

97240 11 08 40 -77 41 8.51+46

497 0 +60

✓✓

8.52 -408 880 -409

8.53 -415 883 -440  
8.58 -412 882 -425

2.175 8 Mar 79

2.177 9 Mar 79  
2.176

291 16c

156 486 21054

98019

11 15<sup>6</sup> 15 -20 35 78877

(D) (X)

2.64 -62 1208 -411 12 June 66 +33

2.67 -70 1226 -447 24 June 66 77 -4

2.66 -65 1236 -470 18 June 66

~~2.66 -66 1231 -460~~ (2)

(X)

R (X) (7)

4496 7.14

+0.344 52 June 66

2.66 454 1507 424 7.18

+0.336 62 June 66

\* 2.66 456 1501 437 7.18

+0.340

12 June 66

98478 11 18 25 -48 04 8.18612

(D) 8.17 2.96 905-3192.153 -2.6  
15282 8.19 -2.94 911-312-2.153-21 -9  
9.18 -2.50 908-316 2.153

(D) 2.94

7.99 10.196 6282  
8.03 10.209 20282  
8.01 10.202

$$\begin{array}{r}
 98722 \sqrt{\phantom{000000}} \\
 11 \quad 19 \quad 55 \quad -58 \\
 \hline
 -84 \sim 3 \quad -84 \\
 22 \quad 802 + 39
 \end{array}$$

$$\begin{array}{r}
 8.03 \quad -444 \quad 868 \quad -287 \\
 \hline
 8.04 \quad -451 \quad 872 \quad -264 \\
 \hline
 8.04 \quad -448 \quad 868 \quad -272 \\
 \hline
 2.204 \quad 8 \quad 204 \quad 9 \quad 11 \\
 \hline
 2.204
 \end{array}$$

$$\begin{array}{r}
 254 \quad 141 \quad 643 \quad 2641 \\
 1372 \quad 217
 \end{array}$$

78

~~98932~~ ✓ 11 21 55 -16 30 8.1.15 TH  
 98932 ✓

7.59 -407 918 -124  
8.08 -402 906 -117  
8.04 -404 912 -123

2.192 162879  
2.202 62879  
 2.197

97826 ✓

11 21 25 -80 47.5 8.16 +52 FLD

+18

8.10 -375 861 -377  
8.18 -348 861 -391  
8.19 -372 861 -394

2.150 162879  
2.158 670739  
2.154

333 137 524 2631

95058 ✓ 11 22 50 - 21 09 8.1 F6E  
+16

8.08 -377 883 -440  
8.08 -371 867 -412  
8.08 -374 875 -428

2.142 162679  
2.150 67079  
2.146

331 150 482 2622

99332 ✓ 11 24 35 -27 25.5 2.93732  
+86

2.56 -510 914 -207  
2.55 -443 886 -158  
2.56 2.05 950 -198

2.253 162879  
2.247 67279  
2.250

942 0cc 21 441  
147 123 2746



94873      11 28 20 00 44.5 2.410441

(X) (X)

200 +105 1461 454 182/82 -15  
201 +114 1482 462 19" -45 +6  
200 +110 1486 488

6.30 463  
6.29 464  
6.30 464

(R) (H)

[ 8.67 +0.541 ] 62/82  
[ 8.76 +0.543 ] 202/82

100278 11 30 55 -61 39.5 299 G07B

-9.7

+4.76

James

FIB

~~///~~

160 551 ✓ 11 33 10 -12 45 8.1 F5#  
-6

8.36 -384 852 -474 2.144 162679  
834 -345 851 -462 2.150 67429  
835 -374 852 -470 2.147

321 124 439 2.623



101969 ✓ 11 43 02 -04 41 8.1 F42  
+14

7.55 -427 885 -345 2.185 16.2879  
7.56 -433 881 -329 2.179 6.0079  
7.56 -430 883 -337 2.182

272 157 576 2.668

102165

2003500

11 44 25 - 21 22

7.6 F3 TD

+19

(X)(X)

780	-373	843	-337	2.183	18 APR
783	-373	840	-347	2.177	19 APR
<u>782</u>	<u>-373</u>	<u>842</u>	<u>-342</u>	<u>2.180</u>	

