

140283

20 02.0

-21

27

GGII

-19.54C

F01257

7.10 + 1.04 + 1.92

-20C.3W

+0031 -027 2C →

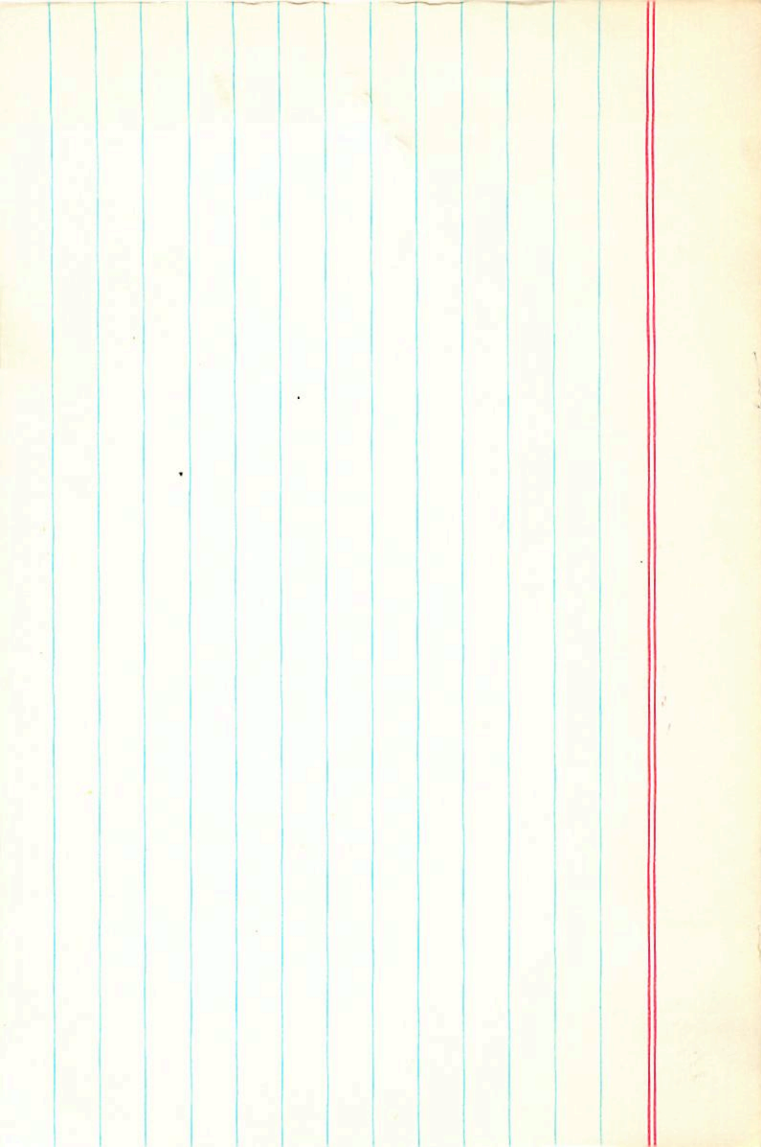
-034 N30

-032 GC

+0034

+0036

+0035 -033



160537

~~13347~~

-301

70 022 431 06

602 tang 104

102312019

46

19

101

301

040 1019

32



W. E. D. R. A. D.

W. E. D. R. A. D.

W. E. D. R. A. D.

W. E. D. R. A. D.

W. E. D. R. A. D.

R.A. : 20.050
 DEC. : 31.100
 PM. R.A. : 46.000
 PM. DEC. : 19.000
 DISTANCE : 5.000
 MODULUS : 100
 RAD. VEL. : -30.100

q1 (U) : 0.504
 q2 (U) : 0.784
 q3 (U) : -0.363
 DU : 164.648
 U : 27.396

q1 (U) : 0.191
 q2 (U) : 0.300
 q3 (U) : 0.923
 DU : 63.76
 U : -21.66

q1 (M) : -0.84
 q2 (M) : 0.52
 q3 (M) : -0.02
 DM : -108.59
 M : -10.79

32

150350

H07671

GC27800

28 62.3 -11 45

SFY

6.42 +0.55 +0.30 1895-

spots

[2] 361 [17]

$\frac{1}{18} \times$

815 [17]

