

2484 6 42.5 +12 57 307-415

TI Sta

~~3.35 -411 870 -283 2.173 2300-78 24"~~
~~3.34 -419 885 -259 2.191 2300-78~~
correct

2489 334-419 885-289 2.191 2344275

7.52 + 0.10 + 0.10

✓

Plum (RT) ✓

see

Sm-2000

44409 ✓

6 47 21

7.78 ✓

7.92

+0.205 ✓

✓ (R) (R) ✓

7.73 + 0.235 3/277

7.82 + 0.23 13/272

7.74 + 0.20 27/276

7.89 - 325 880 - 513

7.91 - 328 888 - 517

7.90 - 326 884 - 515

7.90 282 158 353 1427

7.91 328 888 196

7.90 282 158 353 1427

2.124 6/274
2.133 8/272
2.128

7.71 + 0.20 1/2

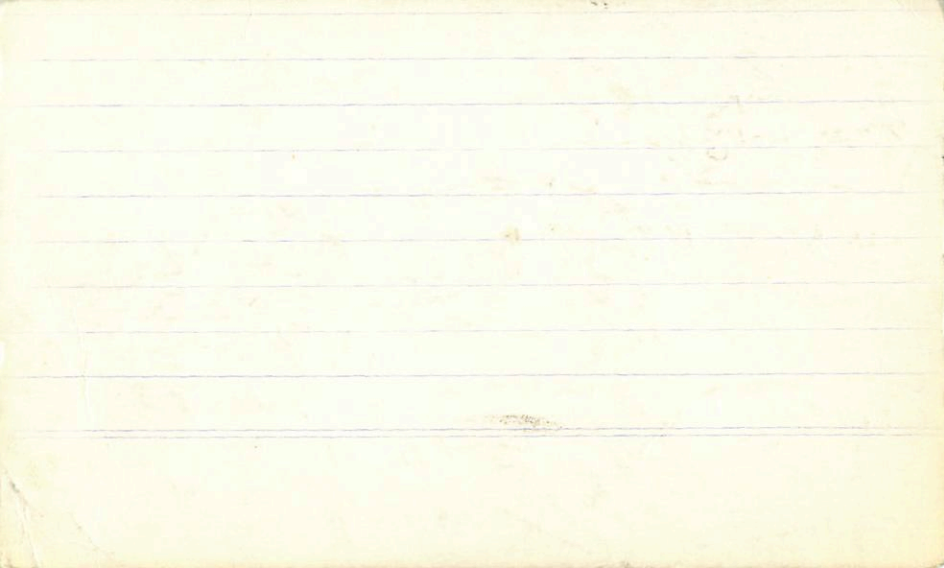
7.76 7/276

7.89 325 880 - 513

7.91 328 888 196

7.90 326 884 - 515

7.90 282 158 353 1427



5222 (X) 4

-7642

6 48 20 -26 49.5

765 65 III
F

-7642 15" N 9.47
10" E

665 70.223 9 Jan
W 2832794
W 2832794
W 2832794

7.02 -194 1064 -426 26 Jan 94
7.03 -180 1092 -456 25 Jan 94
2.02 -201 1070 -464 25 Jan 94
7.02 -194 1064 -426 25 Jan 94

10.33 -379 911 -492 2.127 26 Jan 94

10.31 -355 878 -471 2.140 5 Apr 93

10.32 -370 902 -477 2.134 25 Jan 94
10.32 -380 907 -480 2.130 2

90110th

✓

+105 5014

+58.7 ± 1.5

50568

6

51

05

44

17

2.514050

818 -143

1054 -323 118075

818 751

1063 -350 40000

818 747

1058 382

(25)

RR

7.75

+0.327 24000

7.77

+0.329 25000

7.77

70328

53141 } 60" } 00 00 -60 50 2.74 } AVG
 -600742 } 2.73 -224 867 -26 2.327 1724 } 12.1 } 17.1

+001 +046

+600744 } 00 15 -60 50 9.48 } 17.1 } 17.6
 9.33 -366 874 -244 2.190 1724 } 11.4

° 10.99 -358 859 -350 -009 +046

53407 } 00 50 -60 46 9.2 125.17 } (NO)
 600750 } 9.15 -454 898 -274 2.200 1724 } 022 +040

53444 } 01 10 -60 44 9.8 17.1 }
 9.23 -359 909 -448 2.157 1724 } 014 +026

-600760 } 01 15 -60 39.5 9.8 17.5 } 17.1

110760

950-413 891-204 2.208 17213

250 115 713 2.646

(252) (655)

