

192800

20 122

+66 19

7.9 g₁₀

-50c

+6601276

12603

^s
-0055

-033 -057.642

-41 (3)
-72 (3)

440 (20)

A0513560

192679

20 12.4 + 52

58

7.2 dF5 - 33.01

28114

5" (9.3 dN2 - 3491

17610

21.026 1899.5

+ 52 88

12.46

18931

- 33.8a

$$\begin{array}{r} -273 \\ \hline 20,753 \end{array}$$

$$\begin{array}{r} -9.96 \\ \hline 2.50 \end{array}$$

20,753

41.14

39.750

20.899

881

851

37.4

35.6 1927.9

32.35

7.95

+ 7.59

8.57 2019

8.62

11.52

- 25

11.57

10.10

+ 7.60

$$\begin{array}{r} \hline 20,926 \end{array}$$

+ 173

20,941

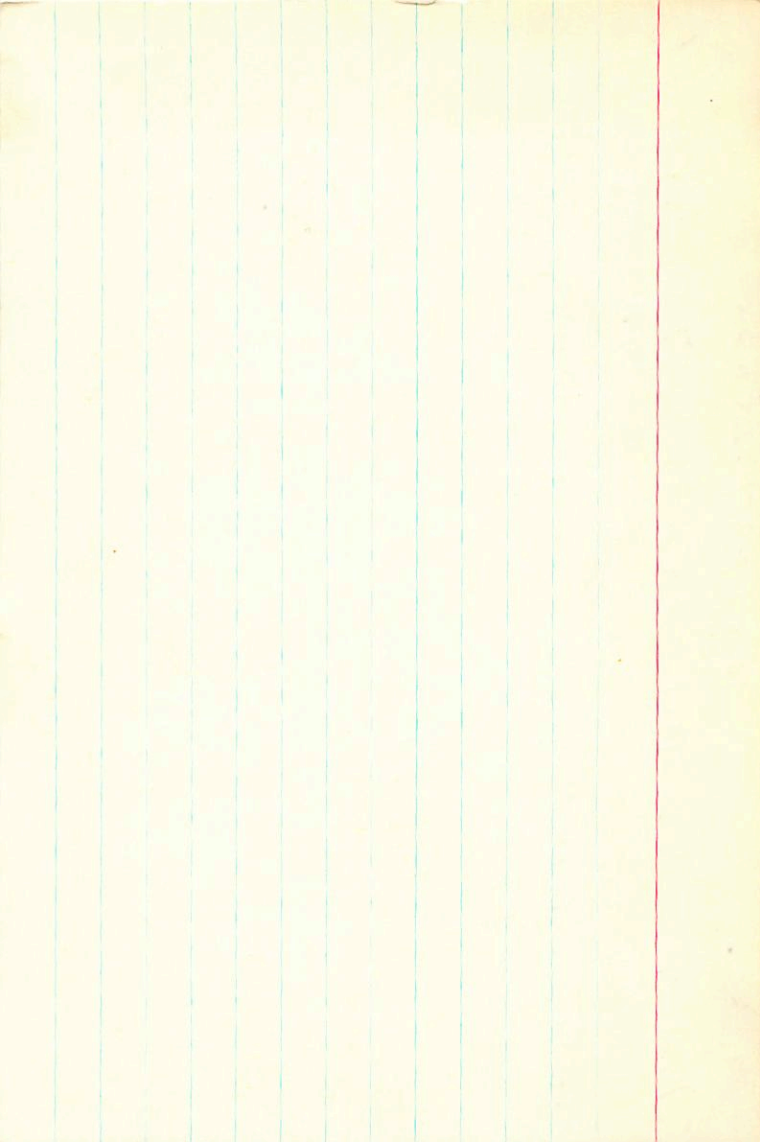
964

73.87

36.9

43.8

1945.97



+0057 + 3.0 +057 + 2.2
+0064 +058

192781 20 12.5 +60 29 13.69 18953
28120 6.2 9125 -0.58

12615 32.634 1898.6 +60 29 13.69 18953

$$\frac{-350}{284}$$

$$\frac{-3.12}{10.57}$$

5.03
27.46
32.51

39.0 1928.8

33.08
51.88

38.2

491- 1060

12.48⁴⁰
12.56

596

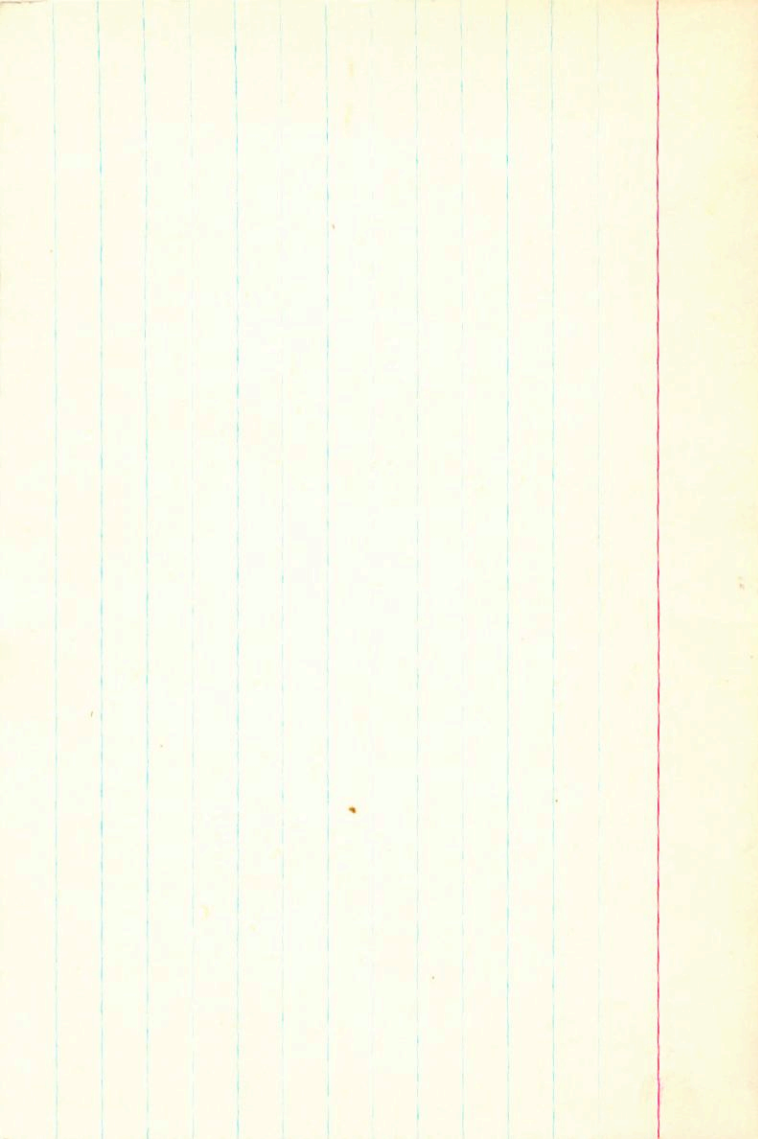
23.58
36.8

32.55
530
569 + 246

13.56
-14
13.40

1944.78
41.5

12.98
+ 2.41



161937

-13.214

20 12.8

-73 05

6.17 18341

$$\begin{array}{r} 51129 \\ \underline{174} \\ \hline 51950 \end{array}$$

$$\begin{array}{r} +003778.7 \\ +0010 \\ \hline -032 \\ \hline 380 \\ \underline{223} \\ \hline 1.07 \end{array}$$

