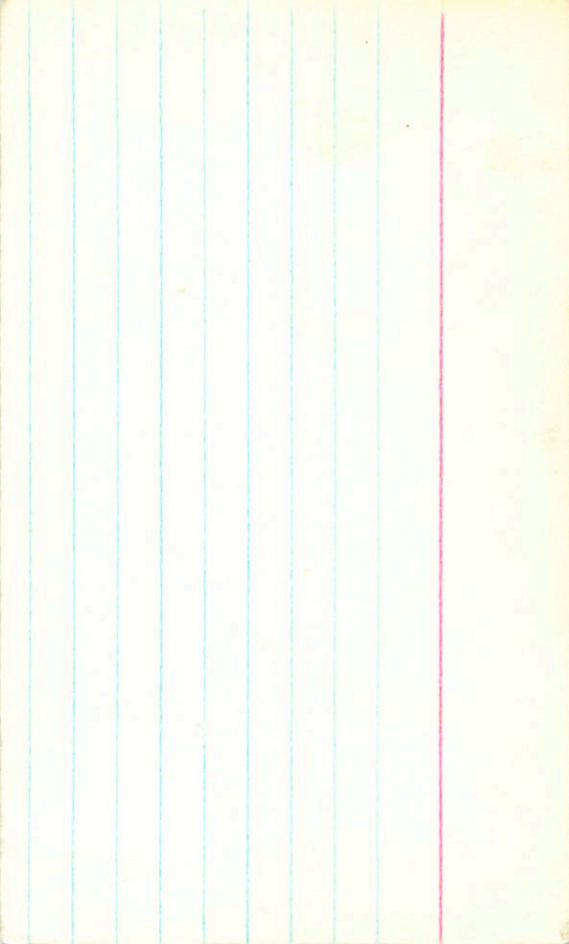
6.00 308 947 -440 6 Jan 77

6.02 308 926 -436 9 " 77 +021
5.82 + 0.205 (3)

6.00 401 (216) 418 1614 (5.64) 70209 6min

409 197 474 1642
411 166 443 1637

6.00 410 182 439 1640 (2) 157 371 20581
411 237 411 20581 SK



3540 ✓ 8 54 20 +28 02 515 88II-II

RR

5.29	-100	1146	-487	2 Apr 78	24"
5.17	-135	1145	-485	18 Apr 79	16"
<u>5.00</u>	<u>-118</u>	<u>1148</u>	<u>-486</u>		

4.92	+0.350	17 Mar 78
4.95	+0.362	18 Mar 78
<u>4.94</u>	<u>+0.356</u>	

3543 8 46 40 -79 25 575 122

(2) (X) (e)

$$\begin{array}{r} 577 + 255 = 832 \\ 832 + 664 = 1496 \\ 1496 - 446 = 1050 \\ \hline 1050 + 664 = 1714 \\ \hline 1714 - 446 = 1268 \end{array}$$

(X) (X)

15 14

$$\begin{array}{r} 7.21 \\ 57.14 \\ \hline 64.35 \end{array}$$

7.20

3548 ✓ 8 53 00 -40 21 646 ROTAS

mmw (V)

6.45	-95	1056	-619	7 Apr 78	24"
6.46	-114	1070	-623	8 Mar 78	(34)
<u>6.46</u>	<u>-105</u>	<u>1063</u>	<u>-621</u>		(2)

RR

6.06	+365	13 Mar 74
5.54	+338	17 Mar 78
5.93	+329	21 Jun 79

3550 ✓
 8 54 40 +11 42 5.56 gms
 546 +171 1568 -630 10 Apr 39
 548 +183 1562 -663 2 Apr 75
 545 +141 1601 -655 19 Apr 76
 546 +176 1565 -650 (3)