250 236 515 2.35

220 11
—
060

$\checkmark \checkmark \checkmark$
 54046
 7 06 42
 +15-BB⁶
 782 + 505⁻⁰⁰⁵

54110
 7 66 54
 +15 55 772 582⁻⁰⁶

7.79 348 148 410 1348
 2.135 840 79
 2.135 10 " \rightarrow 2.108

7.81 -361 862 -475 540 76
 +0.22 1340 76

7.77 -355 874 -517 740 76
 +0.18 527 76

7.79 -358 868 -498 -80 680
 7.65 +0.215 390 77

7.71 -368 851 -512 840 76
 7.70 +0.215 390

7.66 -360 841 -499 7 " 4
 7.65 7.65 7.65 +0.22 5 1340 76

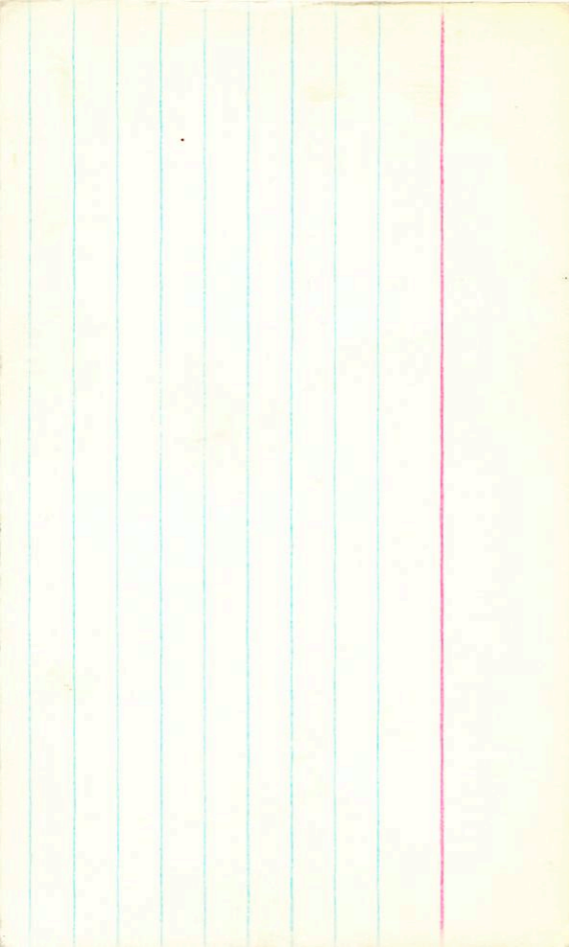
7.68 -364 846 -500 7.60 7.60
 7.68 342 123 402 1284 76
 +0.21 390 77

2B

RV

$\checkmark \checkmark \checkmark$

2B



3 Stern ✓ 07 03 00 +20 36

368 - 4.16 18.15
83° 57"

205 525

11.5
+2.9
8.6

→ 11.46 + 0.45 + 0.06
60"

1023

774 (243) (576)

258 166 628 2703
516

11.51 444 893 (287) 2214 2 Jhr 50

11.52 454 899 307 2.219 1 Jhr 7

11.53 448 929 322 2227 2 Jhr 8

11.53 450 907 315 2.220

56 (255) (559)
252 179 609 2710

11.45
325
8.2
E₂ + 0.20

~~56555~~ 55195 7 08 45-49 57 ~~1012-010~~ ~~1012-02~~

55195 95° 29" { 8.6 (H) 9.3 (10?) Free

8.75-439 796 ~~2.129~~ 2.129 8 Mar 79

8.75-498 788-354 2.189 17879

8.75-491 812-336 2.174 62879

8.77-431 788-346 2.158 7"

8.78-437 796-346 2.186 (4) 8 Mar 79

10.33 73 1308

10.36 72 1316-459 2.101 17879

10.35 +10 1300 -448 42879

10.35 -14 1316 -438 22479

10.35 000 7310 -448 (4)

B

$$\begin{array}{r}
 1463 \\
 1464 \\
 \hline
 1464 \\
 +6.288 \quad 4 \text{ } 2124 \\
 +1194 \quad 5 \text{ } \\
 \hline
 +212
 \end{array}$$

B

$$\begin{array}{r}
 9.76 \\
 9.81 \\
 \hline
 9.75 \\
 -10353 \quad 4 \text{ } 674 \\
 +10361 \quad 5 \text{ } \\
 \hline
 +10887
 \end{array}$$

