H4153 ✓ 6 19 35 +07 35 8.46 +87 A5 II

8.51 -463 853 +579 2.274 Wder 79
8.48 -457 846 569 2.223 8 "
8.50 -460 850 574 2.274

241 127 1.516 2.228

256176 6 21 40 +09 10.5 955 +12 B2 F/V

✓✓

957 -547 752 -587 2.166 10 Dec 79
1000 -559 747 -553 2.168 11 "
958 -563 750 -570 2167

E_y +233

143 35 336 2647

t_0 9.0

✓ (78) 307 463

h_v -2.6

11.6

+10° 11'4 10.21+05-54

256351 6 22 10 +10 335

B +14'

046 074 040 233 312

10.21 -558 759 -167 2.156 21h 7 s 60"

10.22 -599 765 -166 2.159 22"

10.22 -602 758 -166 2.158

092 233 21.53

F.y +150

11.55

44965 ✓ 6 24 05 +11 41 7.82 +31 -41 B3II

~~2L4 +11~~ ~~S.C.4305~~-76

7.83	-478	682	-621	2.170	4 Jan 80
7.84	-423	687	-625	2.117	5 "
7.84	-420	684	-623	2.117	

~~7.84~~

Δ_v -4.05

~~H.6~~

257746 ✓ 6 29 48 +09 49 9+ 05 III

9.88	-589	747	-598	2.189	6 Jan 80
9.89	-553	771	-612	2.200	
9.88	-591	759	-605	2.194	

100

= +150

9.15

10.1

258883 V/6 30 10 +09 45 8.83 83 IV

8.48 -.633 765 -.619 2.123 6 Jan 79

883 -.624 757 -.639 2.127 8 "

886 -.628 761 -.624 2.125 E +157

065 045 275 2.656 V_0 8.2

(065) [262] (392) M_V -2.1

10.3

B5 III

258985 ✓✓ 6 30 25 +04 44.5 9.68+03

9.67 -622 750 -237 2.240 10Dec79
9.67 -628 802 -236 2.252 11Dec79
9.67 -625 796 -236 2.246

E_y +120
068 077 680 2.741
V_0 9.15
118 (057) (666) (86)
36 M_V = -0.6
9.75

9.21 +20 -23

2460 1278 6 30 35 +06 11.8 BOV

258872 ✓ ✓

Anda

9.24	-486	682	-903	2.130	7 Jan. 80
9.23	-455	698	-913	2.1228	
9.24	-490	690	-908	2.128	
	203	-012	116	2110	

3.25

1.1

140BI9

76489 √ 6 32 50 +04 41 7.7 BI II

223 -369 651 -855 2093 5 Jan 80
225 -360 638 -874 2099 6 ...
224 -364 644 -884 2095

[illegible]-044 [illegible] 2.524

B3 18

258765 ✓✓ 6 33 10 +04 45 9.91 731 -50

9.96 -431 687 -613 2.145 7 Jan 50
9.55 -432 700 -635 2.1416.8 " "
9.56 -432 693 -624 2.143

266 -609 257 2134

E_γ +360
V_0 8.70
M_V -3.15
11.55

46559 ✓✓ 6 33 10 t02 24.5 8.4885-8-II

8.16	-227	669	-199	2.131	4 Jan 80
8.17	-223	625	-189	2.150	2 Jan 79
8.14	-240	692	-218	2.144	8 "
8.16	-230	672	-202	2.142	

480 -231 716 2.624

2622

m_V -3.0

24.2 +08 26 LS IV

255554 ✓ 6 33 35 +08 22 9.21 +06

9.23 -580 734 -720 2.12.5 Jan 80

9.23 -583 745 -739 2.129 8

9.23 -582 740 -730 2.127

E +213

109 033 11.8 2614

V_0 8.3

M_V -3.3 5

11.65

46711 ✓ ✓ 6 33 55 +02 47 SDB3IG

9.10	-38	646	-580	2.138	Wheeling
9.08	-40	633	-571	2.13[illegible]	8 "
9.09	-39	639	-576	2.137	
683	-067	330	2.607	V_0 5.75	
(137)		(153)	(467)	m_V -3.55	
				5.70	

$E_w = 0.780$

46783 √ 6 34 35 TOG 52 79 OBI6

8.07 -437 745 -80 2.1169 GPa 74
8.03 -432 734 -70 2.11068 " "
8.05 -435 740 -75 2.1168

8.01
267 626 847 2646
(106) (554) 1006

-2.45

46483 ✓✓ 31.VI

6 35 00 +10 18 7.80 -141-45

780 -342 683 -780 2.109 4 Jan 80
780 -345 682 -784 2.105 5 "
780 -344 682 -782 2.107

Eq 085

358 -019 116 2.551

(088)

[illegible] 405

11.5

46[1] 1303 ✓ 6 35 90 406 06 81 B2

46966

6.89 436 711 ~~968~~ 2.100 14 Jun 80

7h 07 +6° 13' 08 Cr 106 + Mesh ✱

~~260 57.4~~ ✓✓ 6 36 05 +06 04.5 258-03

47088

Unter?	7.59 -640	755-871	2.129	
Nift.	7.59 -638	729-857	2.127	4 Jan 80
	7.62 -646	730-858	2.130	5 "
	7.60 -640	730-858	2.129	

E -4.28

male C:5 1 8

map 2.0

Fr 3's 40 with -2.86 M_v

→ 9.86

47107 V/ L 36 10 405 49 8.01-03

8.01	632	729	814	2.136	4 Jan. 80
8.01	645	743	826	2.137	5 " "
8.01	638	736	820	2.134	

