

4056 10 16.4

-0023-001

-026-001

123
NUT

-41

25

A0

623

⁹⁶
-32125

842711

618

619

600

-27

127

128

611

826

228

4901

-0032-002 / story

10.25

-41.4

-44

+3

5.7

+23

-00315-001

-0354

033 1003

1049

~~89353~~

~~5-34424 1.49~~ 5.2 + 14

~~E=05~~

.235

~~.068~~

~~1.619~~

2.673

905

052

~~1.572~~

~~1.34~~

~~1.756~~

69

1



19.250

-41.400

-44.000

3.000

5.700

138

23.000

-0.812

0.578

-0.075

135.315

16.947

0.186

0.135

P
10 20.6 +65 49 Aug -0.6a

4.88 -0.05

-0.10 -0.236c

-0.04 -0.23 150

l to R Rm (100) (100) (100)

110 +46 100 -

Y18 - 508 512 410 - 007 - 023 - 0.1 - 021 0 - 0Y3
003 0 006 0 014 025 0 0 0 010

+1 +3 -4

+1 -4 -3

$$\begin{aligned} &+0004 \pm 2.0 - 003 \pm 1.7 \\ &+0006 \quad -00 \end{aligned}$$

45 Dec 10 25.0 +10.01 Ap -5.7 v(3)

$$\frac{-10.0 w(3)}{-7.2}$$

-0.06

0.06(4) -8.2 a

(8067781)

90569

14361

6569

$$0.596 \quad 1894.7 \quad +10 \quad 4.76 \quad 1890.4$$

$$\frac{-22}{574} \quad +18 \quad 4.94$$

$$\frac{.587}{.603} \quad \frac{16}{603}$$

$$\begin{aligned} &+5.14 \\ &+5.6 \\ &-2 \end{aligned}$$

(39.4)

$$4.69 \quad 1933.9$$

$$\frac{4.73}{4.73} \quad 1929.11$$

$$\begin{aligned} &41.330 \\ &19.260 \\ &0.590 \\ &+1.17 \\ &\hline &59.25 \\ &+0.23 \\ &\hline &59.48 \end{aligned}$$

