

184499

19316

43305

604

32.3474

664 347 676 - 472

2468

47

382

6. 64 889 144 315 2.576

60 251

144

-0373 4225

4378  
814  
4.3

-4169 225

566  
218  
424  
8  
1668

R.A. : 19.500  
DEC. : 33.100  
M. R.A. : -560.000  
M. DEC. : 225.000  
ISTANCE : 2.300  
MODULUS : 29  
D. VEL. : -166.800

q1 (U) : 0.396  
q2 (U) : 0.831  
q3 (U) : -0.390  
dU : 6.398  
U : 65.226

q1 (V) : 0.283  
q2 (V) : 0.294  
q3 (V) : 0.913  
dV : -315.941  
V : -161.421

q1 (W) : -0.874  
q2 (W) : 0.472  
q3 (W) : 0.119  
dW : 2445.842  
W : 50.693

184598

19 336

42 58

G0(V) WF6/17

439036

P 1/20/17  
P 1/20/17

C-band yields C13; probably wear  
lined but might be composite

+0104 -0334+C

+154  
-35

+114  
+113-035

4205

R.A. : 19.550  
DEC. : -42.900  
PM. R.A. : 154.000  
PM. DEC. : -35.000  
DISTANCE : 4.250  
MODULUS : 71  
AD. VEL. : 0.000

q1 (U) : 0.406  
q2 (U) : -0.174  
q3 (U) : -0.897  
dU : 245.942  
U : 17.411

q1 (V) : 0.275  
q2 (V) : 0.960  
q3 (V) : -0.061  
dV : -12.160  
V : -0.861

q1 (W) : -0.872  
q2 (W) : 0.222  
q3 (W) : -0.437  
dW : -502.815  
W : -35.597



184511

1.378  
777  
138

19 338 39 57

G5W t/p

-40,13389

96506

277

-0072 -0534

265

798133

quite extreme wear - lined stair  
~~on stone overlap~~ Ca H+N yields F0/2;  
lines seem somewhat shallow as if  
washed out especially Hβ; spectrum  
similar to Hδ 0.69.

-025

-026 -055

101.6  
101.7  
123.2

-34  
-55

6.05

104.0

184672 10.57 111 151 1.132 2.882 10.55

-36,13609 9.05 089 112 886 2.836<sup>75</sup> 10.5

184690 9.77 214 142 709 2.741 10.9

1.42 151.12  
3.15 1.16

9.65 0.94

1.5

R.A. : 19.550  
DEC. : -39.850  
M. R.A. : -34.000  
M. DEC. : -55.000  
DISTANCE : 6.050  
MODULUS : 162  
D. VEL. : 101.000

q1 (U) : 0.406  
q2 (U) : -0.126  
q3 (U) : -0.905  
dU : -17.481  
U : -94.257 *107.4*

q1 (V) : 0.275  
q2 (V) : 0.961  
q3 (V) : -0.010  
dV : -284.657  
V : -47.190 *212.0*

q1 (W) : -0.872  
q2 (W) : 0.245  
q3 (W) : -0.425  
dW : 44.019 *103*  
W : -35.780

8.05 934 147 848  
(437)

R's ~~top~~ NO

184711 557

19 33.8 -89 51 and F

19.55  
-29.85  
-34  
-55

10.0  
+119

806 934 147 848

FM 15

8.00 +1.86 +0.88 (5)

7.23 +0.60 (2)

(104)

WUP  
4/2/20

6058.800

+119.06

685 75  
0.055  
0.025  
10.10

1041 -052

10359 806 147

-0022-053

4+12 FEB 4

0.2

-0252

437

-026-055

S (day) N-M

1 6

144441

184711

144441

+115

665

10 -26

+20 -26 0

11

E (day) +15 -20

101

6.95 494

656  
575

11.144

184711.000\*

19.000\*

33.800\*

-39.000\*

-51.000\*

-0.026\*

-0.055\*

10.400\*

892 1202.264

119.000

-0.018

-0.904

-129.051

-0.284

-0.009

-343.068

0.044

-0.427

2.090

655  
605

-435

184711.000\*

19.000\*  
33.800\*  
-39.000\*  
-51.000\*  
-0.044\*  
-0.052\*  
9.000\*  
630.957  
119.000

-0.055  
-0.904

-141.975

-0.294  
-0.009

-186.632

0.122  
-0.427

25.998

184711.000\*

19.000\*  
33.800\*  
-39.000\*  
-51.000\*  
0.000\*  
-0.052\*  
9.000\*  
630.957  
119.000

0.031  
-0.905

-88.172

-0.237  
-0.010

-150.722

-0.060  
-0.425

-88.632

9.8  
9.12  
-79  
-216  
-105

84 10.4  
478.6 1207

-83

-70

-114

~~280~~

-123

831  
-93.5  
-110  
-783

1009  
0.96 1.986  
109  
R.A. : 19.550  
DEC. : -39.850  
PM. R.A. : 1.420  
PM. DEC. : -51.120  
DISTANCE : 10.400  
MODULUS : 1202  
RAD. VEL. : 101.600

q1 (U) : 0.406  
q2 (U) : -0.126  
q3 (U) : -0.905  
dU : 32.547  
U : -52.835

q1 (V) : 0.275  
q2 (V) : 0.961  
q3 (V) : -0.010  
dV : -231.537  
V : -279.398

q1 (W) : -0.872  
q2 (W) : 0.245  
q3 (W) : -0.425  
dW : -63.811  
W : -119.891



184774

19

374

-44 01

A35 (II<sub>0</sub>)

-44963

Friday early wear-lined

rather than lumines (normal H lines)

4.5

+0028-015-1+c

t34

t030

[+028-017]

→7

7.1

R.A. : 19.600  
DEC. : -44.000  
M. R.A. : 39.000  
M. DEC. : -17.000  
DISTANCE : 7.100  
MODULUS : 263  
D. VEL. : 0.000

q1 (U) : 0.416  
q2 (U) : -0.187  
q3 (U) : -0.890  
dU : 70.419  
U : 18.522

q1 (V) : 0.267  
q2 (V) : 0.961  
q3 (V) : -0.077  
dV : -41.907  
V : -11.023

q1 (W) : -0.869  
q2 (W) : 0.205  
q3 (W) : -0.450  
dW : -132.141  
W : -34.757



+1603524

19 36.0 +16

~~41~~

N3E<sub>1</sub>

22207

P-V

V-I

-387 km/sec  
0.06

8.48

+1.80

+1.49

M<sub>v</sub> ~ -2.4

1510 ps

+023' -037 Y

-6 + 5

+017 -032  
0001

+0010 -029

+0012

+0008

-034

+413 +685 -600

+270 +537 +798

-870 +467 -37

+0282 -0942 / -0660

+0184 -0738 / -0554 +0010

-0594 -0677 / -1271 0

-99.7 + 232.2 = +132.5

-83.5 - 308.8

-191.9 + 14.3

-352.3

-177.6

C19244

19 346 716 (f -280.9

264 2760

11.15 0.66-01

-151-185

151

185

540

698.5

Q.N

R.A. : 19.600  
DEC. : 16.200  
R.A. : -199.000  
DEC. : -185.000  
STANCE : 5.400  
ODULUS : 120  
VEL. : -280.900

q1 (U) : 0.416  
q2 (U) : 0.679  
q3 (U) : -0.605  
dU : -972.553  
U : 52.900

q1 (V) : 0.267  
q2 (V) : 0.544  
q3 (V) : 0.795  
dV : -719.142  
V : -309.848

q1 (W) : -0.869  
q2 (W) : 0.492  
q3 (W) : -0.045  
dW : 355.583  
W : 55.453

475

483

-332

474

35.9

+16 42

-3876<sup>1/2</sup>

+16 3524 19 36 52

+16 45 9.48 +150

B✓ RV✓

960 + 201 + 2085①

+023 -037 = 6 4

-6 + 6

+017 -031

+020 -023

+023 -029

keep at ✓

Var?

10.0

+014 -029

0.000\*

19.000\*

35.900\*

16.000\*

42.000\*

0.023\*

-0.029\*

10.000\*

1000.000

-387.000

-0.049

-0.599

182.983

-0.045

0.800

-354.287

-0.162

-0.041

-146.791

232078

19

36.0

+16

412

128 IP

+1603924

861 + 2.02 + 2.09 (2)

7.38 + 0.865 (2)

-38707

707

106

5.35  
11.5

+0014

+0009 -028 Yob → FRY 5.

10.87 memb.