$$\begin{array}{r} 51084 \\ \underline{-11} \\ \hline 51098 \end{array}$$

68.14

$$3.17$$

$$\begin{array}{r} 51191 \\ \underline{55.8} \\ \hline 3.51 \end{array}$$

$$\begin{array}{r} 5105 \\ \underline{84} \\ \hline 5105 \end{array}$$

192609 20 13.0 +10 00 7.2 F6 -37e

+904461

12624

^s
+0048

"
+055

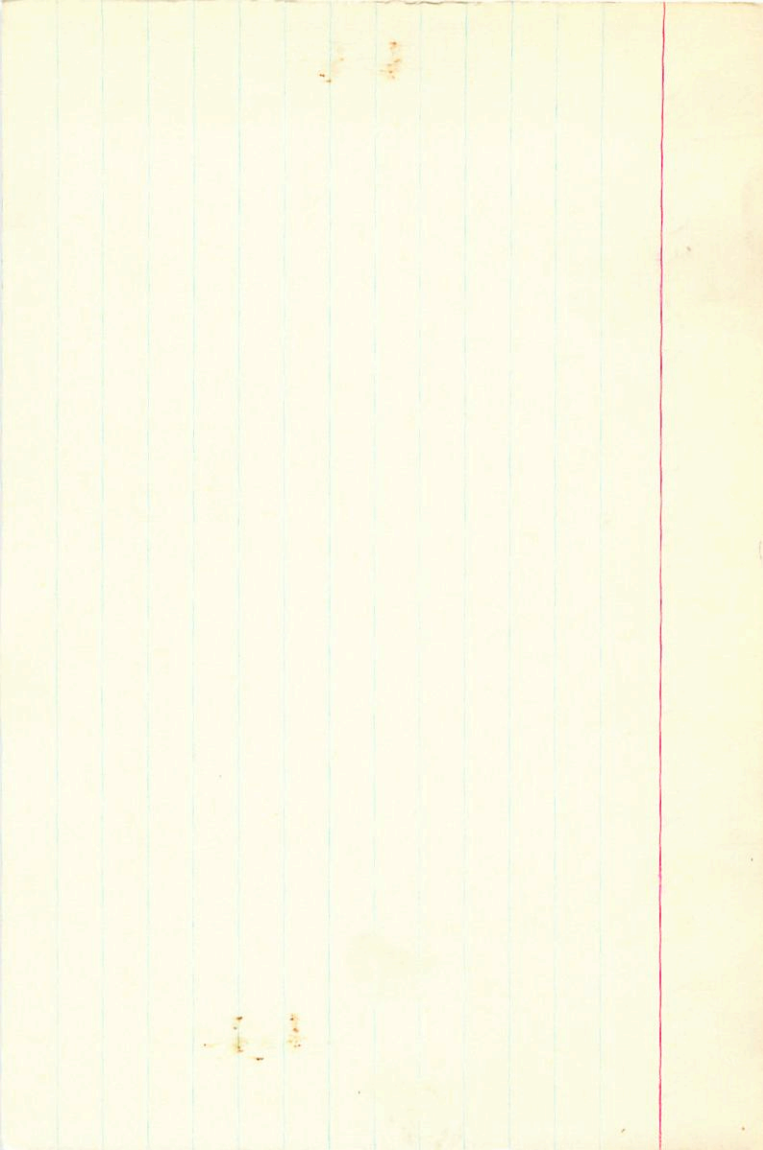
Gm 50

+0070 "