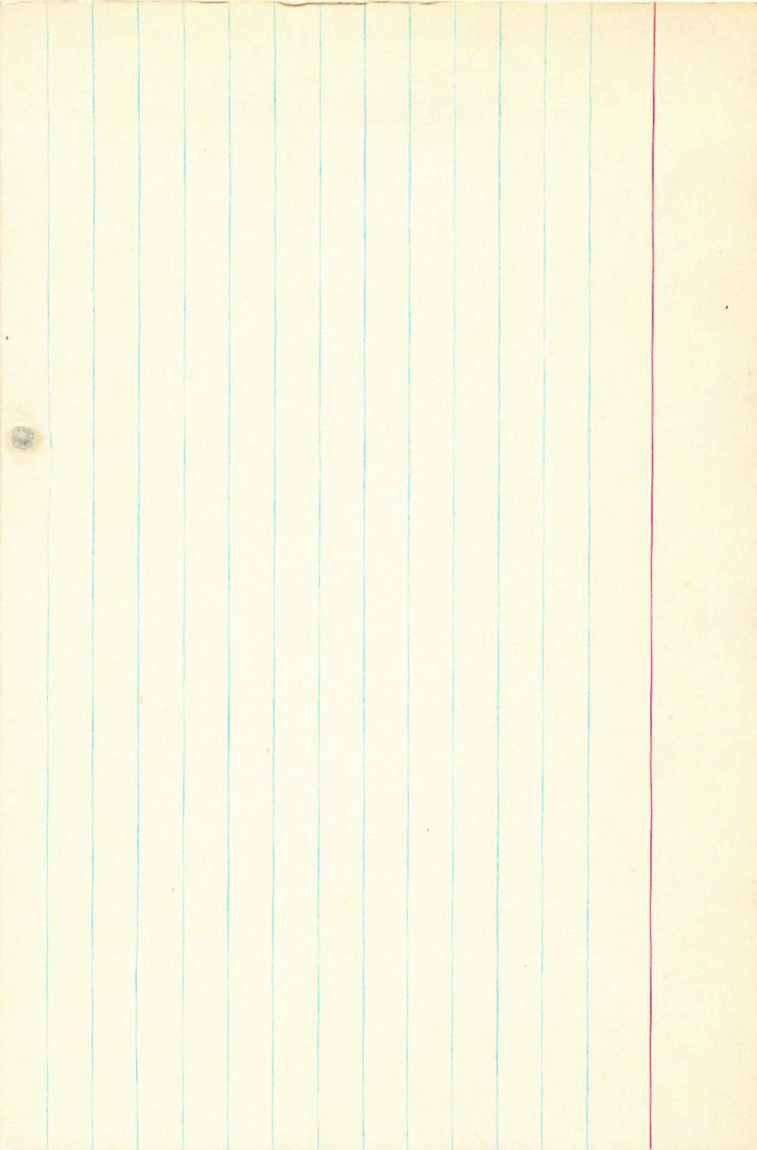
$$\frac{4.57}{-3.7} \quad 1929$$

$$\begin{aligned} &10.222 \\ &34.1 \\ &\hline &43.7 \end{aligned}$$

$$\frac{5.07}{5.07} \quad 1939.21$$

$$0.599 \quad \frac{14}{14} \quad .607$$

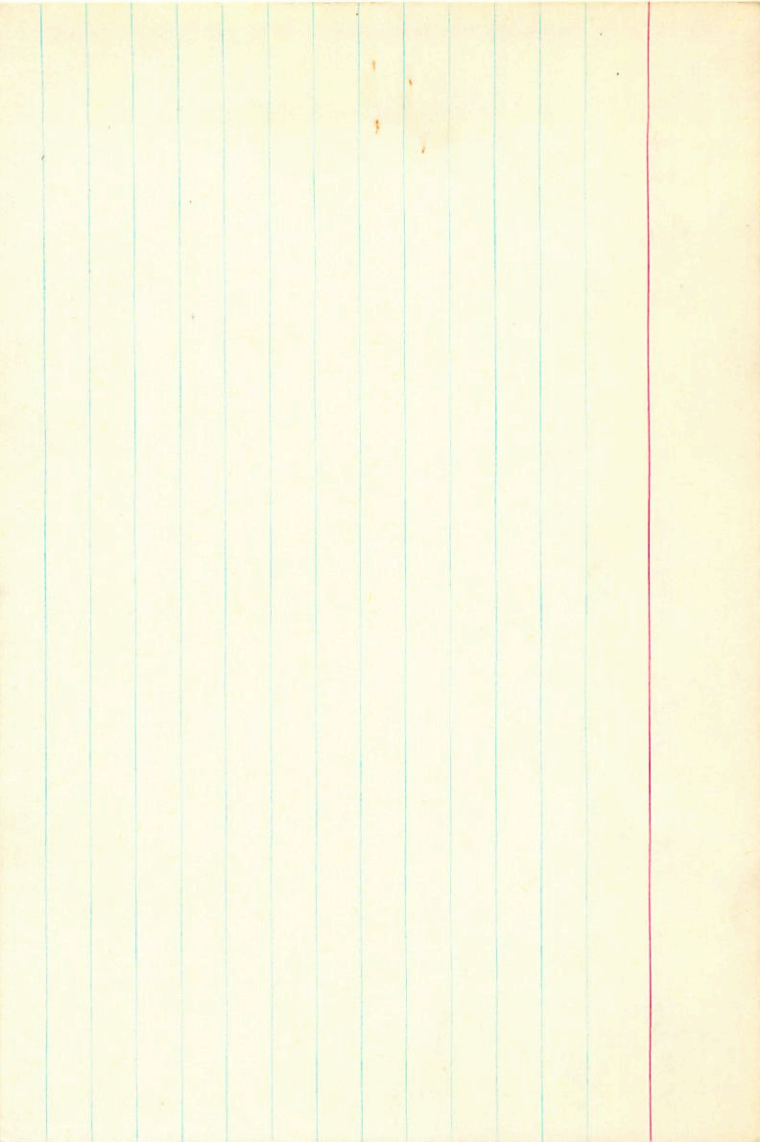
$$4.45 \quad +4 \quad 4.49$$



3.0000
~ 8.2 f

45.00 10 25.0 100 01

5.90 -0.06 -0.09



70

1850

1851

1852

1853

1854

1855

1856

1857

1858

1859

1860

1861

1862

1863

1864

1865

1866

1867

1868

1869

1870

1871

1872

7

1873

4101.000*

10.000*

25.000*

10.000*

0.000*

0.000*

→ 0.000*

5.900*

151.356

-7.800

-0.015

0.370

-5.180

0.040

-0.493

9.915

0.032

0.787

-1.26'