D

$$\begin{array}{r}
 13.65 \\
 13.65 \\
 \hline
 13.65 \\
 +10.234 \quad 9 \text{ } 2124 \\
 +10.224 \quad 5 \text{ } \\
 \hline
 +1027
 \end{array}$$

F

$$\begin{array}{r}
 14.56 \\
 +10.22514
 \end{array}$$

C

$$\begin{array}{r}
 13.68 \\
 13.69 \\
 \hline
 13.69 \\
 +10.578 \quad 9 \text{ } 2124 \\
 +10.261 \quad 5 \text{ } \\
 \hline
 +1270
 \end{array}$$

Perkins 131

7 07 10

-02 53

80.5

11.78 + 05

(X)(X)

11.84 - 630 771 - 753 2.116 3 Jan 82

11.81 - 627 760 - 762 2.117 4 Jan 82

11.82 - 625 766 - 754 2.116

B + 170

¹⁹⁵ 065 0.50 141 2.586

(070) (128)

(269)

11.1
4.35
15.45

131



55327

7 08 50 -56 19.5 295

CS/100 III

-56024

8.07 554 316 464 → (123) ←
9.54 151 225 794 2800

FO III

55352

7 08 55 -56 20 9.52

560262

8.07 190 1065 451 19200
8.07 194 1053 427 17200 7.69 +0.249
8.08 186 1045 441 18200 7.69 +286
8.07 190 1055 446

Sum 93

18
plu
73

7.71 +277 81613

8.54 543 947 130 2.294 19200

8.53 543 962 133 2.294 17200

8.54 549 961 145 2.265 18200

8.54 545 957 136 2.295 ③

7.70 +291 ②

55817 ~~7-23-55~~

2.22-08

55817 ✓ ✓ 7-12-30 -20-55

More

Edna
Henschel 2940

7-11¹⁰² 2^m 7.55-731 821-465 2.232 13 Jan 78

7.75-714 831-456 2.236 5 Jan 78

ok → 8.62-719 895-500 2.205 23 "

7.89-715 810-462 2.203 6 Jan 79

7.92-725 823-489 2.219 26 January 05:30

7.91-745 850-487 - 13 Jan 86

7.90-726 811-480 2.225 27 Jan 85

170
✓ ✓

55956

7 12 55 - 22

52

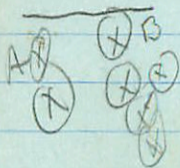
(6-1 B3
9.1 G17)

907+77

HR 2733R

20"

67+500



6.10 → 64-798 → 791

2.142 27 Jan 81

6.36 → 64 785 → 783

2.142 12 Jan 81

6.38 → 64 792 → 788

2.142

4.38 → 078 074 111 2617

6.38 → 090 093 119 2617

8.13 → 229 1045 439

2.115 7 Jan 81

9.14 → 219 1012 416

16 Jan 81 60"

9.14 → 211 994 387

20 Jan 81 60"

9.13 → 199 987 392

2.133 21 Jan 81 "

9.14 → 207 995 390

2.133 23 Jan 81 "

9.12 → 219 997 (-493)

2.121 27 Jan 81 36"

9.12 → 224 980 (-458)

2.124 17 Jan 81 36"

55856

6.38 -090 093 119 2.617
A 6.38 -090 080 0.112 2.617 (2)

4723733

Erz +026 (056) 0.128 (240)

Ba \nearrow

6.25
-3.05
9.30

5.09 506 249 418

B. 9.13 -215 +997 -396 2.130 (6)

9.13 0.459 259 515 2.602

(408) (415)

Schmitt

390 300 340 428

✓✓✓
641-187 + 500
555-10325 (2)