+10478

+04477

-



-003743.9 -10873.1 -34 -110

192787 20 13.5 -0029 733 35 5.8 926 -928

28145 ~~28145~~ -7.815

12630 27.120 1908.7 733 34 36.17 1908.0

45513596 $\frac{1553}{27, 273}$

$\frac{4.54}{40.71}$ 68.1

28.3

28.91 58.300 4.0 19272

$\frac{27.215}{213}$

$\frac{37.86}{313.50}$

~~290~~

$\frac{38.61}{38.161}$

27.200 -194 208

~~357.4~~

~~208~~

$\frac{36.55}{36.118}$

$\frac{38.15}{38.118}$

1929.7

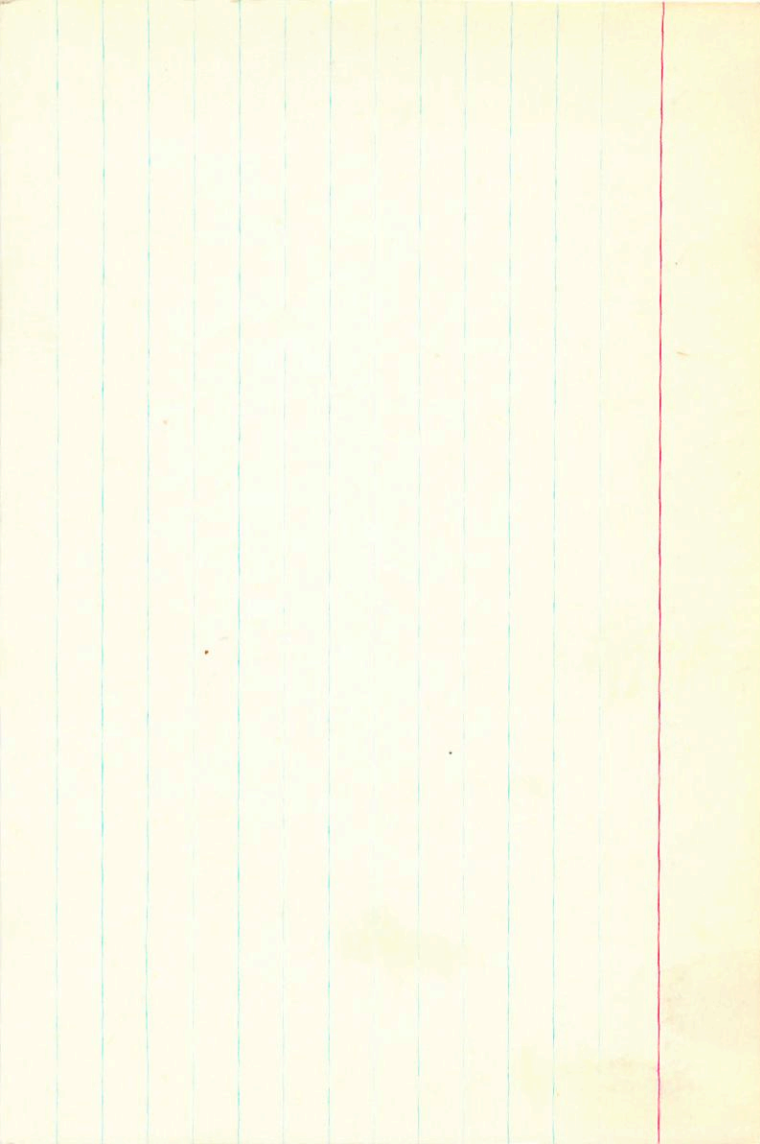
$\frac{208}{-073}$

~~232~~

$\frac{31.50}{-31.5}$

~~37.84~~

38.15



-0054±3.2
-0055

+043±2.9
+048

193030

20

13.6

+64

37

7.2

7965-67.26

28147

12632

34890 1890.5

+64

36 39.95

1586.9

$\frac{321}{35,211}$

35,

$\frac{-2.71}{37,24}$

34891

$\frac{18}{909}$

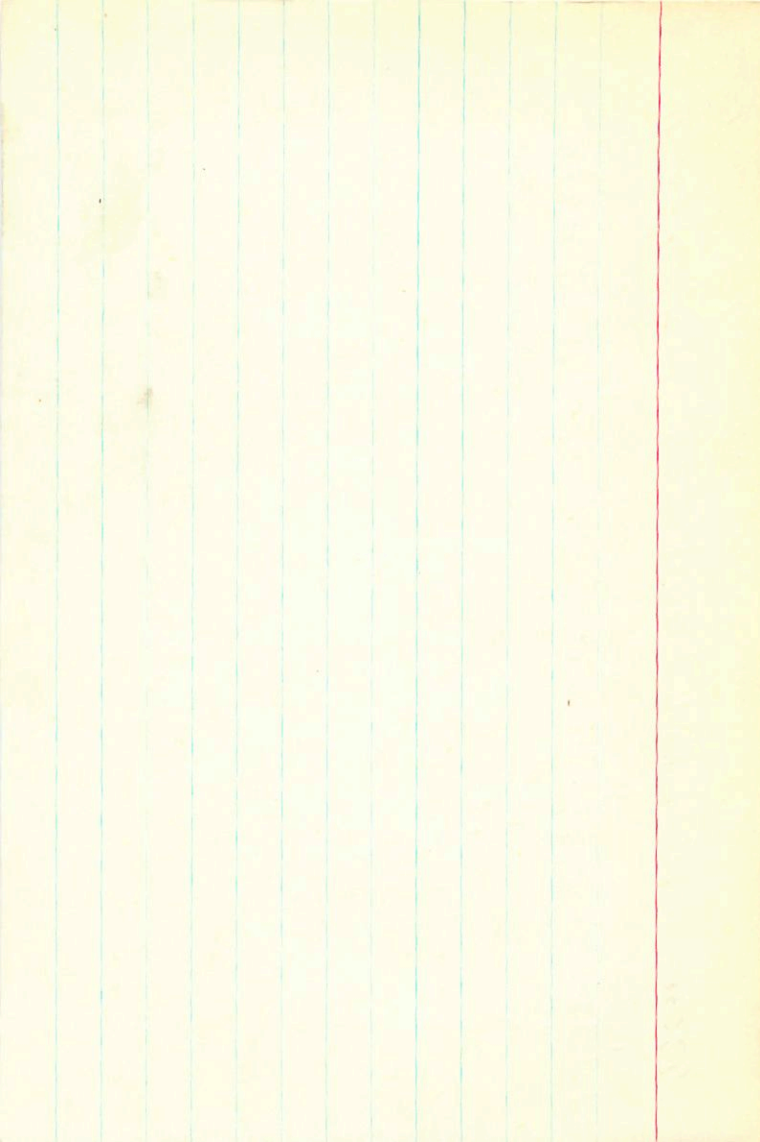
-302

40.18 1945.01

$\frac{-13}{40.05}$

+2.81

~~-4864~~



W12434 20 13.7 427 40 912 72.5

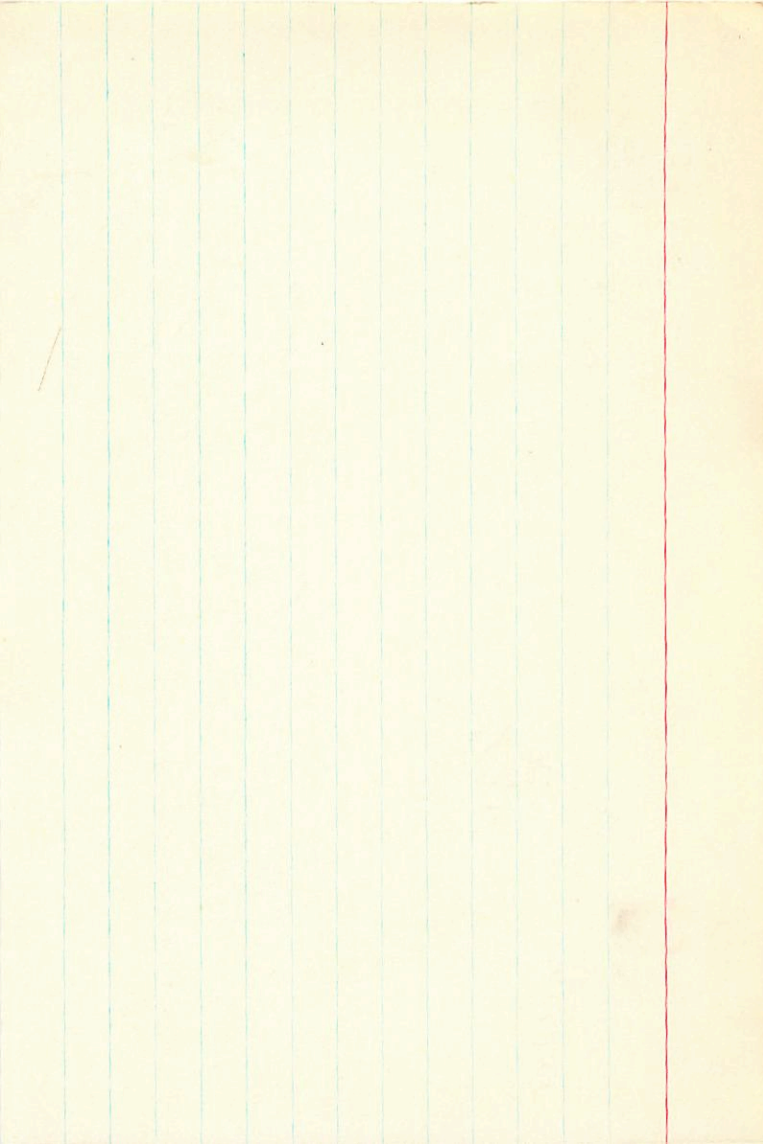
MD142504 474 416 4
1430
1430
1430

1430 405 16
-041 1005
-0031 1012

474
416
4
946
476
5

72.5

532	752	-386	-1035	+0425	-0610	-44	-1.1
167	354	919	-0325	+0201	-0124	-0.8	+2.6
-829	554	-063	+1610	+0315	+1925	+7.9	-0.2



$-7^0 5235$

20

13

56

-7

358

Sum ①

~~-1164 ± 5~~

~~-108~~

~~-110~~

~~-109~~

+319 ± 8 -138 ± 5 Y

-9 +7

+310 -131

2-Sum

8.769 + 0.58 - 0.03 S = +14

15 Sep

-0003 ± 2.9 -026 ± 2.6
-0001 -017

152836

20 141 +21

27 6.2

9141 -4.18

28166

12643

7.845

1503.8

+21 26

38.53

1896.5

014

1.39

~~1859~~

~~39.92~~

7.874

39.11

1933.7

0 1/2

~~39.29~~

9.951

35.13

1940.70

~~-13~~

33.4

~~1838~~

~~39.15~~

7440

~~856~~

~~39.22~~

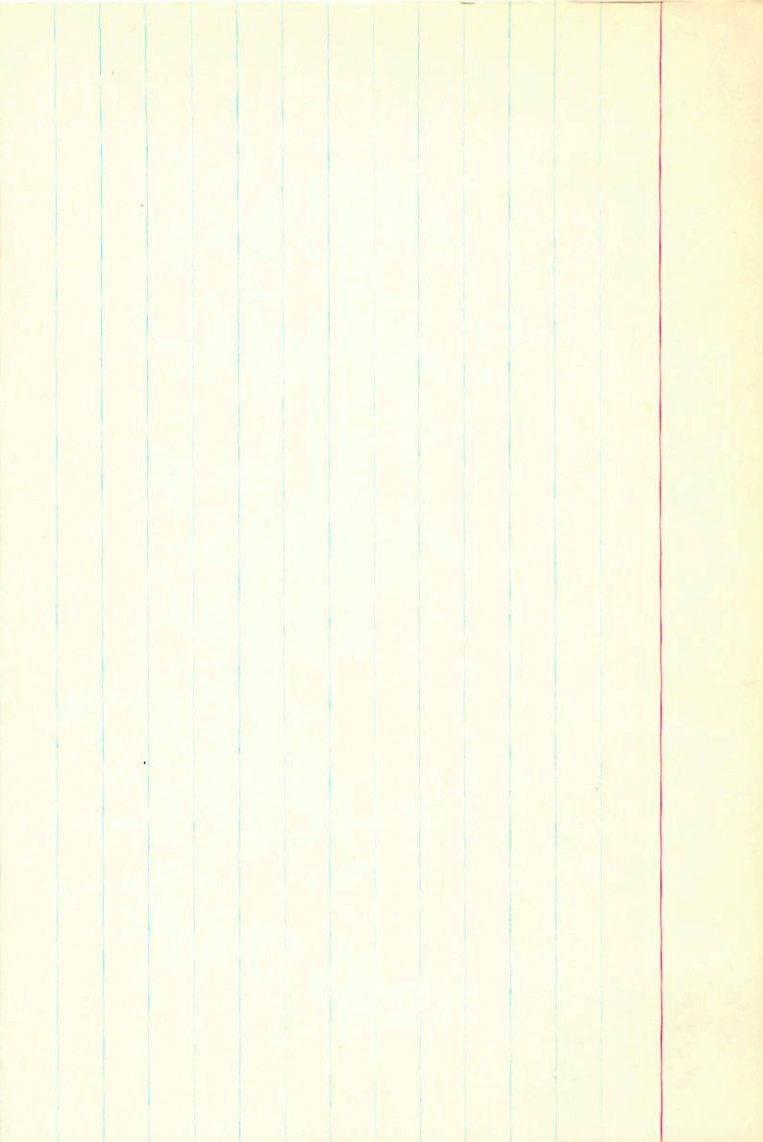
57.2

-003

~~39.22~~

41.7

~~1.70~~



+43° 853-353

20 11.0

+42 30

818

20 14 14.0 +42 47.64

(79601)