FD

4101.000*

10.000*

25.000*

10.000*

0.000*

0.000*

0.000*

5.350*

117.490 135

-7.800

-0.031

0.370

-6.563 7

0.000

-0.493

4.801 15

0.020

0.787

-3.816 3

70



10.400

10.000

9.000

2.000

5.600

132

-7.800

-0.825

0.425

0.373

-30.610

-6.947

0.211

0.843

-0.494

16.858

6.679

0.525

0.329

0.785

25.173

-2.805

ZB

SA esp

10 073 -30 22 89

8118

90972

KLH1

5.11.5

5.55 -04 (-12.5) C

540 -016⁴⁸

116

851 2886

2714924

111

454

222
1076

①

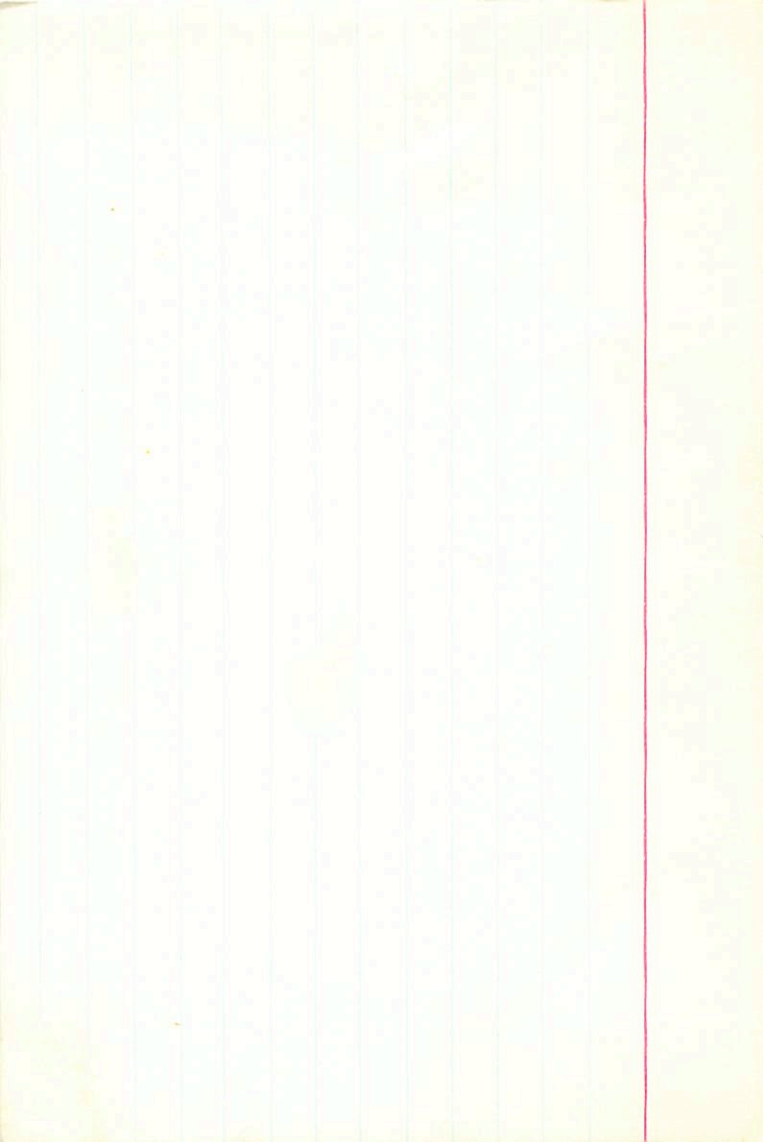
1003 v 002

1005 46

total

1110011111

8242-931
1263-4007



50790

4076

10

19.8

-19

37

40

9.19

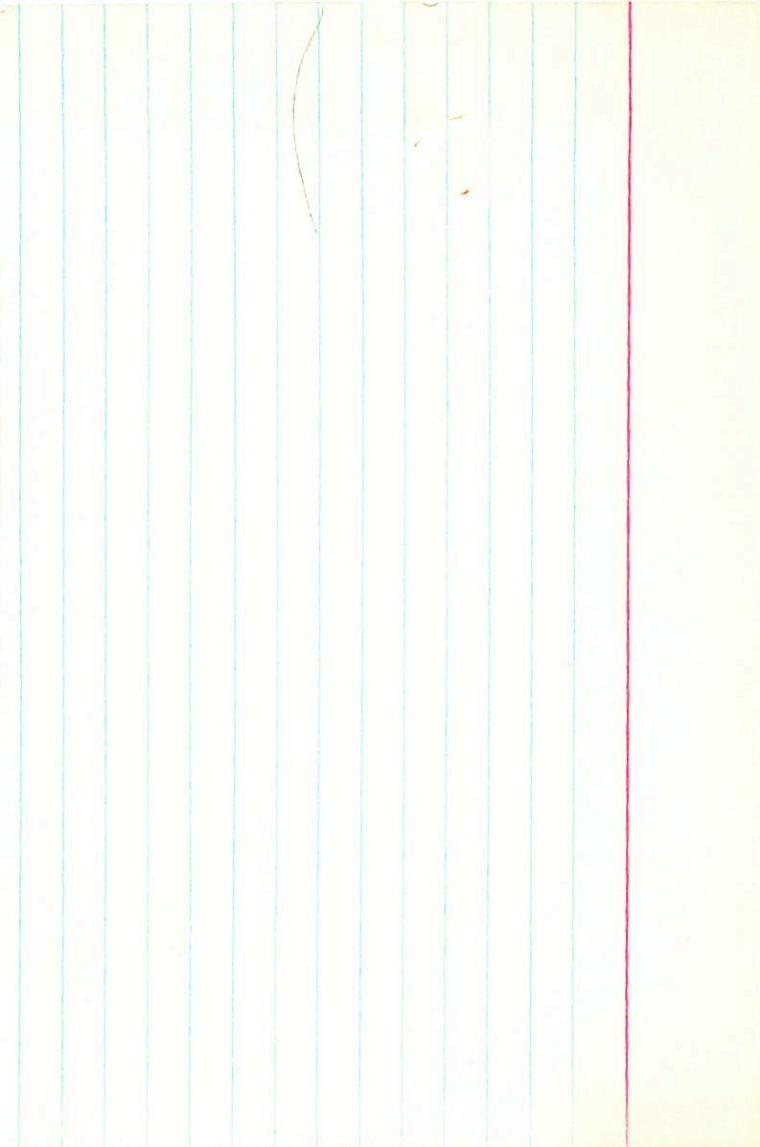
-34.76

WUW

463 0.74

8766

1189



8505 Si I percent maximum other multivalency very sharp lines

(MM) Si (St, Hz) 10 20.5 46.5 49 11.58

4072 Hz

84822

4.98 -06 -16.5

-2.6

-020 126 967 + 100000

-020 140 955 2827
134 959 2924
268
97

176
177

D₂ = 1.7

FIR4

50149 - 0253
+ 88

-50191

-50110 - 0214

Peak

505

+0.3

-0.4

06 149

-020 126 967 400
-020 141 955 2827
-10 139 947 2827

-18 135 956 2827
132 960 2922

264
1224

21

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100

100



100

100

100

100

71

4072.000*

10.000*

20.500*

65.000*

49.000*

-0.010*

-0.021*

5.050*

4.4

5.3

74.4

117.1

102.329

-2.600

0.047

0.567

+2

+4

3.333

-0.098

0.419

-8

-13

-11.085

