

HR1686

5 14.3 +79 11

DFY -9.9a

~~DFS -48.88 apt~~

W3137/8

5.02 +0.46

F4E

-076 +158 Gc

-076 +159M

AOS3864

apt. sp. 9

-082 +160 F

-078 +159

51 A (25)

536 (10)

-0288

+161U W3 50

-8

+160 ✓

828

-0789

-443

159

1.6

-9.9

-083 +159

0223-8401
-7019 5425

580198 582 157 -025 +159 -9.9 156 -9.7

076-153, 015, 031 213 -7.6 -1.9 -0.4 -1.5 06

35 +3.1-15.7-7.4
[-1.6 +2.5 -3.7]

05

44-275
+2.6 13.2 -9.7

[-15.2 +9.4 -8.6]

05

+2.3 -11.8 -7.9

[-13.9 +0.5 -3.5]

33503

5 14.8 479 01 FELI

1686HR

554455

5.15 + 47

AR 5.04 + 88 - 14 2 Eggs

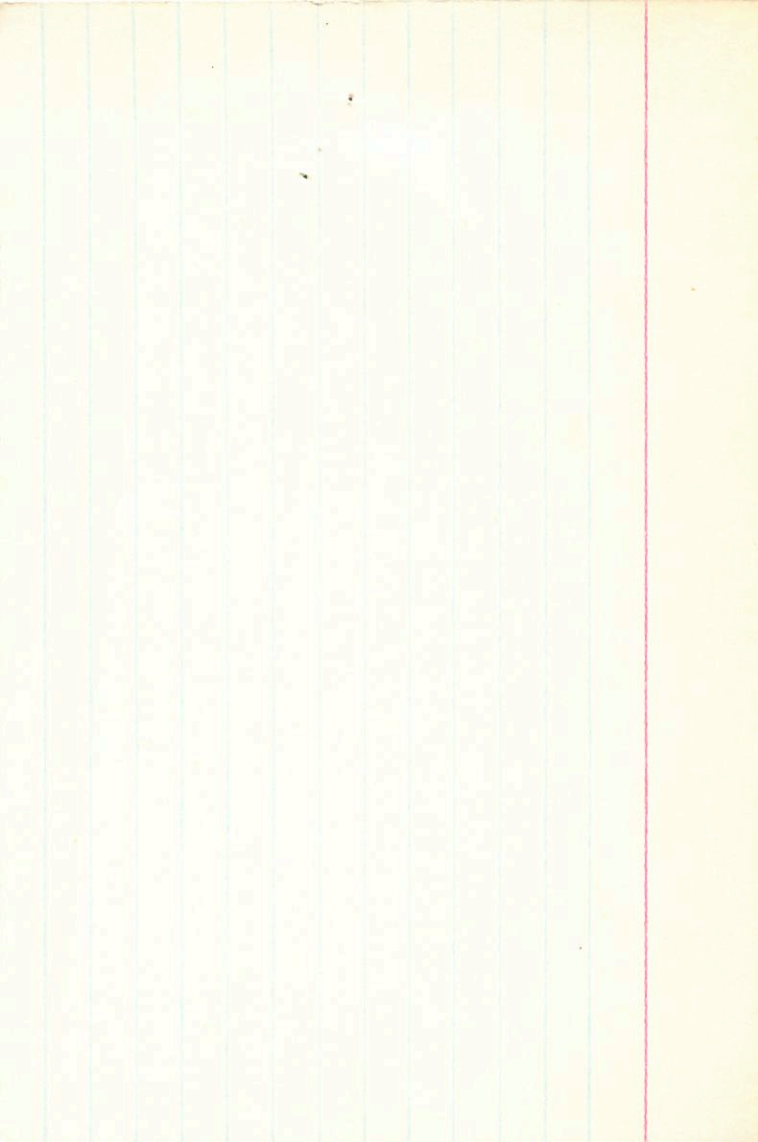
5.05 321 161 431 2635 dm

122
154

521

250

515
444



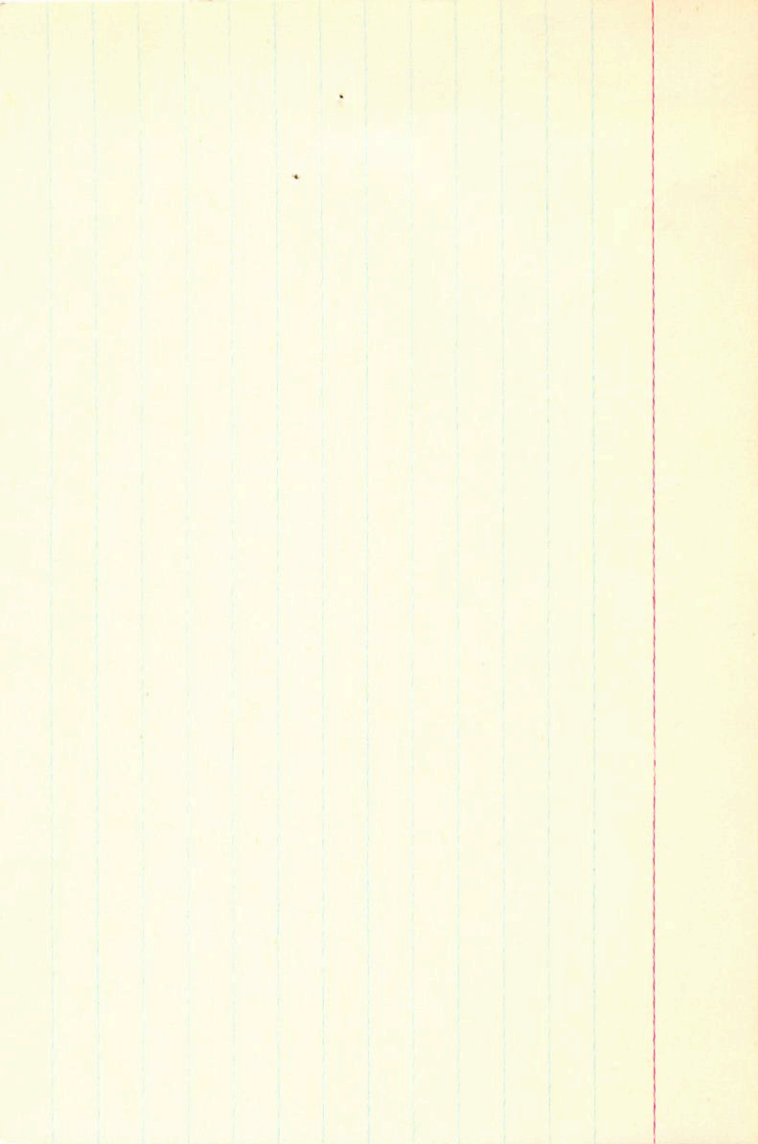
34

5 14.3 +79 11 9.0 PFS -4488

3138

+059 -142

+052 -142 G'(6)



196am

33564

5

14.3 479

11

5.2

d=4-9.9a

3137

6458

A053864A

Optical
Op. 9.0

77

-6271 +159 N30