+0010 -030 members

10.87

+0002 -026 FRY AGR

+0009 -028 FRY memb

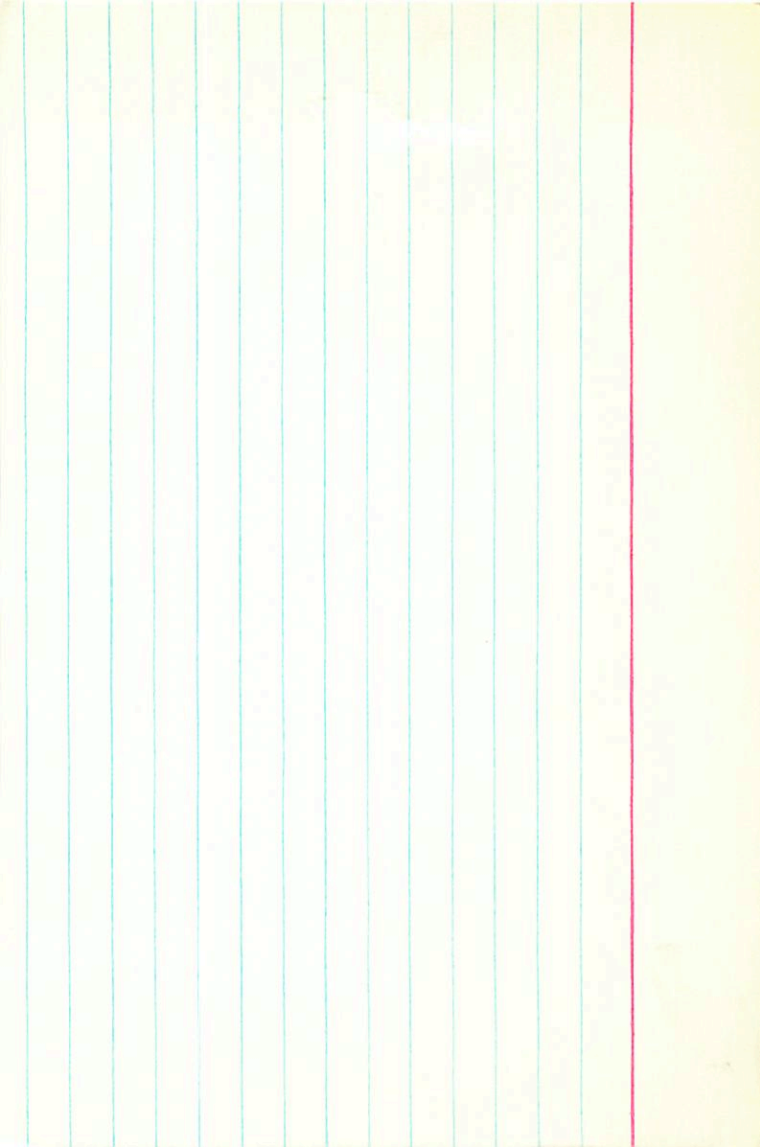
FRY memb

+013

+010 -030

+000





184768 19 33.4 -60 01 dby

2.57 + 0.67 + 0.15 @ 4.50

-55 -116 -62

-89 -186 -81

-14.1

-.004 - .386



467  
212  
310  
916  
2

4605 + 394

10013  
81

TO 0010 TO 0409 & 4 + 5.7a

7 20

504  
492  
492

120

4.0

421 TO 225

427 TO 225 24

436 TO 225 35

470 TO 225 + 79 35

145734

7478

~~1474~~

4494

250.00  
4

888  
MAY 8

48 III-IV

15 374 430 02

228

45-48 42-45 41-42  
1.154 844 206

47376

7408  
145351

19 851 244 34 120 III - IV

5.19 + 0.93 70.6 F

7478.000\*

19.000\*

37.400\*

30.000\*

2.000\*

0.005\*

0.039\*

5.000\*

40  
63 70.8

100.000

5.000

0.158

-0.422

47 +9

13.129

0.069

0.904

49 +10

11.4  
12.016

0.070

0.069

45 +5

7.424

6627364 = 17492

Ben 51

1.42  
1.47

12889 19 41.8 + 33 22 1560

$\Sigma R$   $R-I$   $M_V(M-B)$   $M_V(R-I)$

17494 A	5.01	+0.45	0.00	0	190	+7.0	+7.0	6.5
B	8.55	+1.04	+0.90	+0.2	7.5	+0.38	+7.0	7.5
12889 AB	7.64	+0.58	+0.78	+0.2	7.14	+0.37	+6.85	6.05

70%  $\pi(17494) = 0.049$   
 40%  $\pi(12889) = 0.0485$

8.55 7.5  
 1.74 7.2  
 1.94  
 1.9

Ben 51's  
 +4.72e  
 +0.012 -4.440

23/p2

12889	17494	243.55	2150	Baye (1955)	$1.6754 \times 10^{-4}$
365 (12)	43 A (28)	224.68	2048	Rabe (1948)	$1.7017 \times 10^{-4}$
42 A (20)	50 M (10)			$\pi_3$	$1.14084 \times 10^{-4}$
37 A (8)	56 Y (6 (12))			$M_{\text{sum}}$	1.47
34 Y (11)	51 S (20)			$M_{\text{sum}}$	1.49
039 (50)	50 (70)			$M_{\text{sum}}$	1.47

$\pi_{\text{pt}} 0.485$

$\mu_{\text{pt}} = -0.13$   
 $M_{\text{sum}} = 0.74$   
 1.48

Ben 51  
 1.47  
 1.49

.0485

-36 -7 -23

u v w

789  
343  
751  
7025  
651  
6515+

74  
8  
32  
50

-0.7356

186402 19 43.0 -48 39 68 V-VI

S=+14

10.22 +0.59 -0.02 256

+0.038 -0.335 CA

.274 172° BPM

205156

21 31.5



Feb 28/1

14 482 - 24 30

F 5W A8/F0

818/1848

Probably weeks living in  
Cyril (F0/F0) also week (manuscript in  
Pm & del; G band yields F0/2

(F0/H)

-0.70

APR 1-23

(944/6)

-0.06

(009-063)

-0023 -0617

(0007 -061)

(0015 -061)

34

-63

7.05

-0014 -0606

(-13 -14)

(0027 -061)

(-001) -0615



R.A. : 19.800  
DEC. : -74.500  
PM. R.A. : -34.000  
PM. DEC. : -63.000  
DISTANCE : 7.050  
MODULUS : 257  
RAD. VEL. : 0.000

q1 (U) : 0.456  
q2 (U) : -0.591  
q3 (U) : -0.666  
dU : 156.797  
U : 40.303

q1 (V) : 0.235  
q2 (V) : 0.801  
q3 (V) : -0.550  
dV : -249.358  
V : -64.095

q1 (W) : -0.859  
q2 (W) : -0.095  
q3 (W) : -0.504  
dW : 65.295  
W : 16.783

77

25403

Blank

2216

~~187579~~

19 48.7 - 42 03

GOUWFS

187579

428928

208 + 015 C

-11  
+15

P Falk

5.4

140

R.A. : 19.800  
DEC. : -42.050  
. R.A. : -11.000  
. DEC. : 15.000  
STANCE : 5.400  
MODULUS : 120  
) . VEL. : 0.000

q1 (U) : 0.456  
q2 (U) : -0.141  
q3 (U) : -0.879  
dU : -27.706  
U : -3.331

q1 (V) : 0.235  
q2 (V) : 0.971  
q3 (V) : -0.035  
dV : 59.990  
V : 7.212

q1 (W) : -0.859  
q2 (W) : 0.190  
q3 (W) : -0.476  
dW : 46.774  
W : 5.623

2071

14

5-1.5

+ 18 3.5

1003.3 1005.1

1.24

1.81

17.75

1.21

R.A. : 19.850  
DEC. : 18.650  
PM. R.A. : -2.400  
PM. DEC. : -5.100  
DISTANCE : 12.780  
MODULUS : 3597  
RAD. VEL. : -22.100

q1 (U) : 0.466  
q2 (U) : 0.695  
q3 (U) : -0.548  
dU : -21.824  
U : -66.410

q1 (V) : 0.220  
q2 (V) : 0.505  
q3 (V) : 0.830  
dV : -14.640  
V : -71.070

q1 (W) : -0.85  
q2 (W) : 0.51  
q3 (W) : -0.07  
dW : -3.15  
W : -9.62

-20.4 W(3)  
-23.5 1 wood  
-32 19 53.3

1.2 1.7 -21.1

w/v  
4 way

188753  
+410353  
12273

-20.4

+34.3  
-15.3  
-123.0

9-1418

(-24)

+303 6n25  
-0091  
-2  
-43

25.8  
+31.6  
+41.3  
+26.0  
+25.6

+5.6  
-23.1  
81.2  
2.9  
40.0

A051325  
7.9 } 264  
8.4 }

43

(24)

+45.2  
+6.2  
+33.2  
+1.1300  
+15.47  
+92.92

131  
-14

(5)

81.7 15.4  
4.2 23  
26.1 20

(44)

815

Handwritten signature

+470 7850 -235  
+222 +141 +963  
-954 +505 +123

-1069 +1.2369  
-0505 +2052  
+1943 +7349

180  
195  
2130

29<sup>th</sup> power

-210

37.5

+470	+450	-235	-1.1092	41.2864	1.1277	+335	+49	+385
+222	+141	+663	-0.515	.2052	1547	+44	-20.9	-16.5
-854	1505	+103	+1584	.7349	9333	+269	-26	+243

185510  
+10.4091

G-143-17

12 526 +10 36  
grs

C-852w

6.83 59

(37) 8.25L -

880 416 100 160 2.55-3 (3)

843 417 123 128 (2)