0.020

0.710

0

+1

0.213

~~300000~~

-0007 E1.4
-0007 -023 E1.3
AOP M4g
Sp. A. = 11.6

89822 10 20.6 -027 E65 49 4.9 4.9 AD -0.12

14260

6528

33.032 1904.1 465 49 12.48 1901.1

$$\begin{array}{r} 110 \\ 38 \end{array}$$

$$\begin{array}{r} 1.12 \\ 13.60 \end{array}$$

33.099

~~205~~

$$\begin{array}{r} 12.68 \\ -12 \end{array}$$

194488

$$\begin{array}{r} 109 \\ 10 \end{array}$$

$$\begin{array}{r} 12.56 \\ 12.56 \end{array}$$

$$\begin{array}{r} 12.629 \\ 28.8 \end{array}$$

(34.7)

46.33 1933.3

(37.7)

44.556

48.920

23.346

23.346

0.116

0.116

0.116

0.116

0.116

0.116

0.116

0.116

0.116

$$\begin{array}{r} -33.00 \\ 13.33 \end{array}$$

$$\begin{array}{r} -92 \\ 12.51 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

$$\begin{array}{r} 12.51 \\ 12.49 \end{array}$$

49

$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$

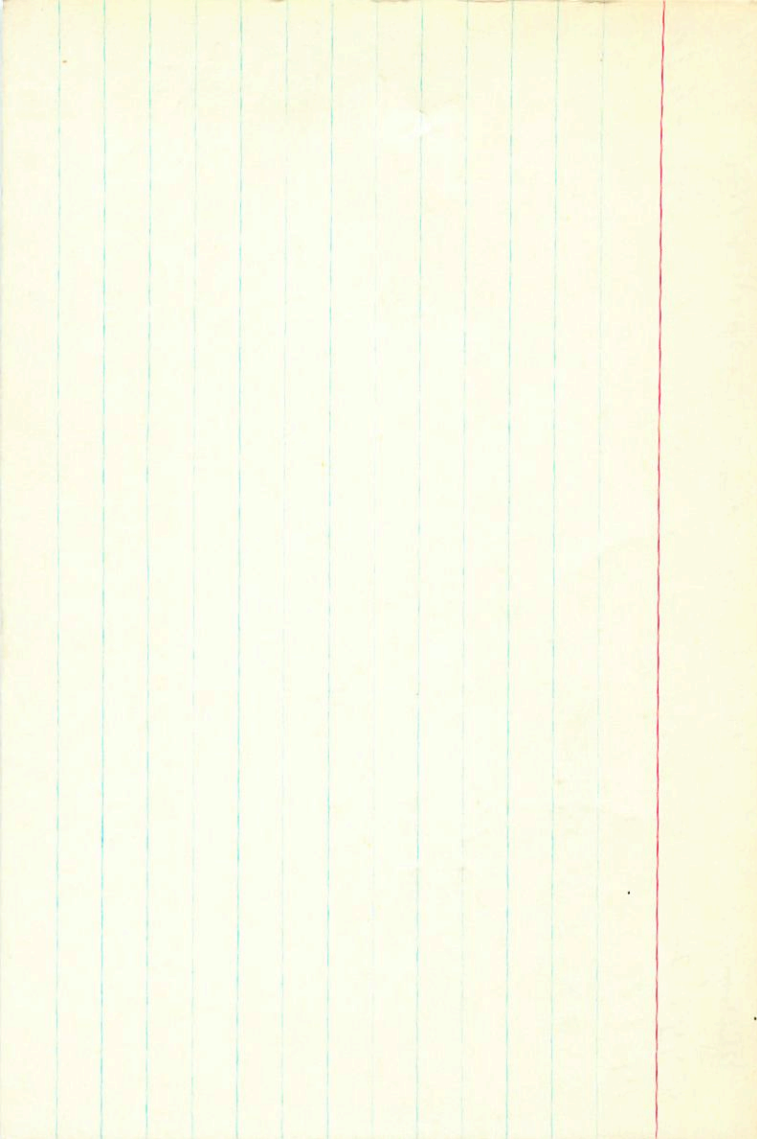
$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$

$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$

$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$

$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$

$$\begin{array}{r} 12.59 \\ -1.01 \end{array}$$



Prof

4072 10 20.5 +65 49 Ap

89822
14260

4.54 -07 -15 3 5

2.924

137 957
-16 020 +137 +554 (2)

28270

274
1233

74
-16
-80144 -0253 F144
+ 40

98
E=0

1233
116
117

(5)

