

2277 06 20 05 +17 47 6.31969

✓

R R

6.30-48

1311-752-30477

6.31-78

1324-761 31"

6.30-73 1316-756

647

5.43

+0.323 3218

5.45

+0.336 50477

(R)

5.43

+0.322 4477

5.44

+325

③

335

227 06 17 20 -52 44 6.40 + 1.46

6.37 + 1.52 + 1.57 ①

RR

641 + 173 (1424) 226 26 d r s  
 640 + 170 1962 - 593 22 d r 77  
 641 + 156 1475 - 576 25 "

(X)

1440 756 1461 1466 1467 1468

5.60 + 5.37 22 m 77

5.56 + 5.5 + 2.5.5

5.55 + 5.35 4 p 28

5.80 + 5.67 ②

640 + 164 1466 1467 1468

443022

2281

06 18 15

-30 21 203 + 0.53

→

20

6258

F8 II

WR R

495  
203 - 232  
204 - 215

294  
1036  
1036  
-293  
-27  
27

205 - 220  
209 - 224

1024 - 223  
1034 - 288

26 X (S)

442  
495

2.136 29mmFD

2.151 30"

2023

1954

2.144 (2)

6.59 + 0.257 2 Jan 25

6.61 + 0.2604

6.60 + 0.258

265

2296 06 21 15 -33 25 384 +0.87

✓

3.86 -190 1026 -417 269277

3.86 -185 1030 -427 27"

3.86 -184 1028 -422

Am

527 291 458  
(283)

010

3.7  
+0.9

216 (444)

348

316

2.2 +0.40

351

325 1000

2283 06 15 30 -71 42 6.63 +0.76

✓ R R

$$\begin{array}{r} 6.63 - 346 \ 871 - 484 \ 25 \ 50 \ 57 \\ 6.62 - 345 \ 883 - 497 \ 26 \ 11 \ 7 \\ \hline 6.62 - 346 \ 877 - 490 \end{array}$$

361 157

$$\begin{array}{r} 6.36 + 0.189 \ 50 \ 27 \\ 6.40 + 0.189 \ 17 \ 20 \ 25 \\ \hline 6.35 + 0.189 \end{array}$$

0.546

335 60

6.61 364 154

(RI) sho 6.35 + 185 1st sh 6.62 + 66 + 185 (3)

2290 44594 6 19 28 -48 43

(+) 664 303 933 -457 2153 26215

665 -288 945 -439 137076

660 -307 921 -432 10 Apr 77

661 -305 924 -441 9 "

662 -305 931 -442 (3)  
2153 (4)

6.35 + 0.19 (1) 1st sh

6.38 + 0.20 12 Apr 77

6.36 + 0.195 (2)

~~(A) (B)~~

6.61 403 220 365 21605 (6)

1/2

2302 ✓ 06 23 35

6.39 + 10.6 + 0.84  
+ 11.05 6.24 6.97

R  
634 88  
6.35 98  
6.35 98  
6.35 98

1201 482 6.40  
1188 435 3.1 den 77  
1191 463 3.1 den 77  
1193 483 ③

5.90 + 0.40 2.80

5.97 + 0.3574 5.6126

5.95 + 0.348 3.7143

5.96 + 0.357 ②

QPR



2305 06 23 05 -11 31 5.22+124

✓ R

5.22+1235+121 ②

5.22 +17 1314 -469 26.667

5.22 +17 1314 -469 27

5.22 +17 1314 -469 27

4.53 +0.5 18.76

4.67 +0.47 2.17

4.67 +0.5 3.17

4.68 +0.5 3.17

4.66 +0.2 1.96

① R

2307, 06 22 25 -31 4/6 6.34 + 0.79

✓ RR 6.33 + 0.50 + 0.565 (D)

6.36 - 173 1062 - 462 = 26745

6.33 - 171 1055 - 454 = 26.8677

6.34 - 176 1064 - 447 = 27 "

6.34 - 173 1060 - 454 (B)

5.75 71250 24.75

5.52 71251 4 (11.1)

