

get

4.500 - 25.4

218

1.500

Drilling

Drilling 1/1. 1968 A-5 23, 560

RS In A

ford arena, J

Wise P

14 75 MW 159, 67

Wise M

0.289 9.66 0.46, 0.320 0.605 2.650

8 m 512  
8 m 30

With a *Spencer* *Warty* cap.  
Adm

GT and CN like V553 loc Carbon bed

G-3767E

V553 km

12467

0.314 8.35 0.440 0.260 0.670 2.639

582

Y 2 - 6 1/2

072

87702

V 897 cars

0.315 8.34 0.480 0.235 0.775 2.658

286.9-84

676

52214PA

~~5152~~ 5500

1537

Montegazza

-500

Pirelli B

201, 109

18

St. Paul

BP lin 880.45

Δ Bombay

0.380 2.54 0.475 0.105 0.895 2683

900

316.2 - 116

1399

1397

-15

Sw Capelin

AS 103, 1635 1992

Evans

5th - 1.88 20.3 AM

R 06E

APG 196

W. M. on 24 040

0.380 940 0.366 0.150 1025 2462  
2052 + 507 953

1460

Antonio 13 1490

Poretti 12. 234/135

+1501

-707

Reddy's - Legend

+19M

137626

L R TIA

0286 280 0.487 0.245 0.786 2.653

28184-76 914-11819 689

-529

479

56-

S-674



DT long  $\Delta B$  0.14  $f_B = 0.35$   $\Delta [G]$  1005  
 $\Delta B_{mag}$  1.58  $f_m$  907

0.39 5.80 0.350 0.195 0.925 2.648  
37 855

768 -108

~~-78~~

330

step

-64

AVLi

0.486 747 0.605 0.130 1.020 266B  
995

314.0 -7.2

-343

-356

-12

S-Exp

RT MME

L 9.007

ΔB 1.081

ΔB 0.65

ΔB<sub>avg</sub> 1.544

ΔFC<sub>b</sub> 0.070

938

0.489 8.78 0.540 0.150 0.480 2.6695

296.5-53

872

-669

12429

8.78

0.535

0.510

0.450

2.669

~~AB 2.009~~

9.00 0.560

0.160

0.915

2.662

PC 2.006

324

803

RTA  $\Delta V = 6.68$   $\Delta B = 0.848$   $f_0 = 0.53$   $\Delta FC = 0.1972$   
DBM 1.535 / 1350

938

0.530  $\Delta V = 0.465$   $\Delta B = 0.210$   $\Delta FC = 2.648$   
~~135~~ ~~747~~

