+63° 21 05 00 04 20 +63 42.5 9.18 +63

9.18	−193	765	+480	2.254	160"
9.18	−191	758	+486	2.254	17"
9.18	−192	762	+483	2.256	

6755 1 08 10 +61 27 7.68 +72

RJ Iron ✓ ✓

GC 1342

C=320

0.5 H2O

7.74 -241 837 -520 16 Wet 80

225 -229 830 -513 17 " " "

7.74 -235 834 -516

477 117 341

31 DYE

AD 52566 3 28 60 +52 51

26" (7.29 +1.39 +134 2ID
10,42 +60 +11 2ID tp

50 min

7.34 +134 1305 -456 6 @ 80
7.32 +134 1317 -454 7"
7.33 +134 1311 -455.

10.45 -319 861 -371 2.214 6 @ 80
10.43 -302 847 -349 2.205 7
10.44 310 855 -345 2.210

GO Ia

6477 01 05 40 +63 40 7.62+.62

✓ ✓ ✓

2.50	+276	1006	+43	2.172	18 ctrl 80
2.48	+273	1000	+33	2.175	19 " "
2.48	+281	983	+38	2.174	21
2.49	+277	996	+51	2.174	

F2 H

+62° 4 ✓ 00 07 00 +63 14 8.82 +62

8.82 -254 792 +642 2.263 1 Gauss

8.81 -250 728 +651 2.263 1 Gauss

8.82 -252 785 +649 2.263

27 ✓ OV 09 15 +45 57.5 5.0 F2 H

✓

11"

(7) 5.04 -439 864 +203 2.182 Sleet 80

5.07 -444 857 +209 2.176 11 " " "

5.03 -442 860 +206 2.179

240 1.137 2.661

1.095

HOLL √ OV 09 40 40 41 8.260 I5

8.27 +34 940 -301 2.156 16 electrod
8.26 +27 942 -256 2.154 17 "
8.26 +32 941 -253 2.155

1180 -1.7 +915 +1721 -54

+56°14

7.0643

725 √ 00 10 40 +57 09.5 · 7.1F5I6

7.07 -279 853 +494 2.224 16 "

7.07 -283 850 +509 2.214 17 "

7.07 -281 852 +502 2.219

R

+55° 12' OV 11 40 +60 08 10.4 60 II

(X) (+)

10.35 -14 824 +30 2.186 4 left 80 3 in
10.25 -51 817 +61 2.190 5"
10.30 -35 823 +45 2.188

11F -1.5 +.003
+.187
-56

+58" 16

23634b ✓ 00 12 50 +59.15 8.9 F02

✓

check these

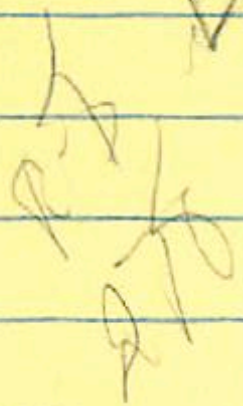
8.87 -89 243 +451 2.258 no load

8.87 -88 239 +452 2.27 17"

8.87 -88 2.253

+59° 30

1457 ✓ ✓ OV 17 58 +4.0 13.5 7.5 FOT



O-Gas

7.89	−292	799	+720	2.252	18 Ext FD
7.84	−268	773	+731	2.254	99 " "
7.86	−280	786	726	2.253	

+62° 9' 00 29 15 +63 34 10.7 P2I

(XD)

9.03	+45	772	+526	2.235 (1.3m)
9.03	+43	765	+544	2.2455 " "
9.02	+44	768	+535	2.240

3123 00 34 05 +62 52.5 7.27 F2I

D23

7.27 -294 791 648 2.227 23bt80

7.24 -277 782 +654 2.228 19bt80

7.25 -291 784 +654 2.238 20bt80

7.27 -288 788 +641 6h 2.230 21"

7.26 -284 778 +654 2.235 22"

727 ~~285~~ -290 785 +654 2.232

B 10.80 -501 717 -690 2.141 23bt80

2.616

+58°77 00 34 10 +59 12 8.7 F4 I

✓✓

o.g.m

9.14 −70 728 +302 2.225 176 at 80

9.14 −78 747 +278 2.231 18" "

9.15 −74 738 290 2.228

4266 OR
+550157 00 44 35 +56 40 2.6 F=25

✓ ✓

m
04

6.56-420 840 +458 2.258 20.8 50
6.55-413 840 +459 2.260 21"
6.56-416 840 +458 2.259

207 √ 60 45 30 +59 28.5 64 GOIG

16'

436'

6.41 -42 1028 -326 2.142 Elect80
6.40 -42 1048 -348 2.138 11 " " "
6.40 -42 1035 -337 2.140