5.50 71250

45067

92

2313 786 24 00 -00 55 5.86 +56

5.89 -371<sup>44</sup> 888 -426 10 Apr 77

5.89 361<sup>44</sup> 989 -435 2 Jan 77

5.87 -334 (859) -415 6 "

5.85 -352 882 -416 9 Apr 77

5.88 -354 986 -423 (4)

6.74 ✓ +0.195 12 Jun 77

350 150 (187) 1454

5.70 +0.19 24 Jun 77

5.88 345 163 475 1447 (0.195) <sup>Cyber</sup>

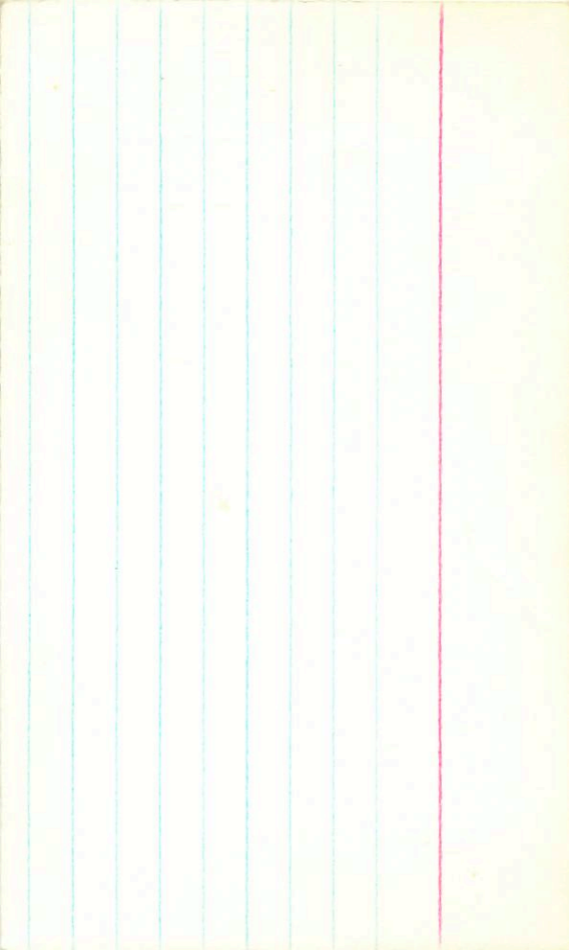
(5.66 +0.225 2 Jan 77)

373 135 496 1461

5.76 +0.205 12 Apr 77

7 Jun 116 395 2168 00

5.93 +0.20 (3)



2316A 06 23 15 -36 41 5.61 +1.03

✓ ROR 9.2 13"

5.63 +1.055 +0.12①

5.63 708 1148 -434 2640.77

5.64 -105 1151 -432 27"

5.64 -106 1150 -433 2258 +0.884 1.24 23

5.20 332

5.15

+1.324 2.475

5.27

+0.333 1.540.75

5.20

+0.328

①②

2317 06 24 40 -03-52-6.36+102

✓ RR  
6.35 - 99' 1143 - 544 26788  
6.34 - 93 1168 - 512 - 264800

6.34 - 102 1169 - 504 - 27'

(X)

~~6.33~~ - 107 1197 - 525 (A) 17moss

6.34 - 100 1177 - 520 (A)

• 5.52 - 13263 Jun 25

5.52 - 13242 Jun 25

5.52 - 13247

43154

2215 6 22 45 -28 46 6.24.69

1.36 221 931 -506 2.134 6/Jan 83

6.40 -317 914 -405 2 Jan 57

6.40 -542 ~~888~~ -962 6/11

6.38 -348 ~~986~~ -495 2.134 (2)

6.40 1104 173 441 1548 (5)

|      |       |                   |    |
|------|-------|-------------------|----|
| 6.11 | 11.07 | +0.195 29/Jan     | 76 |
| 6.07 | 6.07  | +0.2153 31/Jan 77 |    |
| 6.09 | 6.09  | <u>+0.205 (2)</u> |    |