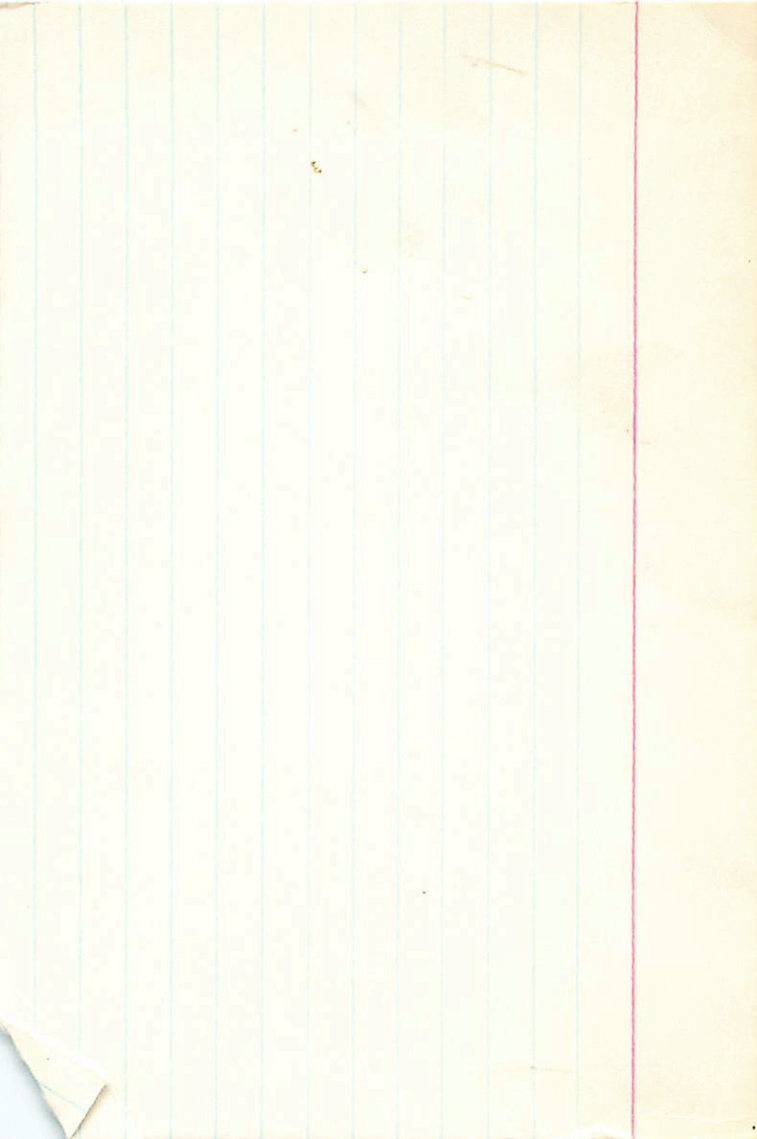
1933, 15, 1933, 15

3- 60

450 + 8.5 - 9.9 + 1.6

-15 -53 -35

Steph



0005 ± 2.4 - 0.12 ± 2.4
0

4459
190350

20 62.3 - 11 45 = 6.5 g FY - 12-10
-0.13

27950
12439

20.04
54.0
-0003
-00075 - 0.123

-0022
-001-017.5

7611 μ 19.783 1845.2 - 11 44 32.32 1842.3

027
810

.64
31.63

20.05
- 11.75

56.995 19.789 32.40
22.955
19.854
1.824

46.06 1933.99

-1
-175
8.0

41.5

33.71
31.30

348 - 12.1

822
808

19.799
794 - 0.12

32.441
32.439

36.7
44.0

52.02
32.34 1939.49
+10

32.26
32.14 - 51

33

1000
1000
1000
1000

190306 20 02.3 -33 09 C.L. B8 -

+0012±63 -019±5.4
+0010 -014

27851

12440

20.940 ¹⁸⁹⁵⁶ -33 8 35.78 1893.4

-065
1874

+1.08
34.70

6.8-8.6
0.6

45.239

35728

20.967

60

507

17

890

920

+046

20.949

+1
950

46.0

48.98 1928.45

11.98

37.00

31.50

35.50

+25

35.25

35.45

8
35.53

8330

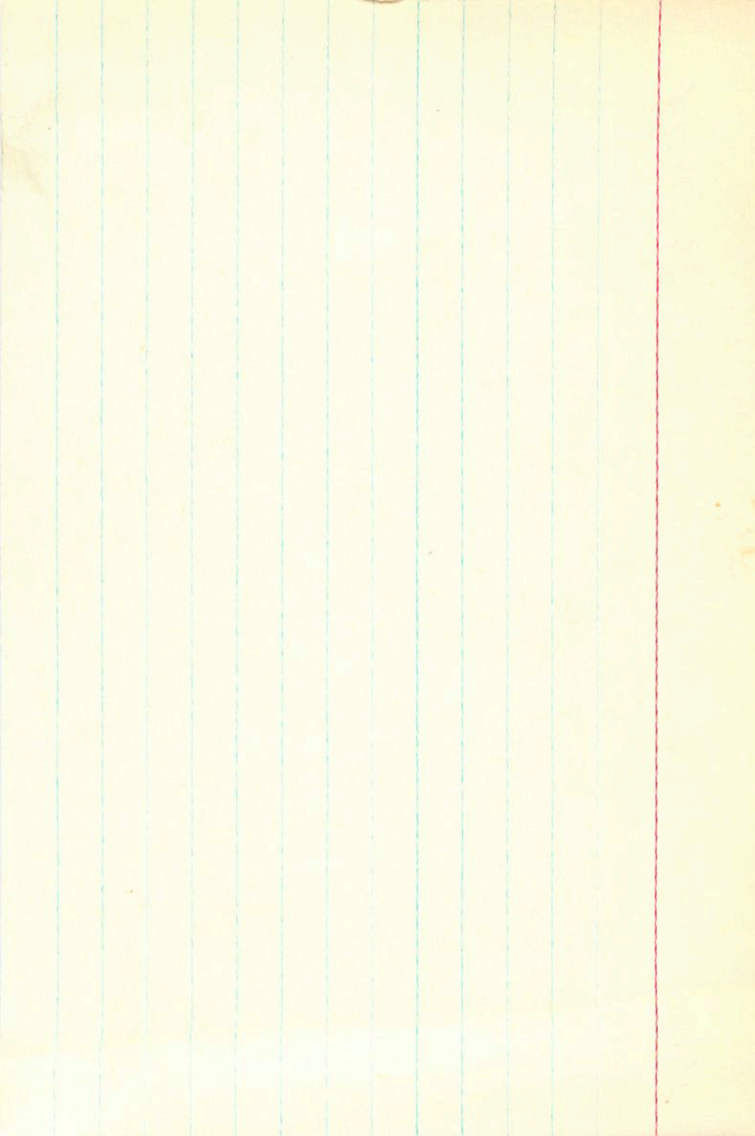
41.6

48.2

35.34

.69

1954.85

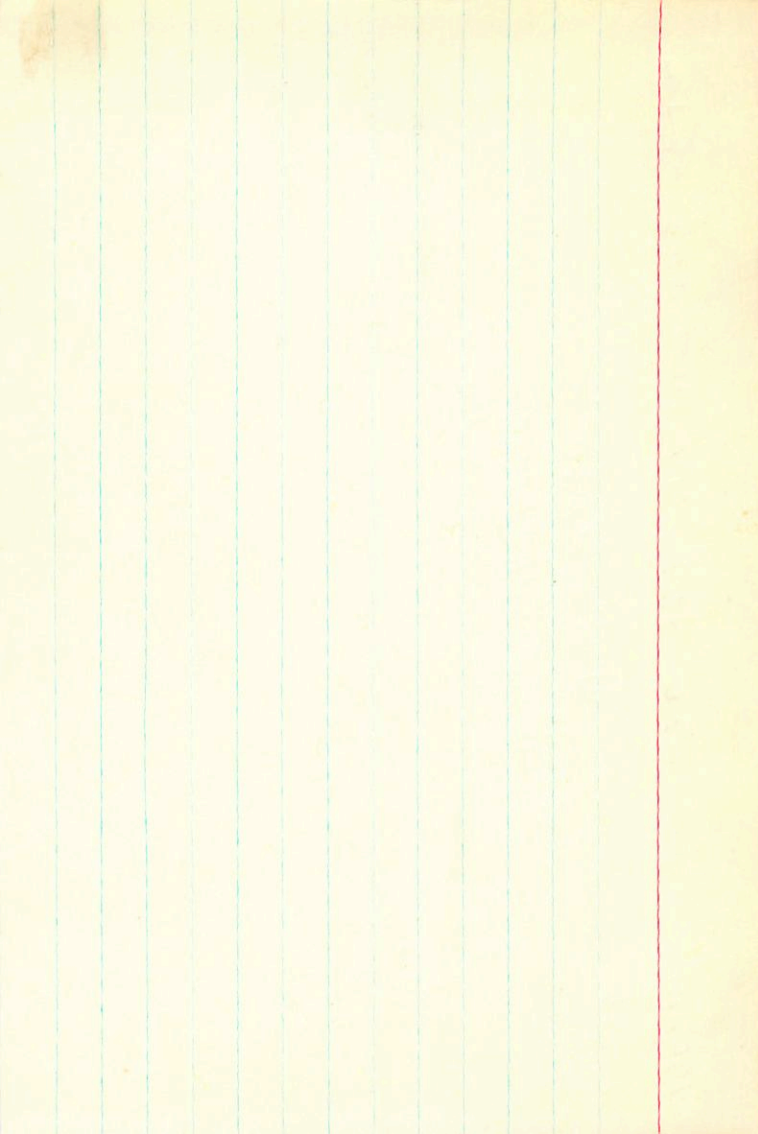


190940 20 02.6 +67 44 4.7 g112 -9.2a

27856 -9.0②

+0020⁴¹ +052 v²M30
+0016 ±1.54051±1.2 GC → M30

12443



190309
27861

20

02.7

-44

29

C₂ -57.0 ± 0.4 (6)

7.86 +1.13 K1 III cups

+63 -32 +12

005

+68 -41 +7

.004

+73 -56 -1

0038

7017 -043 cups

+0018 ± 13.0
+0006