596 0.24 1.30

5.15 6.0

955

437

M.C-AC +.013 -.061

10.4: MOP +8.7

8 -57 2800

1006 54

5880

0624 0564

08300

-8980

6715

1564

r

W12647

20 14.4

+27 37

885.
1770

GC28173

4770

-770 29? 663

HD192913

23

+0005 ± 3.8
+011

1325

22.524
-027
497

1896.8

14.32 1891.7

497

52
1484

37.7

32.6

22.492

15.46

1928.72

-11

-44
15.02

29.4

22.494

482

15.7 1929.7

-486

-015

-25
15.45

15.24

263

15.40

67

541 747 -386

+0177

+4.7 +2.4

160 361 918

+0085

12.22

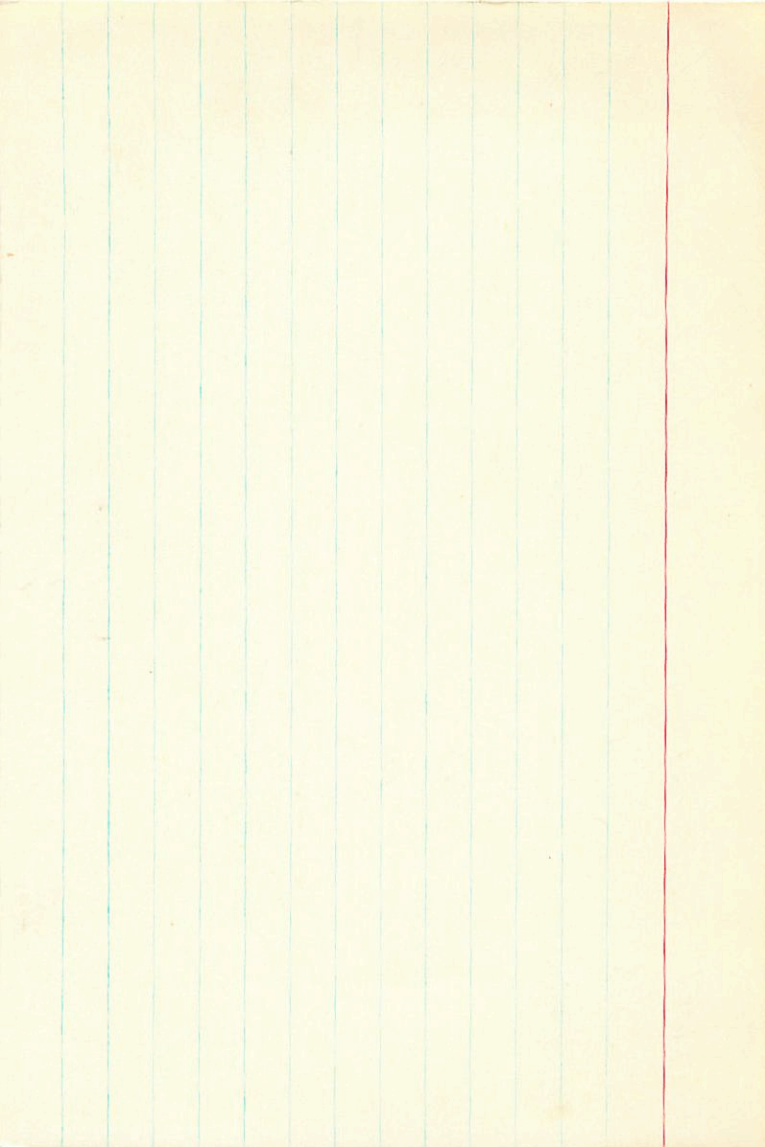
556

-826 558 -076

-0133

-3.5

+0.5



192985

20

14.4

+45

26

5.9

d/FY

-40.48

60

28174

12648

425 +05

5.87 + 0.40 - 04

360

480

30.202

0

-051

+0003 ± 3.6 - 054 ± 3.1

23.274 1896.1

31.28 1891.6

541 830 -137

160 060 885

-826 559 100

-2006

-6.1 +5.5

-0.6

-0145

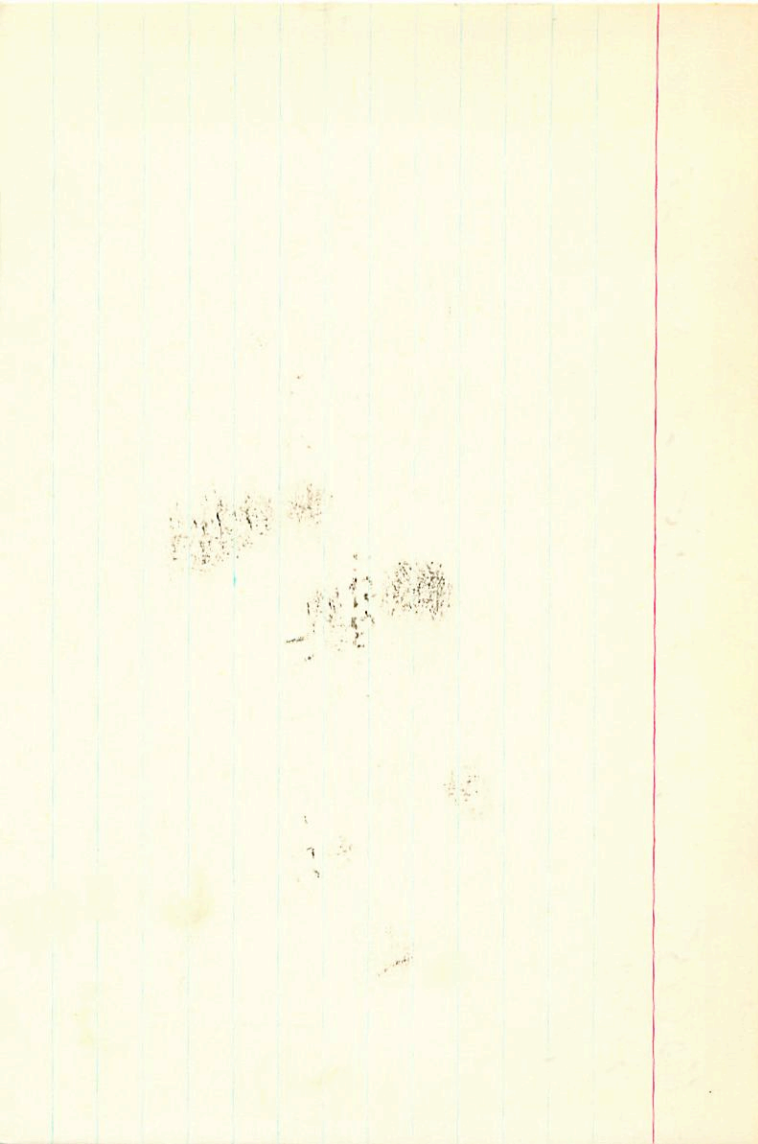
-0.4 -39.8

-40.2

-1339

-4.0 -4.0

-8.0



+5202666

193054

20

14.5

+52

21

7.39145

-54.08

12651

-0011

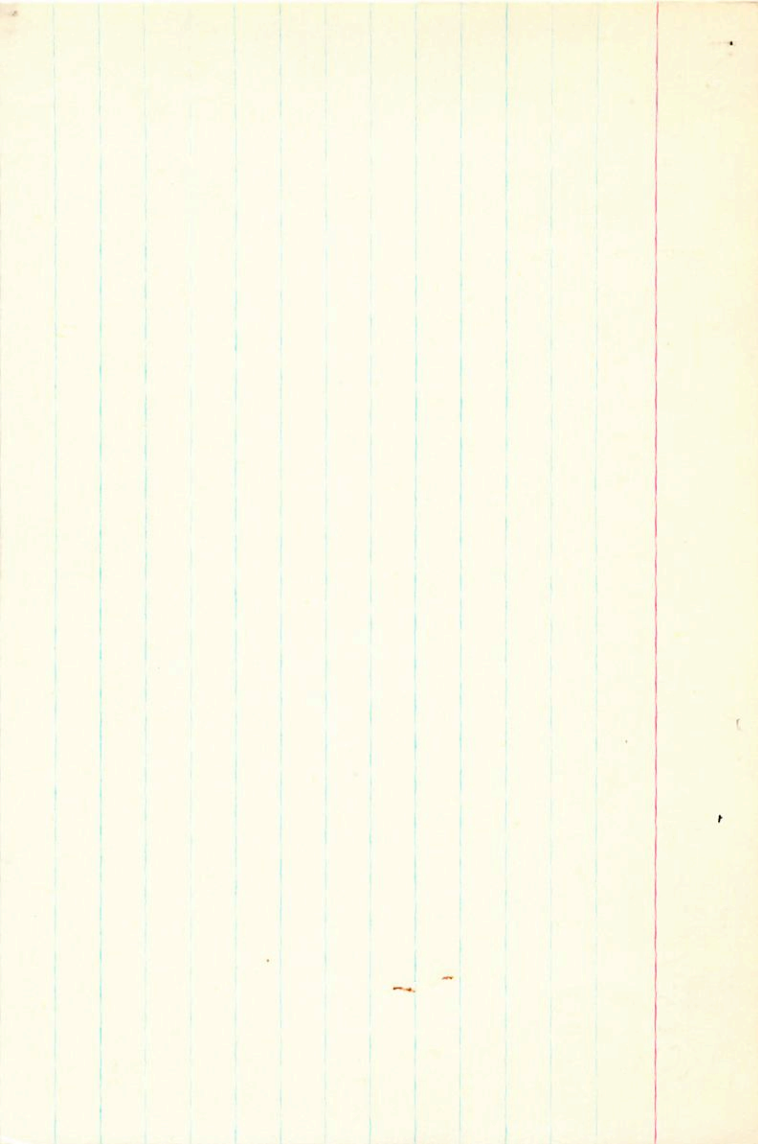
0

-017

+1

-016

4



7225 5 lot 20 0.50 1.50

80 80

5.46 427

5000