(\*) 248

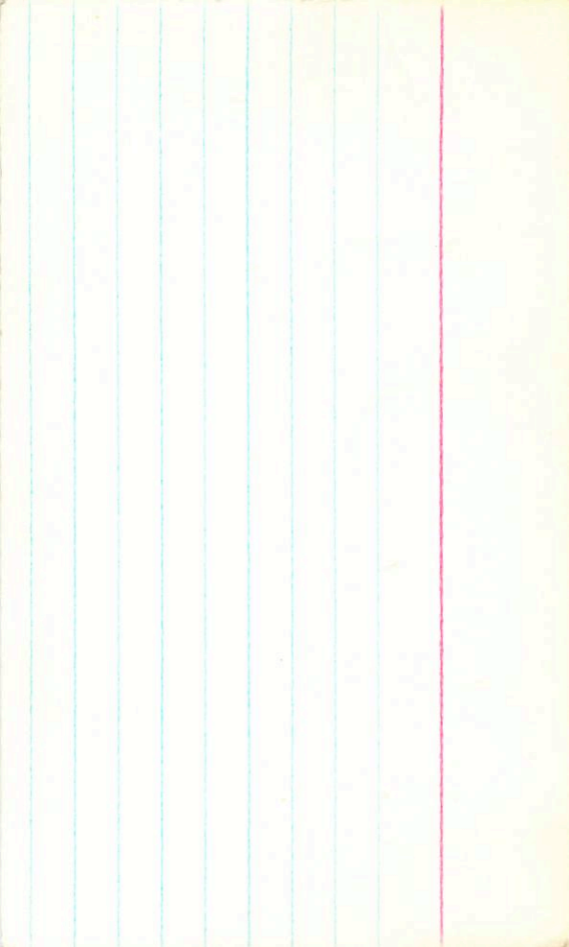
337

207 207 2597 60

438 438

(1) 01m'e 2.134 (1)

137





2322 06 23 05 -52 10 5-97 +1.03

✓RR

5.56 + 105 + 0.73 (1)

5.57 - 85 1141 - 428 27 Dec 77

5.58 - 98 1159 - 439 24 "

5.58 - 92 1150 - 434

627

5.41 + 1331 3 part

5.50 + 1343 1 part

5.45 + 1337

2329 06 24 40 -35 02 6.24+136

✓

6.27 +99 15051 512-26285

6.24 ~~15051~~ 0544 825-528 26287

6.25 ~~15051~~ 1518 8151 537 27

6.25 8051 15051 537 27

(10<sup>14</sup> 10<sup>11</sup>)

⊗

5.14 40.445 26287  
5.12 40.436 22  
5.13 40.440 2

194 RR

2334 ✓ 06 26 05 +00 19 5.19 +1.18

fresh ✓

R

5.20 - 4 1824 - 566 201117

5.21  $\frac{11}{8}$  1381 - 574 31''

5.20  $\frac{120}{1328}$  570 466 + 0.395 (35th)

5st

2154

4.75 + 1.368 46675

716 567 336

7204 + 0.34 9/14/87

2337 743 190

210 348

2337 743 190 + 380 60000

4.74 1381 1381

5th

2233

06 26 10 +02 56 5.54+1.04

VV

R

|             |             |             |             |           |
|-------------|-------------|-------------|-------------|-----------|
| 5.55        | -94         | 1160        | -420        | 30 Apr 77 |
| 5.56        | -107        | 1175        | -425        | 31 "      |
| <u>5.56</u> | <u>-100</u> | <u>1168</u> | <u>-422</u> |           |

5.07 +0.36 27 Jan 72

~~5.06 +0.33 31 Jan 72~~~~5.10 +0.344 17 Jan 78~~

① R

② V

R ✓ 5.10 +325  
 5.14 +315  
5.12 +315 → 325

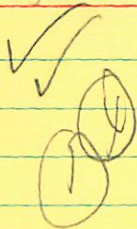
[ 2.45 +0.315 ] 14 Apr 81  
 [ 2.52 +0.370 ] 17 Jan 83