-084 ± 13.0
-037
-043 CP

41.223 1903.4
-084
+0014
-44 29 7.37 1903.4

$\frac{-084}{139}$

$\frac{3.91}{3.46}$

41.157
-157

5.40 1955.50

$\frac{-157}{136}$

$\frac{-8}{5.48}$

140333

20 62.8 - 43 21

Bd 5.4:11 1.7

8-2

GC2765

9.20 40.66 ~~44~~ 822

*58.25.00(15)

174
129

923 427 200 297 (P) -041 H 007 77 -23252 CR

134 204

922- 420

203

428 201

(297)

5 9633

-250 CR

444 29

-0080715.0

-2475.5

-03650 -250510 644

-0058
+ 7

-0051

-343
+ 6

-237

-44 -64 -31 .020
-50 -79 -30 .015

0.1

0.1

0

0.1

X Eye

20 02.9 +20 30

+26 d

380 m.

$$\begin{array}{r} -15^{\circ} - 30 \text{ HR} \\ +3 \\ \hline -12 = 3 \end{array}$$

502	704	-502	-0357	+0100	+0457	-28	-13.0
195	473	858	-0138	-0067	-0205	+16	+22.3
-842	530	-102	+0599	-0075	+0524	+14	-2.6

$$\begin{array}{r|l} -0286 - 0100 & -0386 \\ -0110 - 0067 & -0177 \\ +0479 - 0075 & +0424 \end{array}$$

$$\begin{array}{r} 6.50 \\ 6.12 \\ 1.38 \\ \hline 9.77 \end{array}$$

X₈₀

5.9.7 - 5.9

5.5.4 - 8

190229

5.6.7 - 10 - 48

+ 07

6.20

12449 20 02.9 454 20 1100 -9.08

1800454

140780

+0070 -122 Y

-5
+0065
-121
+3

7.72 +0.535 +0.65 2 20"

672
+1.00

14m

+0065 -118

190781 20 03.0 +48 05 6.0 A0 -13.58

27869

12452

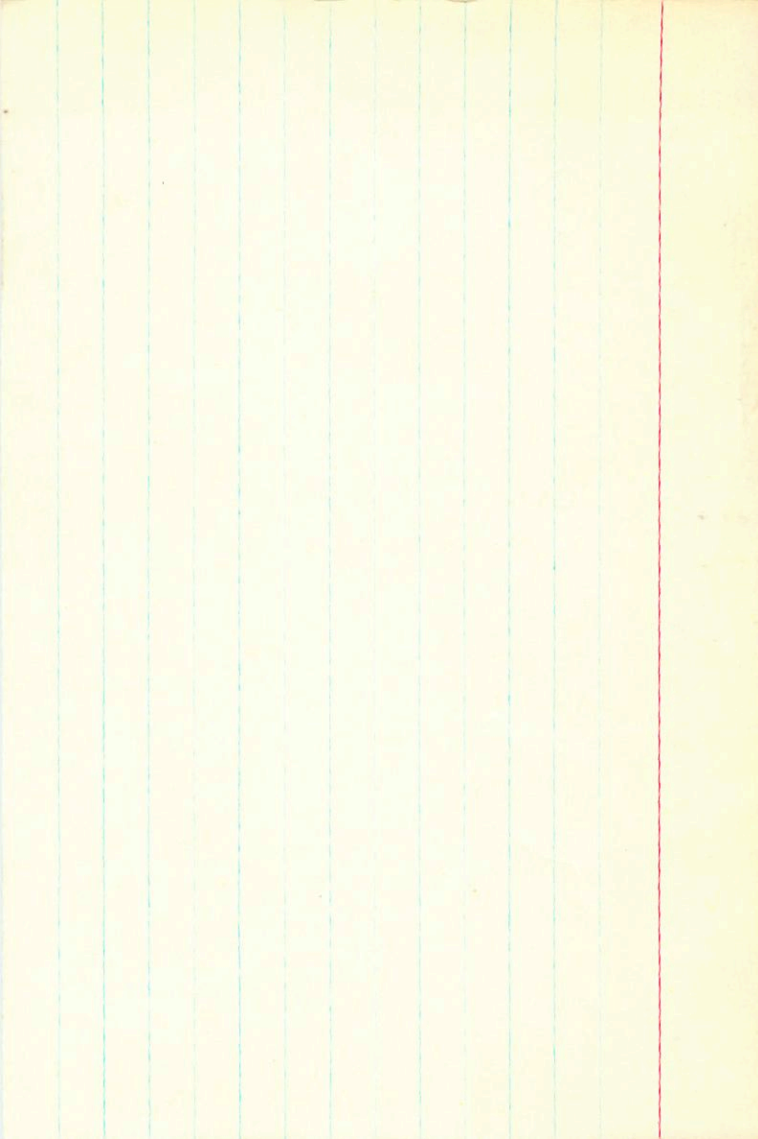
+0004¹⁶ +0003¹⁹ N30

+22.