~~414 F~~
384 K

680 297 576 2.614

+5 4.0

1223 33

+557
+890
-60

236656 ADE
+5-50265 / 1 11 20 +56 18 83 FY I

0.4 12 Pins

8.75	-254	834	+265	2.214 Nelstro
8.71	-310	840	+275	2.221 17 y
8.23	-305	840	+273	2.220

+59.25

+406 01 27 5 +59 56 7.2 F3 J6

7.12 -215 860 +424 2.210 18 " "

7.11 -214 853 +840 2.205 " "

7.12 -211 841 +436 2.203 17 " " "

7.12 -214 851 +430 2.205

+5P 24
1952

01 25 35 +54 35.5 7.8 F5J

0.5m

7.24 -119 875 +128 2.191 17let80

7.80 -127 893 +121 2.195 18 " "

-123 884 +124 2.193

9549 01 33 28 +45 29 P.7 F5 Ia

V V

0.9m

8.70 -507 923 -35 2.273 17ft 80

8.70 -508 918 -28 2.275 18"

8.70 -508 920 -33 2.274

0.191 0.191 840 2.775

HD

9923 01 37 45 +60 59 6.58 +57 PSIa

√√

6.91 -127 847 +387 2.192 9 " "
6.89 -121 848 +375 2.184 11 " " "
6.90 -124 848 +383 2.190

594 125 1.319 2.674

1.200

237 -84 1053 -5.47 1.51

264 244 946 -37

(X) (X)

PHIM PLIS

10303 1 38 55 -48 ~~05~~ 06 9.5

-48 440 448

Chuck

1 38 55 -48 06.5

9.02 -438 473-197 2.242 1 July 87

9.03 -440 980-208 2.238 3 July 87

9.02 -434 976-203 2.240

263 243 714 2.734

7.30+121 (ST)

10494 / 01 42 40 +61 46 ~~7.5~~ FSIA

√ √ √

70

7.29 +135 732 +619 2.210 23 out 80 0.4

7.30 +129 736 +624 2.218 18 Out 80

7.29 +124 735 +611 2.216 19 " "

7.30 +129 747 +608 2.206 21 "

7.24 +139 726 +627 2.204 22

7.30 +133 736 +618 2.211

964 1.687 2.699

12405 ✓ 1 59 50 -34 75.5 8.2 GG II

M_V -0.9

8.06 -103 1051 -448 21 μm FU

8.24 -123 1053 -444 23 μm FU

8.14 -114 1052 -446 (2)

1 8.46 +0.266 23 μm FU

(IR1) (1) 8.35 +0.300 15 μm FU

8.43 +0.302

+59°389 02 01 15 +60 04.5 B9 FOIb

check

0.9 m

9.05 +36 678 +044 2.287 19deltaO

9.06 +45 670 +057 2.266 20deltaO

9.06 +40 674 7.60 2.276

TOD 45? 02 06 ~~15~~ 20 +58 3/4 8.5 FCI

12 x 42

dirty

Uncle Ervin

8.49 -142 833 +216 2.199 17 @ 80

8.50 -142 831 +233 2.215 18 @ 70

8.48 -141 832 +209 2.208 19"

8.49 -142 832 +219 2.207

+62 1452 -581
775 650 324

12640 2 11 05 -42 34 9.1 12.1

9:1

8.85 +62 1345 -580 23 NOV 11
8.90 +0.50 1439 -564 21 JAN 12
8.87 +63 1458 -583 19 OCT 11
8.84 +60 1448 -576 8.30 +0.412 27 OCT 12
8.25 +0.409 26 OCT 12
8.33 +0.401 25 JAN 12
8.24 +0.420 21 OCT 11
8.30 +0.410

+0.427

777 670 330
912 175

1.9

363

+62 1452 -581
775 650 324

+56046

B754 02 14 50 +57 31 9.5- F1 J

.B ✓

. ✓

0.4

9.72-75 741 +530 2.260 150 @80

9.73 -74 746 +543 2.270 20"

9.72 -76 755 +537 2.265

7/4 ✓✓ 2. 24 20 -60 24 5.34 $F_2 \Pi_p$

(II)

5.37 -463 907 -176 2.217 (Hollow) 24

5.37 -468 906 -120 2.2072 Hollow 24

5.37 -466 906 -123 2.212

235.109 .945 2.701

698

+15

GF II

15589 2 2 y 35 -36 8.94

36935

8.45 -35 1290 -767 23 sec

8.46 -32 1283 -757 21 sec

8.46 -34 1286 -760

684 524 140

83

8.44 +0.37 10 jan

8.47 +0.37 13 jan

8.46 +0.37

15589 ✓2 28 30 -36 14 8.53+1.15

8.52+0.425 (1)

8.47 -56 1303 -748 1 Jan 73

8.47 -37 1297 -747 28 Nov 74

8.46 -35 1265 -7417

8.46 -43 1305 -806 12 Oct 75

8.46 -42 1300 -754 (4)