2335

102,65

06 26 05

-00 15 5.54 +1.28



|             |      |             |             |           |
|-------------|------|-------------|-------------|-----------|
| 5.53        | +114 | 1492        | -533        | 6 Jan 73  |
| 5.54        | +114 | 1455        | -531        | 30 Jan 77 |
| 5.54        | +106 | 1474        | -544        | 31 Jan 77 |
| <u>5.54</u> | +114 | <u>1493</u> | <u>-536</u> | (3)       |

IRP R/R

|             |               |           |
|-------------|---------------|-----------|
| 4.92        | +0.457        | 22 Jan 80 |
| 4.87        | +0.462        | 23 "      |
| <u>4.90</u> | <u>+0.460</u> |           |

5.97 + 0.305 = 6.275  
 5.85 + 0.305 = 6.155  
 5.82 + 0.305 = 6.125

5.89 + 0.305 = 6.195  
 5.85 + 0.305 = 6.155  
 5.81 + 0.305 = 6.115

5.71 + 0.305 = 6.015  
 5.70 + 0.305 = 6.005  
 5.67 + 0.305 = 5.975

~~119 = 119~~  
~~119 = 119~~  
~~119 = 119~~

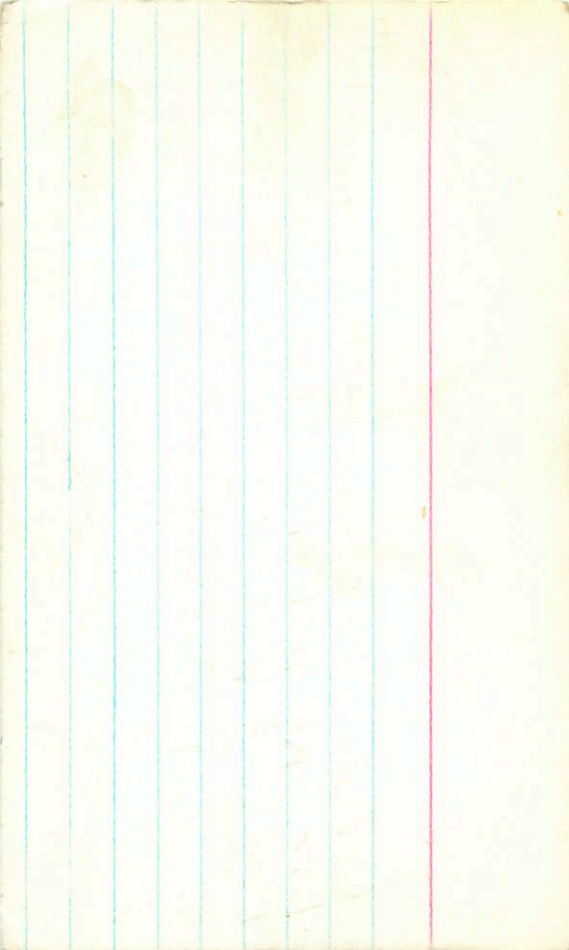
1055 - 450 = 605  
 1053 - 467 = 586  
 1056 - 433 = 623  
 1057 - 450 = 607

1083 - 441 = 642  
 1097 - 449 = 648  
 1106 - 450 = 656  
 1115 - 450 = 665

6.24 + 0.885 = 7.125

① ②

119 = 119



267  
L9C  
250

1702340

6.24-184 1691 691-691 1528  
6.26-180 1066-440 1828  
6.26-184 1083-445 2128  
~~6.25-183 1080-444~~ @  
6.22-161 1053-450 @ 19217

532 341 466



2342 06 27 00 +10 20 45 6.12 H0

✓/ R  
6.16 -22-1324 504 6.16 +1.175 +1.1350  
2.5 mm 24  
6.16 -31 1324 -475 1 Jan 75

6.15 -35 1341 -508 3 (Dec 77)

