

M : -103.686
 MP : % -1501.425
 (M) : -0.570
 (M) : 0.564
 (M) : -0.597

W

U : -88.139
 (U) : % -1588.020
 () : 0.768
 () : 0.624
 () : -0.144

U : -83.250
 (U) : % -1246.899
 () : -0.291
 () : 0.540
 () : 0.789

W

15.700
 63
 4.000
 -530.000
 30.000
 9.700
 22.000

M : -103.989 2/2
PM : X-1201.432
(M) : -0.258
(M) : 0.258
(M) : -0.258

U : -88.130 2/10
UP : X-1288.038
(U) : 0.598
(U) : 0.598
(U) : -0.598

U : -88.328
UP : X-1349.060
(U) : -0.361
(U) : 0.240
(U) : 0.285

REG : 12.500
FNS : 23
MCE : 4.000
EC : -230.000
D : 30.000
EC : 0.500
D : 30.000

17
55
ACH
473

535

1761
3858
9227
8564

11-12
384-26

158 m. + 529 + 29
work
14 m.

479 + 555 12
5.56 + 1.45 + 1815

5.073

340-5300+

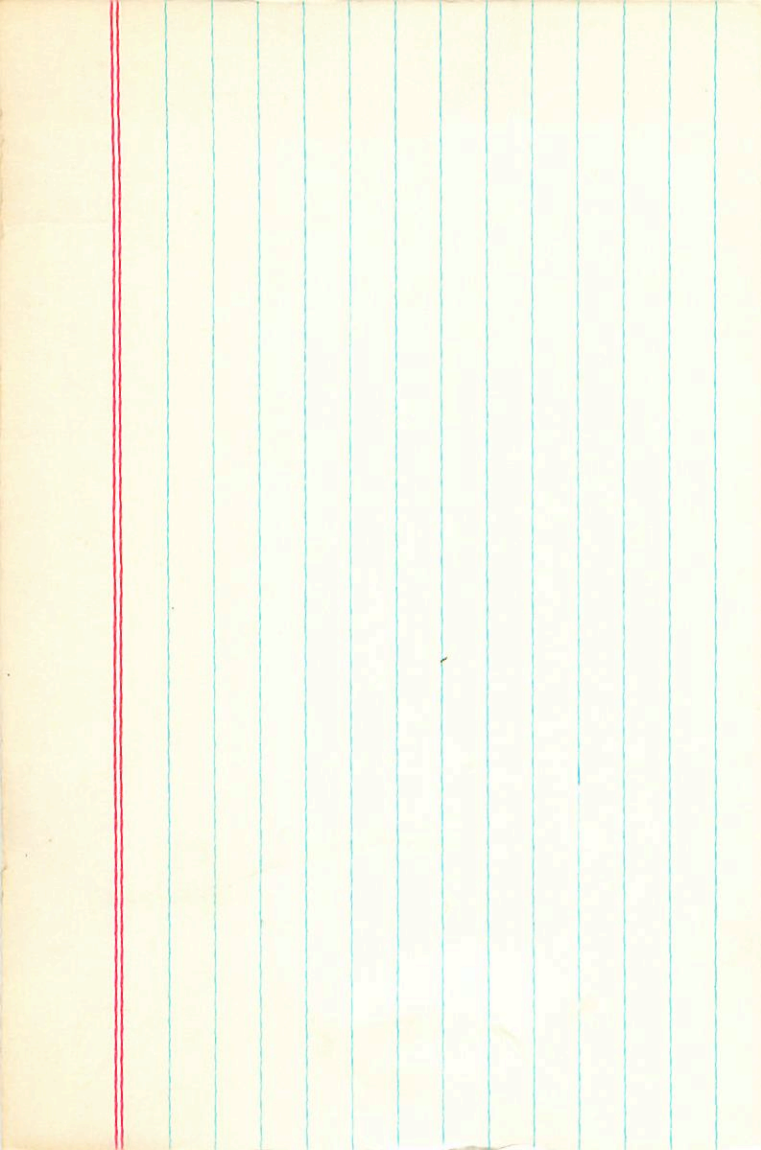
70 270-1801
AD 310-6807

turn out

from 2-265
pm

209529 22 02.4 22 53 53 11-434

5.5



-0002583 -01857.5

209709 27 02.6 +14 34 6.7 gm2 -3.76

30883

13572

38.250 1910.0 +14 34 21.63 1507.7

M(B)

$$\begin{array}{r} 008 \\ \underline{258} \end{array}$$

$$\begin{array}{r} 82 \\ \underline{22.45} \end{array}$$

$$\begin{array}{r} 14 \\ \underline{38.262} \end{array}$$

$$\begin{array}{r} 15 \\ \underline{22.09} \end{array}$$

$$\underline{276}$$

$$\underline{22.24}$$

$$\begin{array}{r} 20 \\ \underline{38.237} \end{array}$$

$$\begin{array}{r} 5 \\ \underline{21.95} \end{array}$$

(27.3)

