

BPM 47268

.807 143 BPM  
.83 144 8-  
815 141 818 142.5

1 36 52 -21 16

LFT 143 ✓

1 85.7 -21 24 13.7 +2

L654-14

12.0 12.9 k

G-272-58 Again ✓

40x

x

11.07 +0.515 2500  
11.07 +0.495 2700  
11.07 70.50

6272-58



GL 2050

LFT 153

1 39.8 +20 02

H50279

5.25 +0.85 +0.28 (2)

HR 493

4.88 +0.29 (2)

107mc

X

VM 47

62-18-238

LFT 155

40.2 + 63 35

620229

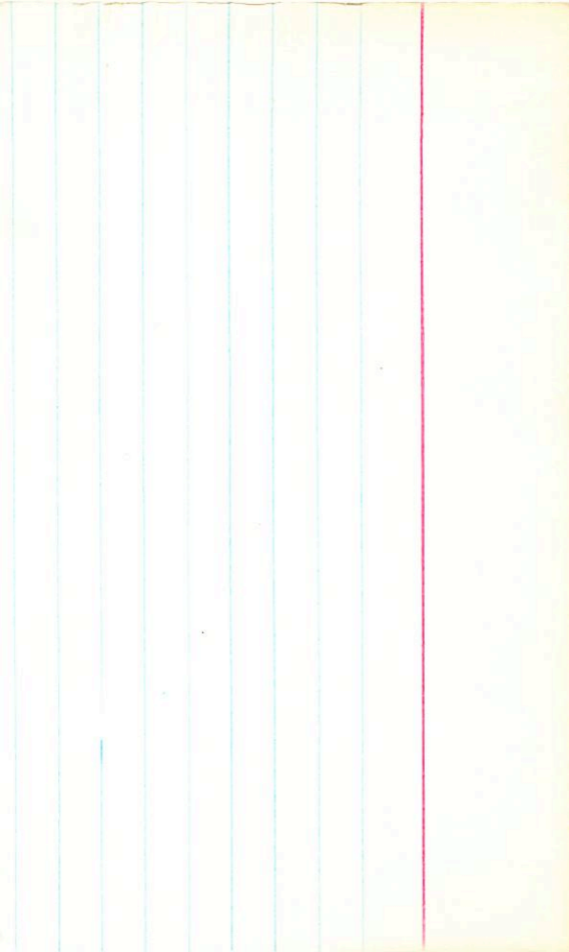
6244-33

073 (52)

8.40 + 1.22 + 1.12 (2)

7.65 + 0.48 (2)

172 218 6



662339  
X Eni

Do RI

LFT169 1 540 -51 57

K

HRS66

370+85 +46  
(slit)

52 17  
main

332 +308

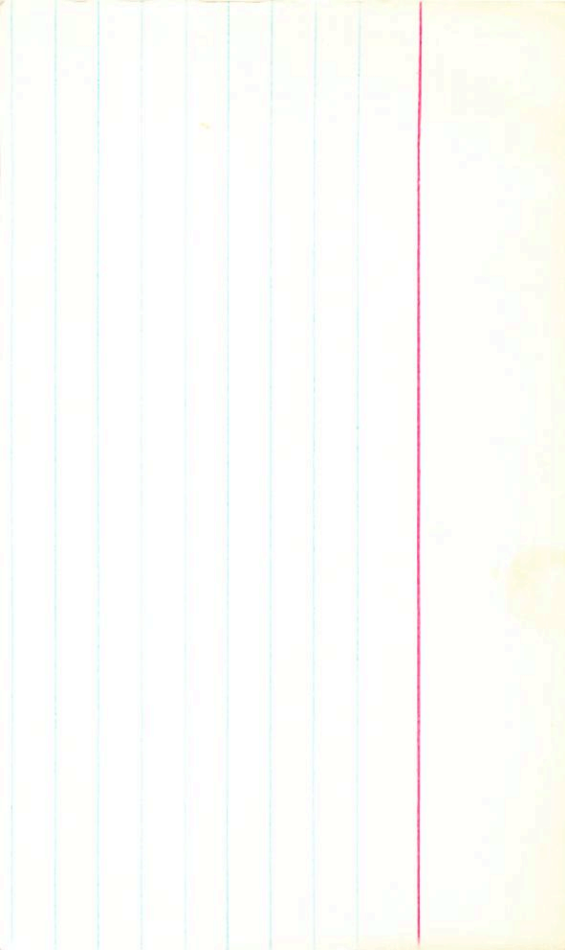
354

330+31

3.02  
X

~~330+31~~ → 46

466+245 -6.3



Alg 2 +40545-234

1 42 06 +4 12

.88 2056

✓ 1 40.9 +4 05 B.1 +1

G-3-14

415-740 m H  
meth

112 (3)