✓/ 1 mm 24  
6.16 -30 1330 -506 5.22 +0.37 2.4 Jan 75

5.69 +0.38 9 mm 74

5.59 +0.41 13 mm 74

5.70 +0.76

2344 06 26 15 -28 50 6.06 754

✓ RR

6.06 -370 887 -450 26.11.77  
6.06 -366 882 -443 27.11  
6.06 -368 884 -446

2344

0.06 289 180 286

5.87 70.17 23.78

5.87 70.16 74.11

5.87 71.70 23

2354 06 24 15 -63 25 6.45 +0.66

✓ VRR

646 -302 927 -434 27.477

646 -304 924 -447 29°

646 -303 928 -440

406

626 +0.192 -1 Dist

615 -1.82 -4 Dist

619 -2.12 -7 Dist

620 +0.104 ③

(27)

2359 ✓ 06 27 35 -17 27 576 +112 -  
5.76 + 1.14 + 0.54 ①

✓ R

27 Dec 77

5.77 -52 1158 -442 26 Dec 77

5.77 -47 1154 -442 (5.21 + 1.14 132m 24)

5.77 = 50 1197 -442 5.18 + 0.41 52/74

5.24 + 0.40 13 Jan 78

5.21 + 0.40 ②

5.26 387

5.28 393 → 406

①

263 10.44/6 ✓ 395 386

7.58 + 0.38 188/19 April 78 ✓

2366 06 29 50 +16 58 6.06 N2 III

9.28"

✓ R R

6.17 -48 1276 -502

6.18 -44 1281 105  
6.18 217 1278 -502

Small  
1281 105  
1278 -502

5.77 +0.363 4 Jan 78

5.78 +0.363 6 Dec 77

5.72 +0.36 9 Mar 74

5.65 +0.40 13 Mar 74

5.76 +0.363 2

6.07 +1.135 +10.5 ①

2367

06 29 10

-10 04

5.52 + 125

26

✓ R R

8.50 + 116

8.52 + 127

1384

1355

5.52

24

✓ (MWR) ⊕

5.52 + 124

1352

1365

5.52

26

27

✓ (MWR) ⊕

5.53 + 125

1365

1387

5.53

27

27

✓

✓ (R) ⊕

5.52 + 124

1352

1365

5.52

26

27

✓ (R) ⊕

5.52 + 124

1352

1365

5.52

26

27

✓ (R) ⊕

5.52 + 124

1352

1365

5.52

26

27

✓ (R) ⊕

5.52 + 124

1352

1365

5.52

26

27

✓ (R) ⊕

5.52 + 124

1352

1365

5.52

26

27

2366 06 26 40 -57 59 58 57 +1.25

✓ 5.83 + 1.29 + 1.86 (2)

582 + 287 1383 - 416 2424 87 (80)

574 + 45 1385 - 471 27. Dec 77

5.83 + 42 1375 - 448 29"

5.83 + 44 1371 - 468

116  
89

Done!

5.17 + 0.46 7200 74

5.82 + 0.45 8200 79

5.16 + 0.48 8200 78

5.20 + 0.420 (2)

6059 10 5  
003 06 25 40 -69 41 538 +0.92

✓R

5.39 -125 1079 -447 272.77

5.40 -136 1088 -430 29 "  
5.40 -130 1084 -438

Ⓟ

588 373 472

5.26 +0.397 1.218

4.95 +0.326 4.425

4.89 +0.355 2.642

~~1.11~~

4.98 +0.320 2.670

4.89 +0.372 2.772

3.90

4.95 +0.322 2.3

4.90 +0.326 4.425

Ⓟ

323

4.89 +0.340 2



2375 06 31 00 +11 42 602 1001

✓

10<sup>m</sup> 33 " 617

$$\begin{array}{r} 6.07 - 88 \\ \underline{6.08 - 75} \\ 6.09 - 81 \end{array}$$

$$\begin{array}{r} 1295 - 537 \\ \underline{1282 - 525} \\ 1288 - 531 \end{array}$$

$$\begin{array}{r} 168 \\ \underline{165} \\ 143 \end{array}$$

$$\begin{array}{r} 5.70 \\ \underline{5.61} \\ 5.73 \end{array}$$

$$\begin{array}{r} +0.345 \\ \underline{+0.335} \\ +0.228 \end{array}$$

$$\begin{array}{r} 5.70 \\ \underline{5.67} \\ 5.68 \end{array}$$

9.10 + 374 17 Jan 73  
 345  
 5.65 + 337  
 5.73 - 628

5.70 + 330  
 $\underline{5.70}$   
 5.61 + 332

5.68 + 336

④

# 2379 06 30 20 -12 22 5.15 +127  
518 4027+140 (3)

✓✓ R

13 m 15 "

