

R.A. : 18.700  
DEC. : 37.550  
. R.A. : 30.000  
. DEC. : 20.000  
STANCE : 3.600  
MODULUS : 52  
. VEL. : -26.000

q1 (U) : 0.225  
q2 (U) : 0.899  
q3 (U) : -0.376  
dU : 110.575  
U : 15.579

q1 (V) : 0.402  
q2 (V) : 0.266  
q3 (V) : 0.876  
dV : 70.559  
V : -19.074

q1 (W) : -0.887  
q2 (W) : 0.348  
q3 (W) : 0.302  
dW : -67.023  
W : -11.369

13

+1.72  
+1.56  
+1.61  
+1.4m

18 439 -1 01 Am + 4m

7059

173654 (A) 588 054 4356

257B AB 588 + 14 + 10 596

0131444 7582 2896 17419.0  
(51)

787 + 31 + 08 804 + 08 396

110-100

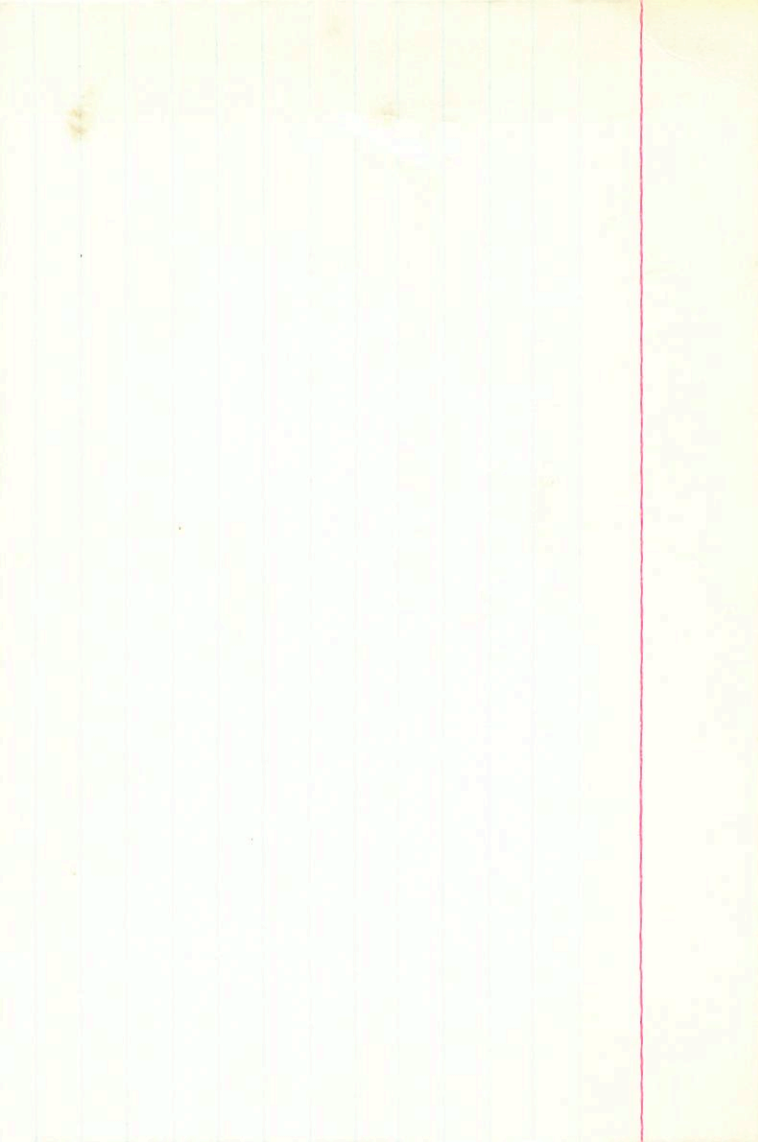
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1.7  
4.25

115 1011 985  
116 1012 986  
117 1013 987  
118 1014 988  
119 1015 989  
120 1016 990  
121 1017 991  
122 1018 992  
123 1019 993  
124 1020 994  
125 1021 995  
126 1022 996  
127 1023 997  
128 1024 998  
129 1025 999  
130 1026 1000