✓

9.78  
9.77  
9.74  
9.76

+1.015 230g77  
+0.565 256g76  
+1.015 140g77  
+7.00 (3)

+



G3-14

— • —

woef 1530

LFT 160

G3-17

gwh

1 43 38

1 42.8

12.65

12.58

12.56

12.60

X

+16 13.5

+3

+1.30 23 Aug 77

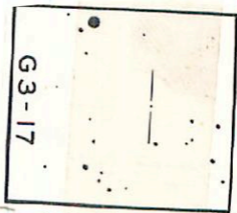
+1.285 13 Dec 76

+1.295 14 Aug 77

+1.29 ③

183 2426  
178 242609  
805 211

G3-17



R020555

LFT166

G271-168

1 50 35 -10 55

✓ 1 49.3 -11 03

Sd +9.55 L+M

IT 089 IT<sub>A</sub> 0851m

$$\frac{K_n}{T_n} = 42 !!$$

760

✶

Radial Vel.  $\frac{1}{5}$  10<sup>18</sup>  
Sun from Ap  $\frac{1}{5}$  10<sup>18</sup>

1.8  
-11  
573 0.7  
-510

(0)

.805 132.5 G

136.72

11.3 12.2 MY

10.66 +0.92 256076  
10.70 +0.96 281277  
10.68 +0.94 (2) 2991

G271-168



✓  
1 55 35 -36 22

LF1170

1 54.5 -36 29 138 m

h489-12

Requiere

927

15

05

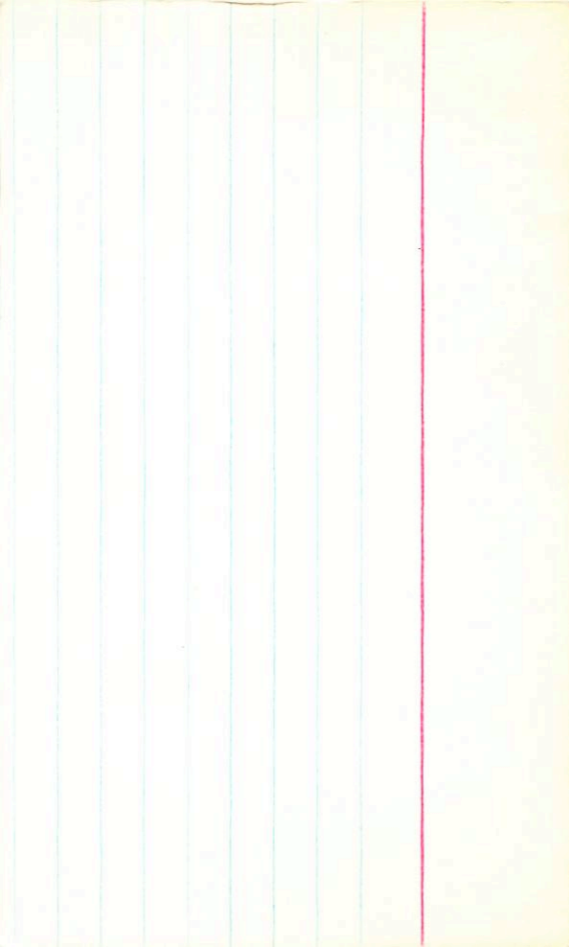
(00)

12.80 +0.50 22m.8

12.75 +0.52 3m.77

12.78 +0.51 (2)