127

338

Pen 2.643

3.7-98 - 4.66

sup B

hcr

46

606 125.4525  
✓ 680 135.0368  
✓ Z CMA

Stobria R 1979  
Bukura L PMAAS 109.64

0.495 9.30 0.645 0.090 1.140 2.183  
284 1.011

B(BW)  
9.267 239.9 MY

844011

505

-923

82

Strong point Camp

FN Agl

$\Delta V$   
8.35 ΔB 930

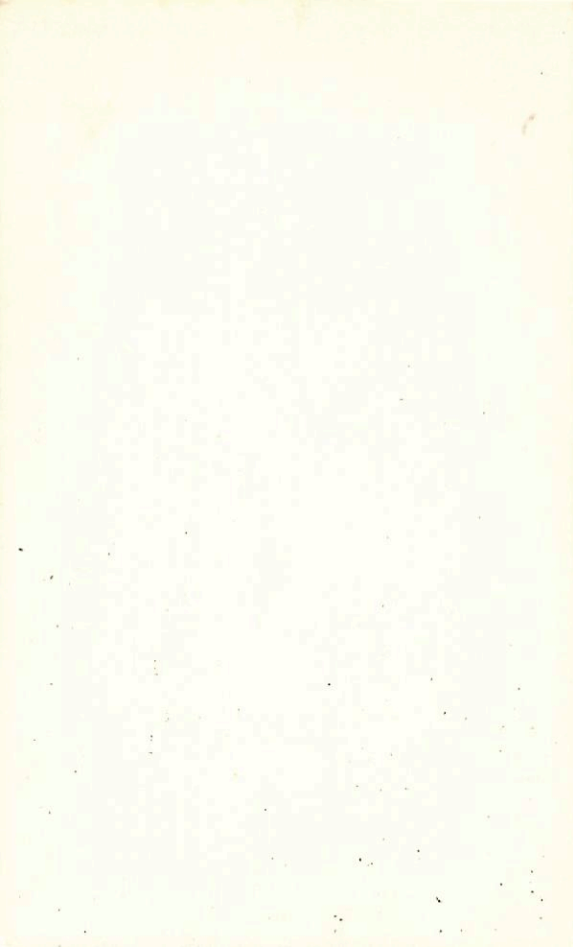
8.36 0.850 710 740  
0 (46.5) 670

0.977 8.44 0.890 0.230 0.755 7634  
352 577

39.5 31

903  
+918  
62

8.35 0.850 710 740  
0 (46.5) (607)