36176 ✓ 7 15 322 426 455-600

(Met) ~~11 + 118~~

640-181 1033⁸⁹ - 4169 4280

634-176 1019 - 470 580076

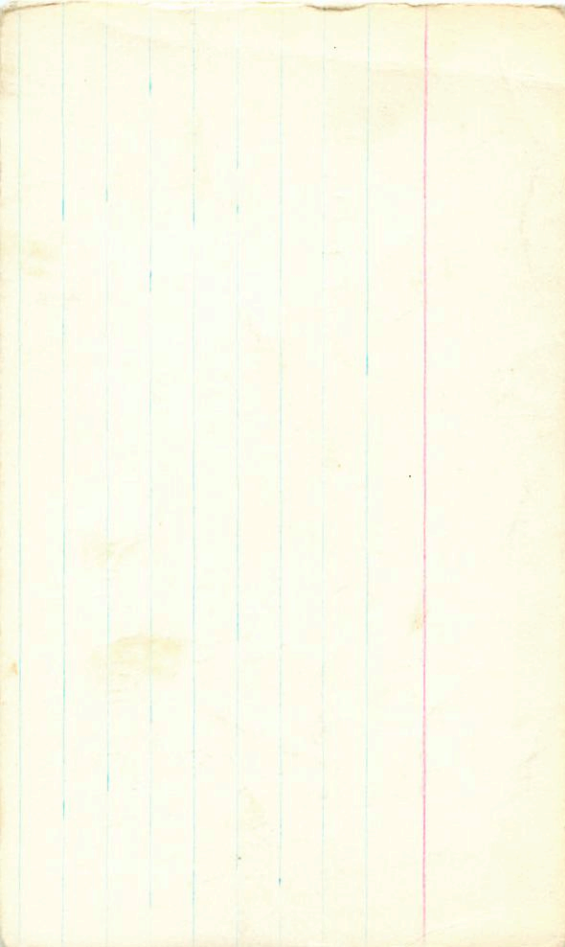
637-204 1046 - 454 7 " "

638-204 1023 - 448 12 " "

637-194 1017 - 488 281008

638-188 1037 - 465 (4)

826 + 366 19 new
834 + 0.308 26.648
839 + 0.348 27.648
593
7893
5.99 + 0.311 (2)



HR2764 7 15 45 -23 ~~17~~ 17
25" 4.76 MO
6.01 F02

B V ✓

223

6.03 -553 978 -74 2.302 20 km 87 60°
6.02 -551 974 -86 2.293 21 km 87 60°
6.04 -538 939 -63 2.281 21 km 87 36°
6.03 -552 976 -75 2.297

144 243 847 2802

2768 ✓ Do A var? ✓ no

2 " 202
55
1734

(Am)

2778 ✓ 16 00 -30 52 } 2023 A
38" } 27.7

Sleepin + B (12.76) ~~B~~ Apin open

6.35	-599	969	+111	2.319	10 Apr 76	2 Febr 76
6.34	-591	959	153	2.315	18 Jan 76	
6.37	-587	962	188	2.324	14 Feb 76	
6.35	-592	963	+109	2.320		6.29 103121

8.07	-527	949	-147	2.266	10 Mar 76	
8.05	-535	955	-95	2.265	18 Jan 76	
8.08	-529	949	-59	2.262	14 Feb 76	
8.07	-530	951	-143	2.265		

43760
34228
2
Σ 3
288
191
7

51 - *

1
1
234A. 2403

661
2562

Random 143 7 17 5/8 +02 35
38

11.74+01

(4)

11.23 -6.48 8.48 +115 2.318 5 Jan 52
11.76 -6.54 8.58 +122 2.315 3 Jan 52
11.74 -6.57 8.53 +118 2.316

0.0000

0.40 130 9046 2.425

11.55
11.55
11.55

143

2

RV ✓

89-13114

23 21 19 55

M. J. H. ✓

7 21 20 + 8 57 9.37 + 91 + 66

8 5's

9.36 ✓ - 184 1110 - 459 4 Dec 23 5 2
 9.34 - 155 1120 - 461 29 Dec 76
 9.38 - 212 1140 - 459 29 " "
 9.36 - 204 1130 - 460
 9.36 510 815 147 2 Dec 11 (2)

10.44 - 353 772 - 521 2.12.4 4 Dec 23
 10.41 - 356 793 - 511 29 Dec 76
 10.41 - 397 813 - 502 29 " "
 10.41 296 203 - 506 0

9.07 + 0.285 27 Dec 76
 9.07 + 0.315 3 Jan 77
 9.10 + 0.29 1.27 Jan 77
 9.04 + 0.30
 10.30 + 0.20 27 Dec 76

10.30 + 0.225 3 Jan 77
 10.45 + 0.215 12 Jan 77
 10.35 + 0.215 (3)

10.41 323 84 402 1162 (3)



1. 11/11/17
DRETT
57675

Buy 240
one more

425
7 146
4 236

7 21 10 01 10
-01 44 8.75 100

551
+80000

X

(425)

8.74 - 238 975 - 465 10 11/11/17
8.76 - 240 975 - 465
8.77 589 - 970 975 - 465
8.78 975 - 975 - 465