~~020~~
274
116
117

120-010-

MV=0

82

4072.000*

10.000*

20.500*

65.000*

49.000*

-0.010*

-0.021*

5.000*

38 48
91.2

100.000

-2.700

0.047

0.567

2 3

3.167

-0.098

0.419

8 -10

-10.900

0.020

0.710

72 0

0.095

49 Leo TX Leo 5.70 +06 +07 16" EB SP.B, P=2.44 71654 0020
 91636 10 32.4 +8 55 5.70 AO 7167a

145-11 (K145) 24.819 1858.6 +8 5.4 33.28 1895.7
 -0038 ± 2.3 -011 ± 1.6
 -0036
 -0043

6618 24.72 695 3335 +60 8595 -9670
 195 24.72 695 3335 2816 -2732
 19 14
 744

ADG 737 24.72 695 3335 +60 8595 -9670
 8802 9910 25.014 33.88 2816 -2732
 4746 0458 24.863 33.21 23.54 1934.5 -10.257
 20 24.72 695 3335 34.2

SMV 25 6.088 887 35.6 1928.48
 213 18.930 887 33.57 77.97 1528.48
 24.9275 -12.7 -43.90
 24.9275 66.34 33.97 200 33.67
 8.17 35.434 33.67
 5.1 33.67
 5.1

24.819 1858.6 +8 5.4 33.28 1895.7
 24.819 1858.6 +8 5.4 33.28 1895.7
 21 33.51 1939.59
 719. 33.51 1939.59
 21 33.51 1939.59
 719. 33.51 1939.59

ADG 737 24.72 695 3335 +60 8595 -9670
 8802 9910 25.014 33.88 2816 -2732
 4746 0458 24.863 33.21 23.54 1934.5 -10.257
 20 24.72 695 3335 34.2
 35.6 1928.48
 33.57 77.97 1528.48
 -43.90
 33.97 200 33.67
 35.434 33.67
 5.1 33.67
 5.1
 24.819 1858.6 +8 5.4 33.28 1895.7
 24.819 1858.6 +8 5.4 33.28 1895.7
 21 33.51 1939.59
 719. 33.51 1939.59
 21 33.51 1939.59
 719. 33.51 1939.59

52.74 - 5.56 9556 - 2900 } 0532
705 0-99 2816 - 2080 } 1040

23

4124 10 24.0 +32 89 A01B

91120

5850807

14455

202

590674 657 1034 2.855

A01B

(S)

179 1019
558

435
215

-155

024 172 1024 40.3

10.5
+32.66
-16
+8

5.65

5.35

-614 +001

-0135 +005

4775
-15.5

W (M) EP
M



1.355 99.3

1001222.6 - 100222.3

12.19 41.6

△

10.500
32.660
- 16.000
5.000
4.750
89
- 15.500

- 0.832
0.260
0.490
59.288
- 2.311

0.228
0.966
- 0.127
0.357
2.706

0.506
- 0.006
0.862
- 32.459
- 16.261

74

9138

10 251

-71 44

91375

51436

27.94 - 20.04

1260 0.47

9286	4141	0289
		0815
	-9102-	
2710		

15011091

4131

91311

$655 - 07 - 01259$
 $+53$
 $10 \ 30.6$
~~46~~ AD

$-004 \ 152 \ 6025 \ 2.852$
 $151. \ 1074$
 202
 $\frac{1381}{109.}$

$109.?$
 1381

$-046 - 032$
 -0245

$+2:$
 -039
 $-005266 \ -022740$
 -033
 $36.184 \ 1.40034$
 $2.114 \ 853$
 1.62

052
 $\frac{439}{439}$
 $-0045 - 0235$
 $0047 - 0305 \ 22.74 \ 1146 \ 1844.7$

-7
 001
 0017
 -31
 $\frac{21.15}{21.15}$
 020

1091-039

6.4
 10.5
 $+53.75$
 -62.5

-26
 6.55
 $72.$

25



18.588
-59.758
-62.588
-26.888
6.558
204
2.888

145

-8.832
8.866
8.551
137.545
29.185

430

8.228
8.946
8.329
-156.484
-31.491

-36

8.588
-8.316
8.882
-49.688
-8.548

9

~~AS~~

4/5214

10

148

44

44

608

609

5.5	-08	102	247	2166	166	+00	-20	228
6.1	-0811	101	564	21648	150	+020	-145	255
								265

-0002	-008	10.5
-0005	-010	5.48
-0005	-004	-1.5
-0003	-006	-2
		8.65
		0

-0002

-001-002

76



10.500
-44.800
-1.500
-2.000
7.650
0.33
0.000

-0.032
0.535
-0.148
-0.873
-0.296

0.228
0.086
-0.978
-1.964
-0.666

76

0.506
0.841
0.193
-10.522
-3.565

4187 10 40.6 +57 27 B9

92728

14734

-02 -10

+015-057

+015-583

10.66

+57.5

-623 149 1011 2862

142-1016

+28

TOU 16 22.1 055 21.6
TOU 16 22.1 055 21.6

-53

57.5

34689 995

4431 942

-18.5

TOU 16

TOU 16

TOU 16

TOU 16

TOU 16

4185

10 38.5

-64

50

Apr

'50

92649

14685

5.52

-17 -56

34257

39.5

10014521

-0581.5

44.21 54.2

$\frac{-95}{692}$

10022

-660

$\frac{324}{4753}$

100205-059

4467

4491

34742

+00187

-0577

$\frac{-118}{44.49}$

$\frac{-1}{691}$

10151

1015-053.15

4135/b

10 29.8

-44 H8

08 (2) 14"
08 6.5

~~8/10~~

~~10000~~ ~~10000~~ ~~10000~~ ~~10000~~ ~~10000~~
-10000 -10000
10000 -10000
10000 -10000