-0271 ±1.2 +159 ±1.1 GC → N30

65

R.A. : 79.200
 DEC. : 79.200
 R.A. : -443.000
 DEC. : 159.000
 EXISTANCE : 1.000
 MODULUS : 21
 RAD. VEL. : -9.900

p1 (U) : 0.102
 p2 (U) : -0.793
 p3 (U) : 0.938
 pU : -919.380
 U : -19.189

p1 (V) : -0.271
 p2 (V) : 0.479
 p3 (V) : 0.997
 pV : 282.921
 V : 2.937

p1 (W) : 0.814
 p2 (W) : 0.434
 p3 (W) : 0.380
 pW : 0.723
 W : -3.878

P
 P

R.A. : 5.250
DEC. : 79.200
PM. R.A. : -443.000
PM. DEC. : 159.000
DISTANCE : 1.600
MODULUS : 21
RAD. VEL. : -9.900

q1 (U) : 0.105
q2 (U) : -0.763
q3 (U) : 0.638
dU : -616.230
U : -19.189

q1 (V) : -0.571
q2 (V) : 0.479
q3 (V) : 0.667
dV : 585.691
V : 5.637

65
q1 (W) : 0.814
q2 (W) : 0.434
q3 (W) : 0.386
dW : 6.723
W : -3.678

1734 5 16.0 +33 56 AS +723

3444 +190

6504

+0034-017
+042-017

148 154 820 791

2757 ③ SAC

57
-17
497
723

66

34721
5C6511

5 16.6 -18 11

100 440 C
+340w(3)
+48. Md(2)