+0003±3.5 +004±2.466 → N30

+7

-22



5 Feb
 190421 20 03.6 -53 02 4.9 M2 +3608 SA?
 +004 ±4.1 +002 ±3.6
 -0014 +007

→ 450

27879
 12456 33.829 1909.7 -53 1 33.56 19073
 -09

1139 +0082
 FRS

$$\frac{064}{893}$$

$$\begin{array}{r} 33.889 \\ -43 \\ \hline 846 \end{array}$$

$$\frac{840}{853}$$

33.50 1925.05

$$\begin{array}{r} 33.59 \\ -9 \\ \hline 9574 \\ 47.4 \end{array}$$

$$\frac{33.88}{40.1}$$

$$\frac{9533}{47.7}$$

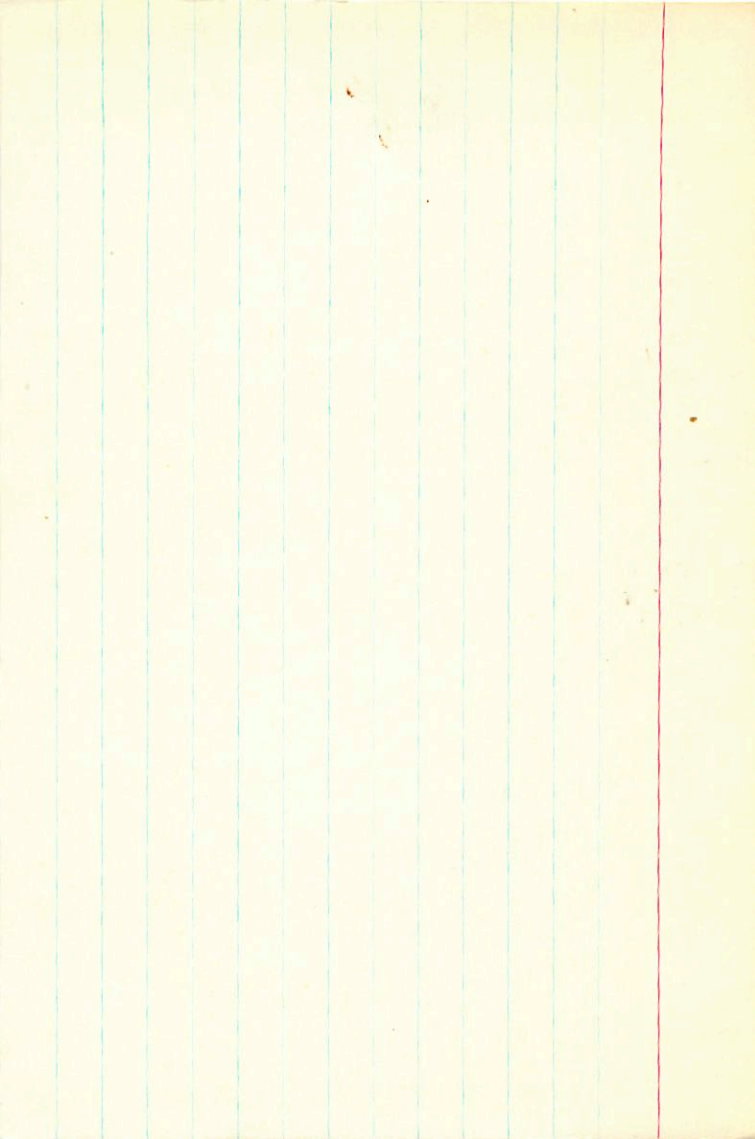
 380

+0.27

33.880
 -47
 1533

1956.25

33.13 1926.69
 -3
 192.16



7687 20 03.6 -4 15 120

-218

6046 + 1.16 + 1.00 60

P.C.

048	+2	
+2		
1050	-038	

5.5

-2.1
slippin

34

12

12

7681.800*

20.000*

3.600*

-4.000*

-15.000*

0.050*

-0.030*

5.500*

125.893

-2.100

0.043

-0.740

6.925

-0.097

0.503

-13.421

34

450

3 Tel. 20 03.6 -53 02 gm2 +36.0a

BR7673 4.95 +1.66 gm -0.13 +001 FN3.