8.46 -36 1276 -757 (2)

686 519 +143 (2)

8.52+0.425 22 Oct 72

8.53+0.415 30 Oct 72

8.45+0.372 1 Jan 74

8.50 +0.409 (3)

8.45 +0.362 1 Jan 74

8.46 +359 +439

8.46 +360

New Bern Th

15589 2 27 54 -36 14 8.9 NO

8.99 +1.15 +0.82 21 Cent 72 8.52 +0.435 22 Cent 72

8.52 +1.145 +0.88 26 Cent 72 8.53 +0.415 20 Cent 72

8.50 +1.15 +0.85 8.52 +0.425

~~+55 0678~~
~~+54 6854~~

2 39 05 +56 11 25 ROT

11.460

(A) (1)

				O.G
249	-362	844	+102	2.226	Illegible
253	-357	844	+112	2.228	Illegible
251	-360	844	+107	2.227	

800 2 42 45 444 13 5.5 Gold

VV

Agent

6401

333 K

313

327

1433 -140

452

337

-137

5.45 -166 1030 -221 2.148 226.0 0.9

5.46 -168 1026 -212 2.176 Glass

5.44 -166 1044 -240 2.141 " " "

5.45 -167 1033 -224 2.145

549 345 693 3.12 604

1046

AOL

~~4.8257~~ 2 42 00 −28 14 2.2

17(0)5

−24°07'11

6.82 −22 987 −354 2.113 15 Nov 84

6.81 −24 974 −387 2.109 23 Nov 84

6.82 −22 983 −341 2.111

485 249 522 2.580

395 425

337

8.28 +0.324 15 Nov

8.28 +0.322 10 Jan 85

8.27 +0.326

6.40 +0.253 240

8 Sta

856 (X) 2 52 05 +16 24 6.25 F5 II

1715 (X)

6.28 -428 890 -16.8 2.196 22 My 80

6.29 -420 888 -11.3 2.190 23

6.28 -422 890 -16.5 2.193 (2)

282 163 254 2.678

24 2.68

+1.06

+5905.64 02 54 20 +60 19 175 F7Ia

1997

X X

0.5

7.77 +16 801 +445 2.203 16Ber80

7.80 +18 802 +448 2.212 7Ber80 1.3

7.78 +17 802 +446 2.207

74r 1.354 2645

1.236

18145 2 53 45 GF II 6.58 +1.02

-10450

-10 07 5 1196 -472 31 Jan 52

6.55 -97

6.56 -85 1182 -460 29 Jan 52

6.54 -87 1184 -473 30 Jan 52

6.55 -88 1187 -468 (3)

334

8.42 +0414 5 Aug 52

8.40 +0405 15 Aug 52

8.41 +0410

6.03 327

(37 16.8
47

2 54 15 +57 35 6.84 GOIa

18391

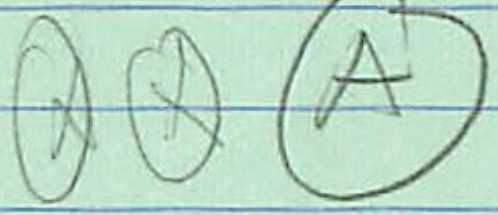
√ √

27

6.92 +573 1075-242 2.174 16 "
6.97 +567 1092-256 2.179 18 "
6.97 +575 1083-244 2.180 22 "
6.96 +569 1077-285 2.185 28 "
6.96 +571 1082-257 2.180 (4)

9/1 3 08 10 -79 04 5:56 +31

5.68 +175 1558 2.761 GO 16" 8.05 +174



60"

8.05 -418 8.69 -416 2.180 2 fast 2

8.05 285 144 495 2.662 ①

9.06 284 152 485 2.668 GO

5.67 -543 927 -47 2.267 2 slow 2

5.69 -523 927 -43 2.270

5.68 -523 925 -45 2.268

174 164 494

F2/3 5/2

21190 3 11 55 -83 37 8.2

(1) (X)

7.62 -775 943 -119 2221 22ly 20
7.61 -464 937 -134 2219 23" 0
7.67 -470 940 -129 2.220
20" 221 217 780

(2) 10.58 -334 921 -454
32 192 450

1017 ✓ ✓ 3 22 55 +49 47 1.5 FTIB

+ Rev ✓

Quarterly Forecast

1.82	-414	920	+223	2.173 BBO 80
1.84	-418	928	+217	2.176 BBO 80
1.82	-410	902	+231	2.173 BBO 80
1.83	-414	912	+224	2.174

289 184 1.155 2455 (B)

578 (271) 1097

Ry II

+64°854 03 26 20 +65 13 8.81 11.01

✓ ✓

0.9m

8.82 -13 740 +42 2.190 [illegible]

8.83 -23 802 +7 2.188 18"

8.82 -18 796 +25 2.189