1747

W3148

5.95 +0.54 - ceape

71213

8272 +063
~~10358~~ +061214

-1801051

+382 +059

+37 -43 +21 .04
+35 -38 +12 .050
+34 -37 +9 .059

546
574
3206

+383 +056 130

+352 +062 65

BBN
385600

+361512 +071597
7328 +064

3825 +059 130+

390 1.15
3837058

59513

$$\begin{array}{r} 36.930 \\ 1.136 \\ \hline 37.794 \\ 36.684 \\ \hline +1.11 \\ \hline 37.894 \end{array}$$

7.6

$$\begin{array}{r} 70268.54 \\ 0264 \\ 0270 \\ \hline 6258 \\ \hline 34.8 \end{array}$$

$$\begin{array}{r} 7062.44 \\ 2.63 \\ 55.24 \\ \hline 57.87 \\ 56.30 \\ +1.5 \\ \hline 57.8 \end{array}$$

0.53
0.10
7.6

$$\begin{array}{r} 32.402 \\ +1.6 \\ \hline 34.0 \end{array}$$

(6780)

$$\begin{array}{r} 53.58 \\ +1.2 \\ \hline 53.8 \end{array}$$

$$\begin{array}{r} 32.443 \\ +1.6 \\ \hline 34.0 \end{array}$$

(64.19)

$$\begin{array}{r} 54.20 \\ +1.6 \\ \hline 54.14 \end{array}$$

9



1. The first part of the document
 discusses the importance of
 maintaining accurate records
 of all transactions. This
 is essential for the proper
 management of the company's
 finances.

The second part of the document
 outlines the procedures for
 handling customer inquiries.
 It is important to respond
 promptly and courteously to
 all customers.