x



159 68 -27 27

0.923 1850

158.0 -27 34.1 14.6 15.5 k

LP 484-77

5

-72  
-200

4.6

0.0

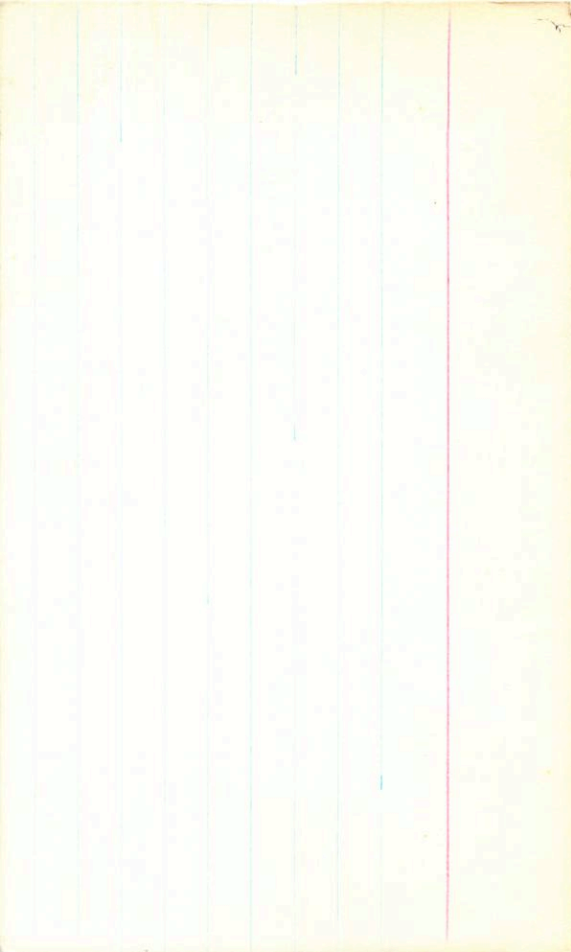
13x1

①

13.72 + 0.66 24/2/76  
13.69 + 0.69 23/2/77  
13.70 + 0.675 ②

+





Ross 17

LFT 184

2

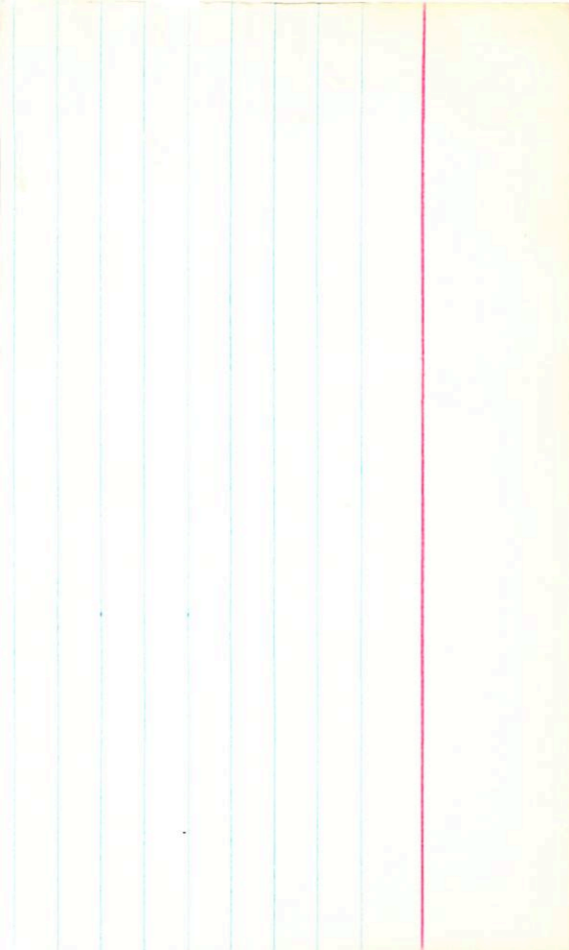
07.1

584

~~12~~

15.4

C74-4



✓

1 55 34 +3 25

176 100 G  
182 55 LP

G-71-45

1 54.3 +3 17.5

16.2 #3

17.9 15.7 k-m

40

1365 +1235 230477  
1362 +1223 130476

1361 +126141477  
1363 +124③

x



X

1 55 49 + 12 09

.71 176 6-

G 3-29

1 54.5 + 12 01.5

16.3 + 2

+ 028 - 697

Stund

14.85 + 144 + 101<sup>Stund</sup>

(14)

0.013 ~~1003~~ Stund

38

14.07 + 0.605 13 Aug 76

14.01 + 0.63 23 Aug 77

14.04 + 0.62 (2)