-0.14 +00266

~~-001~~ +005430

-002 +004

+10 300

9/14

18 420 4.2 + 54 12

00048 + 0750 = 2.500

0027 + 0827

- 31
+ 0022 + 090

6.21 + 1.03 + 3 1 895

668099

872
102

-0011090 -11.96

.278 .155 .535 @ 500 2.071
284

205 + 16

479 + 7/54

420 + 220 - 14.9 + 11.3

+ 27

+ 320 - 48 + 203

3.50

35

-0008 ± 3.1 +077 ± 2.6
-0000 +080

191096 20 04.2 +56 12 6.2 g F4 -1198

27899

12470 ✓ 13.317 1891.1 +56 11 45.97 1887.2

047
1,364

-4.90
41,07

39.25
34.128
13.378
365
365

1926.7

26.3 1927.2

17.45
43.52
41.27

45.0

359
365
-005

999

41.27
48.00
44.36 +3.93

7216

36.1

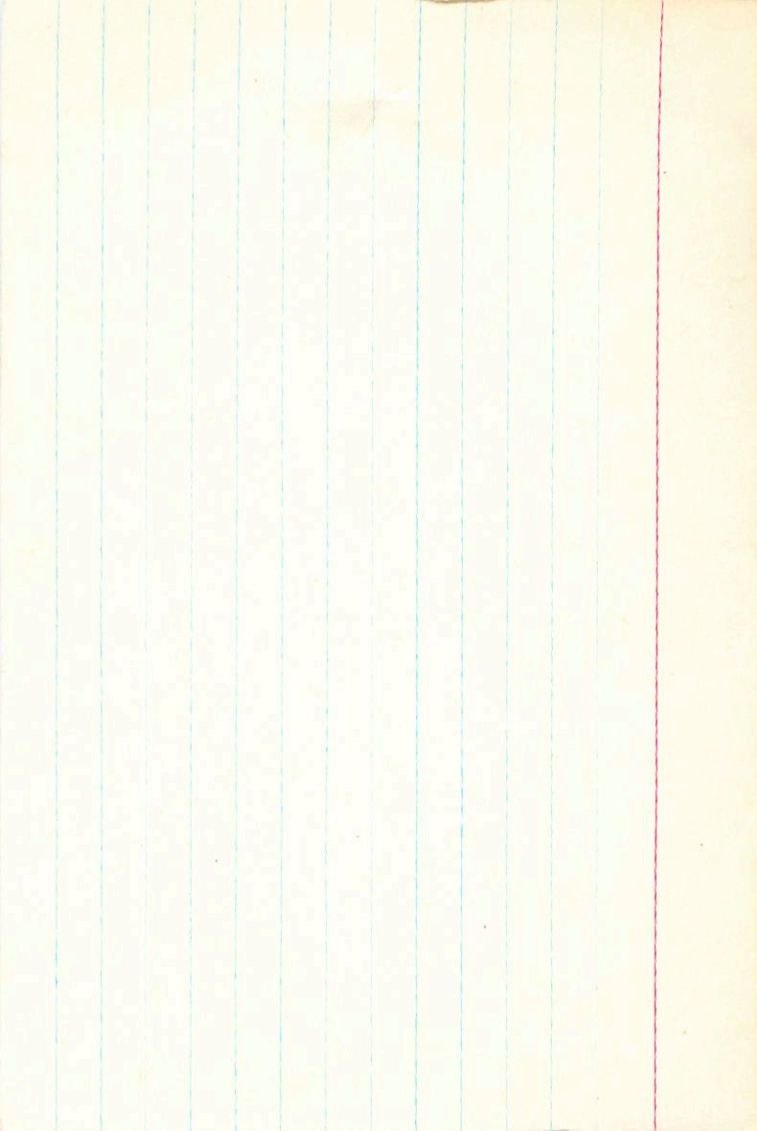
48.9

13.347

45.93 1944.96

-30
45.63

353



6622a

191277 20 04.8 461 51 5.6 g 113 +5.58

27911

12480

+0162²¹ +074²³ N30

+0164±1.5 +076±1.16C → N30

1154 75

243
25

6.0

6.5

26

R.A. :
DEC. :
PM. R.A. :
PM. DEC. :
DISTANCE :
MODULUS :
RAD. VEL. :

20.100
41.850
243.000
75.000
4.000
158
5.500

p1 (U) :
p2 (U) :
p3 (U) :
pU :
U :

0.513
0.623
0.072
285.222
92.781

p1 (U) :
p2 (U) :
p3 (U) :

0.100

R.A.	:	20.100
DEC.	:	61.850
PM. R.A.	:	243.000
PM. DEC.	:	75.000
DISTANCE	:	6.000
MODULUS	:	158
RAD. VEL.	:	5.500

q1 (U)	:	0.513
q2 (U)	:	0.853
q3 (U)	:	0.092
dU	:	582.222
U	:	92.781

q1 (V)	:	0.185
q2 (V)	:	
q3 (V)	:	

+0238 #2.4 +257#2.1
+0232 +257

191195 20 04.9 753 01 5.7 dF4 -40.76

481 ②

280 156

12482 54.839 1893.5 +53 1 1.79 18955

$\frac{-14.01}{47.78}$

$\frac{1.345}{53.494}$

1095

$\frac{36.8}{18.58} - 1927.4$

1926.4
46.74
3.14
3.66

15.34

38.922

$\frac{34.269}{753}$

257

989

54.731

$\frac{494}{989}$

$\frac{732}{+}$
1,000

7114

11695

$\frac{37.1}{14.1}$

$\frac{55.98}{56.06}$

43.1

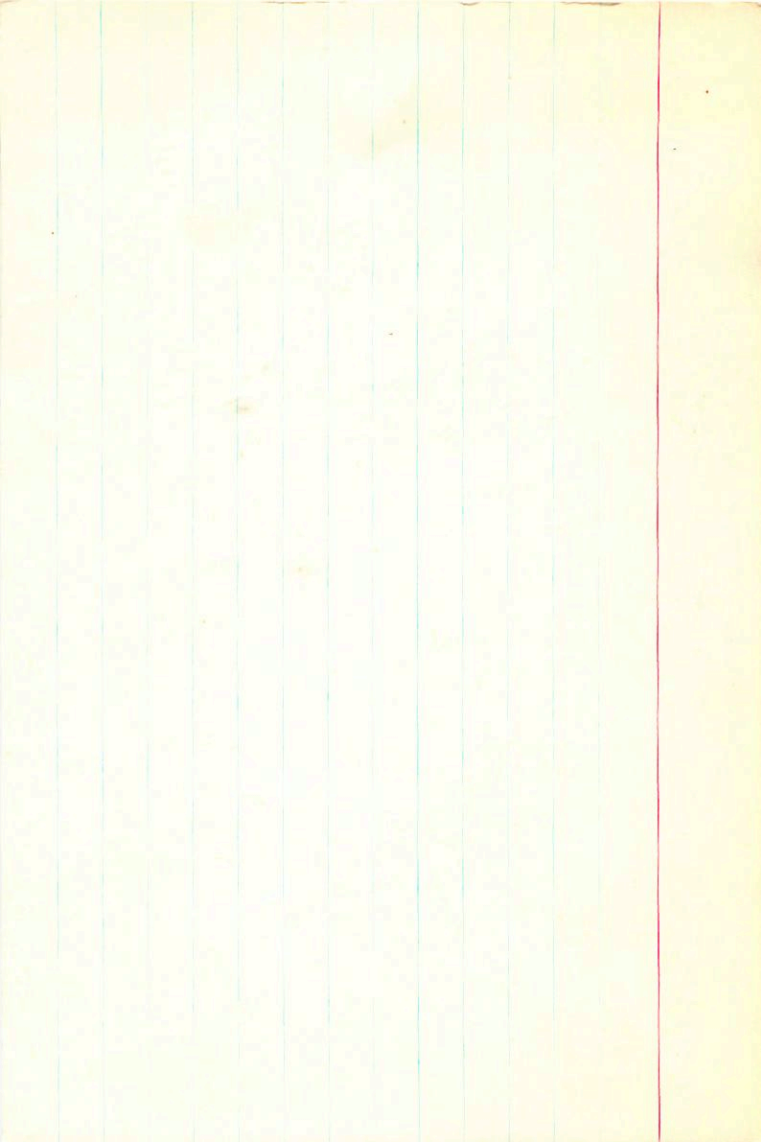
41.6

1.19 1946.74

$\frac{-30}{0.89}$

$\frac{58.48}{10.70}$

1980
1980
1980



H0190779

20 05.1

-46

27

GP -43.0 ± 0.8 C₂(5)