76 - 87

102149 11 44 20 26 17.5 2.86 N1 #

-3507416

9 m 20" 5 E

⊗ ⊗

+32 -70

+36.5

7.86 -41 12.57 -47.5 18.98 2

7.87 -45 12.66 -48.1 16.24 2

2.86 -44 12.62 -47.8 18.98 2

[9.81 . +0.440] 2024 2

⊗ ⊗ ⊗

+

737 +0.362 6.74 2

245 +0.381 20.24 2

$\frac{141}{7.41} = 19.17$

102657

11 48 00 -09 00.5 2.56000

(+) (+)

$2.41 - 96$   $1208 - 403$   $8882 + 14$   
 $2.40 - 98$   $1197 - 413$   $14812 + 9$   
2.40 -92 1202 -468 (2)

R (+) (+)

$6.52 + 0.327$   $5.882$   
 $[9.29 + 0.403$   $6.7182]$   
 $6.52 - 324$   
 $6.52 - 330$



$$102652 \sqrt{11 \ 48 \ 00} \quad -12 \ 30 \ 8.3 \text{ F2} \quad \frac{12}{12}$$

+14 Vars

$$\begin{array}{r}
 8.47 \quad -451 \quad 853 \quad -340 \quad 2.197 \quad 162879 \\
 8.44 \quad -440 \quad 858 \quad -357 \quad 2.213 \quad 62079 \\
 \hline
 8.46 \quad -446 \quad 855 \quad -348 \quad \hline
 \quad \quad \quad \quad \quad \quad \quad \quad \quad 2.205
 \end{array}$$

10370 11 51 85 -63 035 7.70 141711

~~rad~~

~~6242~~

Dumy

141711

154415 ✓ 12 00 20 -21 24.5 83.88  
+61

Sum  
20.00

118

✓

AD5 5054  
511

45-118

826 324 881 505-188 422-9218

644271 281-2

104724 12 02 35 → 204.5 299050

+244

(2) (2)

8.03 ~~-221~~ <sup>4</sup>932 ~~-419~~ 24282

~~8.04~~

8.04 -234 967 412 25282

8.05 -231 955 -429 3mm52

8.04 -234 961 -435 (2)

RS

(1) (1)

476

476

2.28

+0.223 20282

2.21

+0.267 89mm52

2.24

+0.267 (2)

2

105187  
85205

12 05 40 - 09 18

8.1 F7E

-6

(4)

8.62-393 866-408 2.168 182182  
8.64-394 875-428 2.164 192482  
8.63-394 870-418 2.166 (2)

105577 ✓ 12 08 15 51 80 42 43.5 ✓  
243 FEB +6.7

up.

(0)

254 354 887 -428  
255 370 878 -424  
254 377 882 -420

325 140 498 2144

100  
for

(22)  
(423)

440

105736 ✓ ✓ 12 09 15 -55 00.5 8.06 +42 +46-39 +326

8.09	-430	870	-352	2.152	8 Mar 79
8.10	-420	854	-323	2.1479	"
<u>8.10</u>	<u>-425</u>	<u>862</u>	<u>-362</u>	<u>2.150</u>	

278 138 550 2.674

105956

12 10 <sup>72</sup> 35 -4) 09 2.82 WITH

(9) (X)

284 -6 1065 -277 31 Jun 53

2.83 -14 1064 -248 24 Apr + 6.6

2.84 -12 1092 -313 28 Apr = 10 0

2.87 -17 (1030) (175) 3 Mar ✓

2.86 -25 1060 -274 20 Mar ✓

2.85 -15 1078 -274 (4)

2.88 +0.401 202 Apr

2.81 +0.405 19 Mar ✓

2.35 +0.403

Arjuna

(X) (X) (X)



106906

12

16

45

-55-

55

5.15

7.78

74

4.5+

44-30-



782 -412 874 -410

782 -412 874 -410  
782 -412 874 -410

2.173 874

2.173 874  
2.173 874

291 147 505 521 147 2662

8.34 1585

19-61 48

-15.7

Fall HC

+267

2.211 31110

+257

2.206 8"

+268

2.210

853

229

837

737

211

810

948

220

535

1521 121 2705

107544 ✓

108203 ✓ 12 24 45 84 44 8.1 FEB -15

8.20 -362 848 -495

8.20 -385 860  
8.20 -374 854

554 -454  
-477

2.157 162475

2.158 820070  
2.154

331 131 432 2.631

108468 12 26 30 +1757 256577

+1592611

-24

(8) (8)

747-145 1087453 25452

-20 -25

747-125 1078446 30002

747-136 1082450 (2)

(8) (8)

7.11 10329 202652

7.05 10327 190002

7.08 10328

109035 12 30 50 -20 ~~52.5~~ 7.3 120TH

200366 ✓

(X) (X)