X



G3-29

✓  
C159-34

2 03 10 -2 00  
02 01.9 -2 07

86 2236  
826 225LP

15.6 +3

12.9 15.0 mm

12.41 +1.215 131/10/76  
12.45 +1.235 23 Aug 77  
12.73 +1.225 ②

+



G159-34



LP 645-66/67

430

2 11 18 - 8 10.5

2 10 03 - 8 17.9

12.1 13.1 4

12.2 13.2 4

450 1.5

10.94 + 0.93 17 Jun 76

X

0.259 2250

WAG 3455

LP. 865158

2 12 50 -25 37

X

LFT 191

2 11.5

-25 47.3

L584-7

1360

12.8 14.2

12.65

+0.368 10 Sq 880

LP 829-30

12.64

+0.36 23 Aug 77

+ 6R

12.79

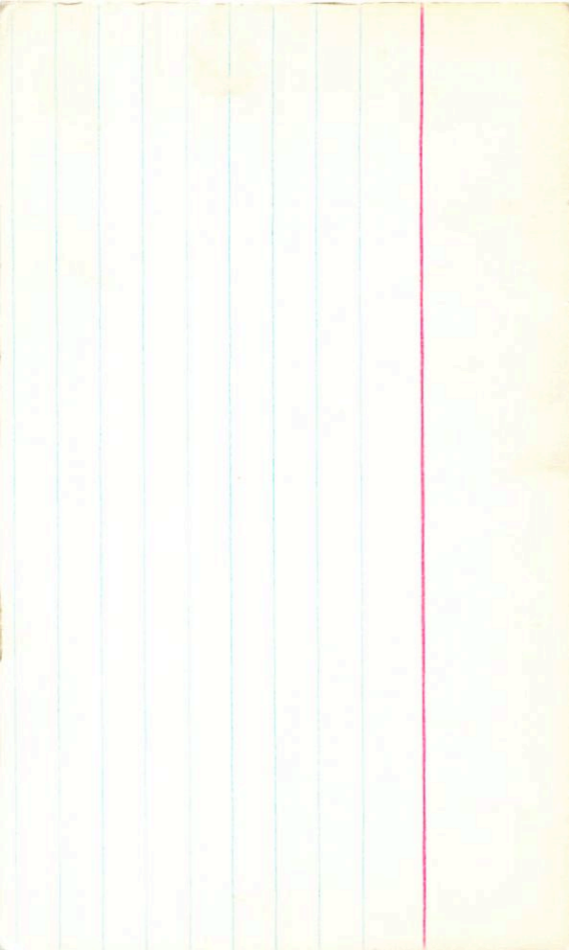
+0.385 13 Aug 76

12.67

+0.365 14 Aug 77

+0.364 (3)

X



LP, 945 1060

2 12 41 -32 08

LFT 153

2 11.6 -32 15 ~~Ham~~

-320828

10.7 11.2 R

454.1 105 (6)

4771 -548

644

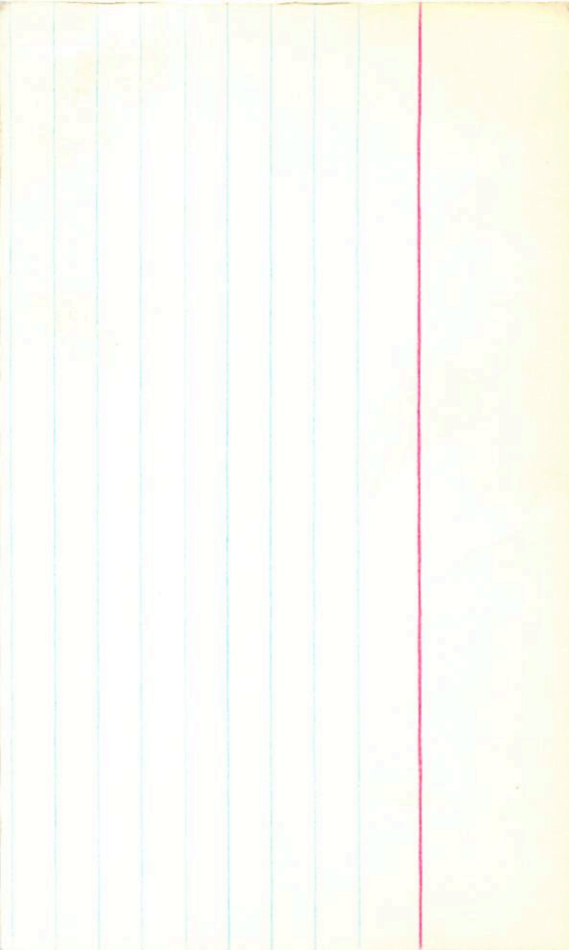
9.21 +0.94 23 Nov 77

9.23 +0.92 26 Nov 77

9.24 +0.94 14 May 77

9.24 +0.935 (3)