910



7077 18 46.7 1412 H/m 42.8

179115

15m=0.00 100 233 500 2874

6.755-0.15 1267

1004 100 2 Candy

1006 100 2

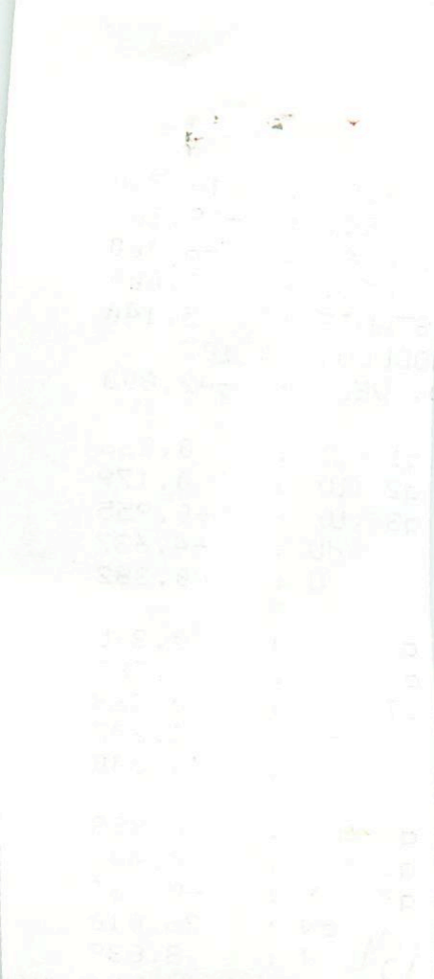
-6  
+2

42.27  
42.10

5.14  
-42.8

035 735  
6.44 42.21

154



R.A. : 18.750  
DEC. : -19.200  
R.A. : -6.000  
DEC. : 2.000  
DISTANCE : 5.140  
MODULUS : 107  
VEL. : -42.800

q1 (U) : 0.236  
q2 (U) : 0.179  
q3 (U) : -0.955  
dU : -4.637  
U : 40.382

q1 (V) : 0.395  
q2 (V) : 0.880  
q3 (V) : 0.263  
dV : -2.277  
V : -11.500

q1 (W) : -0.888  
q2 (W) : 0.440  
q3 (W) : -0.137  
dW : 28.010  
W : 8.839

154

7219

19 01.7 +3 15 +2 -13

671 -048 1474

177332

26223

672 +23 +13 C  
071 204 1077 2863  
067 208 1.088 @5PC

→

220

10017 4025  
① 40725 4025

440  
1075  
1514  
63

+06 4  
+2

25  
25  
605  
-13



1505

7327

19 17/6 22 30

-top

181240

hsc

Ann

152 24 8 20 21

5.5 17 06 11 85

7.15  
~~0.05~~

1004+025

-6  
25

1704+025

365  
-6.4

156



R.A. :  
DEC. : 19.300  
R.A. : -22.500

V57

R.A. : 19.600  
DEC. : -39.550  
M. R.A. : 68.000  
M. DEC. : -52.000  
DISTANCE : 4.400  
MODULUS : 76  
RAD. VEL. : -35.800