5.16 +42 1412 -505 -26 June 17  
5.16 +42 1411 241 + 91.5  
5.16 +42 1411 241 + 91.5  
5.16 +42 1411 241 + 91.5

461 +1441 + 3/25  
447 +0405 52479

968 643

448 +0405 13779  
452 +0405 13779

312  
450 +0.287 19441

VRP

106 - 11 411  
352 411  
457 411 1574

2387 ✓ 06 30 45 - 08 08 5.42 + 1.35

✓

R 5.44 +101 1439 - 532 - 26 Dec 77  
5.44 +114 1431 - 554 27  
5.44 +106 1438 - 5473  
5.44 +101 1434 - 5473

5.44 +101 1434 + 1444 - 3 Jan 75  
- 543 467 + 0.48 5473

4.78 + 101 8 mm 74  
4.76 + 101 6

Q

2.15 + 101 1438

2.13 + 101 22 15 Apr 81

4.80 4.27 4.47  
4.80 4.27 4.47  
4.84 4.84 4.84  
4.81 4.81 4.81

2392 06 31 05 +04 53 5.84 +0.79

✓ R

$$\begin{array}{r} 5.86 - 119 \quad 1134 - 4 + 53 \quad 11247 \\ \hline 5.86 - 117 \quad 1138 - 4 + 53 \quad 11247 \\ \hline 5.86 - 118 \quad 1136 - 4 + 53 \end{array}$$

✓

5.42 + 0.33 267m75

$$\begin{array}{r} 5.49 + 0.27 \quad 24775 \\ \hline 5.45 + 0.228 \\ \hline 5.45 + 0.318 \end{array}$$

[ 274 + 0.310 ] 1544 19 Apr 5.45

5.46 315

324

2388. 06 30 25 -35 14 5.82 -0.92

✓RR

5.84 -216 1029 -344 26.4077

5.83 -217 1032 -345 27.11

5.84 -214 1030 -346

5.50 26.6

[7.84 +0.26] 14 Apr 78

5.44 +0.276 4 Jan 78

5.52 +0.30 15 Mar 78

5.48 +0.28 ②

R ✓

2389 DL 29 05 -56 50 5.21 +1.09

✓✓ RR

5.20-74 1185 -424 242197 30

5.21-62 1172 -427 272a77

5.20-42 1180 -423 29"

5.20-68 1178 -425 (3)

669

more  
(X)

4.71 +389 177m75

4.70 +1396 18"

4.70 +393

2390 06 30 15 -40 54 6.19 + 1.40

6.20 + 1.42 + 1.60 (3)

✓ R

6.19 + 113 1471 - 523 25 June 77

6.18 + 119 1473 - 541 26 "

6.18 + 116 1479 - 532

5.55 + 0.464 22 June 78

5.43 + 0.462 27 June 78

5.50 + 0.416 (2) (181) (R)

5.43 + 0.462 2 Jan 75

5.42 + 0.412 24 June 74

5.48 + 0.535 16 June 74

2391 06 32 15

+14 10 542 9 12

✓R

$$556 + 1105 + 0.55 \textcircled{1}$$

$$\begin{array}{r} 5.57 \\ 5.56 \\ \hline 5.56 \end{array} - \frac{76}{55} = \frac{07}{60}$$

$$\begin{array}{r} 1255 \\ 1249 \\ \hline 1252 \end{array}$$

$$\begin{array}{r} 1255 \\ 1249 \\ \hline 1252 \end{array} - 467 = 31 \text{ Jun } 77$$

$$- 459 = 1 \text{ Jun } 75$$

$$= \frac{463}{5.09 + 0.39} \textcircled{2}$$

$$5.15 + 0.357 = 4 \text{ Jun } 75$$

$$5.12 + 0.351 = 2 \text{ Jun } 70$$

1957 R

$$5.14 + 0.354 \textcircled{3}$$



2292 06 31 45 -11 09 6.38 Nop

VRR

6.29 -57 1311 -950 26.11.77  
~~6.28 -54 1322 -966 27.4.77~~  
~~6.28 -56 1316 5.87-958~~