X



G159-50

GC2694

LFT 154

-10306

+995-78 06

1013(22)

G2V +192

~~848+0.48~~

942+0.22(2)

2 13 23 -1 19

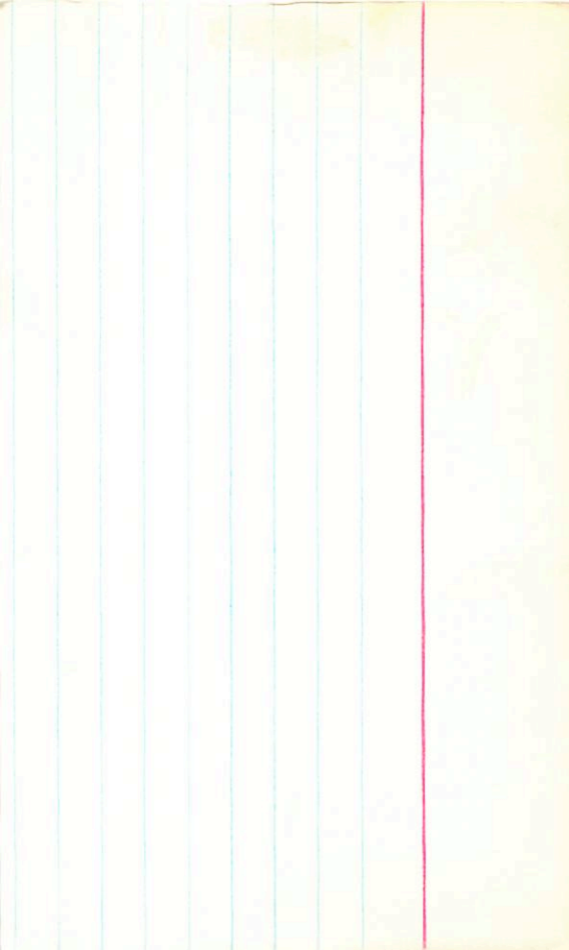
2 12.1 -1 26

9.10 +0.58 -0.08 (2)

RT

x





✓

2 10 46 -63 21

LFT188

2 10.1 -63 28

135 m

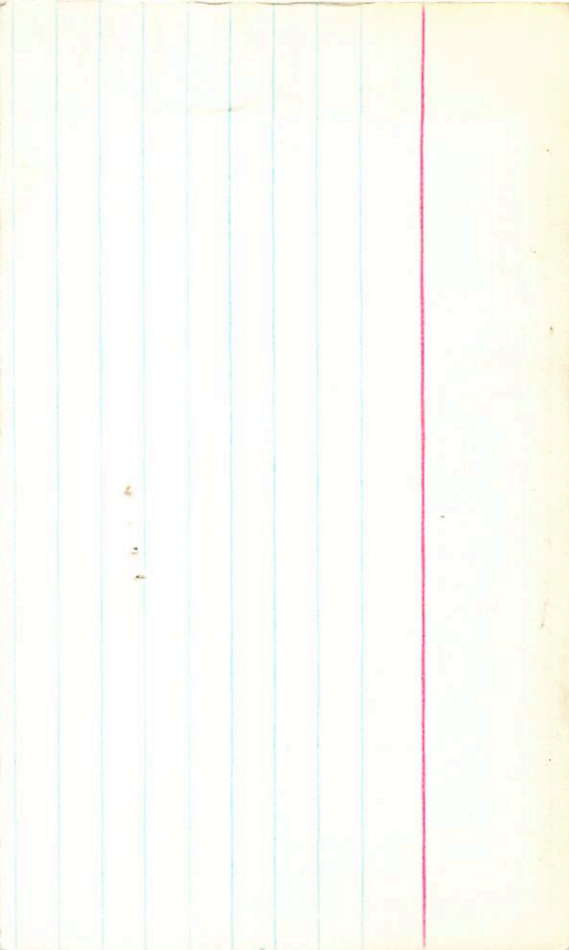
the obs: 15-5217

289242 15-9217

apls

10.97 +1.05 17 Jan 76  
11.06 / 11.01  
+1.06 28 Aug 77  
+1.05 55 2

... ✓



N



2510

PEEL

10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20