q1 (U) : 0.416  
q2 (U) : -0.117  
q3 (U) : -0.902  
dU : 132.394  
U : 42.323

q1 (V) : 0.267  
q2 (V) : 0.964  
q3 (V) : -0.002  
dV : -171.186  
V : -12.901

q1 (W) : -0.869  
q2 (W) : 0.240  
q3 (W) : -0.432  
dW : -275.114  
W : -5.388

737

7532

14 452 73 50

-7.7

18684

85

86 252 88 2872

1.09 009 1225

4222  
4222

1026-024  
1026-024

30  
24  
380

4245

424

1026-024

-7.7

158



R.A. : 19.750  
DEC. : -13.850  
R.A. : 30.000  
DEC. : -24.000  
DISTANCE : 3.800  
MODULUS : 58  
VEL. : -7.700

q1 (U) : 0.446  
q2 (U) : 0.289  
q3 (U) : -0.847  
dU : 28.691  
U : 8.173

q1 (V) : 0.243  
q2 (V) : 0.872  
q3 (V) : 0.426  
dV : -65.662  
V : -7.055

q1 (W) : -0.861  
q2 (W) : 0.395  
q3 (W) : -0.319  
dW : -163.918  
W : -6.979

158

1106  
130

19 48.9 + 9 30 40

6.23 180 1.419

6.25 + 10 + 8 C  
049 203 1020 2882  
052 202 1.018 2.879 etc

36

~~1000-016~~  
1000-016

1000-016  
1010-016

199

452  
082=a  
038=a

211  
428  
1008  
1430  
1525

+1.35  
4.9

10  
16  
498  
+204

9562  
187753  
27491

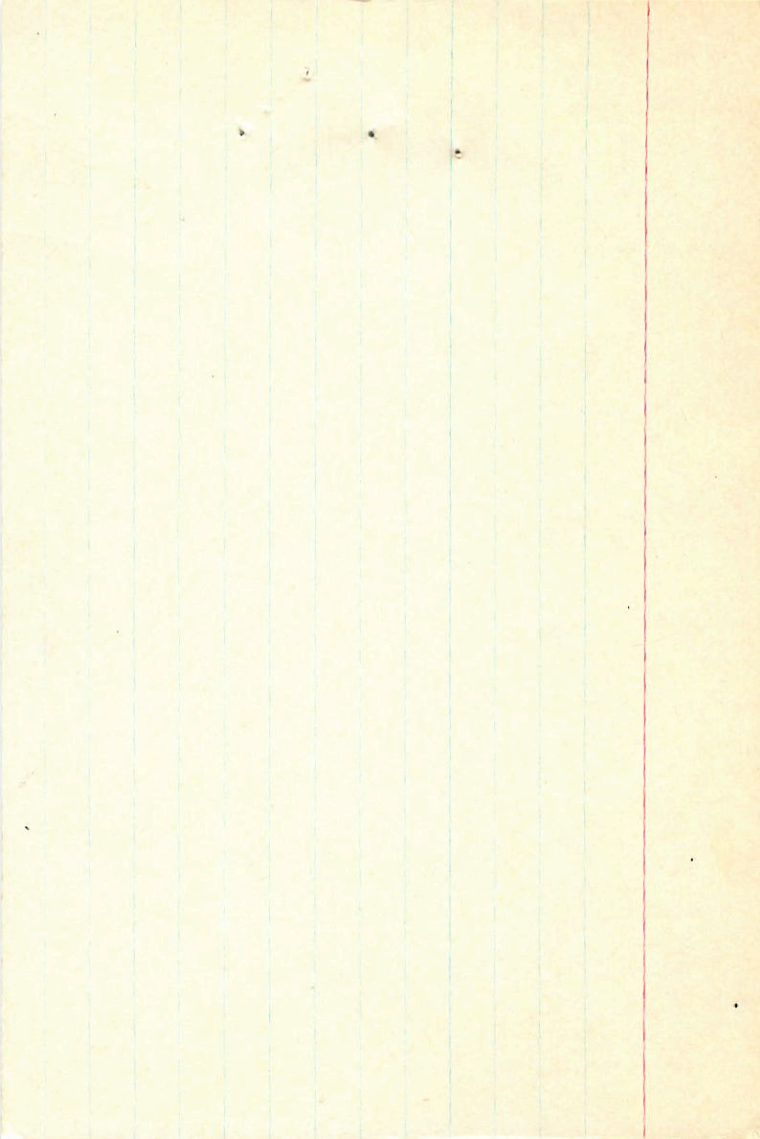
159

Am -10 5 Sta.

HD188097 19 53.5 -69 18  
 4574 9027 4804  
 4510 4811  
 4804 -9070  
 +0187  
 +0137  
 -100 02  
 -092 030  
 -12.7  
 2481 +145  
 -17 +148  
 -14

ASZ 644  
 5.74 + 0.22 (1.60)  
 +0147  
 076  
 159  
 -643  
 +198  
 -104  
 34  
 +33.6  
 1796  
 -187  
 407  
 -12.7

111 245 895 2848  
 5.92 011 1.245  
 478 -511 -714 +1767 +2301 4068 +22.5 +11.1  
 215 457 -464 +0795 -3859 -3064 -16.9 +7.3  
 -851 -070 -520 -3146 +0315 -2831 -15.5 +8.1



188097 19 53.6 -69 18 A<sub>in</sub>

5.74 + 0.22 (1.60)

7574

555 = 513 ps

0144 GC → 104

-10.0 Bunch  
5 min

255

+0137<sup>2</sup> -092 → N30

205

+016Σ -100 GC → N30

19

1.44

+0150 -096

487579

5.6

1.53

60

51.3 ps

470	-517	-712
220	853	-474
853	-068	-518

+1760	+2352	-4112
+0824	<del>3881</del>	+3057
-3194	+0309	-2885

+21.1	+7.1	= +28.2
-15.7	+4.7	-11.0
-11.8	+5.2	-9.6



$4212$   
 $4201 - 4066$   
 $1286$   
 $0197$   
 $32857$   
 $5800$   
 $2777$

97

551 240  
 $10144$  104  
 $10122 - 109$   
 $10119$  101

$5787$  54  
 $424$   
 $4703$

22

$32692$   
 $-29$   
 $13$

$13$   
 $13$

$10120 - 105$   
 $00120$

$10137 - 1022$

$5066$   
 $-14$   
 $5080$

4044

10724

1070-104

3814

644

37224

33087

$-14$   
 $808$

$5354$  2025  
 $-4$

1285  
 0197  
 658  
 0144  
 4.22





R.A. :  
DEC : 10 -

161

187 2-25-920 2.740  
+0033±5.8 +030±3.7  
+33 +039

192342 20 11.5 +24 05 A0 -37.6

192342

(+07723 28094

9920 10<sup>m2</sup>

412555

31.688 1893.7 +24 5 10.10 1884.4

6.5 Am

+045

+33 +35

+047 +0297

AD513543  
46.25 180  
167 228 20 2743 1502

+0033 +034.5  
-1.97  
82.113

...

31.615

+0492

+0036 +038

9.54 1928.72

138

617

+052 +036 202

9.80

+241

441 057 1091 +67

167

283 693

+36

155

3.65

2.790

240 705

-37

-840543 408 913 4046 4030 -37. 012 -15 125  
039 010 025 007 152 164 -33.5 -15 +28 01

-3 +45-2

$\boxed{+39-23-6}$

+1+49 +1

008

$\boxed{+41-19-9}$

009

-1+47-1

HR7723

20 11.5 + 24 05 Am

-38.55y  
-22.50z  
-372

6.45 + 0.32

6.45 + 0.30 GC

~~6.45 + 0.26 + 0.4~~

6.33pm

0.17

6.57 + 325 + 105 a 20"

