

20 80 50 5 ✓
20 20 20 20
50 50 50 50
6.9 6.9

82626
97728

488041-

8472 135 154 531 21278
665 475 145 531 599

AD

86358 9 54 40 69 055 B95 67

4/8/11 ? (X) P

687-728 REC-689
824-828 REC-23236
24 24

80029 9 54 50 - 8 44 6.5
63

62008
L3C208-

6.69-51.3 932-121 2251 26 75

X

(1)

SHCCB
)

01 00 55 -28 65

Aug 87 B4

7.01 - 245 935 +17 2.311 20 mm 5
7.00 - 246 945 -4 2.322 248 5

87130

✓ 190 01 40 -20

19.5 / 19.5 (6.9 AD)

7902867

6.83 593 868 +147 232155
2024

⊕

87019 ✓ 10 00 45
61028 10 00 45 -23 42.5 (6.8-6.5)
-23892

⊙ ⊙

681-115 1122-452 2645

87652

10 04 15 -51 13

6-6-2 89

7.3

7.5

0.3

✓
6.27

718 818 -184 2.285 19mms

97627

W

04

25

42

04

65620

655-93 1180-438 20 mm 76

8) 556

10

64

25

-25

86

6-84 AD

28

6-94-687 813

+184

2.343 19 mm TS

810

0"4

7.1 89 IV

88572 10 09 50 -67 10

1601194

4511092

①

6.92-635

132855

①

97419 10 10 25 -18 57.5
20 mar

87

624 +351 1160 +10 +10 20 mar 85

78352 10 09 25-47 55 683 120

686-184 1075-395 15 MMS

88,976.

10 14.0 -41 36

6.55 ~~6.55~~

~~ADT/A~~

20

6.55 - 597 897 +33 2.319 8 Jan 84

6.56 - 597 900 +14 2.319 10 Jan 84

6.56 - 597 899 +24 2.319

685C9 71 2h- 00 h1 01 19588

6.74-204 813 -20 2.324 14 marks

89518

-6401238

10

16

55

-65

20

6.9 $\frac{A_{11}^2}{W_{11}}$

DD

6.81

-572

-

18285

89263

11 17 50 717 485 662AD

688-682 878 +137 2385 19 Mon

099 42 42+ 55 C1 01 4534
CA1

51 284-486 1419 5014 62.7

89044

10 13 20 - 67 57.5

- 6701239

6.4 B6V

(1) (X)

6.77 - 6.61 - 13 24.5

6.59 A2

10 20 15 -13 41

95246

6.57 137 871 +180 2.349 20 mmf0

8999 10 21 10 504 04 4646 NS

6.66 + 265 1430 - 280 19 mm 15

6-56 10-
51 50- 50 02 01 02C58

58mm 02 844-448 20mm 85
15451 5A2+ 999