A -0.4 by 1/2

B Vented by 1/2

10000 -10000

-10000

10000 -10000

25.75

5.76 -84 91
66

296 2.656 (2)

313
1343

564 2.651 (2)

6.14 -44 100
102 87

570

174
744

76

78

4135.000*

10.000*

29.800*

-44.000*

-48.000*

-0.003*

-0.002*

7.900*

380.189

-0.400

0.007

-0.147

2.626

-0.004

-0.970

-1.149

-0.015

0.193

-5.936

78

4203

10

43.1

+30

57

B9V

10.7

+8/

~~-25.5~~

-33.5

5.25

+14

0230

-022-0335

-00179-0375 W50

~~-00175-0350 F114~~

~~00194~~

~~0416~~

~~00192~~

~~0400~~

0234
-023-0330

(+01)

5.36-06-15

49

5.35 -026

132

965

2821 A1V

124

970

248

1218

$M_V = +0.15$

$V_0 = 5.30$

5.15

+13.0
Wanted

F14 (2M) 40 plus

4283.000*

10.000*

43.100*

30.000*

57.000*

-0.023*

-0.036*

5.150*

107.152

~~5.000~~

4017

10 44.3 - 60 20 6.25 APR

Spd 26.40.

-0077581 -018 55.1

24025 612 22.22 941.1

10.700
31.000
-25.500
-33.500
5.250
112
14.000

-0.845
0.297
0.445
40.401
10.758

0.260
0.955
-0.143
-178.566
-22.044

0.467
0.006
0.884
-49.299
6.847





1578.000*

4.000*

53.300*

5.000*

19.000*

-0.003*

-0.011*

5.250*

112.202

21.600

10967

5.2
110

-0.029

0.896

416

16.116

-0.014

020207¹¹

428 10 48.2 -15 00 A0

(A) ³³⁰
-0050-42 -044

88,34 +15, -44
41.45
43.35
1.9

85952 6.5
345
300

88,34 +15, -44
41.45
43.35
1.9

-0076-047

9034
+10
096

-0076-047

9034
+10
096

93.42
+2.5
91.45
43.