~~811 103~~

right year

414 106 188 2.55  
161  
C-852

PHD

404 110 143

-152 252

8E

242E

2.76

~~81.48~~

-162.8



R.A. : 19.900  
DEC. : 10.600  
. R.A. : -38.000  
. DEC. : 292.000  
STANCE : 2.790  
MODULUS : 36  
. VEL. : -192.800

q1 (U) : 0.475  
q2 (U) : 0.610  
q3 (U) : -0.634  
dU : 760.826  
U : 149.644

q1 (V) : 0.218  
q2 (V) : 0.616  
q3 (V) : 0.757  
dV : 813.742  
V : -116.555

q1 (W) : -0.852  
q2 (W) : 0.498  
q3 (W) : -0.160  
dW : 840.241  
W : 61.126

AOS  
13125

Hyades  
Group

19 53.3 44 44  
516 36

P	Q	A	B	C	G	L		
25.71	1936.74	0.46	+0.019	-0.233	+0.232	+0.043	0.247	2.5.6
.02	.04	.00	.001	.001	.003	.003	.005	2.0

Minor improvement over orbit given in

795 also Arpane

240 +0.80 +0.42 2.20"

$$\pi_c = 0.125(29)$$

+5.90  
8.12

$$P = 25.71 \quad P^2 = 6.610 \times 10^2$$

$$G = 0.247 \quad G^3 = 15.066 \times 10^{-3}$$

$$\pi = .0395 \quad \pi^3 = 3759 \times 10^{-6}$$

n.m = 2.32

$\pi_{pt} = 0.375$

1914.49	23.0	0.20	2 A	+1.4	-0.01
18.64	610	0.24	2 A	-1.6	-0.02
19.98	68.0	0.33	2 A	-3.4	0.00
20.53	78.0	0.35	3 VB	+3.2	+0.01
21.56	77.0	0.34	2 A	-3.4	0.00
21.65	88.0	0.31	6 VB	+6.6	-0.03
23.52	92.0	0.38	4 VB	-0.2	+0.04
24.60	96.0	0.31	3 VB	-2.5	-0.03
25.42	101.0	0.33	2 VB	-2.5	0.00
27.65	118.0	0.34	3 VB	0.0	+0.03
31.60	154.0	0.24	3 VB	+0.4	0.00
35.74	232.0	0.18	2 VB	-2.2	+0.04
36.53	270.0	0.16	1 VB	+6.6	+0.03
39.58	7.0	0.19	1 VB	-3.8	0.00

188985

19 56 3 -49 07

<sup>38</sup> / <sup>60</sup> (H) W (P)  
~~188985~~

401115

In strong, with 112 weak prototype

950115  
x0115

-0058 +019 +TC

-050-

6101 681

90

11+

85:

R.A. : 19.950  
DEC. : -49.100  
M. R.A. : -90.000  
M. DEC. : 17.000  
DISTANCE : 5.500  
MODULUS : 126  
RAD. VEL. : 0.000

q1 (U) : 0.485  
q2 (U) : -0.234  
q3 (U) : -0.843  
dU : -154.312  
U : -19.427

q1 (V) : 0.210  
q2 (V) : 0.966  
q3 (V) : -0.148  
dV : 19.263  
V : 2.425

q1 (W) : -0.849  
q2 (W) : 0.105  
q3 (W) : -0.518  
dW : 245.613  
W : 30.921

199403

19 58.2

42 33

AFW 4243

428975

Putaway weak lined rather

than high humidity; metabols absent.

-1001 -1002 -4 +6

-1001

-3  
-4

6.7

-1002 -1004

R.A. : 20.000  
DEC. : -42.550  
PM. R.A. : -3.000  
PM. DEC. : -4.000  
DISTANCE : 6.700  
MODULUS : 219  
RAD. VEL. : 0.000

q1 (U) : 0.494  
q2 (U) : -0.132  
q3 (U) : -0.859  
dU : -2.672  
U : -0.584

q1 (V) : 0.202  
q2 (V) : 0.979  
q3 (V) : -0.035  
dV : -20.671  
V : -4.522

q1 (W) : -0.846  
q2 (W) : 0.156  
q3 (W) : -0.511  
dW : 5.900  
W : 1.291

7.28  
-0.7

5.8

4.7



140513344  
190658

+10  
17  
20

+0019#5.7  
+0024  
03.1

+018#5.4  
+0.20  
21

5.2 SB?  
6.6 gm2 -116.68

27872

12483

8.428

+15

21 22.72 1895.6

107  
555

-101  
327

+00215 +019<sup>85</sup>

-98  
21.74

497  
112  
365

8.406

+00224 +0225<sup>-22</sup>

22.36  
14  
1933.5

42  
28

+034  
+034  
+034  
+034  
+034

+0338<sup>27</sup>  
0363  
40.0

22.850

42  
28

8.437

+036 +020

22.46  
17  
1939.7

13.2  
36.0

42  
28

422  
+09.5  
2.1

22.63  
22.56  
+.82

41.0



190658.000\*

20.000\*

3.100\*

15.000\*

21.000\*

0.036\*

0.020\*

7.800\*

282 ✓ 363.078

-111.600

0.148

-0.562

1102 116.528

0.085

0.813

-59.925

-0.094

-0.150

-17.549

733

190658.000\*

20.000\*

3.100\*

15.000\*

21.000\*

0.041\*

0.015\*

7.400\*

301.995

-111.600

0000  
557

0.145

-0.562

0.42

106.392

0.077

0.813

0.44

-67.662

-0.127

-0.150

+0.3

-21.513

+43.3607

20 072

42 42

Page 786.4 m

C02504

1011 051

G18624 20 276 +24 67 -3214

10.82 0.40 0.23

0.740 140°

*Handwritten signature*

082-226

50

net

500

HARE

R.A. : 20.400  
DEC. : 24.900  
PM. R.A. : 90.000  
PM. DEC. : -226.000  
DISTANCE : 5.700  
MODULUS : 138  
RAD. VEL. : -321.400

q1 (U) : 0.567  
q2 (U) : 0.719  
q3 (U) : -0.401  
dU : -551.069  
U : 52.858

q1 (V) : 0.134  
q2 (V) : 0.400  
q3 (V) : 0.907  
dV : -376.716  
V : -343.403

q1 (W) : -0.813  
q2 (W) : 0.568  
q3 (W) : -0.131  
dW : -922.872  
W : -85.429

+4103735

20 22.8

+41 20

✓TT15972

-162.2<sup>to 5</sup> 2M

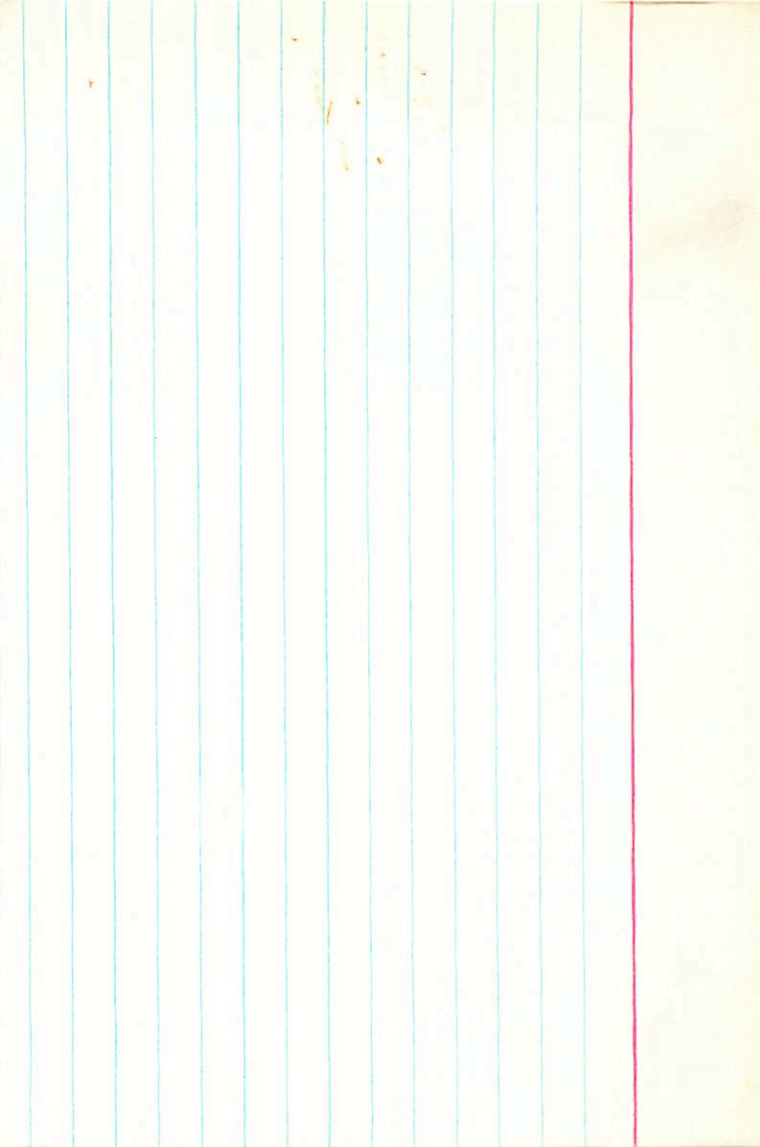
8.8 60

120 227<sup>0</sup>

$+41^{\circ} 37' 30''$     20    22.8    +41    20

9.10 +0.605 +0.105 (2)







702  
194722

20 25.7 55 17

F5WFO

-853357

$\rho^{(1)} - 37$

2074

Overlapped; looks somewhat weak here.