207 8.26  
208 8.10

SXVed

0.950 8.33 0.115 0.235 0.859 2.635

259

1185  
8.50 512 905  
118 118  
118 118

559E

per

1516

1516

1516

194  
352  
225  
511  
511  
511

171



AZ Gen

$\Delta V$  8.12

$\Delta B_{0.4}$

58 0.37

DECJ. 024

9-8

$\Delta B_{0.4}$  1.54

0.507 8.60 0.425 0.170 1.000 2.670

9.5

292.8-0.2

-477

1134

24

S-Cap

BG W C

0.524 5.50 0.360 0.195 0.950 2666  
872

3004 #3.4

766

283

+14

Funov 402 1040

AB0.74  
DB<sub>M</sub> 1.525

0.78 245

0.535 10.36 0.886 0.125 0.860 2.161

6.97

Blue Compressor

0.2.1.50

1993 ~~1988~~ 88, 88

55 Set

LV 8.23

DB 0.717

DB<sub>m</sub> 1.514

$f_D$  0.48  $\Delta I_{CJ}$  208  
8-11

0.565 8.14 0.630 0.180 0.845 2.647

270

52

3

719

B<sub>C</sub> 2.647

5

252 - 1.8

650

885

1408

308

90301

4x low 6V 882 4B 1.174 ± 0.23 4F6J 111  
4B 1.574 B

0.566 8.23 0.400 0.205 915 2.6 1.9  
~~0.875~~

325 815 835

2848 -424

40.2 -1604 +6

2661  
650  
+5

8:30 425 2.08 895

PRT Ann ✓ 20054 0.206 ♂ 0.254 0.51 1.51 1.51 1.51

0.57 ✓ 5.46 0.395 0.210 0.865 2.635  
45 786

1004 2011

8 10003 1001 2000000

9 2557 730 317

2465

111  
62

120

Q



R.A. : 6.400  
DEC. : 30.500  
R.A. : -4.500  
DEC. : -11.000  
DISTANCE : 6.200  
MODULUS : 174  
VEL. : 20.000

q1 (U) : -0.158  
q2 (U) : -0.020  
q3 (U) : 0.987  
dU : 3.962  
U : 20.434

q1 (V) : -0.443  
q2 (V) : 0.895  
q3 (V) : -0.052  
dV : -38.525  
V : -7.742

q1 (W) : 0.883  
q2 (W) : 0.446  
q3 (W) : 0.150  
dW : -39.452  
W : -3.850



144572 ✓ Q 5 Nov

0.575 8.95 0.00 0.00 0.00 2.65

0.88

0.88

0.76

0.88

0.88

6.51

1.24421

0.76

6.51

0.88

2 Hmi ΔB 0.27

AP 5 4/4 500 1993

0.554 2.04 0.345 0.248 0.463 2.636  
0 744

12.33 + 26.68

-46

+20

+37

BF  $\alpha$ ph  $\angle \alpha$  7.37

AB 0.860  
1.497

$\delta_B > 0.61$

221  
916

0.109 7.35 0.590 0.198 0.810 2.670<sup>43</sup>

697

84  
111  
20

$\rho_v$  2.644  
659

99 + 7.1

-279

1214  
+ 54

AHVH

42571

AB 0.536

1441

$f_B = 0.41$

ASTA

878  
KED

0.676 5.70 0.345 0.222 0.560 2.653

891

2624 ~ 7.0

6.5  
5.5  
1.0

S-6p

460

453

54

V val

<v> 7.58

AB 1.060  
1.475

S<sub>B</sub> 0.025

ΔE<sub>2</sub>

175  
8.14

0.641 7.57

0.505

0.190

0.888

2.635

77

939

70

318

P<sub>v</sub> 2036  
65/6  
11

V492 SW 2.97 ✓ AB 0.508 800635 AF4] 177  
1.489 850 850

0.656 7.58 0.665 0.165 0.868 2.646 ✓  
282 ✓

3594 + 0.2

0.2005  
657/16

- 972  
- 48

+ 3

G1 can <u> 8.30

68 0.463  
1452

68 = 0.251 255] 0016  
996

0.686 8.30 0.450 0.200 0.555 2.670

905

187

240.0 x 2.0 = 480

240.0

144

1162

1254

5 - 144

T Val CW 7.99

AB 1013  
1.475

FB 0.653

ΔIC Δ 9.37  
808

0.666 7.97

0.600 0.220 0.295 2.638

2.475  
6.75

2.03  
33

245.5 -3.8

Grand - Pacheco, E. 1976

787

ATA supd 25, 154

A103

273

FB 2.1035  
6.57  
1.15

Red Green minor



PY 6 Mar 6:28.09 AD 1094  
1423  
381

58070

~~58070~~ 58070  
969 159

20 0.670 8.00 0.540 0.220  
0.278 0.825 2.658

747

650 8.0 545 220 529 2650  
716

Pr 2654  
650

226070.3

916  
548  
7

ΔB1078  
145  
372

5 0.71 ΔTCJ 178  
849

S KM CVD6.59

✓

0.671 610 0.510 0.215 0.830 2.644  
728

151  
353

12

Fv 21044  
59  
14

3033+44

ATA 261, 130

Fundamental

(A) 11  
-400  
808  
454

2

Sx can 609.12 681.165 58 0.769 ΔL5J 073 /  
1.45 935

0.687 9.05 0.600 0.150 0.950 2.677  
F30

36

P<sub>v</sub> 2.650  
650  
0.200

2867 + 1.3

-573

1911 /  
F45

AP Syn  
657  
658

151  
151  
KSE109

0.820 f

651  
105

0.704 655 0.525 0.220 0.845 2.143  
829 902.0

740

151

151  
151

Ru 249  
619  
00

Pre-118

0.8

1114

22

V350 Sgn  
AB 1.087 1.45  
802 2070  
1976

0.712 7.43 0.625 0.195 0.815 2.650  
1976

13.8-8.0  
1976  
1976  
1976  
1976

1976

1976

WZlow

2.17  
9.33

AB .943  
1.475  
9B.403

ΔG .209  
4.25

0.710 9.25 0.560 0.2278 0.800 2.235  
688

499

46

2873-20

0.2.634  
1592  
10.1

0.11  
0.828

94

Ad loc 588 08.577 58.437 60.257  
587 711

0.722 5.50 0.495 0.185 0.675 2.653

526

13<sup>2</sup> (AP) BU.S 0.5 mm  
BM.

2649  
648  
TR

Fundamental

ATA 201,137



A4 len

4.17  
9.15

A.B. 8.70  
1.47  
6.03

8.57

817

0.725 8.97 0.645 0.250 0.880 2.665  
676

(A.B.)