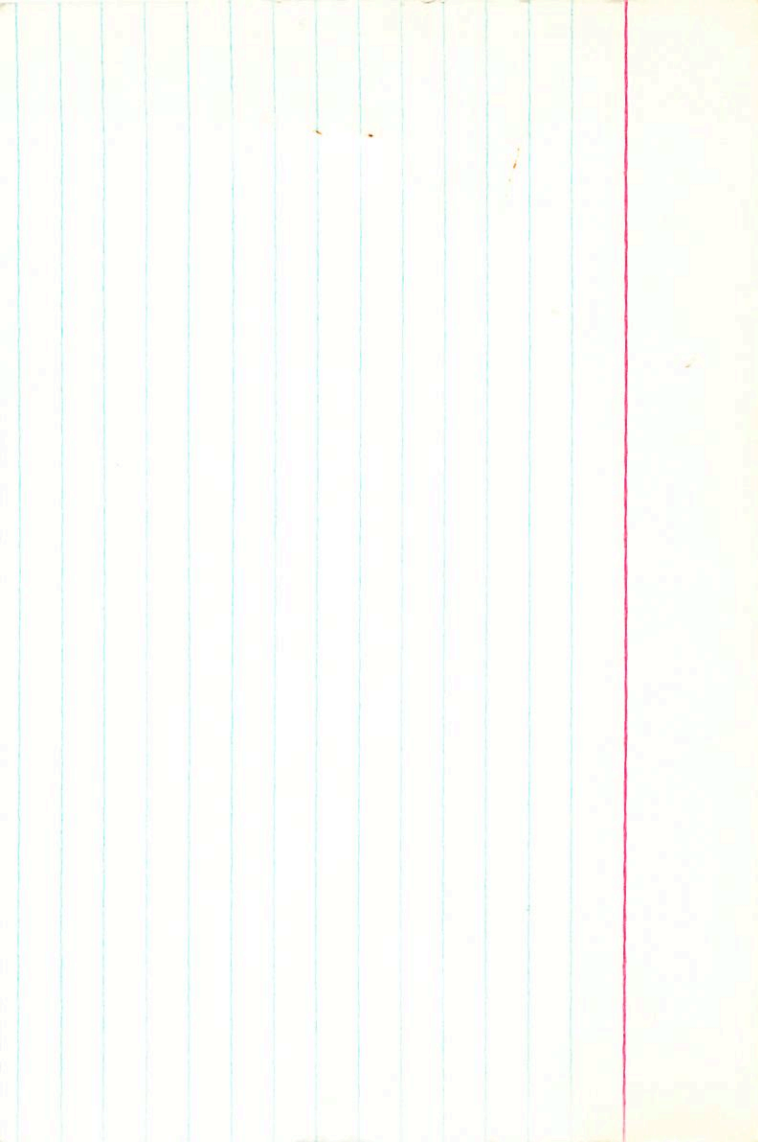
-00575-0468

9034
+10
096

-00575-0468

9034
+10
096

Group
1 on hand



5.25 - 0.8 1.34 - 13 05 15

4221

10 45.0 - 56 30

93563

46 25 6

-029 105 741 2.664

100 747

200

947

5.1

-2.25

7.35

+31.0

-0016 -0145

-00147 -0091

-0122

-010 -005

8535
~~86352~~ 9 54.5 -51 06

56.131
060
 .091

19126

-0016 ± 5.7
 -0016
-0006
 -0003 -012

-012 ± 3.7
 -017
-008

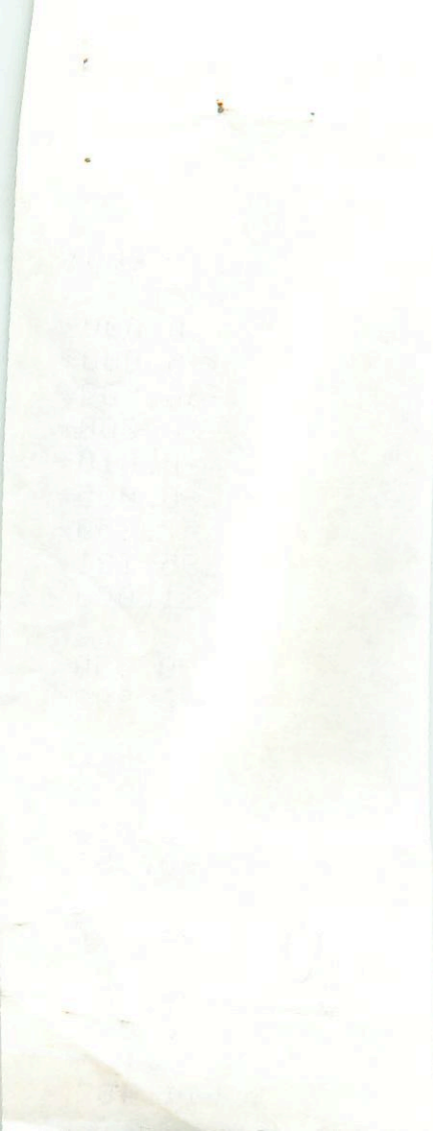
35.73 19054
54
 35.19

56.094
+015
 56.109
 038

56020
+15
 56035

35.39 (70.17)
-00
 35.64

35.59 1941.40
-21
 35.80
 -61



4221.000*

10.000*

45.000*

-56.000*

-30.000*

-0.010*

-0.005*

7.350*

295.121

31.000

0.030

-0.283

-0.056

-0.010

-0.958

-32.767

-0.043

0.036

-11.487

80

4221

10

45.0

16

30

8 1/2 Me

5.2

025099772 2.684

(090)

747

(929)

0010-012
0108

014-010
012-006

008.5-008

10.75

56.5

755

8

5026.95

131

6.25

|

81

$$P = 15.5$$

wumc 10 51.1 +4327

-17.4a

1+R4248

4.80

+046-0306c

W6753

AIV

+052-025N

+048-029

10041-021 PAS Aug 7

100-201
Lno
100

425

999

915 -113

Mundo Q450

1348

1400

1348

1400

1348

1400

2.96 - 9.55 ✓ 68F 72.5 ✓ +0.44 - 0.29 - 17.4 - 0.20 - 12.0 - 0.55 ✓
-0.15 0.06 - 0.47 0.19 - 1.61 - 1.94 - 12.6 + 12.0 - 3.7