+32

-26

-2

+136

5	525	706	-443	
32.3	174	418	892	
5	833	545	-094	

+1125 + 1308

+0372 + 0752

-1784 + 0982

2033 + 16.4

+124<sup>46</sup> - 83.0

-0502<sup>15</sup> + 3.5

+30

-26

-2

-940  
1843 543 405 913 405 1030 -37012 -154128  
036 010024007 147 141 -33.7 -18 +28 017

$$-9 + 38 - 7$$
$$\boxed{+29 - 26 - 1}$$

162

112

113

114

115



20.200  
24.100  
57.000  
36.000  
3.650  
5370

5495 - 37.000

0.532  
0.725  
-0.437  
254.867  
29.871

t20

0.168  
0.416  
0.894  
112.392  
-27.834

27

-0.898  
0.549  
-0.211

7833 4.36

20 27.1 4.9 5.5 Am

195217

28588

6.57 + 24 + 09 3849 (78)  
1540 2-837

1501100

010 160 1.042 (2) SPC



6.55 0.34 1.176

1501100

142

324

10404

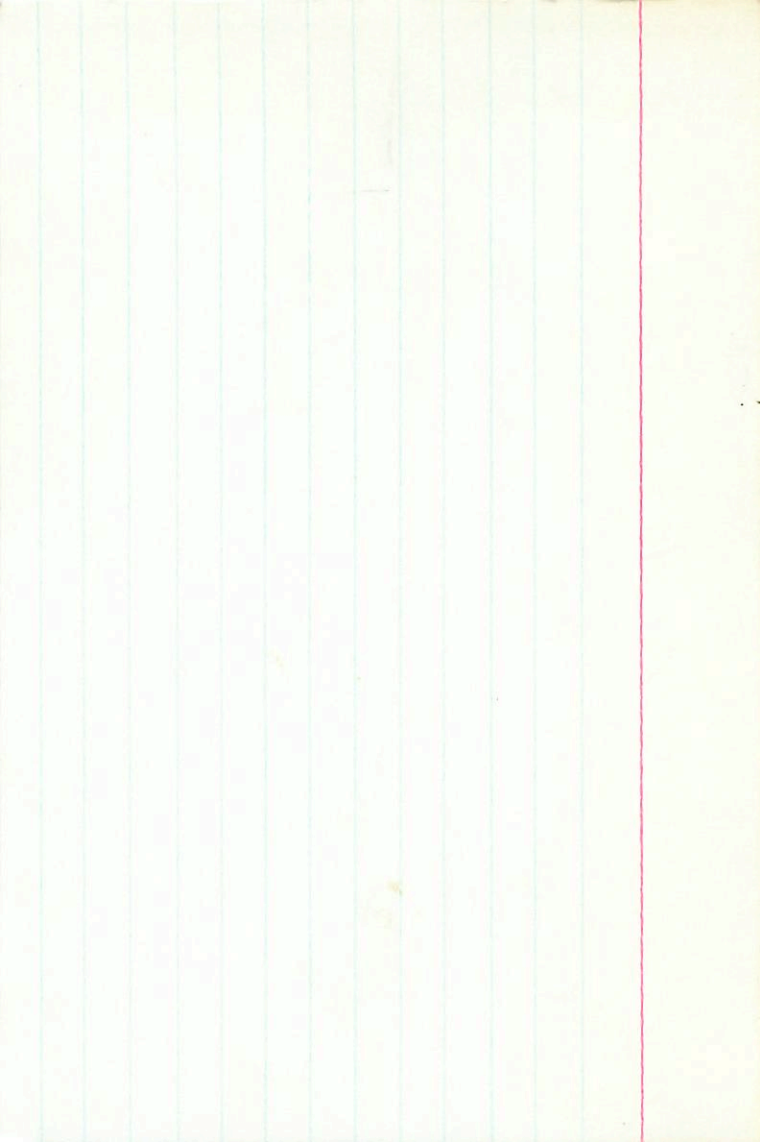
1342

142

10.34

4.35





$+2004602$   
 $+106353.5$   
 $+0077$   
 $+04353.9$   
 $+054$   
 $195479$   
 $20$   
 $28.7$   
 $+20$   
 $26$   
 $6.0$   
 $A2$   
 $-40.28$   
 $28540$   
 $Ann$