27917

u³¹

8.23 + 0.42 FSU

879.2

+061 -091 Cape

4.2011902.5

-46 26 47.94 1899.2

-252

949

4.88

43.11

+33

-42

4.234

219

+40

+30

+7.93

1554.95

219

48.00

+24

-044
-0053

-40

-53

-44

+46

+17

-855 519 -725 688 +061-091-43.0 066 831 -255 ✓
052 056 032 034 085 ✓ 417 ✓ -296 -15 +25 17
-10 +50 +13

A0513401

+0299 ± 7.8
+0297

+176 ± 10.6
+174
3W

191633 26 05.7

+72 57

8.1 d60 -35.78

27926

12486

16.796 1906.2

+72 50 59.65 4089

13^{m2}

-1.310
15,486

-9.23
52.42

31.6

16.556
161

852
426
1000
+940

59.21 1945.21 757
-15 190 37.8
59.06 198.9

16.205
35
236

56.1 1930.5
-26 57.45
55.84 5.03

1026 ± 173

1129 ± 173

437
173 ± 7 ± 5.7

9764 + 4135 211
-2159 9705 6459

20

685

569
27 27
685
26 26
292
23 23



R.A. : 20.100
 DEC. : 22.820
 R.A. : 487.000
 R.A. DEC. : 173.000
 DISTANCE : 4.700
 MODULUS : 87
 SAD. VEL. : -32.700

p1 (U) : 0.213
 p2 (U) : 0.338
 p3 (U) : 0.353
 p4 : 0.880
 p5 : 7.847

p1 (V) : 0.183
 p2 (V) : -0.323
 p3 (V) : 0.281
 p4 : -2.020
 p5 : -0.413

p1 (W) : 0.338
 p2 (W) : 0.413
 p3 (W) : 0.353
 p4 : -171.333
 p5 : -27.448

2

R.A. : 20.100
DEC. : 72.850
PM. R.A. : 437.000
PM. DEC. : 173.000
DISTANCE : 4.700
MODULUS : 87
AD. VEL. : -35.700

q1 (U) : 0.513
q2 (U) : 0.820
q3 (U) : 0.253
dU : 986.001
U : 76.847

q1 (V) : 0.185
q2 (V) : -0.393
q3 (V) : 0.901
dV : -209.666
V : -50.413

q1 (W) : -0.838
q2 (W) : 0.415
q3 (W) : 0.353
dW : -171.332
W : -27.540

-854 520 301 954 1078-016 45-005-29-011

067-004041-003 332₄₇ 175₂₅-906-47+77

0+102-39 007

172-75-35

WZ Sgr 20 05.3 +17 32

(111)

18

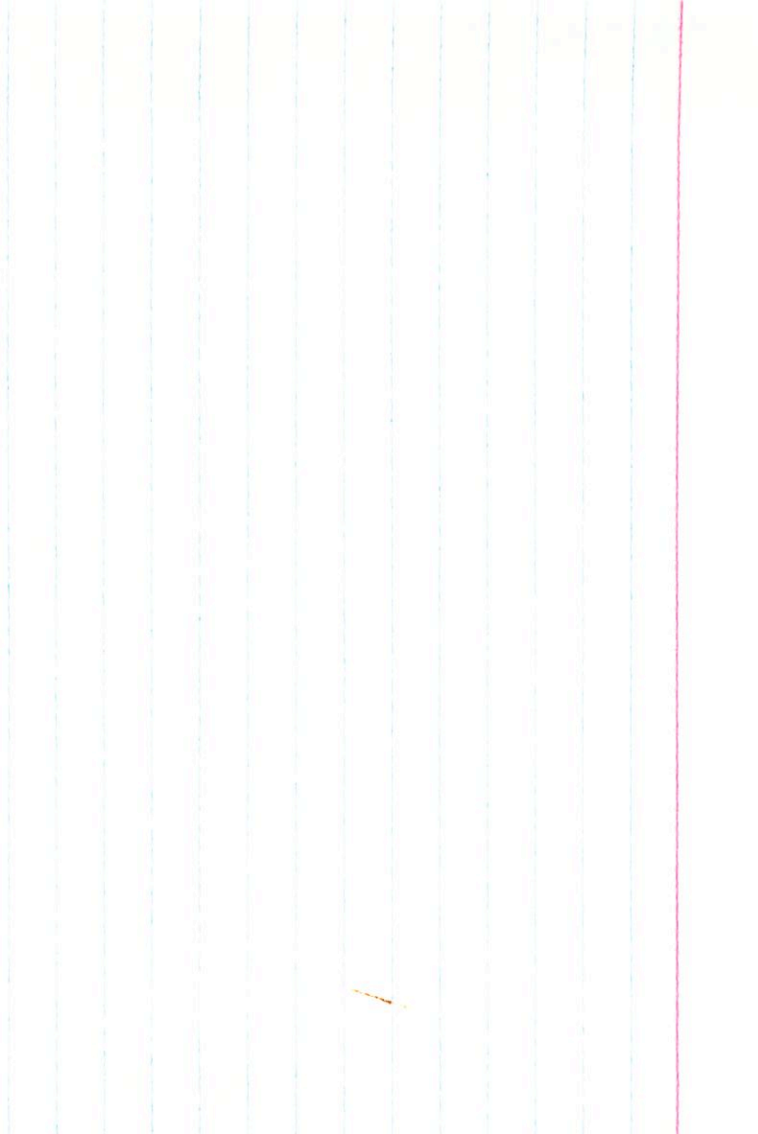
(-30) Kruyf

15.2 + 1009 - 9.71
5.5
9.4
-20

+078 -016
46.0
25.0
4.1

$\theta_0 = 120^\circ$
 $\theta_0 = 102^\circ$
P.L.V. - 9.4

+510	+674	-533	+1654	-0511	+1343
+158	+518	+834	+2696	-0343	+0303
-839	+526	-137	-3102	-0344	-3502
			1000		
			+294		
			-220		
			-350		