17742 .11702 -0009

1344-2 1400 ✓

40223 40224-011

169 188 897 2.752 2.92

231 963

MV=409

20.1

-89.1

+1580

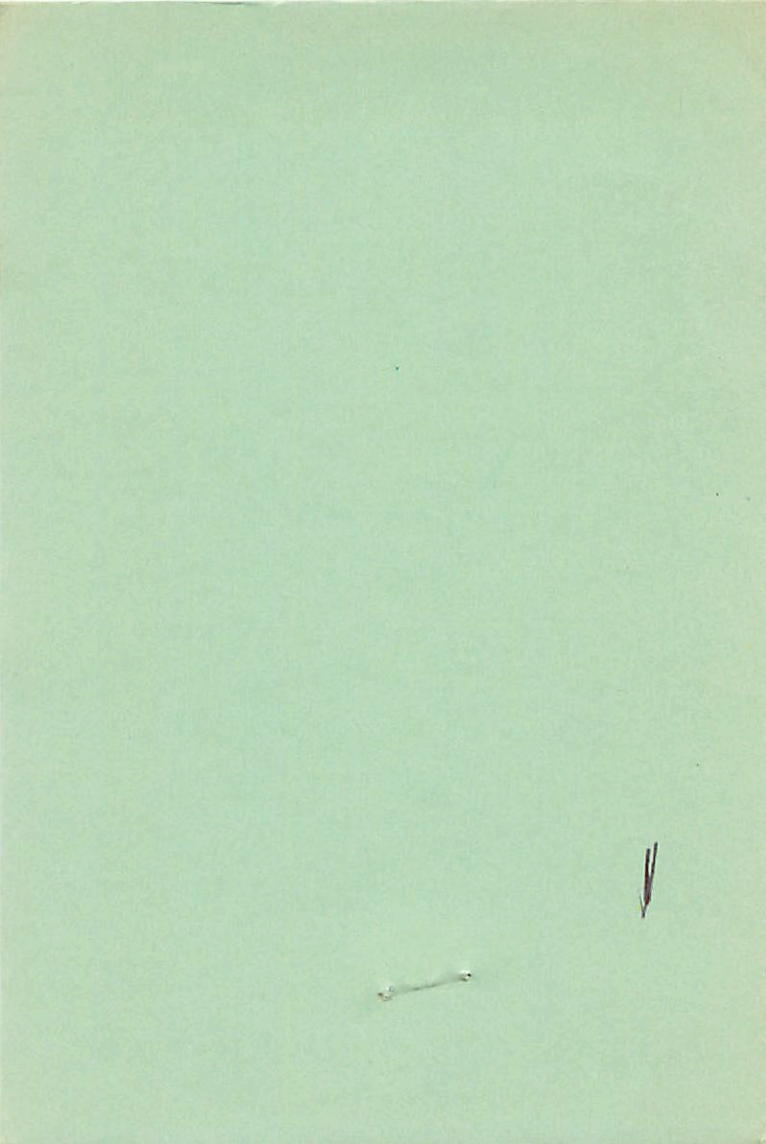
4.55

11.9

193 240 622

1009 221

167



193102 20 16.2 -14 27 2.4 g RD -47.80

28225

12675

-0.826
-0.318
-0.465
-26.461
-11.751

0.159
0.660
-0.734
-16.429
-10.075

0.541
-0.681
-0.494
96.395
1.955

20.250
-89.110
1536.000
-11.000
4.550
81
11.900

σ Cap
193150

20 16.5

-19 17 5.5 g 124 -10.66

28233

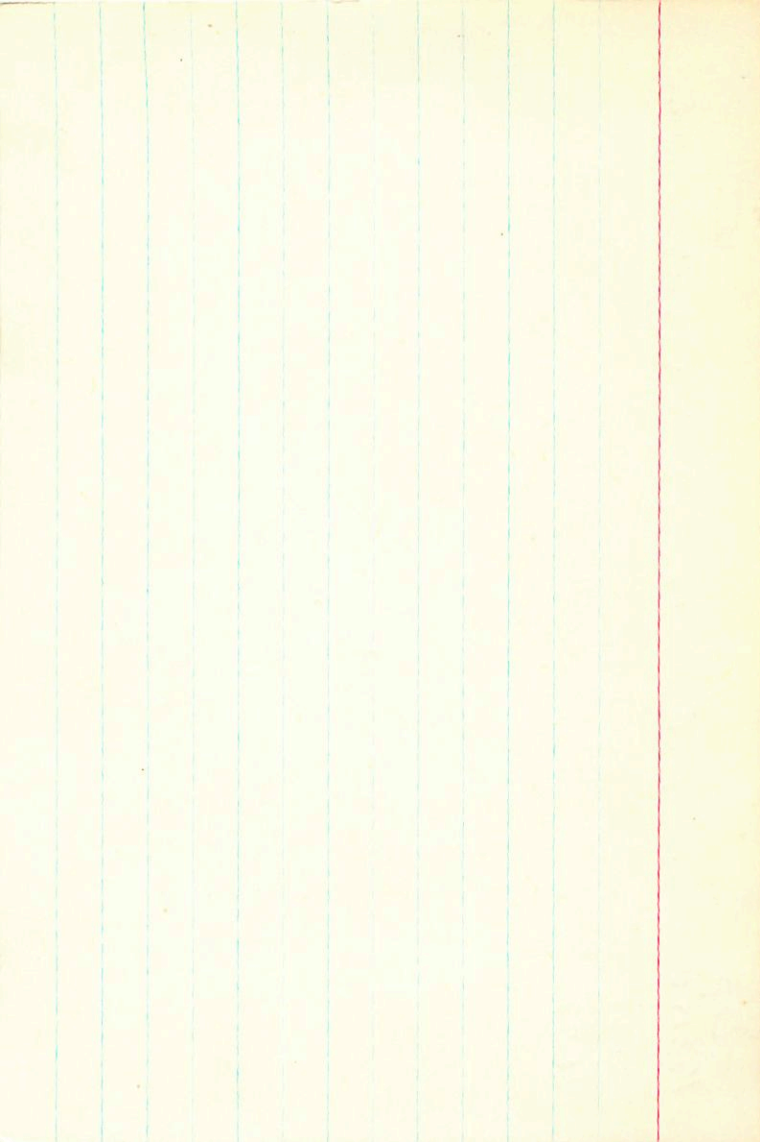
12677

A0513675

+0005³⁵ -010³⁶ N30

+0006³⁵ -007³⁶ ±1460 N30

110①



190492

193194
3404807

20

17.0

-34 44

6.07

1259

7.22
4.55
4.97

+039²-052 sleep

pit

+0418-0498

$\frac{1}{2}$
 $\frac{3}{3}$

+0512

+0505-050.5

6154 7692 0724

9882-1350-0189

-7.2

0123

HR778/

20 17.2 +55 14

DA7 +1C

38 (24)

W12687/E

5.76 10.10 +0.03

DF3 -8C

-009-0256C

7.43"

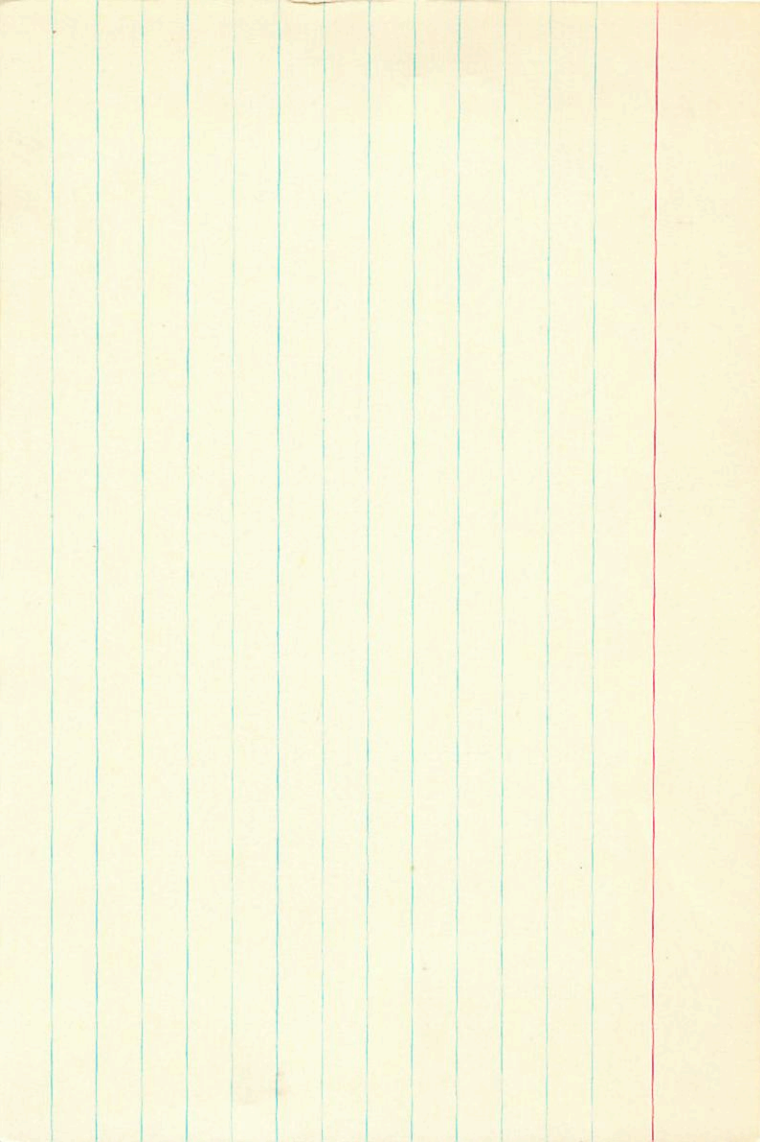
-024 (2)

A0510692

$\Delta m = 1.42$

10A(2d)

-18M(10)



193231 20 17.8 -0266 ± 11.3 -155 ± 9.0 (3/15)
28281 -0268 -54 58 -121 -26.1 ± 0.6

8.39 +73 1.78 -80.5 (3)