-0021 +073 Super  
-0015 +074  
-0015 +073

-30

+71

5.5

$\boxed{-017 + 071}$

-0023 +072

+2 -2

+6 +4

-0015 +074

R.A. : 20.400  
DEC. : -55.300  
PM. R.A. : -30.000  
PM. DEC. : 71.000  
DISTANCE : 5.500  
MODULUS : 126  
RAD. VEL. : 0.000

q1 (U) : 0.567  
q2 (U) : -0.273  
q3 (U) : -0.777  
dU : -137.742  
U : -17.341

q1 (V) : 0.134  
q2 (V) : 0.962  
q3 (V) : -0.240  
dV : 312.749  
V : 39.373

q1 (W) : -0.813  
q2 (W) : -0.032  
q3 (W) : -0.582  
dW : 55.020  
W : 6.927

RSU

20 24.2 +16.06

60.8

(1.07)

+0.36 -0.01 1.07  
-1.2

+0.51 -0.01  
+3 -0.03

b = -1.30 + 3 = -0.03  
P.L. +0.37

90

+0.5

1.37  
1.34

4.93

4.75

4.93

4.77

2.46  
5.1

+0.34 -0.03

-1.05

2.15  
1.45

5.15  
5.00  
5.15

1.45

5.179 2.12

5.09  
2.12  
2.915 84

0.000\*

20.000\*

26.200\*

16.000\*

6.000\*

0.037\*

-0.003\*

8.650\*

537.032

-105.000

0.091

-0.501

101.699

0.015

0.836

-79.833

-0.150

-0.223

-56.904

20 28 08 +27 41 51 75 89

424 4000

+2703773 20 28.7 +27 47 8.8 112.77

8.064 + 1.14 + 1.06 ①

7.65 + 0.40 ①

7.27

6.71

9.9 ①

+053 +038 AGR2

+045 +061 Y →

+047 +059 & Ready →

+049 +053

+052 +050

+045 +061 Y ±6

+045 +058

+042 +058 Ready

+2 +24

+44 +56

+043 +057 ±4.5

+0467 +0685

+050 +058

186

20.450	0.000*
27.800	
59.000	20.000*
50.000	28.700*
8.000	27.000*
398	47.000*
-17.400	0.050*
	0.050*
0.576	7.700*
0.735	346.737
-0.358	-17.400
316.698	
132.302	0.339
	-0.354
0.125	
0.353	123.764
0.927	
114.639	0.126
29.504	0.928
	27.377
-0.808	
0.579	-0.031
-0.111	-0.117
-62.681	
-23.022	-8.699

187

CZ 2/24

20 31.2

+0.9

21 90-10.2

10.5

+904578

9.25

-16.5

→ +1010 +002

-162.0 ± 0.5

9.25 +0.28.5 -001.5

+5.9.0

Remain

+21 + 20.0  
+0003 +002  
+004 +005

-17 + 9  
+111 +008

111.6

Purchase

+008 -003  
+006 +001  
+2 -20.0

+019 -002  
-8  
+011 +003

111.6

Remain

+008 -003  
+006 +001  
+2 -20.0

+019 -002  
-8  
+011 +003

111.6

10005-006

KNAD

→

+008 -003  
+006 +001  
+2 -20.0

+019 -002  
-8  
+011 +003

111.6

-146.3

400P

+011 +003

550A

584 584 -513

+001 +008

+017

+011 +003

550A

1117 626 771

+002 +015

+017

+011 +003

550A

-803 516 -248

-0168

+13

+011 +003

550A

+47

+48.7

+48.7

+48.7

+47



CALL 20 21.2 +9 21

6.47 198

6.09  
4.57

6.39 1545

Vol Babcock (Thomas) Annual

6.4

4.55  
B2408

Report M. Wilson and Nelson

4.17

6.24 1.81

Remembrance, 1943-1944.

4329 (89)

→ 200-165

CALL

2.95 +16.5 +185

-3.3 +105 -116 +47 +4 -1620 120 E 7.108

+904578

6.4 +1.17

8.7 +2 +2 0 +5 pms -180

408



196917.000\*

20.000\*  
38.300\*  
-31.000\*  
-47.000\*  
0.106\*  
-0.056\*  
6.950\*  
245.471  
-97.300

0.284  
-0.790  
146.677

-0.214  
0.170  
-68.985

-0.443  
-0.589  
-51.492

0.000\*

20.000\*  
31.200\*  
9.000\*  
21.000\*  
0.010\*  
0.002\*  
9.250\*

707.046  
-165.000

0.033  
-0.561

116.264

0.011  
0.770

-119.045

-0.033  
-0.333

26.000

C2 5-8.9-17-6

196499 20 36.8 40 35

GENCOOP

40.7420 Strong CH

9 Feb 1967

198991 20 49.0 -49 41 A5/P2 W

Full overlapped; primary water - lined;

P<sub>1</sub>, 30

Ca-HIV yield 48; H line's yield 243;  
metals yield about A7 B.

-0013 T0037FC

-013 -22

0

1.4

-014 T0037FC

R.A. : 20.800  
DEC. : -49.700  
M. R.A. : -22.000  
M. DEC. : 0.000  
DISTANCE : 6.400  
MODULUS : 191  
D. VEL. : 0.000

q1 (U) : 0.634  
q2 (U) : -0.148  
q3 (U) : -0.759  
dU : -42.746  
U : -8.145

q1 (V) : 0.065  
q2 (V) : 0.988  
q3 (V) : -0.138  
dV : -4.373  
V : -0.833

q1 (W) : -0.771  
q2 (W) : -0.038  
q3 (W) : -0.636  
dW : 51.989  
W : 9.906

+1104463  
 21 014 +11491950 8458  
 20 59.0 +1138 8.7

933 275M. 9222

+0677074 AG123

+055 +074  
 $\frac{-8}{+063}$   
 $\frac{0}{+063}$

644 587 462	+1583 +2254	+4237 +126	+10.1
020 597 482	+0090 +2292	+2882 +50	-17.6
-710 547 279	-2231 +2100	-0131 +5	+8.3

press

4404551

20 43.5 44 50 5.4 FS

9.72

592

$\rho = -118$

4023 4087 Y

4404.

-03 486

6216 535-518

+0474 +2434

+2908

~~4~~195

125  
467.0

-8 +7  
4015- 4094

674 684 726

+056 +3112

+2165

-54

130  
185.6

+1 +2  
415.9 416.6

-776 446 259

-0588 +2257

+1664

4114

124  
415.9

416.6 415.6

4 58 27.5 114600

5C  
F2V-VI -73.9±1

21 03.3 -46 28

200703

FD1267

8.80 +60 (1.67)

8=107

+027 -0.240 CR

+0013 -232 +TC F04

+013<sup>r</sup>

-73.9

+013-235

3/5

200703.000\*

21.000\*

3.300\*

-46.000\*

-28.000\*

0.013\*

-0.235\*

3.500\*

50.119

-73.900

0.123

-0.736

60.572

-1.109

-0.080

-49.643

-0.002

-0.672

49.538



2.14.2019  
2.15.2019

Wulf <sup>11063</sup> ~~48~~

21 06.7 +59 02

6231-27

-260 (5W) van  
46.4.2019

-940 -1925 Wulf  
-1010 -1500 Spide (2)

189141

645

5B(46)

w 13296

21 06.8

+59 33

adm

260W(S)

CC 1263

Apr 13.0

6627

~~W918~~

W918

- 940 - 1.52

CC

30 W 110)

M 01558

-686 728 962 508 -94 -1.92 -260 -1.655 -224 -4.62

-645 -1.135 -684 -1205 2.453 -8.618 -1321 -96 +91 .04

-30 -124 -340

-271 -214 -113

W13294 21 06.8 +59 33 ad m1 -260 c

-54 -1.92 cm  
06

W 35(10)

+54<sup>0</sup>246/

20 59.3

+55 06

As studies

throughout

in W. 1000!

W

-707 707 962 507 -94 -1.92 -260 -1660 -225 -4.660

-662 -1.170 -662 -1.170 2.400 -8.700 -93 +93 04

-30 -110 -154  
-16 56 -259  
-249 20 -159  
-33 -125 -340  
-272 -215 -110

-45 -81 -317 05

-223 -225 -96

-4 -11 1/16  
-22 34 1/11

39 13

259-1-94

21 21.2 10.09

1010.8 - 1037

108

107

104

101

10.52

R.A. : 21.400  
DEC. : 6.150  
R.A. : 10.800  
DEC. : -5.700  
DISTANCE : 10.220  
DULUS : 1107  
VEL. : -74.000

1 (U) : 0.720  
2 (U) : 0.534  
3 (U) : -0.443  
dU : 22.239  
U : 57.357

1 (V) : -0.040  
2 (V) : 0.669  
3 (V) : 0.742  
dV : -20.103  
V : -77.175

1 (W) : -0.692  
2 (W) : 0.517  
3 (W) : -0.503  
dW : -49.212  
W : -17.222



202560

21 14.3 -39 04

9/6)  
+19.4±0.7

G-29741

6.68 +1.42 MOE

+230 W(3)

W13369

+20.7 3 Str

75117

5.78 +69 str

631  
21

-39 04 197

-3.269 -1.154 col

-3.283 -1.146 con

-58 -20 +28 : 25-8x

2577 (18)

~~250~~ (17)