191250 20 06.6 -20 44 7.3 dF2 -6.86

27960

12505 38.244 1905.1 -20 44 25.13 1902.5

-090

.154

+3.56

21.57

10.586

27.670

38.256

-35

2.21

-13

2.08

38.218

-14

204

total 074

total 076

28.5

total 076

206

+052

0762

0191

8457

8814

-459

8765

21

-26

-48

45.30

20.30

25.00

135

23.65

+30

23.35

24.34

+14

24.20

755 6713

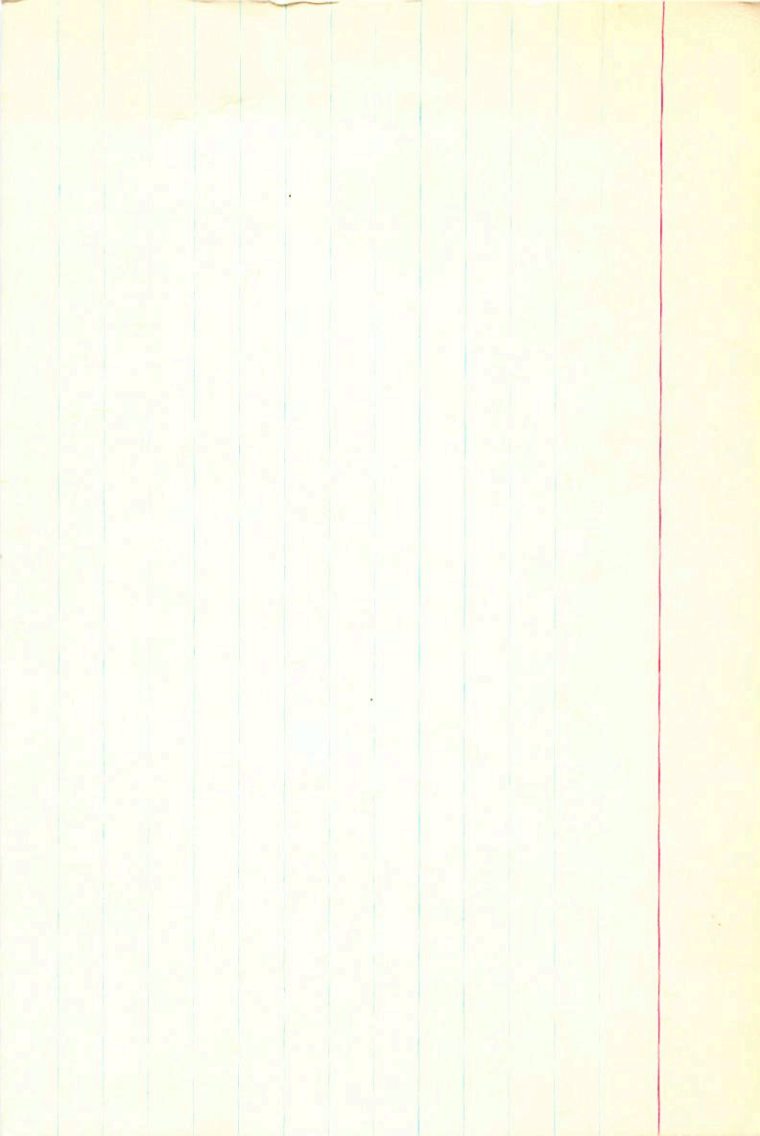
33.6

31.1

1938.90

23.78

-2.21



667

70-2.4

190879

20 05.5 -47 13

-57.0 50.85 (14)

6.44 + 1475 + 1.78 @

6.45 + 1.50 145 III

5.55 + 0.57 @

7050-054

537
96
8.0

+ 00 42-055 Stay 1960

+ 34 + 40
18454 - 0510

+ 035-077 CP

1052-050
+ 042 1045-053

~~1045~~
1045

5.35 7.50 = 313 po

+ 104
- 53

~~1045~~
~ 94

4.55

565
535

475

~ 40

512
1974

854 521 - 734 674 + 038 - 077 - 57.0057 + 42 - 246 ✓

032 049 020 030 - 38.7 - 20 + 33

⁰⁰⁴ 327

-18 + 42 - 3

0055 ✓

+78 - 52.0

-17 + 142 - 40

003

+103 - 102 - 27

38

1880
1881
1882
1883
1884
1885
1886
1887
1888
1889
1890

190879.000*

20.000*

5.500*

-47.000*

-13.000*

0.045*

-0.053*

8.000*

398.107

-57.000

0.158

-0.837

12/11/80

20 07.1 -46 53

C₂ -50.6±0.3(4)

29967

6.81 +1.16 181 ID

6.9:11.5 7"