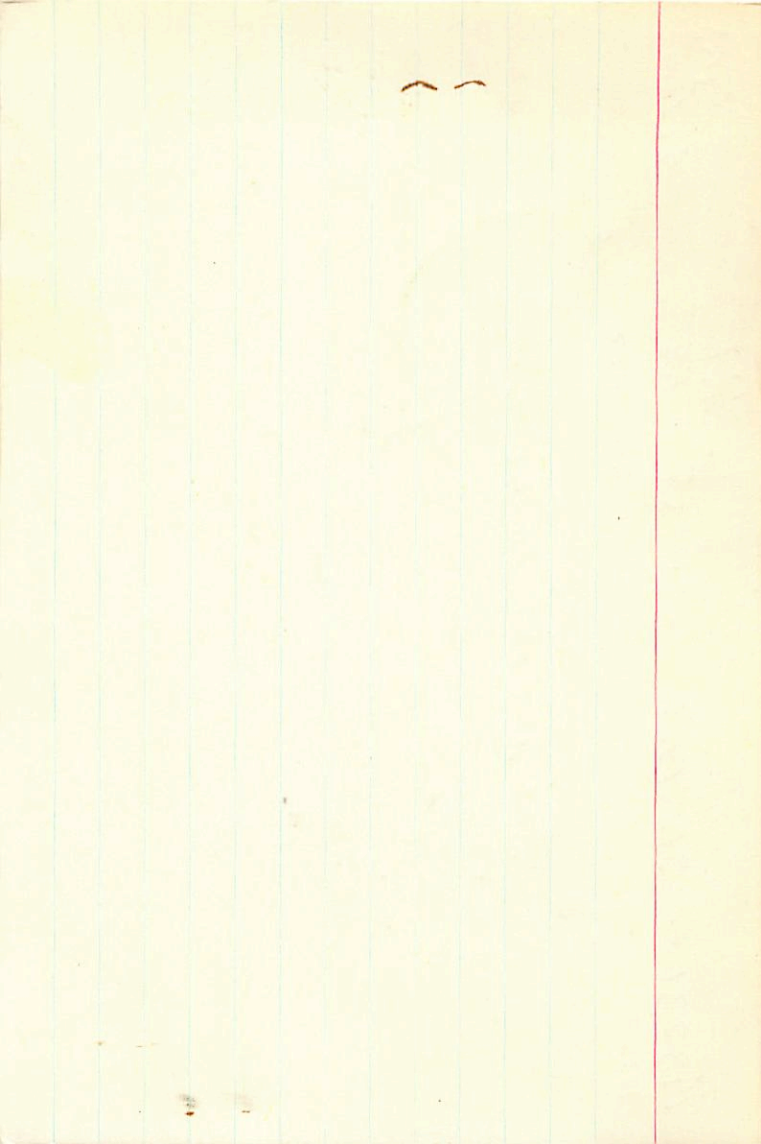
47.968 1905.1 -0271 -115 ± 4 CP
-0253 -218 ± 7 0.99 ± 7 CP
-54 58 12.80 2901.0

1.194
49.162
2.60

258
-264 +155 GG
-268 -121 NW
-271 -115 CP
-253 -99 CR

9.6 1938.7
9.77

-264 -112
+155
-249 -106



+0010 → 4.6
+0004

-035 ± 3.7
-049

193579 20 18.1 +17 38 6.0 9.15 -32.57

28292

12702 5.096 1901.8 +17 38 4.08 1897.1

$\frac{-048}{5.048}$

+1000 -042
+3 5.93

5.058 +100 -039 3.85 1933.9

$\frac{060}{060}$

5.064 3.74 1939.75

$\frac{0620}{0620}$

+21 3.95 36.8

+014 3.97 39.7

-1.96

35.0

39.7

193579.000*

20.000*

18.100*

17.000*

38.000*

0.010*

-0.039*

6.500*

199.526

-32.500

-0.097

-0.503

-3.072

-0.088

0.845

-44.954

-0.139

-0.181

-21.814

2

AD513723

20

18.2

+45

12

-26.0

Woolly

6.98 + 455 00 → 20.0

750

+0022 -026

-2

+0020

-022

↓

600
25

193707

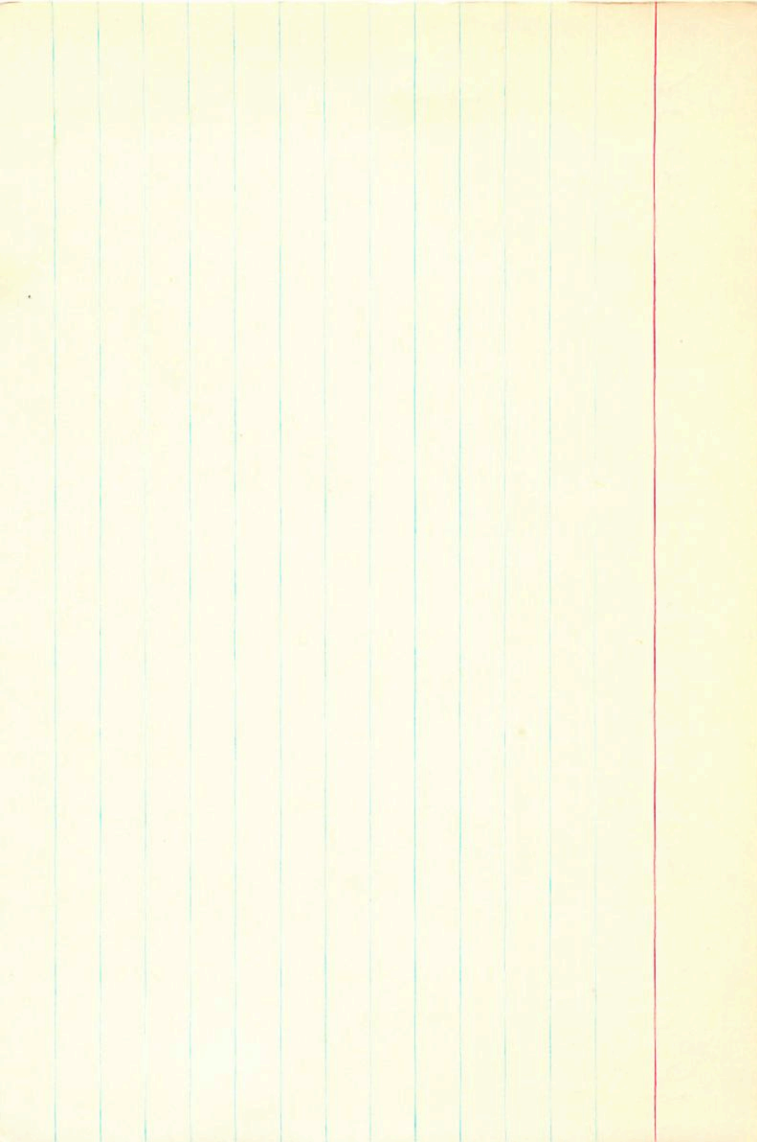
20 18.9 714 57 6.6 A1 -22.38

28307

12708

toooq -014 Cambridge

to13-014



H 7

+360 4028

20

19.7

+86

45

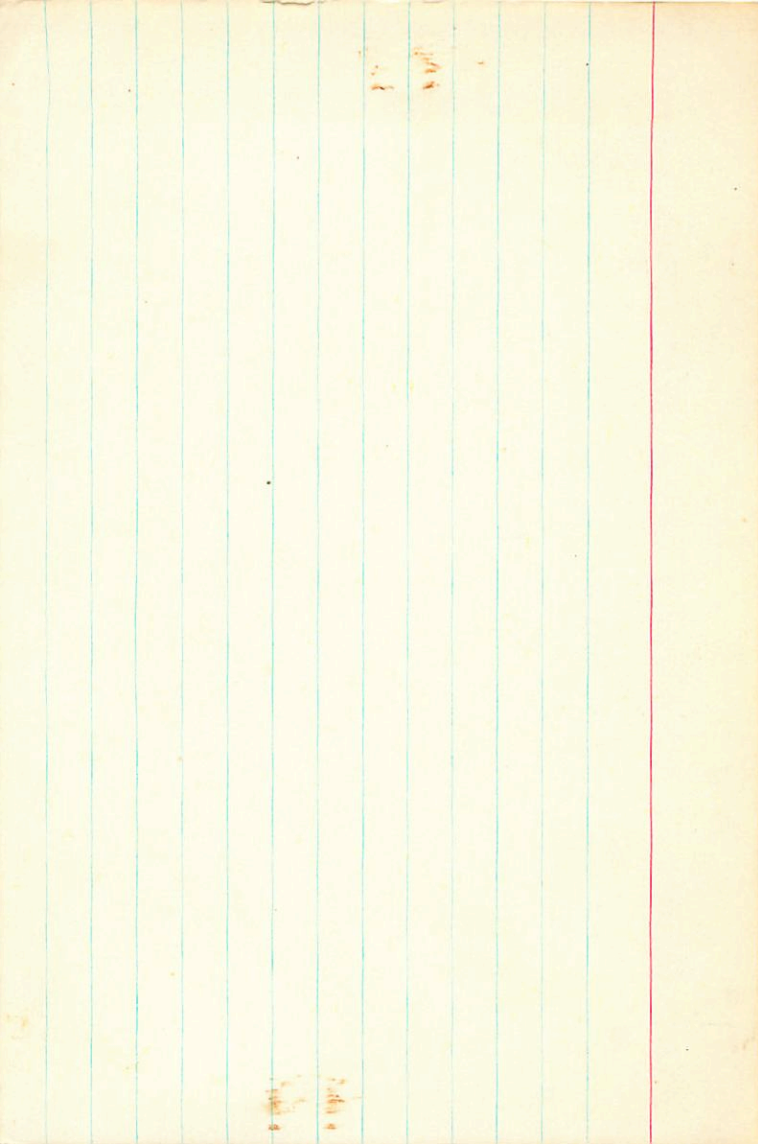
W.H. 6

+54

(30)