→

+4

OK: -34 +54

7.29 -52 1237 -458 252/12 ✓

7.34 -68 1237 -441 3 mm ✓

7.32 -60 1237 -450 (2)

R (X) (X)

6.75 +0.368 14 Apr ✓

6.80 +0.356 pg Mar ✓

6.74 +0.362

~~109695~~ 12 35 38 -21 ~~125~~ 2.90971  
 203674 → +9

Check  
 7.77 7.74 7.00 1450 -722 25.2572 + 400 + 25  
 7.77 7.43 1247 -525 8.0005  
 Check 7.76 7.46 7.01 145 -541 20.0005  
 7.76 7.56 7.51 1402 -535 ②

R X ① 2.09 7.0457 14.0005  
 7.10 7.10 7.10 7.10 7.10  
 7.10 7.10 7.10 7.10 7.10

111344

12 48 00 -09 07

7.6 102 II

502424

7.6

(X) (X)

7.57-32 1301-491 2424 ✓ +15-24

7.58-38 1306-481 2545 ✓

7.58-34 1304-486 (2)

(Am)

(X) (X) (X)

2.18 +0.354 2024 ✓

7.06 +0.369 19mm ✓

2.04 +0.362 3243

7.05 +0.366 (2)

112039

12 52 35 - 23

00.5

8.42 + 44

Doc -

✓

8.46 - 387 858 - 474  
8.48 - 388 850 - 457  
8.47 - 388 854 - 466

317 131 443 2635

2.155 8 Mar 24  
2.159 9 "  
2.157



112239 12 54 20 -21 38.5 8.64 622#

8.70 -318 894 -475 2.130 <sup>3 hrs</sup> -2823

24 8.46 -314 874 -451 2.125 -65 -8

8.168 -327 903 -457 2.141

8.118 -320 -892 -457 2.132 (3)

-460

8.118

RS

(FA)

8.54 40.224 20242

8.44 40.206 19222

8.44 40.215

112574

12 56 50 13 02

8-1 F7D

1203729 (D)

8"

-10 Van?

98-90

ADSS 117

Vm - 11/11

842-363 875-444 2.162 20 Mar 5

835-370 875-458 2.163 21 Mar 5

840-366 877-450 (E)

113049

13 0245

→ 81 03 22011004

⊕ (X)

-15.5

7.26-96 1142-455 22mm Δ

7.25-97 1153-456 21mm Δ

7.26-96  $\frac{1148}{1148} = \frac{456}{456}$  (2)

⊕ (X) ✓

✓

1 ?

~~1 6.75 + 0.322~~ 29 Apr 52

6.83 + 0.363 12 Apr 53  
6.75 + 0.342 32 Apr 53

113 449

13 02 50 -05 03

2.5857

~~403404~~

U var?

~~(4)~~ ~~(1)~~

~~7.69 -210 1039 -444 24218~~  
~~7.70 -214 1045 -508 25218~~  
7.70 -212 1042 -504 (2)

RF

~~(4)~~ ~~(7)~~

771	+0.343 202182
<u>772</u>	+0.324 19 Mar 18
736	+0.334

118612 13 04 05 28 24.5 769 6870

①②③④  
⑤⑥⑦⑧  
⑨⑩⑪⑫  
⑬⑭⑮⑯  
⑰⑱⑲⑳  
㉑㉒㉓㉔  
㉕㉖㉗㉘  
㉙㉚㉛㉜  
㉝㉞㉟㊱  
㊲㊳㊴㊵  
㊶㊷㊸㊹  
㊺㊻㊼㊽  
㊾㊿

① 7.73-203 1005-435 5284  
7.76-217 1006-430 20 mar 8  
7.74-214 1018-454 21 mar 5  
555-212 1006-434 ③

②③④⑤  
⑥⑦⑧⑨  
⑩⑪⑫⑬  
⑭⑮⑯⑰  
⑱⑲⑳㉑  
㉒㉓㉔㉕  
㉖㉗㉘㉙  
㉚㉛㉜㉝  
㉞㉟㊱㊲  
㊳㊴㊵㊶  
㊷㊸㊹㊺  
㊻㊼㊽㊾  
㊿

11421 13 1305 -41 06 700857

①

7.21

0 he

7.66 -112 1166 -480 22 mar 22

7.64 -112 1151 484 21 mar 22

7.65 -112 1162 482 20 mar 22

①

7.21

7.21 70.324 14 mar 22

7.20

7.20 70.325 14 mar 22

7.20

70.325