+0310 8 Jan 75

BW T

5.86 +0303 2 Jan 75

5.81 70.34 20 Jan 75

5.87 - 70.32 55

5.86 +6.313

665 586 -065

2344 06 3135 -37 40 52.5 + 0.95

✓ R R

5.24 + 1.00 + 0.65 ①

5.26 - 131 1112 - 475 26.46 77

5.25 - 125 5011 524 - 435 27 "

5.25 129 1108 440 4.76 + 0.365 ② 8.12

5.50 364 470 4.80 + 0.328 4 Jan 75

10.11

4.88 4.88 6.88 75

0.345

2400

06 30 45 - 51 48 5.54 to 5.54

✓✓ R R

Ag

5.59 -36 2881 -384 27 down 77

5.60 -370 881 -378 24 "

5.60 -376 881 -381

329

5.58 335 182 460  
341 176 437  
143 534

5.35 +0.168 8 Jan 25

5.40 +0.187 8 Mar 27

5.35 +0.184

2403 06 32 25 -20 54 6.40 +0.83

✓ R R 6.42 +0.82 +0.42-0

6.42 -211 997 -435 2700.57  
1.38 -206 994 -433 30"  
1.40 -208 996 -436

6.03 +0.2872 part  
6.04 +0.2793"  
6.04 +0.283

4 474  
26 203  
506 113  
4 14 511

2407 06 32 25 -38 36 6.44 +1.00

✓ R-R

6.44 117 1152 -474 31 Jan 83

6.45 -123 1143 -461 29 Jan 77

~~6.44 -118 1129 -446 30~~

~~6.44 -120 1147 -467~~ (2)

555

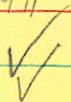
(1A)

6.07 +0.328 15 Mar 75

6.03 +0.322 +7 Mar 75

6.05 +0.326 -

2411



06 33 071 -36 12 5.41 +1.44

108.42

5.42 +126 1527 -52329.77

5.40 +126 1518 -50730 "

5.41 +126 1522 -515

194 RR

4.75 +0.483 22.80

4.75 +0.471 23

4.75 +0.477 23

484

2416 06 32 55 -52 18 6.18 +1.10

✓ R.R

6.22 -67 1182 -455 26 485

6.22 -78 1164 -430 29 467

6.19 -72 1162 -452 30"

6.20 -72 1169 ~~452~~

6.45 -456 B)

(X)

5.71 -1357 17 Mar 5

5.70 -1369 18"

5.70 -1363

2426 06.36 20 +10.52 6.46 120

✓ 6.28 +93 1427 -447 981 Jan 83 5.64 458

6.39 +21 1430 -464 1126 78 40 176

6.38 +46 1421 -458 1 Jan 79 8.07 +514 176

6.35 +94 1426 -456 3

1/11 → (R) ✓ 570 +514 22 Jan 80

5.71 +50 (R) ✓ 570 +514 22 Jan 80

5.74 +49.5 (R) ✓ 570 +514 22 Jan 80

5.70 +46.5 (R) ✓ 570 +514 22 Jan 80

5.72 +46.5 (R) ✓ 570 +514 22 Jan 80

5.74 +46.5 (R) ✓ 570 +514 22 Jan 80

5.71 +46.5 (R) ✓ 570 +514 22 Jan 80

5.70 +46.5 (R) ✓ 570 +514 22 Jan 80

5.71 +46.5 (R) ✓ 570 +514 22 Jan 80

5.72 +46.5 (R) ✓ 570 +514 22 Jan 80

5.73 +46.5 (R) ✓ 570 +514 22 Jan 80



2429 ✓ 06 35 40 -19 .13 3.95 +1.06

✓V

3.98 -86 1265 -509 290.77  
3.98 -84 1278 -526 304  
3.98 ~~88~~ 1272 ~~518~~

3.98  
3.98  
3.98

3.98