9.93

— —



193807

F01050

630.5
730.5

14m20"

1002 1024

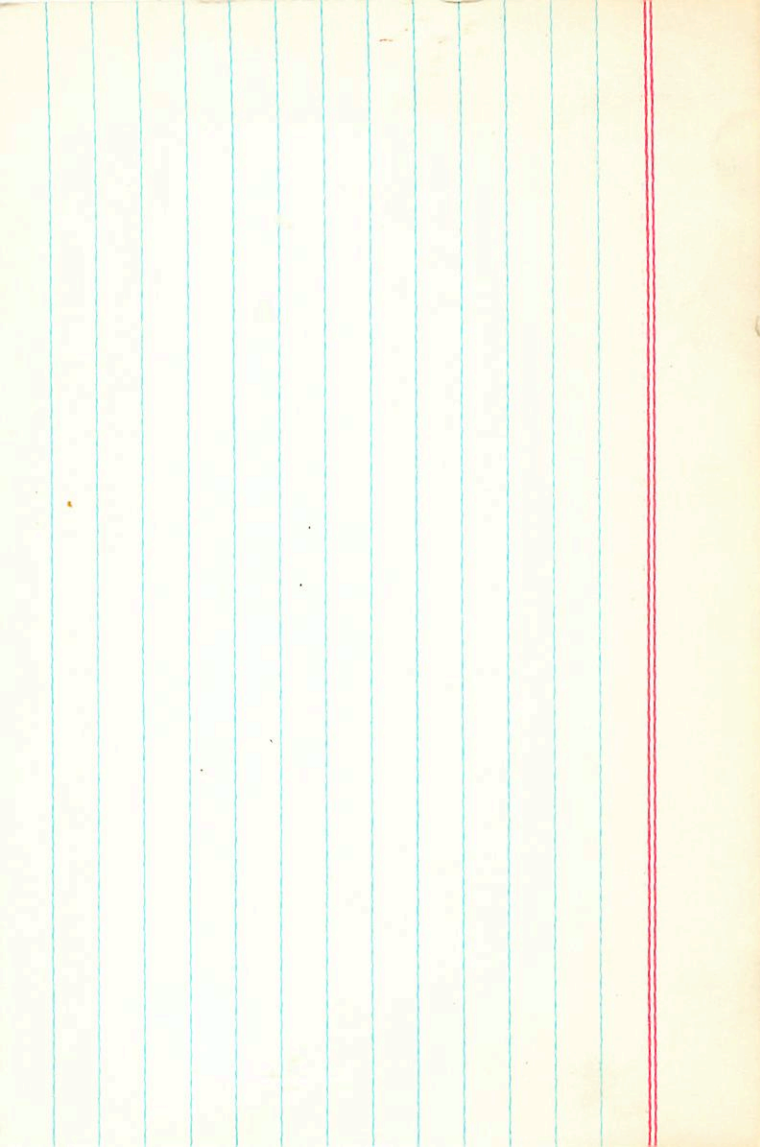
1001 1028 130
1003 1027 020

563 + 20 (1.57)

-8 054

00 00.5 -42 35 4314 +8.372.1

42



7796
37 2 Ceylon
28338
12723

20 20.5 28

40° 6'

440.1

+10040 +10030

F.V.S

-7.5a

2.32F8P

0.496	0.834	-0.240
0.201	0.159	0.966
-0.845	0.527	0.088

AOS 13769
194298

28340

12725

-0010 ± 6.0 + 024 ± 3.8
0
+018

20 20.5

+63

49

5.9

945

+30.28

+268 ②

+86 ④

+158

14001

1898.1

+63

49

10.42

14001

$$\frac{0.52}{.112}$$

$$\begin{array}{r} 7.81 \\ 21.3755 \\ 29.1605 \\ \hline .129 \\ \hline 136 \end{array}$$

$$\begin{array}{r} 29.111 \\ \hline -18 \\ \hline .093 \end{array}$$

$$\begin{array}{r} 229 \\ \hline 114 \\ \hline +042 \end{array}$$

$$\frac{-1.20}{92.2}$$

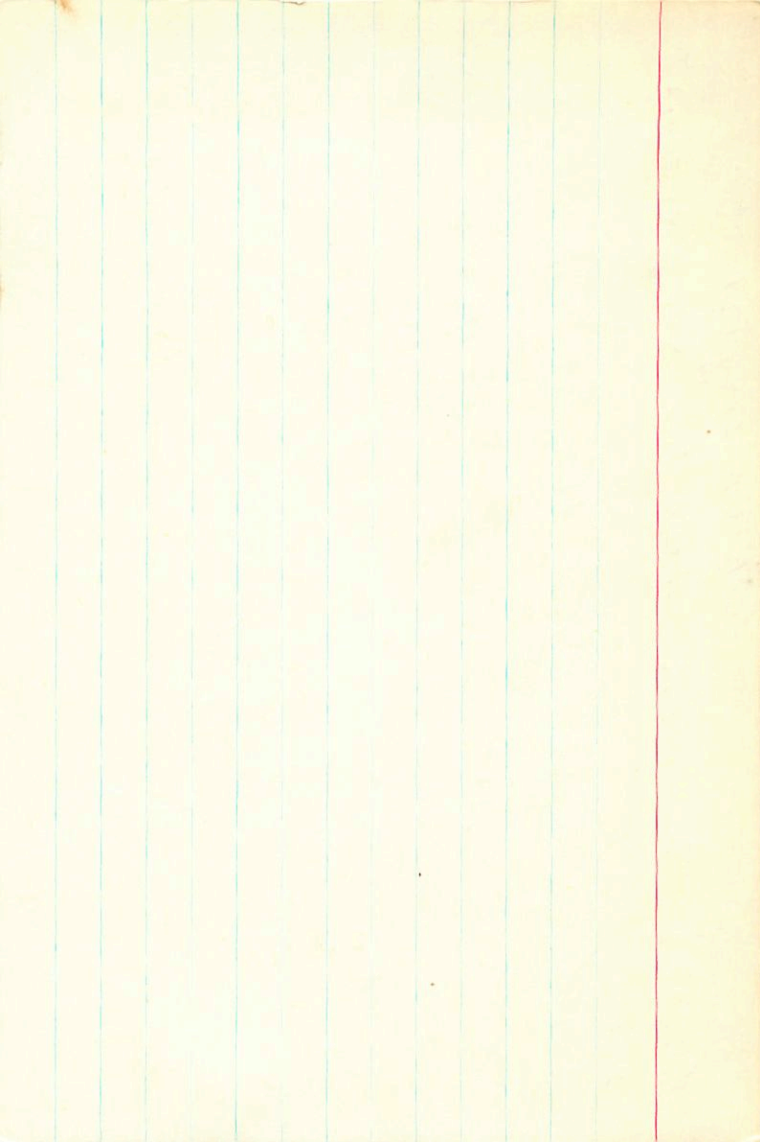
$$\begin{array}{r} 21.8 \\ 47.65 \\ \hline 9.45 \\ \hline 30 \\ \hline 9.75 \\ \hline +14 \\ \hline 9.91 \end{array}$$

$$\begin{array}{r} 7084 \\ 35.4 \\ \hline 1944.94 \end{array}$$

$$\begin{array}{r} 7084 \\ 35.4 \\ \hline 1944.94 \end{array}$$

$$\begin{array}{r} 9.94 \\ -16 \\ \hline 9.78 \\ \hline 9.84 \\ \hline +62 \end{array}$$