+050 -072 Cape

+69 -39 -3' .007

+61 -22 +7 .010

~~-229655~~

+003447.3
+0044

-05575.1
~~-051~~

4740 1904.8

-46

5-2

5-8.66

1906.7

~~1371~~

4703

+2358

56.88

79.69

1929.65

+20.52

59.17

11.66

57.51

85.45

42.7

36.0

17.541
47.355
DB 4.929
1.07

16.98

8.49

+1.146

1955.80

4.896
-020
.876

5-8.61

58.66

14.17

5-8.03
-1.85

191190 Card II
H190

V
-166

-850 526 -729 685 +043 -051 -50.6 +037 +36.9

037 031 023 019 085 256 -183 29.5 018

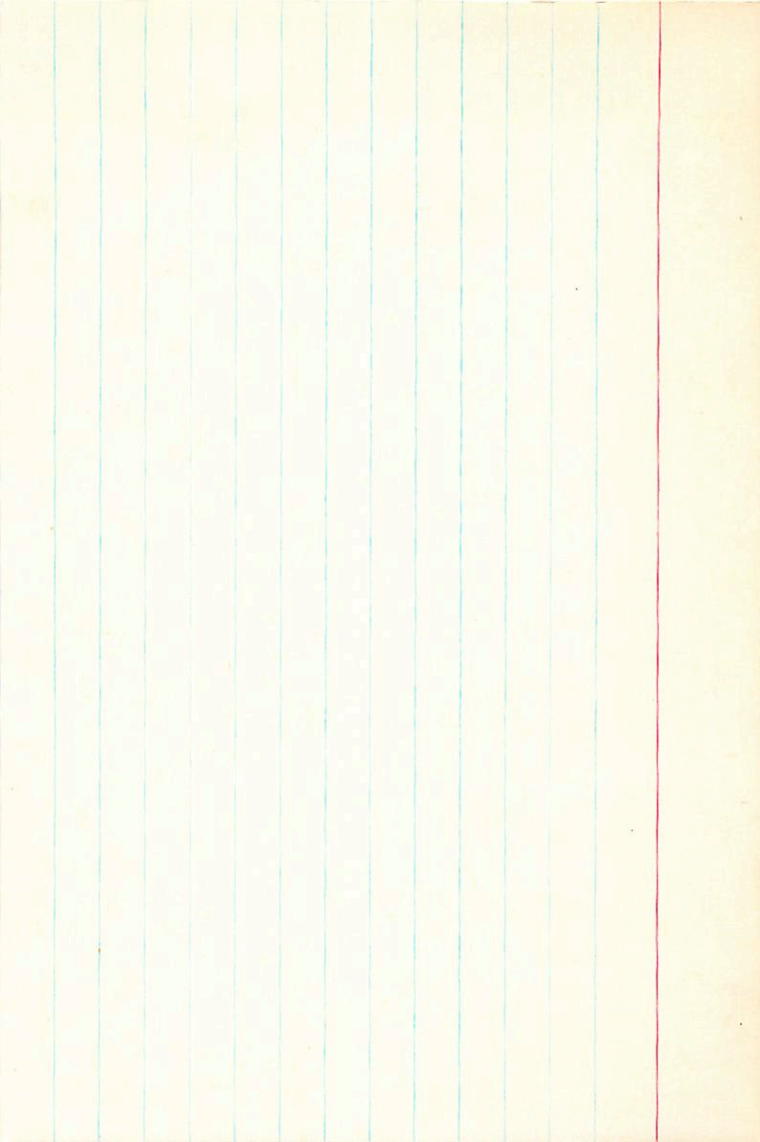
-13.6 43.7 +27.7
51.4 -5.4 +17.6

-1.2 38.5 12.9
-6.4 -19.6 20.8
11.8 -7.1 12.9

-141 +22.3 +28.6 02

1.3 33.4 14.7
-7.5 -17.0 23.6
13.5 -6.2 14.7

-15.5 39.0 31.4 03
46.8 -0.9 +227.0



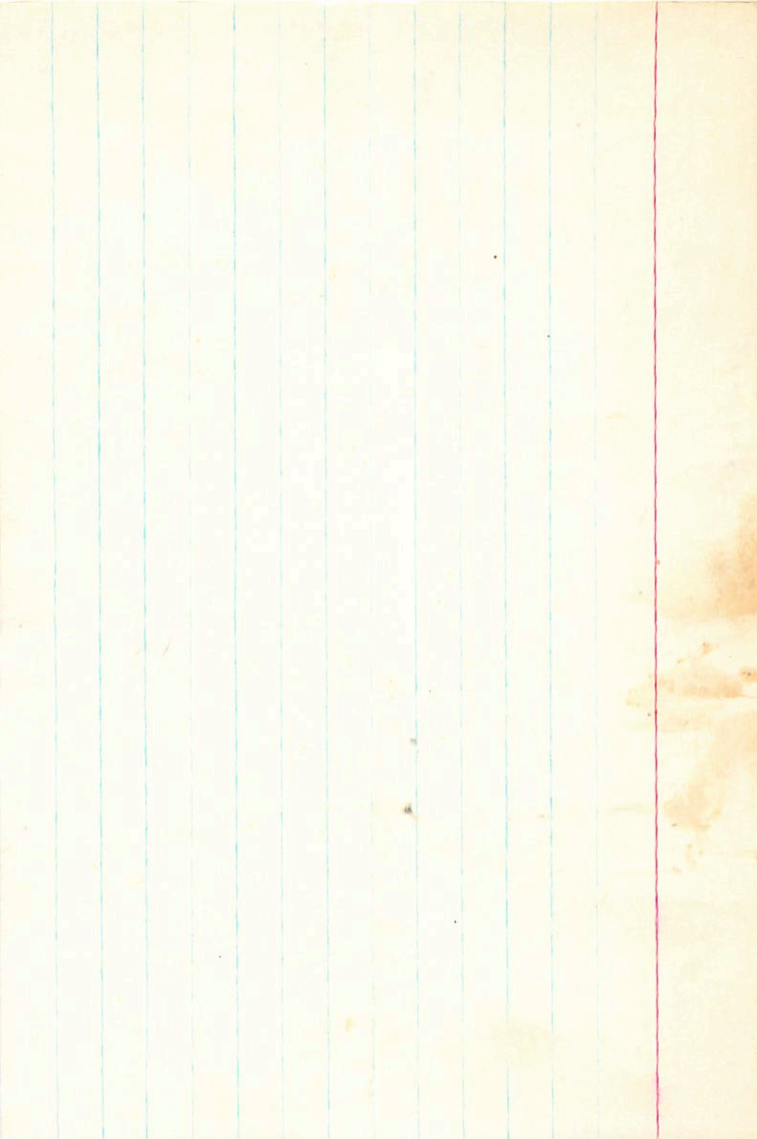
1752e $\Delta m = 2.36$ +0035 ± 2.0 +099 ± 1.8
 191570 20 07.7 +20 46 +092
 27987 12'' (8.4 dg-5 -43.0)

12520 44.147 1896.0 +20 45 55.05 1890.4
 43.958 $\frac{189}{189}$
 44.094 $\frac{49.115}{-5.90}$

53.98 1933.4
 53.18

44.155 236
 -13
 142
 118
 +160
 40.4

53.75 1939.46
 53.77 266
 53.47 36.4
 47.0
 +432



191615 20 07.8 +25 23 120π -54020.7014

+2504124 7.80 +0.94 +0.83 6.8π R

+54 -73 +17 .015
+59 -72 +22 .01

+002
-3

+034
-3

+005 = 9 +03764

$+0012 \pm 6.3$ -019 ± 5.4
 $+0010$ -014
 190306 20 02.3 -33 09 6.6 B8 -18.38

27851

12440

6.8-8.6
 0.6

20.940 ¹⁸⁹⁵⁶ -33 8 35.78 1893.4

-068
 \hline
 ,874

$+1.08$
 \hline
 34.70

45.239

35728

20.967

-60
 \hline
 .907

-17
 \hline
 .890

20.949 $+046$
 \hline
 950

46.0

48.98 1928.45

11.98

\hline
 37.00
 \hline
 1.50

35.50

+25

\hline
 35.25

35.45

-8

\hline
 25.53

8330

41.6

48.2

35.34

\hline
 .69

1954.85