34721.000*

5.000*

16.600*

-18.000*

-11.000*

0.383*

0.058*

1.150*

2674

16.982

40.000

0.380

0.675

353

33.466

-0.868

-0.564

-4106

-37.317

67

1.573

-0.475

1514

7.729

1740

5

16.7

+33 54

ASTB

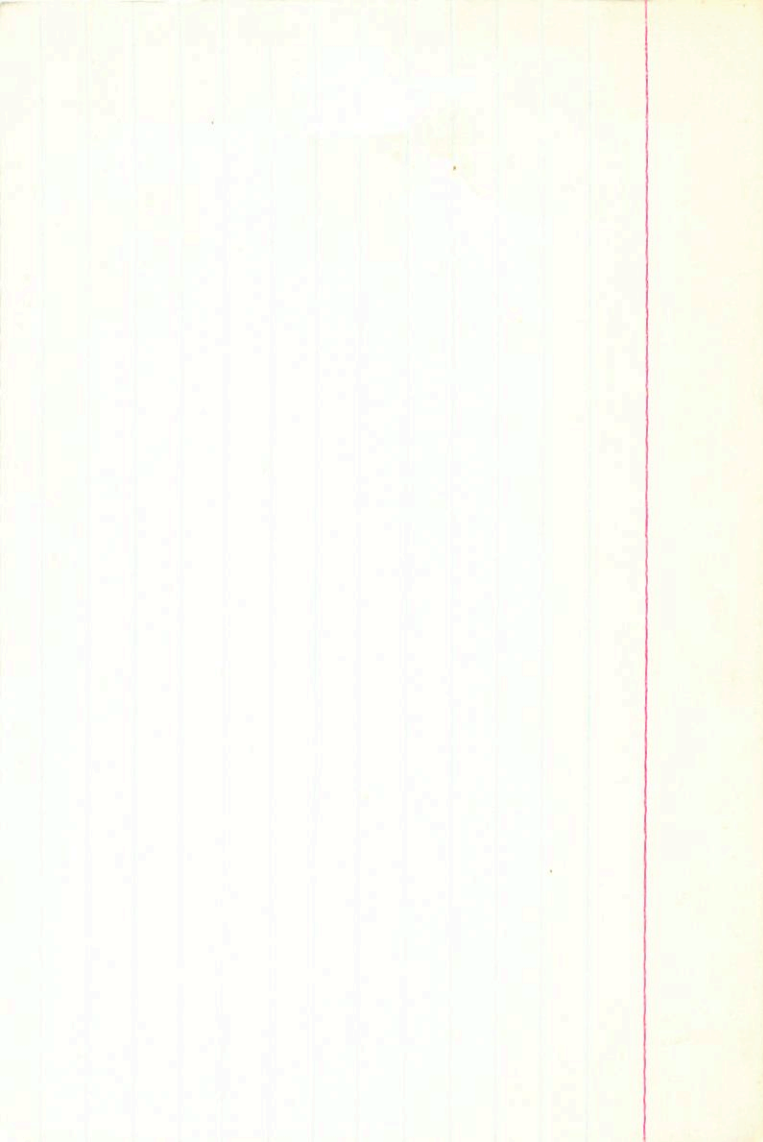
34578

6515

5.02 + 0.28 + 0.40 = 23.4 -

226 060 1.559

② 508



1745

S

217

+ 7756

AY

-160

34653

32422

and sold

138000

A 0 5

MS

612-007

1811 921 880

1511 220 1516

256
-76
414
-160

-627

030 6.41

68

1774

5 20.8 + 14.35

A > E

35189

6.06 + 13 + 13 15.95 ~ ~~14.8~~

6423

6

075 164 672 - 2875 (2) S.A.E

47
11

180
300

114

$\Delta M = +38$

Bud 51

058 + 180 1.057 2875

20
20

1056
416
1444
56

$M_v = +1.0$

-6019 -018
16
-0206 0168
+5
-0295

$M = 5.05$

+20916

410-620
-029-017

69

1774.000*

5.000*

24.000*

15.000*

39.000*

-3.029*

-3.017*

5.050*

102.329

23.900

-3.029

3.973

17.423

3.011

-3.131

-1.572

-3.156

-3.182

-13.916

69

1777 5 208 + 5 17 A0

35240
6626 10016 10017

6.34 + 0.12 + 0.08 C

10016 + 10017

~~063 183 991 2.869 at of~~

570
A=85
N=38

366
13577
126
1483

978

27
+ 496
+ 90

69

1073
1073
1073

067171 999 2.866

986

1045

518

1.33 - 0.53 1.387

036 618

206
1.4
4.9

70

35850 5 248 -11 57 1F17

H1R1817 6.30 +0.54 +0.25 239

GLB726 1351 .195 .304 2.634 @ 2441

[m] 258-5

[C] 234 /

+0010 -0.47 2.618
+0006 -0.49

+0088 +011-050

5.4
-11.95
+11
-50
1.3
+18.8

2.00 +8.4 -17.3 -8.8
-145 -150 -28

44926 114

$$\begin{array}{r} -31 \\ \hline 44957 \end{array}$$

$$\begin{array}{r} +10008 \\ +10012 \\ \hline 20020 \end{array}$$