ESC
1944.94



194013

20

20.7

+05

11

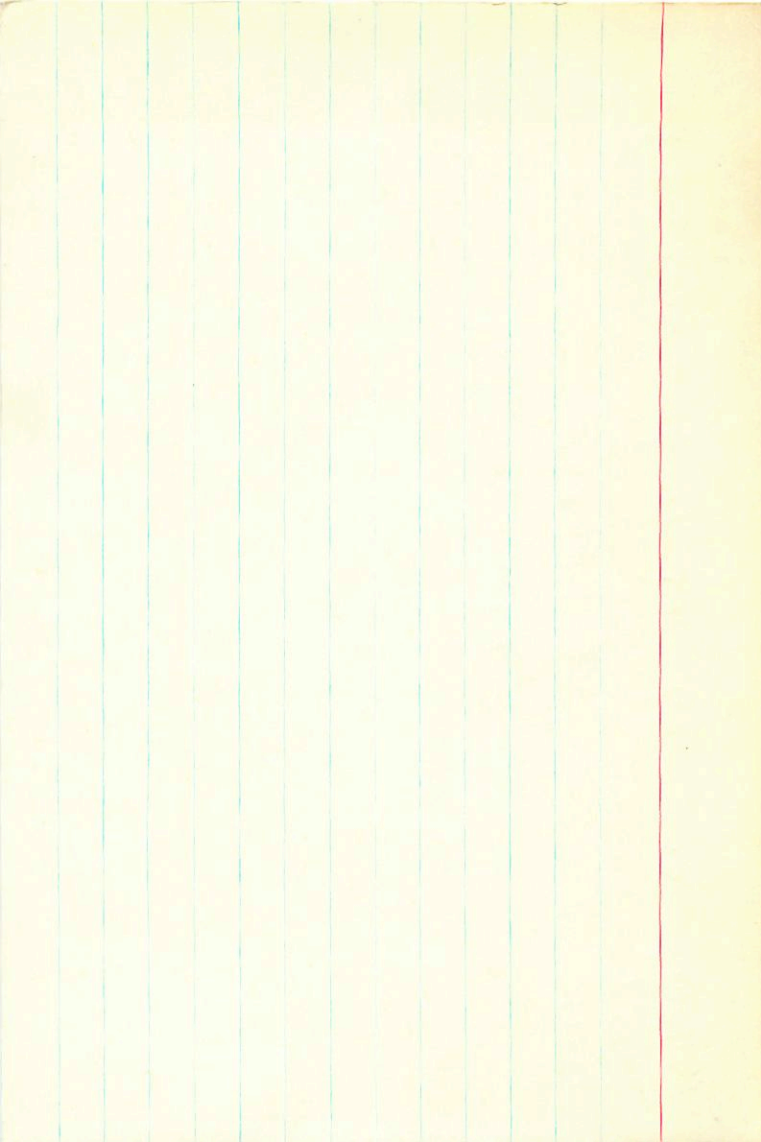
⁵⁴967 -11.7a

28351

12781

-0021 43 -036 39 N30

-0019 ± 2.7 -038 ± 2.7 66 → N30



ADS13786

194220

28364

12735

20 21.2

+42

49

6.3

No. III 120 -20-18

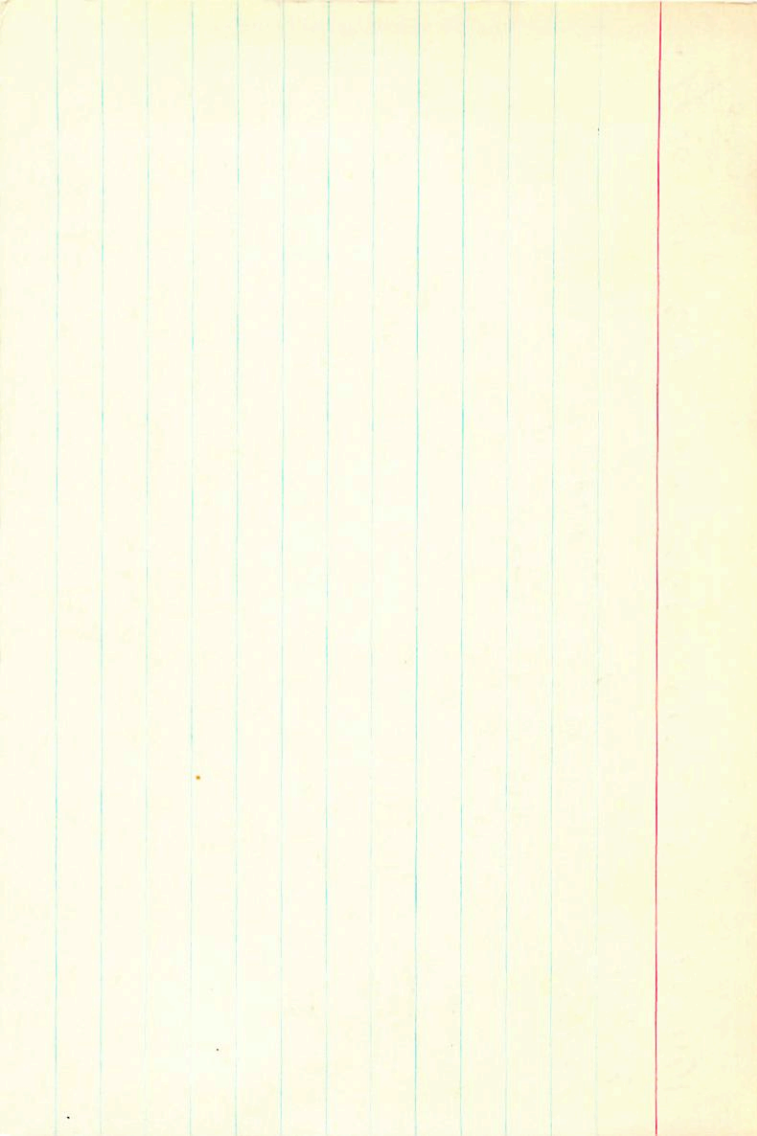
+0048¹⁷

+046²⁰ N30

+0042±3.4 +038±23

184 (2)

+0.400



+31,000 ✓

WR743

20 219

+3202

9 NS -1466

AD194317

584/4

HR7806

288/6

① 112-10

655
1390
+037-002

+0028 000 →

" 4036

672
551052
69

562 765 -312

+0960 +5.2 +4.5 +6.6

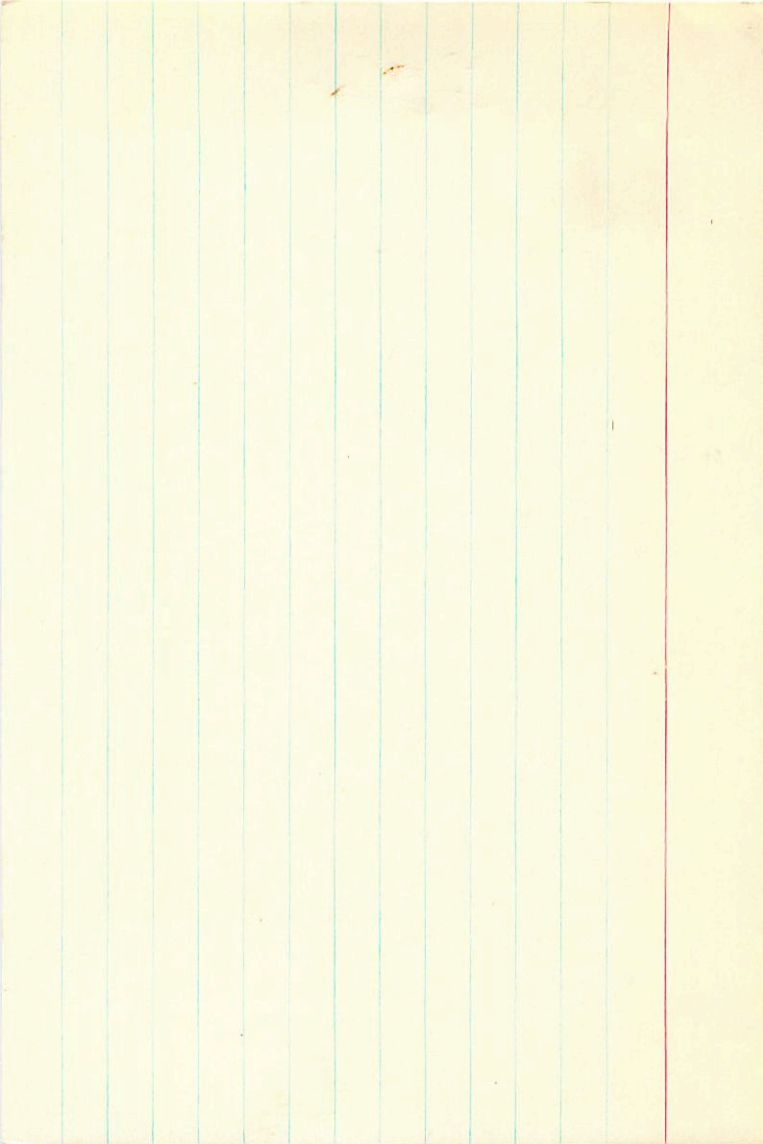
138 285 948

+0236 +1.3 -13.8 +1.6

-815 577 -055

-1390 -7.5 +0.8 -9.7

9 493
1.74
1.52
44
21



174251

20

224

25

28

1084041

8 Aug

$+1004 + 004$
 $+ 00025 + 003$
 $+ 000105$

TOTAL
 1084041

017 0 - 0025

-725

P = 377.6 Aug

1084041
 1084041

3



20.400
-29.800
16.000
10.000
5.000
100
-7.250

0.567
0.103
-0.817
42.556
10.180

0.134
0.968
0.214
54.762
3.922

7799

20

225

-40

58

102115

-0091

+5

-0086

-0596

-088

+5

-083

Stey 1471

Ca. 157444

Sp. B. P = 117.8

$\gamma = +42.3$
curve

4

7799.000*

20.000*

22.500*

-40.000*

-58.000*

-0.098*

-0.083*

6.000*

158.489

42.300

-0.232

-0.823

-71.618

-0.454

0.005

-71.719

0.333

-0.568

28.717

4