145 440

8.45 + 0.247 247
8.45 + 0.246 25
8.45 + 0.246

R R

2790 - 4300
9603 5577

59573

7

22 45

-79 09

75 102~~4~~

-780266

Case m
Projectal
=

47" 2360 12.7

7.61 +61 1314 -472 21 Jan 84

7.61 +62 (1299) -456 172485

7.59 +61 1318 -455 247485

(X) (X)

6.95 +0.459 9 Jan 84

6.96 +0.458 22 Jan 84

6.95 +0.457 (2)

12.51 +0.301 9 Jan 84

59110 ✓ A ✓ important

26 15 -34 16 2.00449⁻⁰⁵

mixed data 17" { 8.15 76.35⁷⁰⁷

(B) hnd, larch / 2.164 bleedle A 6.00 + 0.15 (E)

~~2.115~~ 24 2079 0 2.77 + 0.205 (E)

2.161

13 Jun 79

207 - 385 856 - 425
207 - 386 853 - 430
207 - 386 854 - 425
319 131 482

6.86 + 0.69 47854
6.81 + 0.155 3082170
6.84 + 0.155

13 Jun 79

8.19 - 305 898 - 486
8.20 304 988 - 492
8.20 304 893 - 489
405 167 419

7.60 + 0.202 48779
7.86 + 0.210 3082170
7.90 + 0.205 218270
7.79 + 0.209 (E)

2.125 bleedle
2.121 24 2079
2.123

LDS182

59100A

7 25 46

-34 14 2.00 + 0.49

17"

B.

3.20

8.15 + 0.63

LTT 2840/41

380

7.00 + 0.49 - 0.05 (3)

8.15 + 0.63 + 0.04 (2)

485

6.81 + 0.155 30 Dec 70

6.80 + 0.15 31 Dec 70

6.80 + 0.15

Σ chud sp. 2.11 = 3.20
43.8 pm.

+72 -39 -54

+10 +6 -10 / 10 pm.

642

617

320

297

250

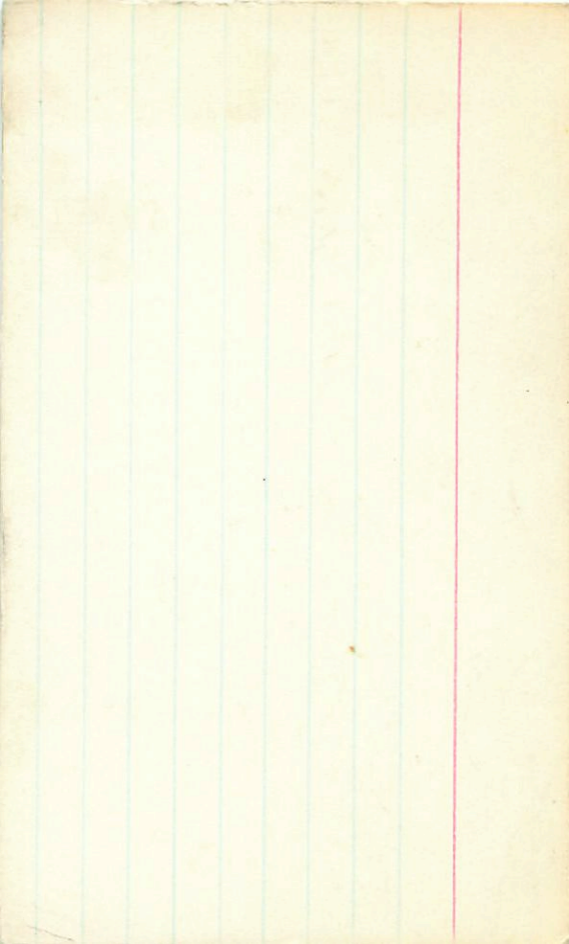
720

320
480

7.86 + 0.21 30 Dec 70

7.40 + 0.205 31 Dec 70

7.88 + 0.205



WDS182

HD 59002

7 25.1

1565

1937 70 + 49 - 03

P=+71

LT 2840
2841

17" } 7.9

7.01 +49 - 3

7.00 +0.49 - 0.07

7.02 +0.50 - 0.09

7.00 +0.49 - 0.02

7.00 +0.49 - 0.08 (3)