145

(1)

47240 6 36 50 +04 58.5 6.28176

6.19 519 714 -890 2.091 Ledderz

E_y = 300

300

.02

V_0 4.9

179 -027 012 2.571 a m_v -5.15

6.16 180 -033 013 2.565 Cap 10.05

6.19 179 002 006 2.556 Egg

6.18 179 -020 010 2.564 (3) (034) (-026) (042)

260986 √ 6 36 55 +09 54 9.72+33-35

√ 9.75 -412 704 -607

9.80 -413 713 -439

9.75 -409 704 -599

9.77 -411 707 -603

2207 53480

2177 81

2185 9

2290

Ey +382

Hil 591 10.04 -592 945 +32 2.377 23480

8.15

1.4

M, -1.15

(048) 277 4120

BD.5 I

47810 W 6 37 20 +04 88.5 8.19-13

8.25 -510 701 -829 2.099 6 Jan 80
8.26 -527 713 -821 2.105 8 " "
8.26 -516 707 -825 2.102

176 005 851 2.582

F 1.260

(558) (02)

A_V -4.3

11.3

47984√ √ 6 40 25 +06 08 6.8 A0FG

7.03	-470	749	+319	2.203	4 days
6.98	-473	737	337	2.198	8 "
7.00	-472	743	328	2.200	

228 029 1262 2.686

48717 √ √ 6 43 50 +03 42 8.1 B2 III

A 6120 6" [illegible] not [illegible] Bamberg

9.29.9

765 -515 722 -626 2.145 Coddler 76

761 -522 722 -619 2.147 8"

763 -518 722 -622 2.146

Eq= +0.75 6 180 009 282 2622 No 6.4

063 246 372

Mv -3.2 5

6.7 0

48414 √ 44 45 +02 31 28 B 5 II

Var? √ √ 034 034 405 2.94

727 -666 768 -467 2.123 (date) 79

713 -657 754 -500 2.098 8 "

723 -657 738 -466 2.086 4 Jan 80

Var 727 -657 741 -464 2.097 5 "

7.15 / 7.30 722 -657 744 -466 2.092 (3)

028 035

(73)

263650 ✓ 6 45 15 +03 39.5 9.77 +12 -49

261807 ~~9.31 +03~~

9.77 -574 758 -507 2.149 8 Jan 80

9.74 -562 753 -503 2.150 9 "

9.76 -568 750 -507 2.150

123 042 356 709

m_v -2.9

11.8

+15 0 14 03
24.3775 6 45 50 +5 38 10.52 +19 -62

136 136

10.49 -508 715 -26.0 2.148 21h 79
10.49 -499 709 -26.2 2.143 22 79
10.49 -506 718 -26.1 2.143

F ×301 193 006 134 24.36 9.2
-7 -2.4
11.6

052 069 954 2.644
450 049 / 050 058 / 65 984 / 988 2.647 2.645
(80) (978)
1138

4.4
-2.55

F_y +026

-050 058 425 2681

510 -059 045 441 2654

085 976
082 -104 -071 2.718
090 005 -007 -071 2.552

6.57 142 -028 1255 5526

142 045 1052 2.649

6.54 4.33

143 035 1.254 2.715

(078) 1.226

+143

1.392

5.95

new
Cp to A 2
Ey +198

V_0 080
-0.45
11.25 123 083 569 2240
(040) (544) 725

11.62 -572 770 -344 2236 152180

106-B 10.55 519 (107) (482) 465

Eq x16 11.3 063 079 501 2.027

11.27 -601 798 -410 2.025 152680

A

174 (62) (150) (275)

E_g +16.0 V_0 8.4 / 10.75 058 045 162 2642

5.08 -634 761 -735 2.15 15%

~~Spt 6~~ Ch 106

~~+6" 1303~~

Eg +186   9.6   +2.1 / 11.7   258 / 186   (070) / 043   202 / 219   (340)   2653

1   10.39   -607   759   -691   2.164   142180

Eg +168   9.1   -1.65 / 10.75   071   (042) / 041   (214) / 228   (336) / 2656

2   Eg +160   9.53   -622   756   -674   2.195   142180

10.5 / +0.15 / 10.50   354 / 118   (131) / 096   (795) / 814   1057 / 2.806

3   11.37   -577   816   -102   2.292   142180

Cr 106-2 +46° 1308 6 36 05 +6 045 8.5 08

Eng 180 40 6.80 042 (03) 040 (019) 025 120 26.01

10.38

7.59 -6 44 755 -871 2.124 15 2680

= 4708

11 55 +10 11 58 6 23.5 +10 09

2358686 6 12 27 55 +10 06 9.7 B7III p

6 29 45 +10 06

Chart ?

See draw ~2" NS

~1 mm

ADS5139

||

9.8 - 11.5 J690

1.5

16497 AB 8.6 - 5.6 1.6"

AC 8.6 - 5.6 8" 57°

14740 8.3 - 13.7 1.6"

38411 9.1 - 5.1 2.1"

48099 07 V

2244

A 542,923

4582G

ROI ab

246095 B1V

264862 E76 +0F B1.5

26/307 931 B5 IV

47417

BO

47395 Bo.5V

4738 ✓ B 0 II

261071 B2 III

47032

80

4(8(?)

B0.5

46847 B0 III

258691 9-711+57 09 VI

636072 7 47 25 87 87.5 8.34 od

-30°35'22

Double "
Rg
Bm NO.