+1.3 - 16.7 - 18.6 0.15 ✓

+23.4 - 5.4 - 7.1

0.1
0.255

-4.1 - 23.1 - 2.19

0.25

+5.7 - 11.3 - 16.0

-16.9 - 4.1 - 10.6

Sp. B. P. =

94334 10 51.1 +43 27 4.8 A0 -17.4a

14974
6753

+0048²² -028 N30
+0044 ±1.5 -027 ±1.2 C → N30

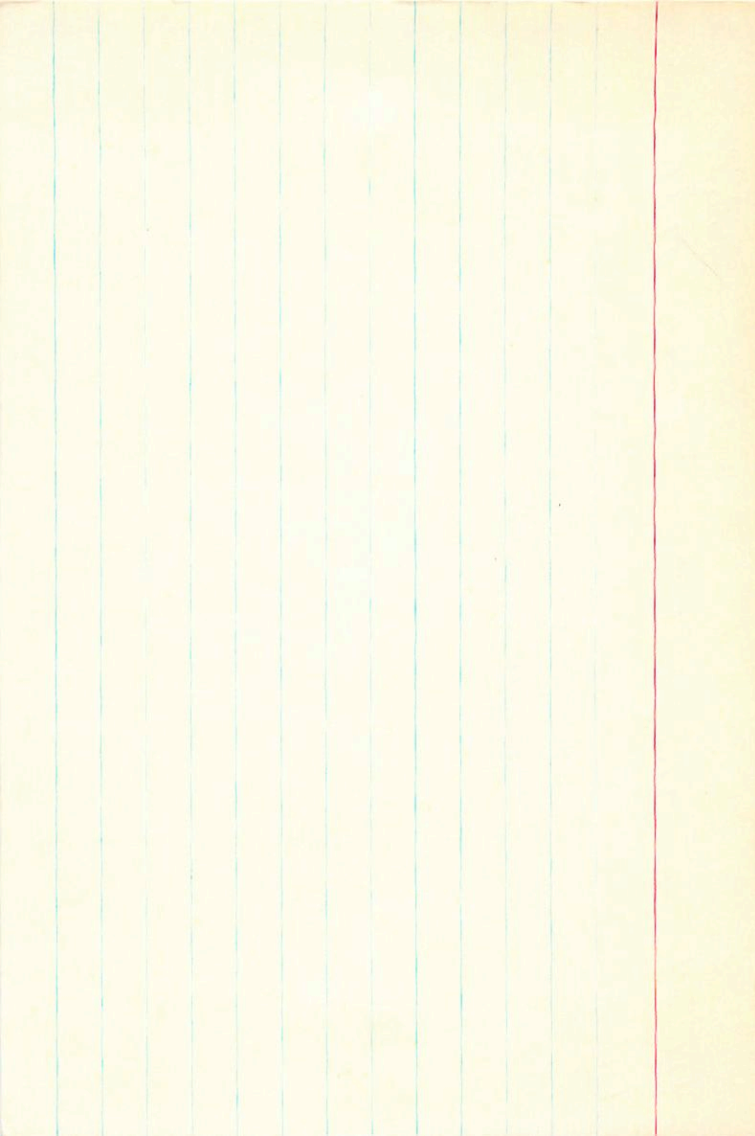
PR5 Sump

+009 1021
+009 1001

1.0000

→0044

1001-021



3p.51 = 0.043

WUMM

01

5/1

+43 27

-124a

JH2h

3h

A15

+046 -0306

+052 -025N

+046 -029F

+045 -029

254-955 688 725 +045 -029 -124 -020 -12.0 -095

-014 006 -046 019 -156 -150 -12.6 +12.0 -3.7 017

+28-149-188
+2.2-5.3-8.3

-3.6 -227 -2.9 01

-30.5 -7.9 -3.2

+4-14-17

019

+1.6 -16.4 -18.6 015

-20 -5 -9

-230 -5.9 -7.4

+4.8 -11.0 -15.3

03

-16 -3 -11

+5-7.5-14.5

04

(25)

-13. -3

B2094 4 25.2 089 269 930 1.002

1213 81592 10 52.7 412 89 611 App SWA

2094 + 1/2

2

9337W

44642 84 -0087 -007 144
152 594
594

2.95 6.7 607 1252
30 2.65
305 39.54 600-8327
Swi 5745

44641 19463
418.48 2.52 1613
658 out 165.596

-0038 -009 + ?
-00367 -0063 8.98

Swi-9430 15 = 0356

6090

3.09 54.88

038.5-002

-004K

445504
6.17 594

3.19 70.20
-17
3.36

9449 1000 / 0960
3148 - Very / 4020

9449 1000 / 0960
3219 - 0185 / 0517

1009
873 26 2001

4292

10 57.7

-43 32

89

10067 + 1058

10065 + 1035

-4.6

10060

10064 + 1018

59
5.90 -42 183 828 2832

120 836

240

1076

10.55

-0068 + 100 + 57

42.284 65.1 10006 1008 14.28 93.2

$\frac{353}{4.137}$ 10071 1002 1005 14.51

420647 -6 10080 10087 15.52 56.87

688 10090 14.0

1002.5 1013

420622

27

629

14.11

69.96

28

-21
14.32

11.000
-43.500
-100.000
13.000
5.450
123
-4.600

-0.060
0.462
-0.216
324.265
40.887

0.307
0.132
-0.942
-97.566
-7.669

82

0.407
0.877
0.256
-85.722
~~-11.723~~

4262

10 57.7

-43 32

08/53
5781

-035 130 730 2821

(19) 83P
23P

11.0
-43.5
-900
+13
87.5
-4.6

-0058 +004 Part

-0067 +010 sty

-0065 +015

-0062 +010

-0675
-0655 +014

83

4263 10 52.8 -41 59 A0.00

! round

4222 1052.0

-70 27

188

4290 10 57.2 -61 03

-24, 127 716 2044 94

6.15 -35 132 204 2803 (2)

122 711
244
955

-1004 + 0005 604

-1004 / 1001 + 15.7

-1005

6.1
4
(5.7)

-0367

-035 + 005

12.874
1904.3

-6036373
-0162

+00944.7
-007
7.98
18925

164

13.038

-47
825

12.455

3.15

12.990

.860

+25

883

-153

~~2685~~

6.15

1.800

7.97

27

8.24

-24

848

-23

1929.01

3



-3.000*
-0.035*
0.005*
5.700*
138.038

15.700

0.152
-0.340

15.575

-0.054
-0.940

-22.163

-0.047
-0.023

-6.918

-0007 12.0 +030 ± 1.7
-0001 +089

60 bu 10 58.7 +20 27 Am -10.27

4300 ~~7.36~~ +0.10 0.2

95608 4.42 +0.07 +0.05 +0.5 -0.07 60

15162 -0.05 +0.37 F

6814 39.777 1904.3 -0.10 +0.30 C
032 +20 26 53.99 1900.0
809

-1.50
52.49

53.57 1933.1

31.8

1611
806
-003

39.815
10
825

53.78
54.04 1939.07

39.766
18
786

12.17
36.1

53.90
+1.41

36.1

259 - 966 350 937 ⁻⁰⁰⁶ + 1075 + 1033 - 10.2 - 10.2 - 4 + 1075
 + 1075 - 003 + 1075 2. ~~1075~~ ¹⁰⁷⁵ - 9.6 + 9 - 2 024
 + 1066 + 1052



+5 -4 -12



HR +1 +3



022

020