8.16 +0.66 +0.02

8.14 +0.61 +0.06

8.15 +0.635 +0.04

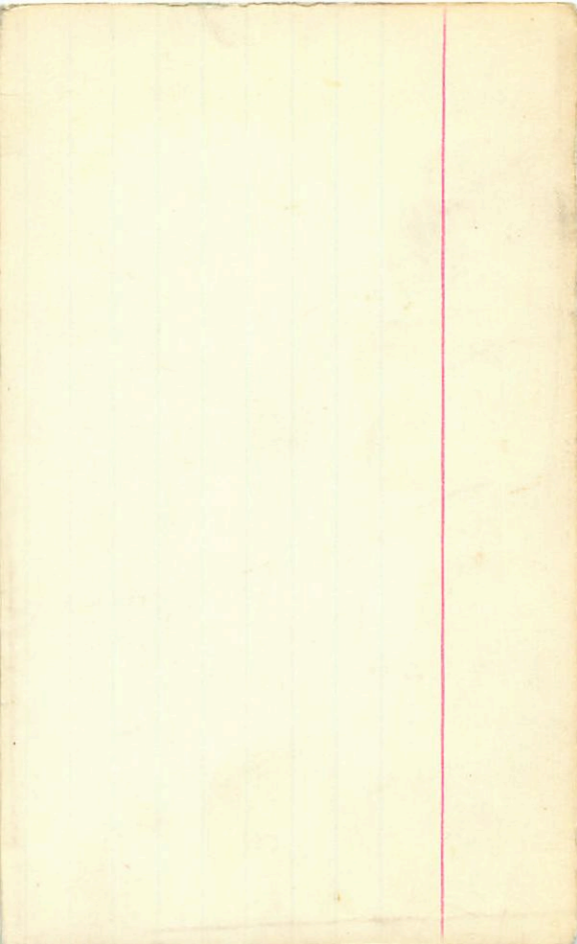
5 mar 67

15 Dec 66 40'

cup

15 Dec 70"

5 mar 67



60721 7 29 55 48 33.5 9.4 40.2

~~(X)~~ 9.50 10.55 845 + 42 2.365

707

AD56157

7 31 00

-8

38.5

8.7 FORT

THE WALLS

SUB 9 MAR 32

(1528)

8.72 + 0.285 = 8.77 - 87 1260 - 574 16 JAN 57

8.72 + 0.285 = 8.78 - 90 1260 - 574 17 JAN 57

8.78 + 0.285 = 8.80 - 84 1271 - 584 20 JAN 57

8.80 + 0.285 = 8.89 - 84 1263 - 580 23 JAN 57

8.89 + 0.285 = 9.17 - 84 1249 - 580 26 JAN 57

9.17 + 0.285 = 9.45 - 110 937 - 110 29 JAN 57

9.45 + 0.285 = 9.73 - 110 939 - 110 31 JAN 57

9.73 + 0.285 = 10.01 - 110 940 - 110 1 FEB 57

10.01 + 0.285 = 10.29 - 110 939 - 110 3 FEB 57

10.29 + 0.285 = 10.57 - 110 940 - 110 5 FEB 57

10.57 + 0.285 = 10.85 - 110 939 - 110 7 FEB 57

10.85 + 0.285 = 11.13 - 110 940 - 110 9 FEB 57

20" 2280

345

734 + 323 19 MAR 57

2.271

2.271

2.271 16 JAN 57

2.268 17 " "

2.274 20 " "

2.271

2.271

AD56157

A

8.77	-87	1260	-574	16 Jan 81
8.78	-90	1260	-579	17 "
8.80	-89	1271	-589	20 " "
8.79	-81	1244	-570	18 Feb 83
8.82	-87	1252	-564	19 Feb 83
8.80	-76	1249	-580	20 Feb 83
<u>8.79</u>	<u>-85</u>	<u>1256</u>	<u>-578</u>	(6)

AOS
6157

B 9.18-444 937 -110 2.271 16 Jan 57

A05932

9.18-503 939 -110 (2.218) 17 " "

9.20-448 970 -110 2.274 20 " "

9.21-444 (92) -91 2.274 19 2/83

9.23-505 936 -112 2.282 19 2/83

9.21-503 937 -100 2.284 20 2/83

9.20 -500 938 -108 2.278 (6)

4960185 ✓
 + 001656
 7 32 10 + 00 12.5 5.3 BF
 - 43

744 - 724 794 - 465 2.178 16 Jun 80
 745 - 725 788 - 463 2.180 26 Jun 80
 744 - 724 794 - 464 2.179
 - 041 003 1145 2671 Ey + 030
 (67) (152 515) Vp 730
 Wp - 2.20 9.5

60872 7 32 15 -43 10 8.57 85

" 21 5 15 "

6pm } 1100 26 "

60 "