8.97

26.229

V1162Ayd

479

117

0.730 7.81 0.580 0.255 0.750 2.63B

634

956

Handwritten notes circled in blue ink:  
K<sub>1</sub>h  
K<sub>2</sub>h

4224

627

-23

7010

4864

-364

~~Step~~  
~~12/12/22~~  
~~35/11/22~~

210  
344

DB

1286

1475  
189

f 840

Δ 6.110

904

344

0730 392 0430 0220 0870 2631

65  
984

657

DB 1.184 5.265 06.117

848

682

1475

168

Vlem

th

0.740 6.76 0.575 0.190 0.890 21.35

248

775

3164 732

585

530

hnt

<v>  
8.18

DB.433  
1.475  
1.04

4.383

DL.071  
936

V419 len

0.741 8.20 0.475 0.225 0.915 2.657  
1.475 1.20

1.475  
1.475  
3.33

1.228  
2.43

502

1252

1014

uXlar 20 8.94 5B 1.104 8.710

66 181  
414

1.471  
391

0.744 8.50 0.525 0.280 0.818 2.64<sub>3</sub>  
710

2572-37

167

2645  
cm

811E

UPL

V659 km

0.750 6.57 0.460 0.180 0.880 2672  
788

307.7 + 0.9

386

-444

410

NY Pump

0.756 5.68 0.408 / 0.218 0.560 2.66 <sup>0</sup> <sub>880</sub>

U

26.3/2.9

476

1500

113



AC 173  
853

5B 196

DB 1087  
1801 80  
1471

HL'S 207 574

1994

466  
394

0.264 5.695 0.550 0.230 0.825 2.642  
715

1.5-2.1

1.5m  
1.5m

1.5h

BL  
2.1h

DL-259  
BCL  
.788

DB 996 5B .444

CM 9.71

✓ 1.474 ✓  
476 ✓

0.768 9.68 0.818 0.215 0.790 2.444  
627

Comp

lim  
large oil  
(+)

ST Val  
MST

454

\$ Amt  $\frac{100}{233}$  DR 1.287  $\frac{50}{141}$  DC .053  
 $\frac{1.479}{157}$  852

0.777 ~~9.274~~ 0.440 0200 0.890 2636  
802

264.5 + 11.1

+301

-3435

+645

PV 500

LVD 60 1.311  
2.06 1.474  
1.63

5.861

OL 146  
874

✓  
0.783 6.97 0.1649 0.185 0.865 26.54  
255 137

347

3504 + S.D

2661  
48  
+16

-787  
-133

+74

207	1.093	8	0.207	80	243
207	1.474	8	0.800	80	800

FMH 1/4

18  
3

0.786 8.20 0.500 0.155 0.820 2.657  
1040

44.3 + 0.9

10.80  
4562

13

684 <u>684</u> 681190 50 220 ΔG . 201  
1474 831

S T A

14

0.801 6.80 0.485 0.260 0.770 2.645  
78 679

18

2.649 3221-82  
6494 5075  
535

1222

55 FOR 94h

922E DEC ASE 999 949

DEC

DEC 059

922E 944

922E DEC ASE 999 059

944

922E 944

944

922E 944

~~922E 944 059 944~~

~~922E 944 059 944~~

922E 944

922E 944

922E 944

BB 944

<V> 7.94 801359 5900 0930 918

AJ Camp

1472  
1115

0824 7.94 ~~0.468~~ 0.226 ~~0.770~~ 2.640  
161 752

~~2543 1.1~~

0.44 <sup>500</sup> 230 910 2.643

July 6  
1050  
148  
380 741

1545 389 727  
0.515 235 831 2.640  
7.64  
1060





607 40 1130 5.728 66 209  
671 1471 825

WGN

0.829 668 0.750 0.205 2640  
322 675 675 2636  
451 675 2636

13.7 - 4.1

550 671 0.255 240 765 2636  
2245 966 614

4130  
- 44