255 = 8

-2807 ± 7.5    -1154 ± 7.5  
-2794            -1143

553 823 -681 776 -3.253 -1.146 +20.0 723 -134.212 ✓

1.815 -400 -2.735 602 5.747 -1.485 +15.5 +13 +86

19.934 1796.3

-39 3 42.57 1893.4

15.074  
35.008  
50.806  
34.950  
25.756  
100  
156  
142  
642

43808  
21.904  
13.104

46.9

18.175  
9  
764

68.32  
37.25

34.65 1930.10  
13.62  
21.00  
113  
9.818  
49

48.51 1956.38  
13  
48.64

68.43  
517.66  
49.8

34.16  
56.91  
48.33  
24.16  
46.91

202759 8244 6.45 -052 115 658 2713  
27 16.0 -34 08 AO (12)w

34.14577 886 -125 (7.7)

NO mistakes; human horizontal  
beam stem

10081 060 444

1101-063

422  
-63  
8.45'

R.A. : 21.250  
DEC. : -34.100  
PM. R.A. : 122.000  
PM. DEC. : -63.000  
DISTANCE : 8.450  
MODULUS : 490  
RAD. VEL. : 0.000

q1 (U) : 0.700  
q2 (U) : 0.106  
q3 (U) : -0.706  
dU : 303.702  
U : 148.747

q1 (V) : -0.014  
q2 (V) : 0.991  
q3 (V) : 0.135  
dV : -302.413  
V : -148.115

q1 (W) : -0.714  
q2 (W) : 0.085  
q3 (W) : -0.695  
dW : -367.131  
W : -179.813

*8.2*

*1326*

*1320*

*1603*

8152  
203010

21 17.8 -50 09 R3 III

171 -174  
V86 -340 ✓  
-328 ✓  
+22.55 C

FD 1273  
GC24858

6.41 +133 +156  
6.37 +132

365 -182 -3  
-214 -177 -166  
-149 ± 8.3 5.0  
+22.5

8th job done

5-1.275 1400.5 -0043

55.44 18968

134  
509

7.63  
47.51

-0035 -178

6  
-003-169

-20

Not done

9.478  
43.158  
5.638  
6.28

12.65 192776  
18.40  
54.85  
5420

Stop

-0004 -167  
-0003 -163

557  
549  
543

8 PM

-0001-158  
-003-158  
-8  
-758  
-4.30  
+5225

9445 0830 1572  
3286 -9446 0161

-0026  
-0027-166

R.A. : 21.300  
DEC. : -50.150  
R.A. : -5.000  
DEC. : -158.000  
STANCE : 4.300  
MODULUS : 72  
VEL. : 22.500

q1 (U) : 0.707  
q2 (U) : -0.086  
q3 (U) : -0.702  
dU : 53.822  
U : -11.891

q1 (V) : -0.022  
q2 (V) : 0.989  
q3 (V) : -0.144  
dV : -740.569  
V : -56.893

q1 (W) : -0.707  
q2 (W) : -0.118  
q3 (W) : -0.698  
dW : 70.000  
W : -8.535

44

574

-8

107.5

-3

12483

8.67

+1.12

+0.96

KIT

-31.9

204079

-159±6 -159±5 Rndy

+26°456

-162 -159 Rndy →

-149 -167 Y →

Not W630

-146 -159 Above

-149 -161

-31.9

-146 -167

2.25

+26°59 49.94

21°23' 17.485

-0.002

17.483

21°23' 17.470

-0.011

.459

-1.143

-0.003

-0.146

-0.001

-0.147

-0.164

-0.003

-0.167

+0.003

-0.164

1928.69

1929.7



204079.000\*

21.000\*

23.300\*

26.000\*

59.000\*

-0.146\*

-0.164\*

0.58 2.250\*

12.91 28.184

-31.900

-1.009

-0.226

-4 -21.229

-0.255

0.932

-33 -36.896

-0.034

-0.285

19 8.126



$7560 > 578$   
 $6-7 = 400$  [m] +28 [c] = +21  
 +02  
 204613 21 26.2 +57 07

543

fund bal 467.26  
 Apr. 5. 2597.92  
 (897)

+0248  
 +2  
 -104  
 +2  
 -102

See movement  
 Buy Bond 1129  
 Apr. 5. 10, 129  
 100 PA. 2000.  
 +40  
 -97  
 -108

+198 +0243  
 100 P. 5.00  
 +135472  
 +0336  
 -9552  
 6520  
~~8795~~ -3278  
 -0404 +0740  
 -18066 -3474  
 769 Ramp -15.2  
~~-87.0~~  
 -110.5  
 -9.1

480  
8 1/6  
13 1/6  
14 1/4  
8 1/4  
3 1/8  
5 1/2  
11 1/2  
15 1/2  
15  
3 1/2  
5 1/2  
7 1/2  
10 1/2  
15  
15

+1104571

21 26.7 +11 58 12.5 dM0 -247c

3w

13502

G176-02 0.55 1640

28W(7)

1.086

2.4

$$1.230 = M_1^2 + \tan^2 M_2^2$$

$$\frac{2.1}{1.086} = \frac{1.086}{1.086} + \frac{1.086}{1.086} \tan^2 M_2^2$$

525

-247

726 574 -378

.6882 4.3060

-6178

-32.4#33

-28 550 806

-0455 -1.3424

-1.3679

-70.2<sup>19</sup>

-656 567 -456

-6503 -1.2300

-1.9403

-101.9

41124

461-970 +11

146155 (2)  
48 104 8PM

11104571

21 26.7 +11 58

G126-2

2

(20)

-247c

10.65 + 0.475 (3)

1027

+195 - 415 G net (12)

+135 - 400 depth + 100gpm

571

57

2.4 + 16.7

+165 - 80

11.5 1.00 175

+135 - 445

1112 668 419 204  
3.8.8 (3)

(3.1)

126.200\*

21.450

11.950

138.000

-445.000

3.100

42

-247.000

0.727

0.574

-0.377

-745.767

62.036

-0.049

0.591

0.805

-1276.866

-252.187

-0.685

0.567

-0.457

-1634.623

44.780

21.000\*

26.700\*

11.000\*

58.000\*

0.165\*

-0.430\*

3.000\*

39.811

-247.000

-0.603

-0.378

69.321

-1.241

0.806

-248.405

-1.692

-0.456

45.299

4.24  
70.5

024

3.1  
1.16

4.3  
92.4

441

464

-289

251

-2

442



126.200\*

21.000\*

26.700\*

11.000\*

58.000\*

0.135\*

-0.440\*

2.400\*

30.200

-247.000

-0.733

-0.378

71.172

-1.262

0.806

-237.121

-1.622

-0.456

63.697

126.200\*

21.000\*

26.700\*

11.000\*

58.000\*

0.135\*

-0.460\*

2.400\*

30.200

-247.000

-0.788

-0.378

44

69.528

-1.318

0.806

~~28~~ -238.811

-1.675

-0.456

47

62.073

126.200\*

21.000\*

26.700\*

11.000\*

58.000\*

0.195\*

-0.415\*

2.400\*

30.200

-247.000

-0.459

-0.378

79.465

-1.205

0.806

-235.419

-1.749

-0.456

59.836



$22704074$     21 28 09    +28 29    +6048±9.5    -125 ±7.1  
 $204642$     21 27 1    +0062    +0062  
 $30091$     +00725    -147    6.8    182111    +18.98  
 $13506$     +0058    -181.    +0058

$4.078$     1988.3    +28    21    56.42    1905.2  
 $-200$   
 $3,878$   
 $4.056$   
 $0.524$   
 $5962$

$-010$     -141    10123    5.00  
 $+076$     -128    66 →    2.02  
 $-030$     -135    4 →  
 $+010$     -135  
 $045$   
 $+167$   
 $4.043$   
 $037$   
 $4020$   
 $-4$   
 $014$

$20.9$   
 $+119$   
 $+18.9$   
 $58.5$   
 $1929.7$   
 $-20$   
 $58.60$   
 $58.72$   
 $-3$   
 $30$   
 $240$   
 $29.2$   
 $115.9$

40

21.450  
28.400  
0.800  
-135.000  
5.750  
141  
18.900

0.727  
0.657  
-0.199  
-420.615  
-63.175

-0.849  
0.338  
0.940  
-216.497  
-12.819

-0.685  
0.673  
-0.278  
-430.913  
-66.120

W 13510 21 27.3 +17 25 10.4 dmy

532177

9427  
1127  
10556  
3125  
0047  
+0.7 0326

1012 388  
FIC  
6 wmd

Row 775

8.57

10627

~~653 8410  
-7548 5410  
0115 8410  
10604  
-0218  
707~~

1010

390

57 +1.010 +390 5CR2  
57.5 +1.012 +858  
8  
2  
12.1 389

858

10819  
63301  
-0529  
9113  
9113  
1004  
1004  
1004

1.1 5.3

7.1

9.75  
8.10

9.10

114

7.76  
2.46  
3  
3

0.1410

-0.804

282

MIS

21 226 81 87

143  
116

3.0  
4.2  
14.3  
21094

R.A. : 21.450  
DEC. : 11.950  
PM, R.A. : -3.000  
PM, DEC. : -4.200  
DISTANCE : 14.930  
MODULUS : 9683  
AD. VEL. : -107.400

q1 (U) : 0.727  
q2 (U) : 0.574  
q3 (U) : -0.377  
dU : -21.540  
U : -168.076

q1 (V) : -0.049  
q2 (V) : 0.591  
q3 (V) : 0.805  
dV : -11.081  
V : -193.810

q1 (W) : -0.685  
q2 (W) : 0.567  
q3 (W) : -0.457  
dW : -1.760  
W : 32.056

+1003 4004 9.6 -23.0

204923

~~21~~

21 28.9

+25

50

103.11

8.04 +1355 +14112

7.28 70.53 2

~~+1063 +1004 7.00  
 - 3 -3  
 +1066 +1000 6.3  
 + 4  
 +1070 +1004 7.15  
 +1072 +1001 6.3  
 +1002~~

-23.0

7.00  
 7.0  
 6.3  
 2.2  
 7.15

~~8.04~~

1044-1002 2053

1070 +1004 7.0

1057 +1001

1060-1002

B?