8.64 1670 743-527 2.154 4 Jan 2 60

10.04 1650 813-247 2.255 4 Jan 2 60

60621 - 2 dia 9 33 W -46 44 9.4 43 III IV

9.50 549 937 -27 2.342 23 Apr 52

9.54 548 934 -37 2.323 24 May 52

9.52 555 931 -57 2.332

~~136 204 986 2333~~

250 152 1483 205 865 2844

113 241 113 208

914
20
114

001997 ✓ > 33 35 1002-003 + 00 B 8.6 Bg

8.48 - 678 883 + 94 2.366 16 Jan 80
8.47 - 677 885 + 82 2.362 26
8.46 - 676 884 + 91 2.364

019 167 1117 2996

014 158 1018 2882

hco

61260 7 35 45 47 12 8.0 8.14

619126-

MA 5 -

~~61260~~

7.92 184 82 171 227 30 9.14
7.95 186 82 170 225 1 10.14

(X) (X)

7.94 187 82 170 227

(120) 002 106 80 270
LOG 800
COI

h.l.i.v
7.94

145241

2706

511

5109-614

121

1026

~~511~~

117

1029

1435

11.8

544

(5)

1263

4680

10

1255

2870

4355

10

6315

6326

2526

65

90

1.

2690

65

90

1.

2690

65

90

1.

2690

65

90

1.

2690

65

90

1.

(921)

-10 -8

61528 7 38 50 -46 40.5 90 ADV

46165 9.15 645 893 +44 2.404 23 APR ✓

9.14 656 904 +61 2.397 25 MAR ✓

9.16 650 858 052 2.400

041 171 978 2.525

8.6
4.7
7.1

61763 7 38 10 -44 47 78 ADV

46174 7.45 655 815 +165 2.250 23 APR ✓

46174 7.58 662 819 +177 2.247 29 MAR ✓

029095 1107 274 ✓

038177 997 2522
9.0
7.3

180/235
7 35 10 45 49.5 9.5 1.2

(X) 9.54 467 886 352 2.226 23Apr 2

+3.15

64 +239 760 561 2.717

Forward

711100 4.2 00 64- 54 58 6
m m 6519

66

25.5
9.5

June 1st 2022

(173 267)

(062)

(450)

2022

1.5 " 10 51

200-201 74-759 2.14g 24 282

(7)

0.51

NOV 29 1958

11/29/58
11/29/58
11/29/58

(A) 8.11 - 6.06 1.09 11.8 8.88 4.89 2.346 24 2852

8.11 - 6.06 1.09 11.8 8.88 4.89 2.346 24 2852

(A)

7.8
+0.5
7.3

(A)

0.90 151 1.114 2.878

66192

66190

HN2402 7 36 45 -14 24 6.53 R 6/12

(F) 6.55 -16.51 1782 -133 2.155 26 APR

-034

20-55
25-42

25-60

58-07.

80-0

44-91

14-01

500

7.21 -338 925 -450 2.137 2.81
369 194 460 2.6.11 (6.8.8.6) 5

8.18 -258 1.009 -468 R-I
453 273 0.441 0.266 (7.7.63) 5
10 59 (409) (350)

8.30 -253 1026 -472
458 289 437 0.261 (4.8.3.5) 5
10 74 (427) (346)

5.79 -444 896 -344 2.198
258 169 583 2.6.84 (7.4.6.5) 2

✓ 62850 (X) 4
579 258 164 564 2644 1 MW 1

58805
59049
59049 41300
721 339 926 458 2.125 3 pmt
721 313 914 467 2.134 30 pmt

59049 41300 79 00 68 14 5.87 11.13 13 pmt
916 265 1014 468 3 pmt
917 233 997 427 30 pmt

828 224 1114 474
828 256 1032 478 3 pmt
828 432 862 358 2.213 30 pmt
880 455 864 330 2.201 18 pmt
2.195 00