476 +52 6 Mar 74
 472 +53 15 Apr 74

✓ R

482 - 40.469 23 Jan 70
 [2.09 + 0.450] 14 Apr 71
 476 476

3554 ✓
5.78 + 79 5431 10 - 75 08 5.90 110

5.76 + 78 1434 - 462 16240
28 2680

5.74 + 78 1418 - 464 25mm 28

5.76 + 78 1432 - 462 ③ 7.11 + 258 1458 - 463
16783

mm

2.50 + 0.509 15243
2.43 + 0.437 15071

RV ✓
①

R

5.10 + 475 6mm 24
5.12 + 451 16mm 28
5.11 + 0.463

5.12 444 Y
5.11 445

3557 ✓ ✓ 8 55 25 +04 19 6.13 +1.00

7644

6.15 -111 1163 -483 19 Apr 80

6.15 -104 (1149) -510 8 May 78

6.13 -127 1164 -482 19 Apr 80

6.14 -114 1162 -483 (3)

2267 604 414 426
595 308

R
5.73 +35 15 Apr 77
5.74 +328 18 Nov 78
5.75 +338

(1Rx) → (335) → 824
826

8.04 +0.324 7 Dec 80

3558 ✓ 5 55 50 +17 14 6.16 N III

6.16 -92 1176 -452 11 Dec 79

Regr 6.19 -85 1166 -451 2 Apr 75 24'

6.14 ~~-124~~ 1158 -474 19 Apr 75

6.17 -90 1170 -452 (2)

(R) (X)

5.81 +345 6 Mar 74

5.77 +35 15 Apr 74

R

5.75 +0.305 23 Jun 70

5.87 +0.315 15 Apr 73

5.81 +0.310 (2)

3564

~~3654~~

✓✓

8 55 30 -16 36 6.15-120

5.95 + 1.58 + 1.79

5.54 + 229 1530-490 25 min ✓

5.95 + 226 1527-507 26 "

5.95 + 227 1528-538

R

5.08 + 615 6 min 74

~~5.14 + 581 16 min 78~~

5.11 + 598

IRI

✓

5.14 + 0.581 16 min 75
11.50 + 1.16 min 81

7.44 + 0.562 9 min 81

5.14 + 0.577 9 min 81

5.14 + 0.576

3512 ✓✓ 8 48 55 -32 41 520+87

-48 RR
.02
277

5.21 -170 1036 -405 4 Apr 28
5.22 -183 1034 -402 17 Apr 28 16"
5.22 -176 1034 -404

539 300 507 [2.17 + 345] 13 Apr 28
[2.17 + 344] 32883

[462] [359] 191



4.79 200
4.74 200 } 3W

0.40

ASAT +040

R(42)

266

4.86 +296 17 Mar 28
4.84 +1312 18 Mar 28
4.85 +301 310



3547 ✓ 8 54 15 +6 03 3.12 +1.00

3.11 -125 1181 -485 19 Apr 28 16"

3.12 -115 1187 521 (A) 1524 97 (30)

3.18 -120 1184 -489 (A) 12 Mar 91 "

3.11 -121 1184 -498 (3)

1659 557 489 410

2262 613 291

1491 596 434 410

2262 613 291

2.70 342

342 300 1300

2.70 + 337 600

76932 also (1R) 5.81 855 5.82+0.51 007²⁵

3577 8 57 32 -16 03
125 291 2.595

163 22 137 24 367 172 274 2565 0
5.81 355 125 291 2595 0-0

5.82 -325 813 -520 18mm77

5.87 -358 (853) -550 11mm77

5.83 -341 819 -524 10mm77

25 June 2
5.74 +0.225

5.84 -342 837 -543 9 "