E(1004) = +10.02

-2.5

204923 +72 -18

8.8

204923 +60 +84

+0.53 -2 -29

570 = 23.0 -70

-0.5  
 -0.6  
 7067 on liability  
 -0.6  
 1000  
 1000

1221

204923.000\*

204923.000\*

21.000\*

28.900\*

21.000\*

25.000\*

28.900\*

50.000\*

25.000\*

0.073\*

50.000\*

0.001\*

0.060\*

8.500\*

-0.002\*

501.187

8.800\*

-23.000

7.95  
389.07

575.440

-23.000

0.256

-0.223

0.202

-0.223

133.408

+8.4

121.219

-0.017

0.923

-0.019

0.923

-29.720

-29

-32.169

-0.232

-0.313

-0.200

-0.313

-109.219

-70

-107.764

4045+061

-17.4

1221

67, 301

M39

205210 -0017 -030  
 205331 -0013 -024 (H) -6011-018  
 205116 -0016 -024 8 13  
 21 205116 20.4  
 205917 -0009 -024  
 205117 -0004 -024  
 205003 -0007 -022  
 205008 -0008 -022

2049.5-018

205917

205008  
 205009  
 205010  
 205011  
 205012  
 205013  
 205014  
 205015  
 205016  
 205017  
 205018  
 205019  
 205020

206-017

205018  
 205019  
 205020  
 205021  
 205022  
 205023  
 205024  
 205025  
 205026  
 205027  
 205028  
 205029  
 205030

20518

210-0182

205026  
 205027  
 205028  
 205029  
 205030  
 205031  
 205032  
 205033  
 205034  
 205035  
 205036  
 205037  
 205038  
 205039  
 205040

205-018

205

205-018

205-018

20518  
 20519  
 20520  
 20521  
 20522  
 20523  
 20524  
 20525  
 20526  
 20527  
 20528  
 20529  
 20530

20510

20518

205 = +0.9

205 + 18.7

205

20518  
 20519  
 20520  
 20521  
 20522  
 20523  
 20524  
 20525  
 20526  
 20527  
 20528  
 20529  
 20530

205

20525

20514

205-018



3.000*		39.000*
21.000*		21.000*
39.400*		33.100*
43.000*		43.000*
13.000*		13.000*
-3.006*		-3.009*
-3.017*		-3.017*
7.000*	7.0	7.100*
251.169	251	263.927
3.900		3.900
-3.075		-3.086
3.043		3.043
-13.924	-21	-22.560
3.002		3.002
3.998		3.998
1.318	+2	1.548
-3.040		-3.030
-3.040		-3.040
-13.060	-8	-3.027

206078 21 35.8 +62 05 7.7 966 -7498 SW

30286 7.11 +97 +68 6877R

13589

$$\begin{array}{r} 50.552 \\ - 320 \\ \hline 232 \end{array}$$

$$\begin{array}{r} 50.51 \\ 24 \\ \hline 43 \end{array}$$

Mt. Wshy 50.552 1891.5 +62 4 37.54 1879.1 3A  
 6.27 + 3.85  
 6.27

106730

$$\begin{array}{r} 100535 + 119664 \\ - 8.79 \\ \hline 29.07 \end{array}$$

$$\begin{array}{r} 10052 + 124 \\ + 865 \\ - 749 \\ \hline 1040 + 118 \\ \hline 4 \end{array}$$

35.00 1929.7

-17 31.83

Mt. Wshy 115.36  
6.41 0.5

8560 + 115 Canyon 90  
 115  
 7  
 2789

206078.000\*

21.000\*

35.800\*

62.000\*

5.000\*

0.040\*

0.118\*

4.000\*

63.096

-74.900

0.495

0.212

15.339

-0.147

0.969

-81.815

0.287

0.130

8.344

R. A. : 21.600  
DEC. : 62.100  
R. A. : 44.000  
DEC. : 115.000  
TANCE : 6.000  
DULUS : 158  
VEL. : -74.900

1 (U) : 0.745  
2 (U) : 0.632  
3 (U) : 0.213  
dU : 417.108  
U : 50.180

1 (V) : -0.075  
2 (V) : -0.238  
3 (V) : 0.968  
dV : -136.923  
V : -94.237

1 (W) : -0.662  
2 (W) : 0.738  
3 (W) : 0.130  
dW : 337.535  
W : 43.753

105  
112.2  
788

345

R.A. : 21.600  
DEC. : 62.100  
. R.A. : 90.000  
. DEC. : 115.000  
STANCE : 7.000  
MODULUS : 251  
. VEL. : -74.900

q1 (U) : 0.745  
q2 (U) : 0.632  
q3 (U) : 0.213  
dU : 493.165  
U : 107.950

q1 (V) : -0.075  
q2 (V) : -0.238  
q3 (V) : 0.968  
dV : -144.546  
V : -108.844

q1 (W) : -0.662  
q2 (W) : 0.738  
q3 (W) : 0.130  
dW : 269.955  
W : 58.067

2059<sup>914</sup>~~14~~

21 36.6 -49 10

F3/6W

49.11465

Somewhat overlapped; probably

Weak-lined; bound yields F516j.

Cast+IV yields 20

ppull  
-57

+056 +017 7+6

+055

+82

+054 +014

+14

5.8



R.A. : 21.600  
DEC. : -49.150  
l. R.A. : 82.000  
l. DEC. : 14.000  
STANCE : 5.800  
MODULUS : 145  
). VEL. : 0.000

q1 (U) : 0.745  
q2 (U) : -0.031  
q3 (U) : -0.666  
dU : 187.473  
U : 27.098

q1 (V) : -0.075  
q2 (V) : 0.989  
q3 (V) : -0.129  
dV : 46.621  
V : 6.739

q1 (W) : -0.662  
q2 (W) : -0.146  
q3 (W) : -0.735  
dW : -178.092  
W : -25.742

→ 206301 21 38.8 -14 16 dca 62B

Y 5229 50 B<sup>d</sup>

29M(7)  
30Y(8)  
20C(7)  

---

29

5.18 + 0.65 + 0.20 (3)  
4.84 + 0.24 (2)  
11.60

$\Delta(B-x) + Y$   
 $D(x-B) + S$

49

~~HB~~  
~~AB~~

$\pi - m = 2.10$   
W U W  
-248 -33.1 -0.9  
-9 -12 -1  
WOLF 630  
PIFF 638



207134

RC30487

W13685

Y15260

+2404473

20 44.1 +25 20 212 -4498 W(4)

6.5

6.25 +1.21 +1.25 133 II R

W(+0.7)

+80 -38 -13 .010

+57 -40 -3 .015

E chel

212 W(7)

+163 +044<sup>cc</sup>

+149<sup>24</sup> +058<sup>24</sup>

+156 +050

207134 21 44.1 +25 20 6.5 912 -44.48  
+0120±30 +044±2.7  
+0114 +084

30487 7.209 1903.2 +25 19 51.51 1898.3  
13685

+117 +0120 +052  
-5627  
6647  
-227  
49,24

7.098  
9  
089 4624  
7.012  
7365  
31.9

51.39 1941.89

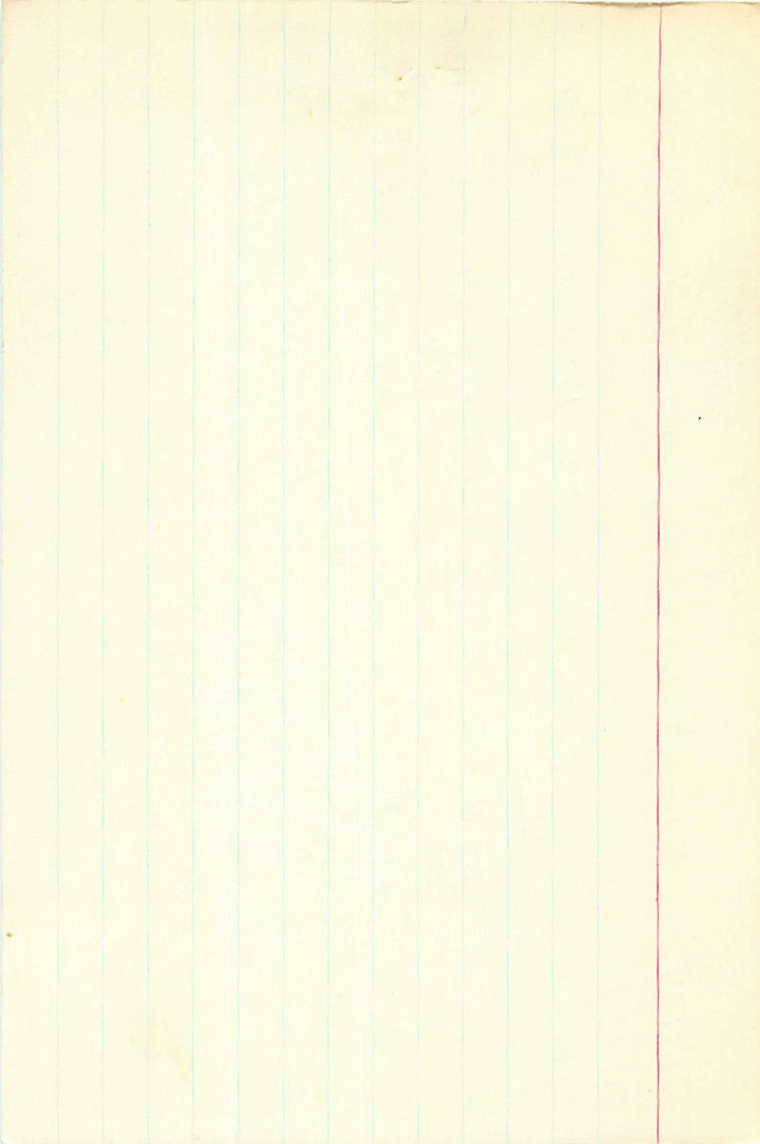
51.48

50.48 1928.29

6.938  
3  
935

50.95 701.8  
3  
51.21 35.1

+1.97 36.8



207134

21

44.1

+25

20

103 III

20"