$12817$   
 $43.866$   
 $1912.7$   
 $+20$   
 $28$   
 $8.71$   
 $1911.6$

$$\begin{array}{r} -235 \\ \hline 631 \end{array}$$

$$\begin{array}{r} -165 \\ \hline 706 \end{array}$$

$$\begin{array}{r} 43.787 \\ -10.7683 \\ \hline 43.7892 \end{array}$$

$$\begin{array}{r} 8.06 \\ \hline 18 \\ 8.24 \end{array}$$

$$8.06 \quad 19334$$

$18.4$

$$\begin{array}{r} 8.05 \\ -4 \\ \hline 8.01 \end{array}$$

$$8.05 \quad 1928.72$$

$12/2$

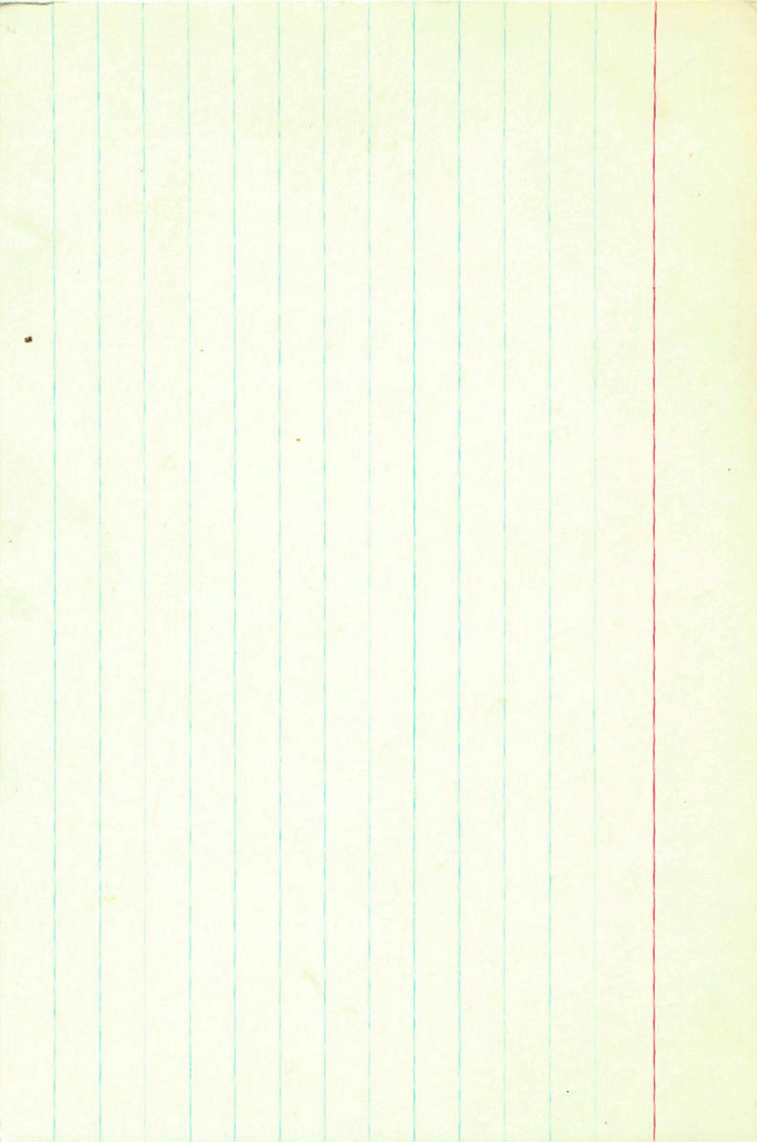
$$\begin{array}{r} 736 \\ \hline 762 \\ +131 \end{array}$$

$$\begin{array}{r} 8.01 \\ \hline 8.125 \end{array}$$

$$\begin{array}{r} 36.1 \\ \hline 19.5 \end{array}$$

$19.5$

$$+1.06$$



~~W20 051265~~

7839

20 28.7 +20 26 Am

195424

6.21 +14 +11 (489) ~

28570

072 216 1.000 @ SPC

10070 +053

1098 +053

10067 +045

10070 +0515

10994

101.5 +046.5

Bund 51

229

458

985

1443

207

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218

958

108

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984

69 0.520239 984

5.5

140

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4.34

-40.2

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51.5

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49

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20.4

1108

446.5

485

40.2

0.019 6.13 +1.78 1.20 9.39

163



R.A.

DEC.

R.A.

20.450

20.450

105.000

53.000

4.360

0356

20 341 20

68 + 83

4 m

410

805651

— 5001 <sup>572</sup> 510 580

05782

6-20-440-02-9

— 110-1600+

110-910+

9774  
+466

136

— 72  
445

710

020 600 166 445



7920 20 404 52 07 49

197157

28860

Banks

4.00 426 107 C

157 211 230 2784 5342

31

1. The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that proper record-keeping is essential for the integrity of the financial system and for the ability to detect and prevent fraud.

2. The second part of the document outlines the specific procedures that must be followed when recording transactions. This includes the requirement to use standardized forms and to ensure that all entries are dated, signed, and initialed by the appropriate personnel.

3. The third part of the document addresses the issue of internal controls. It states that a robust system of internal controls is necessary to ensure that all transactions are properly authorized and recorded. This includes the implementation of segregation of duties and the regular review of records by management.

4. The fourth part of the document discusses the role of the audit function. It notes that the audit function is responsible for verifying the accuracy of the records and for reporting any discrepancies to management. This process is critical for ensuring the reliability of the financial information.

5. The fifth part of the document concludes by reiterating the importance of these practices and the consequences of non-compliance. It states that failure to adhere to these standards can result in significant financial losses and damage to the organization's reputation.

R.A. : 20.600  
DEC. : 83.450  
M. R.A. : 136.000  
M. DEC. : -12.000  
DISTANCE : 4.450  
MODULUS : 78  
D. VEL. : 10.000

q1 (U) : 0.601  
q2 (U) : 0.687  
q3 (U) : 0.408  
dU : 5.134  
U : 4.477

q1 (V) : 0.100  
q2 (V) : -0.571  
q3 (V) : 0.815  
dV : 39.786  
V : 11.239

q1 (W) : -0.793  
q2 (W) : 0.449  
q3 (W) : 0.412  
dW : -83.865  
W : -2.394

104

8177  
20354

21 210 -46 54

-23.9

10045-016

1046-016

629 011 1327

101 246

68

-16

5.13

-23.9

843

963 2535

+0.97

+1.15

165

11

MOD.	DISTANCE	PM.	PM.
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000

MOD.	DISTANCE	PM.	PM.
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000

MOD.	DISTANCE	PM.	PM.
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000
100.000	100.000	100.000	100.000