5.67 +0.19 27 June

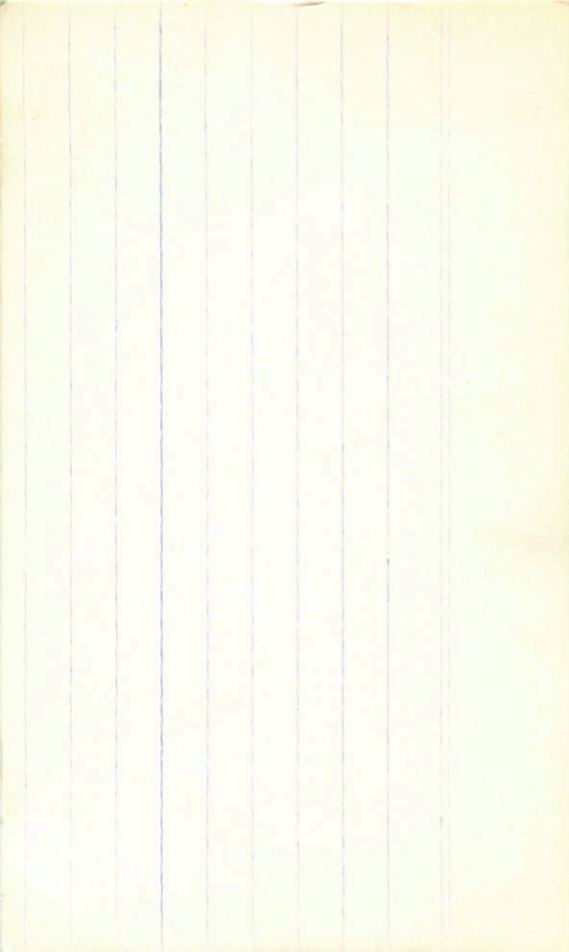
5.84 -341 ~~841~~ -534 (4)

5.76 +0.235 10mm77

823 159 366 102 303 2.595

5.75 +0.23 (2)

1096 213



3567 $\sqrt{\sqrt{8}}$ 56 30 + 9 28 618 + 99

6.18 -119 1163 -490 29 Mar 82⁴⁰

6.21 -103 1150 -471 4 Apr 82 24"

6.17 -128 1166 -455 19 Apr 82

6.18 -124 1165 -492 5.74 2.95

5.72 285

↗

①②

R

5.81 +32 15 Apr 82

5.85 +334 18 Mar 82

5.83 +329

②③

[8.12 +0.295] 14 Apr 82

[8.09 +0.363] 5 Apr 82²⁰

[8.17 +0.356] 20 Apr 82

FI. 04/1/89

372020
3583 ✓ 8 57 10 45 29 585
585

RR

590 88 220 885-532 14 July 50

585 576 1208 513 27 May 74
540 045 80 08 021 3021 3021 27
590 88 220 885-532 14 July 50

590 88 220 885-532 14 July 50

see more

140 322

278 + 387 + 13 Jan
540 + 314
535 + 270
534 + 215

5.72 10.34 18 May 75
5.05 40.31 6 21 Jan 79

~~3584~~ ✓ ✓ 59 40 -19 07 626 P8

RR

6.18	-415	987	-38	2.183	4 Jan 80
6.15	-428	878	-408	2.184	5 " "
6.16	-422	880	-395	2.184	

291 155 11 207

(2)

6.07	+0.132	157m 78
6.12	+1.141	177m 78
6.10	-0.000	

3585 ✓ 8 58 20 -29 43 6.24. +1.01

① R.R

6.26 -116 1162 = 499 29 21 80
6.25 -93 ① 1121 -435 25 Mar 75

6.26 -116 ① 1241 -423 26 " "
6.27 -119 1163 -458 5 May 86

6.25 -120 1170 -480 15 Mar 36
6.25 -114 1165 -462 ③

8.17 + 321 17 Mar 75
5.82 + 320 18 Mar 75
5.84 + 324

3774B

6.57-669 910 +121 2.377 25000 79 60"

6.59-670 912 +709 2.386 12000 74 40"

6.57-667 908 +126 2.389 62190 60"

~~6.58-668 909 +119 2.389~~ ③

~~017 188 1043 2509~~

~~Ey + 009~~

~~6.6.5~~
~~m, 1.35~~

2.55

5.2

690

951