$$\begin{array}{r} -0.54 \\ -0.45 \\ \hline 29.63 \end{array}$$

$$\begin{array}{r} 1.50 \\ 27.73 \end{array}$$

44939

$$\begin{array}{r} +25 \\ \hline 4515 \end{array}$$

$$\begin{array}{r} 67.25 \end{array}$$

$$\begin{array}{r} 30.54 \\ 30.54 \end{array}$$

44935

$$\begin{array}{r} +27 \\ \hline 44899 \\ +20 \\ \hline 44919 \end{array}$$

$$\begin{array}{r} 69.12 \end{array}$$

$$\begin{array}{r} 89.08 \end{array}$$

30.24

$$\begin{array}{r} +2.34 \\ \hline 29.90 \end{array}$$

1819

35509

5 258 + 13 38

+250

+0.50
+1.24

+0.10
109

1605
052177 1026 284

6.34 - 0.30 1.403

+0.001-0.004

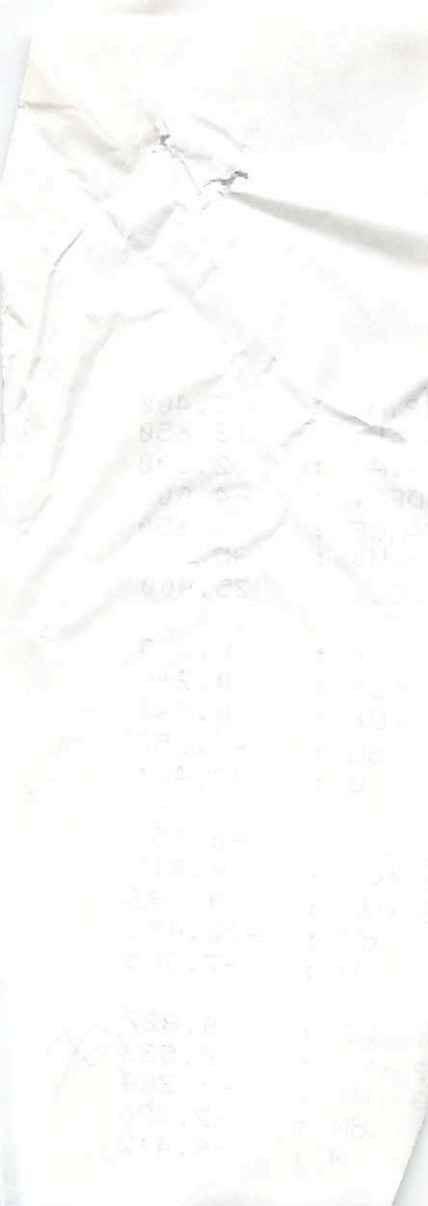
+0.01-0.04

2
-4

5.65

0.50

21



R.A. : 5.400
DEC. : 13.650
R.A. : 2.000
DEC. : -4.000
ANCE : 5.650
ULUS : 135
VEL. : 25.000

(U) : 0.070
(U) : 0.264
(U) : 0.962
dU : -4.357
U : 23.461

(V) : -0.557
(V) : 0.810
(V) : -0.182
dV : -20.496
V : -7.305

1 (W) : 0.827
2 (W) : 0.523
3 (W) : -0.204
dW : -2.296
W : -5.412

3585

5 273

-68 40

H.C

36589

-1011-010

-1016-010

1832 5 27.6 115 20 A35

36162
6505

5.89 + 0.11 + 0.01555 -
+ 0.4 + 146mm

59

20
1/1
1/1
5
10
15
20
25
30
35
40
45
50
55
60
65
70
75
80
85
90
95
100

2800

060 168 1.093 2.856

$\frac{336}{500} = 0.672$
 $\frac{179}{500} = 0.358$

2.0

a = 0.94564

n = 0.880

179
358
1081
 $\frac{6439}{6549}$

-0.177 - 0.517
- 82
- 25
 $\frac{484}{-0.25}$
 $\frac{1500}{-0.34}$
- 120

+ 0.6 ✓
5.15

22



1832.000*

5.000*

600*

1854 5 30.3 + 34 41 A4 \bar{V}

36454

6868

6.27 + 15 + 16

103 168 1.040 ② JPL

2.834 JG 1

-7.4 (unlabeled)