630 + 1225 + 127 (3)

572 + 0.43 (3) A

-44.96

~~+419~~  
~~+611.3~~  
~~+0.57~~ (2)

+419  
+611.3  
+0.57

~~+161.3~~  
~~+116.9~~  
~~+0.55~~ FRY

+161.3  
+116.9  
+0.51

+161.3  
+116.9  
+0.51

+60  
+0.52  
Ca → FRY

+165 + 0.48

-44.9  
6.6

207134.000\*

207134.000\*

21.000\*

21.000\*

44.100\*

44.100\*

25.000\*

25.000\*

20.000\*

20.000\*

0.165\*

0.164\*

0.048\*

0.051\*

5.500\*

6.150\*

125.893

169.824

-44.900

-44.900

0.737

0.742

-0.184

-0.184

101.012

134.272

0.012

0.018

0.915

0.915

-39.576

-38.022

-0.347

-0.334

-0.358

-0.358

-27.593

-40.680

201,995  
-56,976

21 443 -35-53

6000

378

95000

+0030 -158  
+0059 -147  
            
+0010 -178

+034

[+033-182]

-900

+0057 -1596

+59

-182

+ 2 -2

36

            
+ 6 +1

-90.6

+0059 -167

R.A. : 21.750  
DEC. : -55.900  
l. R.A. : 59.000  
l. DEC. : -182.000  
DISTANCE : 3.600  
MODULUS : 52  
l. VEL. : -90.000

q1 (U) : 0.763  
q2 (U) : -0.084  
q3 (U) : -0.641  
dU : 192.332  
U : 67.785

q1 (V) : -0.101  
q2 (V) : 0.964  
q3 (V) : -0.247  
dV : -847.301  
V : -22.272

q1 (W) : -0.639  
q2 (W) : -0.253  
q3 (W) : -0.727  
dW : 117.849  
W : 71.600



207178

21 45.4 -53 15

88W60W

-53.10158

Weak lined; C-band strong  
yields C-S; 10-HK parity  
weak for 88 type.

P Full  
~~4000~~  
-0.47

7006 00 2000

-W4

~~-W16~~ -023

W5-015

~~-W05~~ -012

-W024 -024

-8

+2 -3

-15

~~-W022~~ -027

7.75

+6 +7

R.A. : 21.750  
DEC. : -53.250  
M. R.A. : -8.000  
M. DEC. : -15.000  
DISTANCE : 7.750  
MODULUS : 355  
RAD. VEL. : 0.000

63

q1 (U) : 0.763  
q2 (U) : -0.055  
q3 (U) : -0.644  
dU : -13.429  
U : -4.765

2.4

q1 (V) : -0.101  
q2 (V) : 0.974  
q3 (V) : -0.202  
dV : -66.984  
V : -23.767

122

28.5

q1 (W) : -0.639  
q2 (W) : -0.219  
q3 (W) : -0.738  
dW : 30.047  
W : 10.661

H 4

W13775

21 53.1 t32 24

d6w -177.96m(s)

CC1321

10.8

+71 t18 ai

0507  
+760 +131 Handing

+750 +122 MEZ

-10 +10 -76C

+748 +136

50  
-25 M42

85-26 85-1 536 844 471 418 -177.9 096-95-715  
 323 050 604 082 1.379 3099 -150.1 -128 +79 01  
 +10 +389 -23  
 +332 -196 -83

072 790

W 04/11/43

21 53.1 t32 24

206

G-188-30

11.09 +0.67 -0.06 (4)

-177.9

+760 +130 G'

+755 +120 MC (BTH)

+760 +125

21.862  
28.100  
-186.000  
-114.000  
6.000  
158  
-7.000

0.775  
0.618  
-0.131  
-936.815  
-147.558

-0.120  
0.348  
0.930  
-94.508  
-21.488

-0.620  
0.705  
-0.344  
101.442  
18.482

208174  
30661

21 51.7

-0123 ± 10.6    -110 ± 9.0  
-0124  
+28 06    6.7 dA5 -7.0 8

13759

40.409 1906.2 +28 6 24.96 1905.2

539  
948

4.93  
2989

40.677

22.8

27.37 1928.29

1  
674    666

10  
27.27    180  
29.0

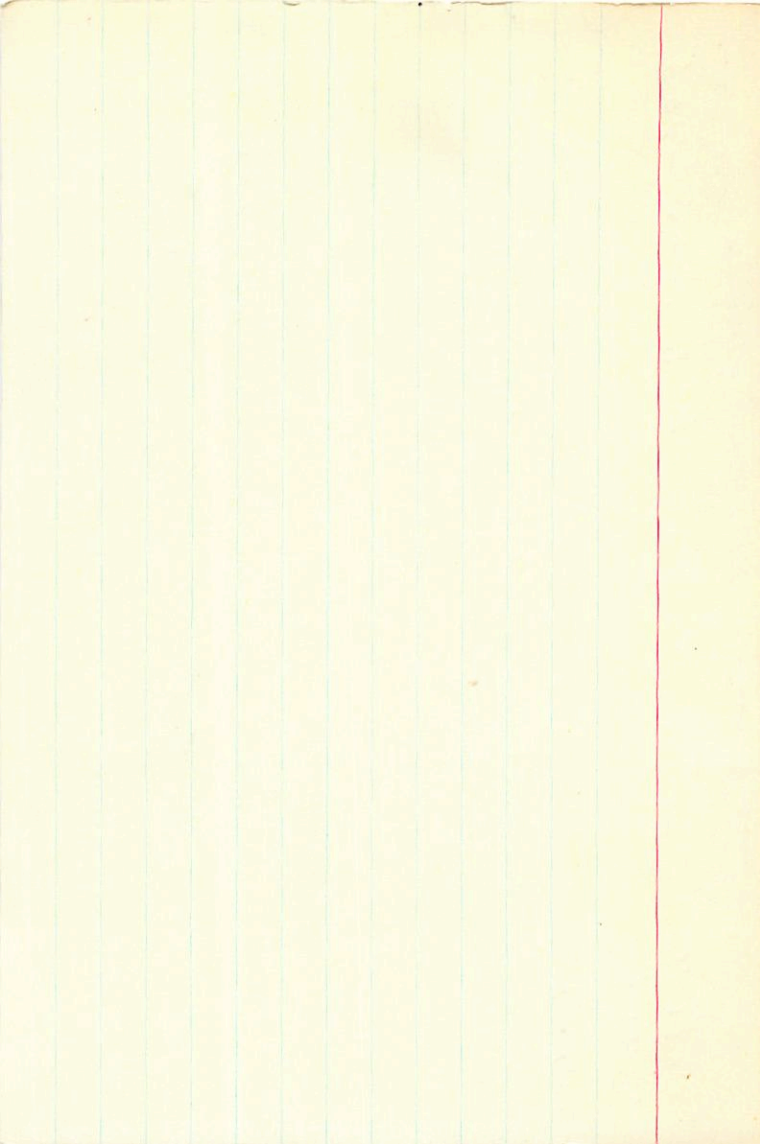
40.66  
5  
655

282

27.1 1929.7 (23.8)