720 -344 940 -440 2.142 18 June 83
726 -347 910 -435 (2.096) 4 June 83

721 -339 926 -457 2.125 3 June 83

721 (-313) 914 -467 2.134 3 June 83

719 -322 910 -451 2.147 18 June 83

~~811 -343 1005 -472 192 June 83~~

~~816 -265 1014 -465 3 June 83~~

817 -283 997 -477 30 June 83

820 -265 997 -447 4 June 83

~~818 -254 1030 -457 19 June 83~~

~~831 -246 1030 -471 18 June 83~~

~~828 -255 1005 -447 4 June 83~~

~~828 -222 1014 -474 31 June 83~~

11 June
785 +256 63

782 +262 17 June 83

784 +259 63

795 +248 11 June 83

792 +240 17 June 83

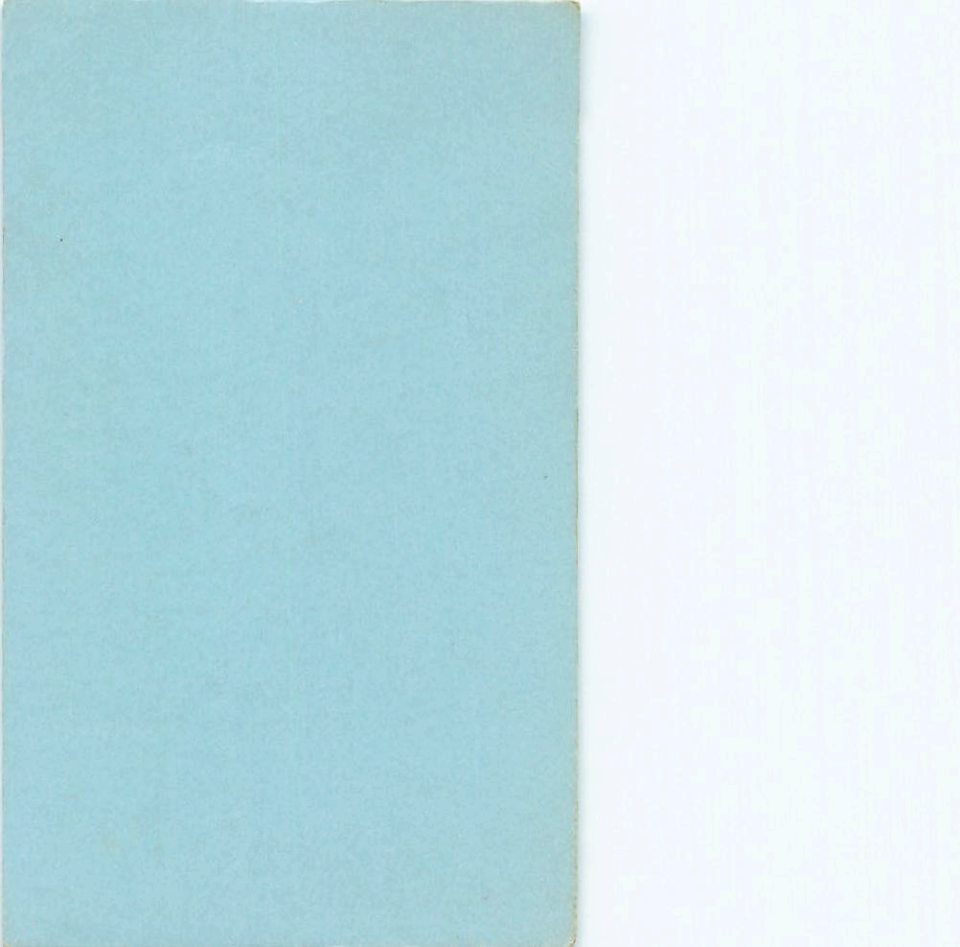
795 +254 11 June 83

792 +240 17 June 83

795 +254 11 June 83

792 +240 17 June 83

795 +254 11 June 83



62301

7

43 35

+35

5 37

628 754

754

Ant. gr ✓ ✓

Fr
25

6.76-349 845-514 2.134 206080

6.76-356 854-531 2.134 21"

6.74-349 843-512 2.133 22'

6.76-351 847-519 2.134



63008

7

43 40

- 50

24.1

682

F82

52
1230

79

M.N. P.H.S.

B1, 225

6.66 - 379 984 - 485 2.159 19 2183

~~6.67~~ - 376 980 - 481 2.155 19 2183

6.67 - 374 978 - 472 2.162 20 2180

6.67 - 376 980 - 480 2.159 (3)

7.60 - 294 934 - 496 2.122 18 2183

7.61 - 292 928 - 485 2.132 19 2183

7.61 - 293 933 - 487 2.131 20 2183

7.61 - 293 932 - 489 2.128 (3)



✓ 19507 44 24 -52 26.1

Apr

63745 9 47 10 -52 31 10.52-10.07

52.1284

10.80-684 944 - 074 2.349 3.688

10.29-679 968 -120 2.331 2.2680

10.26-675 969 -104 2.340 8"

10.28-679 954 -100 2.340 3

0.009 236 808 2.963