Handwritten signature or mark

R.A. : 21.350  
DEC. : -46.900  
PM. R.A. : 68.000  
PM. DEC. : -16.000  
DISTANCE : 5.130  
MODULUS : 106  
RAD. VEL. : -23.900

q1 (U) : 0.714  
q2 (U) : -0.039  
q3 (U) : -0.699  
dU : 160.208  
U : 33.720

q1 (V) : -0.031  
q2 (V) : 0.996  
q3 (V) : -0.088  
dV : -82.373  
V : -6.641

q1 (W) : -0.700  
q2 (W) : -0.085  
q3 (W) : -0.709  
dW : -147.65  
W : 1.28

165

8253 5.79 21 33.3 -26 24 A 3m

205971

30235

1000054

5.71 025 1240

40003-024

112-024

107.81 24.30 5072 +22 (409.5) C

18.59 +0.99 5.73 138 187 551 2822 13297

211104 025  
132156 851 2821

4149  
42.13

4149  
181

396

19 9561 9699 1107  
1549 2625 0049



160

R.A. : 21.550  
DEC. : -26.400  
M. R.A. : 124.000  
M. DEC. : -24.000  
DISTANCE : 3.960  
MODULUS : 62  
D. VEL. : -19.000

q1 (U) : 0.739  
q2 (U) : 0.225  
q3 (U) : -0.635  
dU : 363.686  
U : 34.587

q1 (V) : -0.066  
q2 (V) : 0.962  
q3 (V) : 0.264  
dV : -144.229  
V : -13.948

q1 (W) : -0.670  
q2 (W) : 0.153  
q3 (W) : -0.726  
dW : -370.186  
W : -9.131

166

8 PM

5.72 +22 1.59 F21E -19.0 4C  
Am  
21 33.3 -26 24 -19

H0205471

G030235

+0082  
+0080 ± 2.8 -021  
-023 ± 2.9

14m18'  
9253

17.227 1906.3 +0084 -020  
-350  
76.8 77  
44.15 1903.9  
+106  
43.19

738 233-633  
-065 958 280  
-23 -672 165 -724

+00824-0189

42.98 193986

1120

112-022

1136  
1082 2.150  
0157 4.02  
125  
48

+03  
43.95  