14  
26.97    418  
27.09  
2.80





SD

Rd/F6 and

R000662 21 53.7 +55 54 -672

11.7



$$\frac{\mu_x^2}{\mu_y^2} = \frac{\mu^2 - \mu_y^2}{\mu_y^2} = \tan^2 \alpha = 2.039 \quad 0.32 \quad 55^\circ$$

$$\cdot 1024 - \mu_y^2 = 2.039 \mu_y^2$$



$$0337 = \mu_y^2 \quad \cdot 184$$

$$0687 \mu_y^2 \quad 1262$$

2764 ①

Passbook

21 53.7 +55 57

G232-40

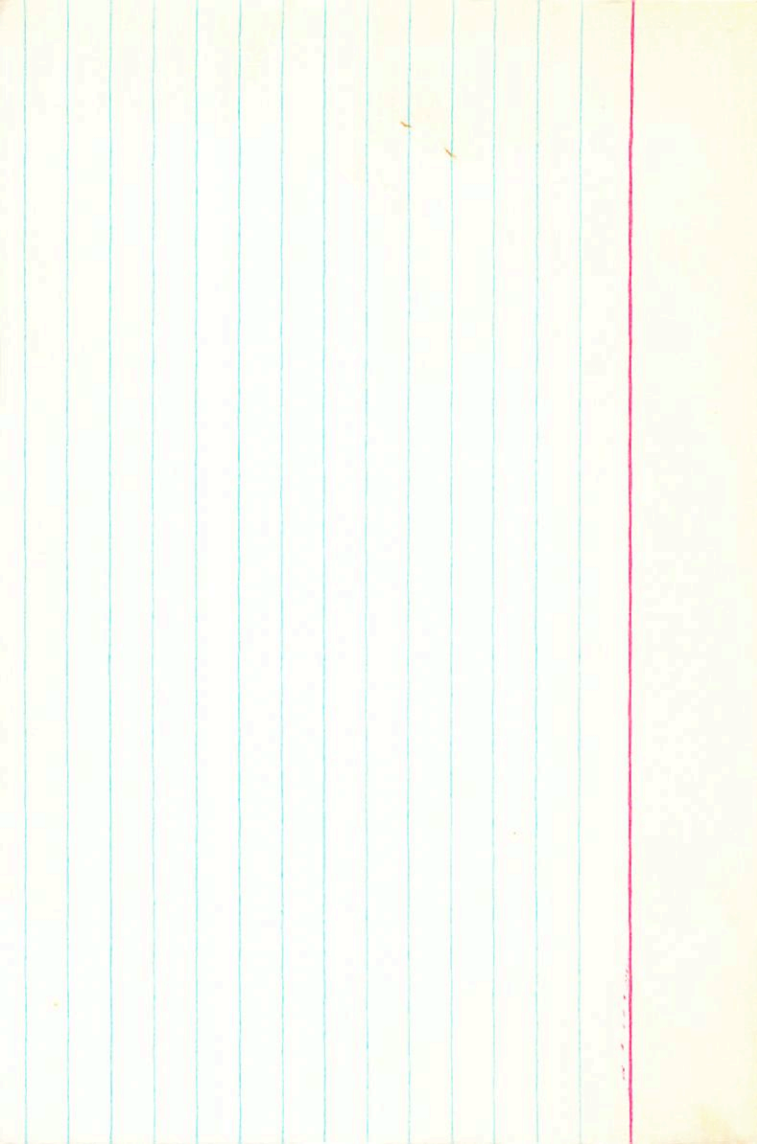
60"

$11.56 + 0.565 - 0.175 \text{ (2)}$

-67c

+260 +185 Pass

+240 +120 (pretax)



209977 22 046 +11 31 7.3 941-65.51  
 30929 -0014 -026 Latvian

13997 35.370 1503.7 +11 31 25.17 18998

6.80 +164 +197③  $\frac{102}{472}$

5.64 +0.855③ 35.457

530 1.10

420 471

7.70 35.440

-7 +3

-0012 -022

-015 -022

-629 -035 +6102

-017 -026  $\rightarrow$   
 -023 -030

-021 -033

33.4

559 82  
 4046 73

1.10

26.27

25.45

15

25.60

25.05

5

25.10

25.35

-92

1422

37.7

37.3

-0022 ± 113 -022 ± 8.5  
 -0002 -025

7.70 = 350 M.

797 543-262

-0566 -0566

-1132 -395

-223 +17.2

-158 607 779

+0112 -0633

-0521 -18.3

-69.3 -51.0

-582-580 -570

+0413 -0608

-0192 -6.7

+30.6 +37.3

22.100

11.500

-23.000

-33.000

7.500

316

-65.500

0.799

0.545

-0.254

-170.622

-37.319

-0.161

0.600

0.783

-75.753

-75.583

-0.580

0.585

-0.567

-29.681

27.799

21114

22

12.4 3510

68W F 18 (11)

2515222

0014 1011 674

$[-0.23 + 0.05]$

28

+

8.4

99114  
18114

R.A. : 22.200  
DEC. : -35.150  
PM. R.A. : -28.000  
PM. DEC. : 7.000  
DISTANCE : 8.400  
MODULUS : 479  
RAD. VEL. : 0.000

q1 (U) : 0.808  
q2 (U) : 0.202  
q3 (U) : -0.554  
dU : -80.998  
U : -38.768

q1 (V) : -0.178  
q2 (V) : 0.979  
q3 (V) : 0.097  
dV : 51.761  
V : 24.774

q1 (W) : -0.562  
q2 (W) : -0.020  
q3 (W) : -0.827  
dW : 60.316  
W : 28.866

93

23.0

23.7

27.0



213657

22 80.8 - 42 19 2nd F

45453

Combinator

1900  
254  
253

964 + 0.43 - 0.24 74"

46.46

-0077 - 250 7TC FHY

-0068 - 236 CCH

45

292

209

4944

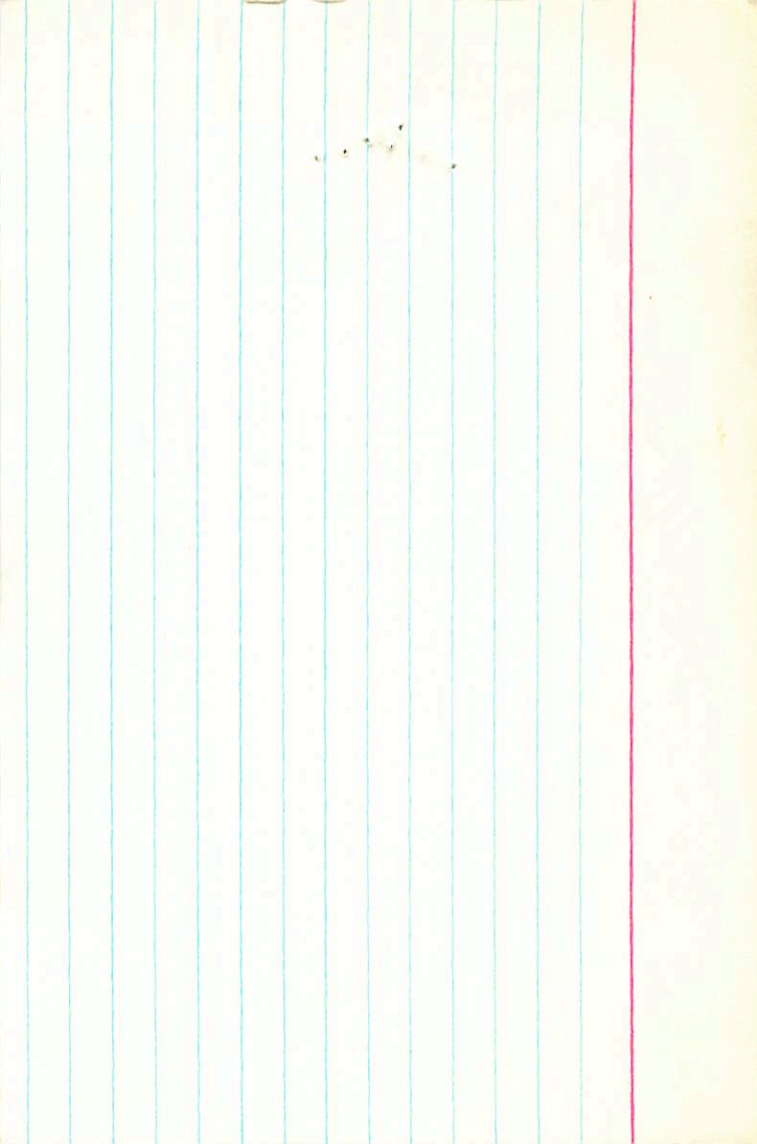
16

4944

5.5

580  
450-580

16



45483 213657  
-42015968

41111111  
22 30.9 -42 19 10.7 FS 47.2  
P2.5

9.64 10.40 -0.24 2 74"  
9.64 10.43 (1.48) FS II Cap

455.14C  
46.8350

-0059 -250 CP  
-0068 -075±4

41  
144  
50  
41  
10  
15

-236 CR

19  
46.4

62  
14  
17  
4  
9

R.A. : 22.500  
DEC. : -42.300  
R.A. : -92.000  
DEC. : -253.000  
INCE : 6.000  
LUS : 158  
EL. : 46.400

(U) : 0.832  
(U) : 0.175  
(U) : -0.527  
dU : -477.620  
U : -100.136

) : -0.227  
) : 0.973  
) : -0.037  
V :  $\frac{1}{2}$ -1093.558  
V : -175.032

) : -0.506  
) : -0.151  
) : -0.849  
W : 343.780  
W : 15.080

710  
-150  
-289  
+51

212630 22 30.8 -50 13

68/NO (II) W

5011713

Methods look very weak;

PF<sub>2</sub>H<sub>2</sub>

CH is strong.

-21

-009-009 C

-005-013

-8

-13

6.5 ✓

R.A. : 22.500  
DEC. : -50.200  
PM. R.A. : -8.000  
PM. DEC. : -13.000  
DISTANCE : 6.950  
MODULUS : 245  
RAD. VEL. : 0.000

q1 (U) : 0.832  
q2 (U) : 0.100  
q3 (U) : -0.546  
dU : -26.385  
U : -6.477

q1 (V) : -0.227  
q2 (V) : 0.959  
q3 (V) : -0.170  
dV : -53.557  
V : -13.147

q1 (W) : -0.506  
q2 (W) : -0.266  
q3 (W) : -0.821  
dW : 28.666  
W : 7.037

6.0

~4.2

8.5

4.4