-1020 - 0209 - 5
+
1110
- 0014 / 020

1853

5 32.2

464 40

A5

36446

6909

1804
36714

5 324 147 41 413.5

1120

158206 } 102851
819 }
901 } 2776

1001108 FIR 5000

1011-018

16
-18

5110
4135

23

R.A. : 5.550
DEC. : 47.700
R.A. : 16.000
DEC. : -18.000
DISTANCE : 5.100
MODULUS : 105
VEL. : 13.500

q1 (U) : 0.036
q2 (U) : -0.321
q3 (U) : 0.946
MP : 29.266
M : 15.839

q1 (V) : -0.542
q2 (V) : 0.789
q3 (V) : 0.289
MP : -95.000
M : -6.050

q1 (W) : 0.839
q2 (W) : 0.524
q3 (W) : 0.146
MP : -1.820
M : 1.778



1872

5 316 +3 44 429 A2

352
1675
429

36777

6496

6.36 +05 +07 293

Callunk

84 176 336

028 168 1081 2.864 2592

X Swan

018 1211079 7951 1403 51

183

173

a=048 ✓

346

n=077 ✓

1.073

-0025 -010

1.421

+0.5 ✓

-037

1.473

4.85

-9

+04

74

1582

14456

11818

05 300 43 3

025

128 302 821

28x

88
82.5-8

4420

85.0 91.3

3.97 + 8504

85048104

618 033 1321
1201 1159

89
54

1047 9656
0599 9996

5384
6209

571
+110.8

75

R.A. : 5.500
DEC. : -64.000
R.A. : 42.000
DEC. : 58.000
TANCE : 5.110
DULUS : 105
VEL. : 10.800

1 (U) : 0.048
2 (U) : 0.998
3 (U) : -0.051
dU : 278.392
U : 28.730

1 (V) : -0.547
2 (V) : -0.017
3 (V) : -0.837
dV : -52.461
V : -14.556

1 (W) : 0.836
2 (W) : -0.068
3 (W) : -0.545
dW : 54.252
W : -0.180



1901

33.2 - 4 53 } FO

37077

524 057 1347

6945

5.26 + 0.24 + 0.18 } 43 -

used towel

903

148 184 558 2.264 } 2 SOC

used towel

035 179

Bank 51

000

+10

162

910

-90

+034

+068

151

025 5.3462

26

STATION	TIME	TYPE	STATUS
101	10:15	W	OK
102	10:20	W	OK
103	10:25	W	OK
104	10:30	W	OK
105	10:35	W	OK
106	10:40	W	OK
107	10:45	W	OK
108	10:50	W	OK
109	10:55	W	OK
110	11:00	W	OK
111	11:05	W	OK
112	11:10	W	OK
113	11:15	W	OK
114	11:20	W	OK
115	11:25	W	OK
116	11:30	W	OK
117	11:35	W	OK
118	11:40	W	OK
119	11:45	W	OK
120	11:50	W	OK
121	11:55	W	OK
122	12:00	W	OK
123	12:05	W	OK
124	12:10	W	OK
125	12:15	W	OK
126	12:20	W	OK
127	12:25	W	OK
128	12:30	W	OK
129	12:35	W	OK
130	12:40	W	OK
131	12:45	W	OK
132	12:50	W	OK
133	12:55	W	OK
134	13:00	W	OK
135	13:05	W	OK
136	13:10	W	OK
137	13:15	W	OK
138	13:20	W	OK
139	13:25	W	OK
140	13:30	W	OK
141	13:35	W	OK
142	13:40	W	OK
143	13:45	W	OK
144	13:50	W	OK
145	13:55	W	OK
146	14:00	W	OK
147	14:05	W	OK
148	14:10	W	OK
149	14:15	W	OK
150	14:20	W	OK
151	14:25	W	OK
152	14:30	W	OK
153	14:35	W	OK
154	14:40	W	OK
155	14:45	W	OK
156	14:50	W	OK
157	14:55	W	OK
158	15:00	W	OK
159	15:05	W	OK
160	15:10	W	OK
161	15:15	W	OK
162	15:20	W	OK
163	15:25	W	OK
164	15:30	W	OK
165	15:35	W	OK
166	15:40	W	OK
167	15:45	W	OK
168	15:50	W	OK
169	15:55	W	OK
170	16:00	W	OK
171	16:05	W	OK
172	16:10	W	OK
173	16:15	W	OK
174	16:20	W	OK
175	16:25	W	OK
176	16:30	W	OK
177	16:35	W	OK
178	16:40	W	OK
179	16:45	W	OK
180	16:50	W	OK
181	16:55	W	OK
182	17:00	W	OK
183	17:05	W	OK
184	17:10	W	OK
185	17:15	W	OK
186	17:20	W	OK
187	17:25	W	OK
188	17:30	W	OK
189	17:35	W	OK
190	17:40	W	OK
191	17:45	W	OK
192	17:50	W	OK
193	17:55	W	OK
194	18:00	W	OK
195	18:05	W	OK
196	18:10	W	OK
197	18:15	W	OK
198	18:20	W	OK
199	18:25	W	OK
200	18:30	W	OK



R.A. : 5.550
DEC. : -4.900
. R.A. : 0.000
. DEC. : 10.000
STANCE : 4.620
MODULUS : 84
. VEL. : -9.000

q1 (U) : 0.036
q2 (U) : 0.556
q3 (U) : 0.830
dU : 26.377
U : -5.257

q1 (V) : -0.542
q2 (V) : 0.709
q3 (V) : -0.451
dV : 33.588
V : 6.883

q1 (W) : 0.839
q2 (W) : 0.434
q3 (W) : -0.327
dW : 20.563
W : 4.672

76