43.84  
-65  
36.55

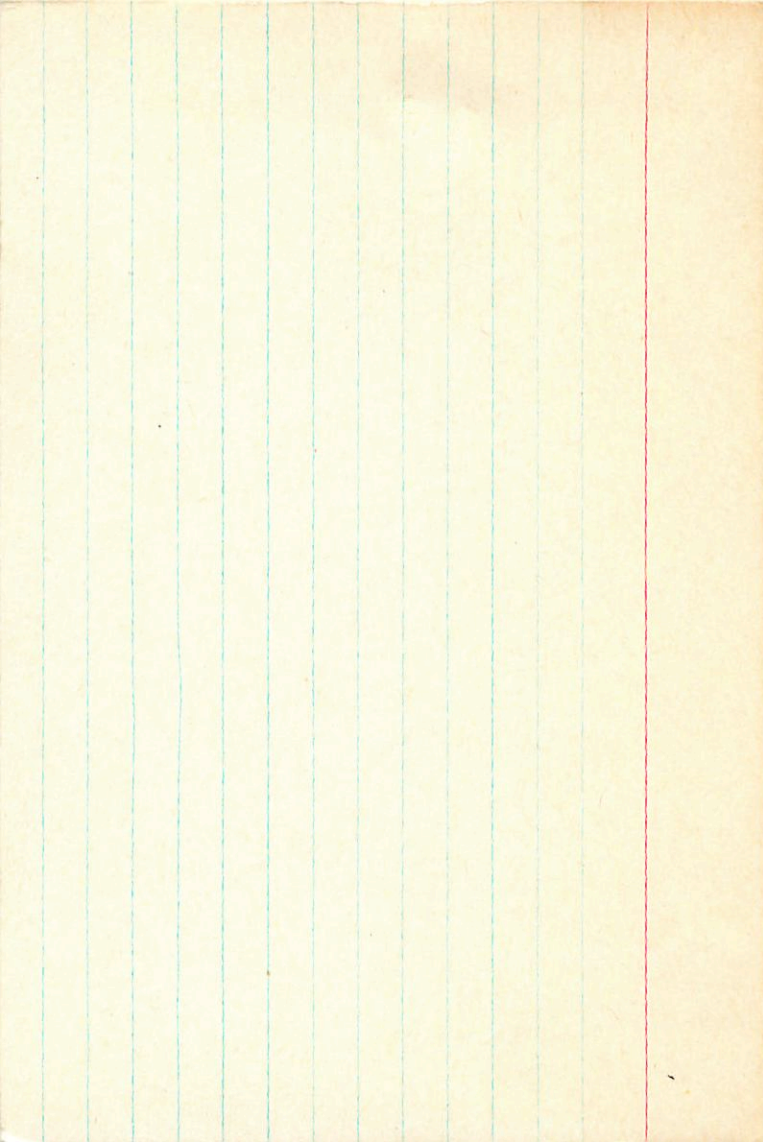
7557 944

8461 1933.27

50.325  
26.758  
17.123  
113

+3922 -0221  
-0345 -0908  
-3571 -0156

40.42 +3701 +12.0  
43.69 -1253 -6.8  
-13.74 -3227 -20.7 +13.8  
-53



8410

22 02.2 - 1 09 Am

209625

5.28 017 1.294

30872

5.27 723 + 15 C

114

124 237 918 2500

117 251 916 2828

117 251 916 2820

151251

111-063

6734 - 4472 - 0635

7753 - 8944 #1808

111-063

18 1006

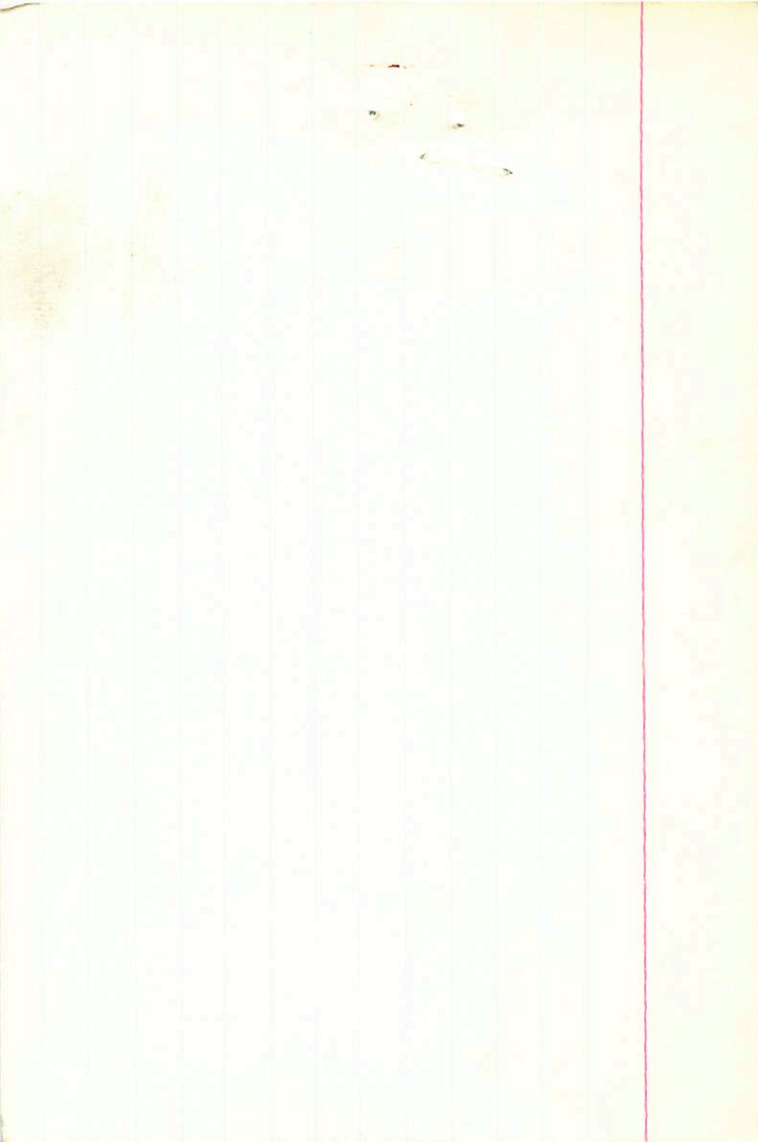
3172

117  
1140  
+

117  
1140  
+

620 5.26 117 1140 3172 - 10/25 1504

117  
1140



122.8d

+154

216220 18.71  
35.1 09

22 02.2

32 Apr

HR8410 4-587 -1 24 Am +20.4c

209625

5.32 +0.22 +0.14 -0.21 -0.45 ac

30872

-0.21 -0.41 N30

13866

-0014 32 -0.41 35 N30

-0.21 -0.41

-0013 ±2.0 -0.47 ±2.0

10011-063

117 251 9N 2.870

0.21

-0011-003 117 251 9N 2.870  
2.870 -0.6 -0.6

-015 -047

130 13 259 9N

-016-063

124 227 915 2.871

115 250 915 2.820

pk. 10011-063

5

7100 200-9224  
10011-063

10011-063-1924

-491 871 0 1 -021 -044 +204 0 0 -205 ✓

-010 0 -015 0 -047 -085 +204 +16 -10 0 2-1

+16 -14 -10

-17	0	-6
-----	---	----

-16 +6 -17



$$P = 7.8$$

32 Agl 22 02.2 -01 09 9 AF +20.46

14R8410 5.32 +0.22 +0.14 -021 -048 6C

W13866  
13.120 9.7  
 $\frac{58}{178}$   
-0014 ± 2.0  
-0017  
-0017  
56.67 8.3  
-2.00  
5467

13.106 65.99 56.86  
 $\frac{-22}{.083}$   
71.20  
92.296  
30.869  
12.165  
113

13.107 71.00 56.96  
 $\frac{-12}{81.10}$

-00162 -0435 -0213  
-60172 -0428  
-0213

50.56  
54.32  
 $\frac{12.27}{56.35}$   
56.35 / 56.20

0502  
0746  
+1.1  
0194  
3.56

0195 -0465

-492 871 0 1 -021-044 +20.4 0 0 -205

-010 0 -018 0 -047 -085 +20.4 +17.5 -10.0 02

+15.4 -14.2 -10.4

$\boxed{-16 +6 -14}$

03

+14.7 -12.8 -6.9

$\boxed{-13.1 +8.6 -15.4}$

015

+14.7 -15.6 -14.0

-18.9 +3.6 -16.5



R.A.	:	22.050
DEC.	:	-1.150
R.A.	:	-16.000
DEC.	:	-63.000
DISTANCE	:	4.060
MODULUS	:	65
VEL.	:	20.400

Q1 (U)	:	0.794
Q2 (U)	:	0.476
Q3 (U)	:	-0.378
	:	-202.381

8722

22

53.9

-48 14

+6.4

216823

242

277

555

114

215

921

2840

-0020-003

5.70

008

1.273

1.79

1.50

-020-003

-80

-3

4.25

+6.4



168



R.A. : 22.900  
DEC. : -48.250  
R.A. : -30.000  
DEC. : -3.000  
DISTANCE : 4.250  
MODULUS : 71  
VEL. : 6.400

1 (U) : 0.856  
2 (U) : 0.185  
3 (U) : -0.483  
dU : -83.669  
U : -9.015

1 (V) : -0.292  
2 (V) : 0.944  
3 (V) : -0.156  
dV : 14.216  
V : 0.010

1 (W) :  
2 (W) : -0.427



8970

23 37.4 +9 23 A2

222377

32578

5.96 + 121 + 11 C

547059 1238

119 218870 (2) SPK

$\frac{115 \ 227 \ 868 \ 2 \ 843}{2 \times 5 \quad 824}$

40053-012

160

90  
-12  
410  
-60

170  
187

078-012

269

1921

DEC 1 1921

DEC 2 1921

DEC 3 1921

DEC 4 1921

DEC 5 1921

DEC 6 1921

DEC 7 1921

DEC 8 1921

DEC 9 1921

DEC 10 1921

DEC 11 1921

DEC 12 1921

DEC 13 1921

DEC 14 1921

DEC 15 1921

DEC 16 1921

DEC 17 1921

DEC 18 1921

DEC 19 1921

DEC 20 1921

DEC 21 1921

DEC 22 1921

DEC 23 1921

DEC 24 1921

DEC 25 1921

DEC 26 1921

DEC 27 1921

DEC 28 1921

DEC 29 1921

DEC 30 1921

DEC 31 1921

R.A. : 23.600  
DEC. : 9.400  
M. R.A. : 80.000  
M. DEC. : -12.000  
DISTANCE : 4.100  
MODULUS : 66  
D. VEL. : -6.000

q1 (U) : 0.875  
q2 (U) : 0.481  
q3 (U) : 0.055  
dU : 299.975  
U : 19.491

q1 (V) : -0.396  
q2 (V) : 0.647  
q3 (V) : 0.652  
dV : -185.078  
V : -16.137

q1 (W) : -0.278  
q2 (W) : 0.592  
q3 (W) : -0.757  
dW : -137.674  
W : -4.556

169

R.A. : 19.300  
DEC. : -22.500  
R.A. : -6.000  
DEC. : 25.000  
DISTANCE : 3.650  
MODULUS : 54  
VEL. : -6.400

q1 (U) : 0.354  
q2 (U) : 0.140  
q3 (U) : -0.924  
dU : 7.330  
U : 6.310

q1 (V) : 0.314  
q2 (V) : 0.913  
q3 (V) : 0.259  
dV : 99.973  
V : 3.710

q1 (W) : -0.881  
q2 (W) : 0.382  
q3 (W) : -0.280  
dW : 68.443  
W : 5.465

1076

7464

19 26.5 -89 23

Var  
-358

585259

647

147 217 855 2843

11.97  
+2.17

(035)

659 033 1207

043

10048 -052

052-052

68  
-52  
+40  
-358

073

2 Bump

157





R.A. : 19.900  
DEC. : -69.300  
R.A. : 177.000  
DEC. : -98.000  
DISTANCE : 4.070  
MODULUS : 65  
VEL. : -12.700

q1 (U) : 0.475  
q2 (U) : -0.517  
q3 (U) : -0.712  
DU : 380.959  
U : 33.869

q1 (V) :  
q2 (V) :  
q3 (V) :

2058

191220

20 141 80 28

101

10154 1008

878

SMARTLINE

114 215-897 2024

614008 1276

234

5

485

101

1192

1214

4.35

100.21  
 100.0-  
 870.0-  
 810.0-  
 800.0-  
 850.0-  
 820.0-  
 830.0-  
 840.0-  
 850.0-  
 860.0-  
 870.0-  
 880.0-  
 890.0-  
 900.0-  
 910.0-  
 920.0-  
 930.0-  
 940.0-  
 950.0-  
 960.0-  
 970.0-  
 980.0-  
 990.0-  
 1000.0-

161