$$\underline{22.07}$$

$$\underline{14.62}$$

$$\underline{266}$$

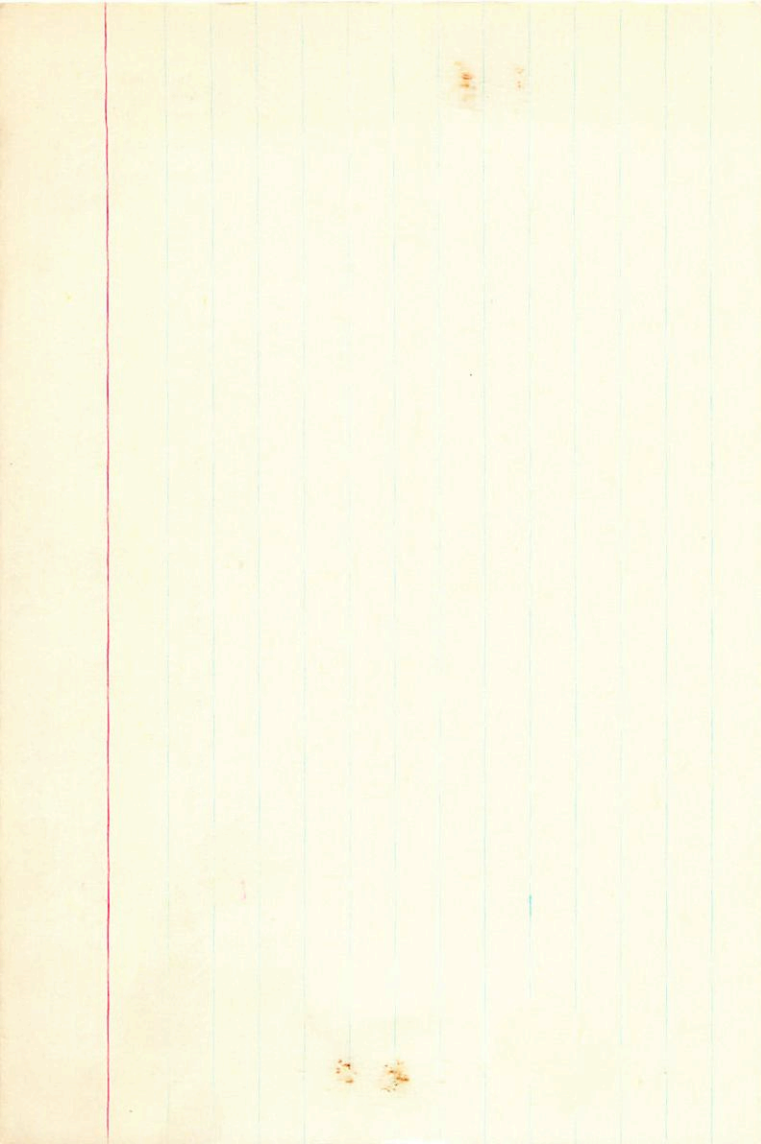
$$\underline{22.12}$$

$$\underline{37.3}$$

$$\underline{-032}$$

$$\underline{-33}$$

(32.6)



205745

22 079 1489 39

$$\begin{array}{r}
 = 24.7 \\
 - 218 \\
 \hline
 - 234
 \end{array}$$

7021014

$$\boxed{7031 - 014}$$

34

14

4011

- 234

117

$\left. \begin{array}{l} 2799 \ 9199 \\ 1188 \ 522 \end{array} \right\} \begin{array}{l} 0340 \\ 1607 \end{array}$

11

52

~~1888~~

Subsidiary

Wm. Pitt

~~1888~~

1888

1888

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q1	(V)	:	-0.102		
q2	(V)	:	0.326		
q3	(V)	:	0.933		
		}	-44.235		
	dV	:	-29.333		
	y	:			
q1	(W)	:	-0.588		
q2	(W)	:	0.729		
q3	(W)	:	-0.351		
	dW	:	-135.633		
	W	:	-14.473		

NS

-252

8415 ✓ 22 0.29 126 25 5.78 9123

+2504671

209961

30887

2772 ①

53641 1507.2 +0018 +0023547 +034534
-058 47.18 19047

543

45181

~~1081 +02460
-1 +3
1080 +037~~

53613
-9

+0020 +637 47.09

1540.25

53604

+0019 +040 47.07

+061

+1.26

!

!

39



15,931

-0,391

0,062

-17,547

0,913

0,053

23,973

-0,115

0,211

-25,000

100,000

5,000*

0,040*

0,026*

25,000*

26,000*

2,900*

22,000*

8413,000*



6.91 + 1.075 + 7.15 + 0.060 + 5.44 + 10.173.5 = 58 P = 244284
 + 6056
 + 633
 100 II - 0.5
 6.5 100 - 23.2a

30890

236 Oct 1st

13876 57444 18973 + 46 59 27.02 15919

100 III - 15 P

- 316

- 2.38

6.75 + 10.2 + 10.2

1.258

10054 + 1010

24.69

58.01

9.2 19264

30.6

16.12

27.9

Hydrolysis ~ 0.1

54.255
57.234

25.31

25.83 36.0

100

30.1
1.249

2.98
11.90

25.816

11.19

100

57.304

25.9

1929.7

Spa 244284

296

light 24.79 (wax)

25.9
25.6

hS

2

Handwritten text in a non-Latin script, possibly Indic, consisting of several lines of characters.

Handwritten signature or initials in blue ink, appearing to be 'S' followed by a stylized flourish.

Additional handwritten text in a non-Latin script, partially visible at the bottom of the page.

209661

22 03.0

-44 13

No III -36.3 4C

FD781

(6.43 + 1.04 (2.08))

GL30891

+0075 ± 6.5 -027 ± 5.5

58.970 1907.1

34.56 1904.4

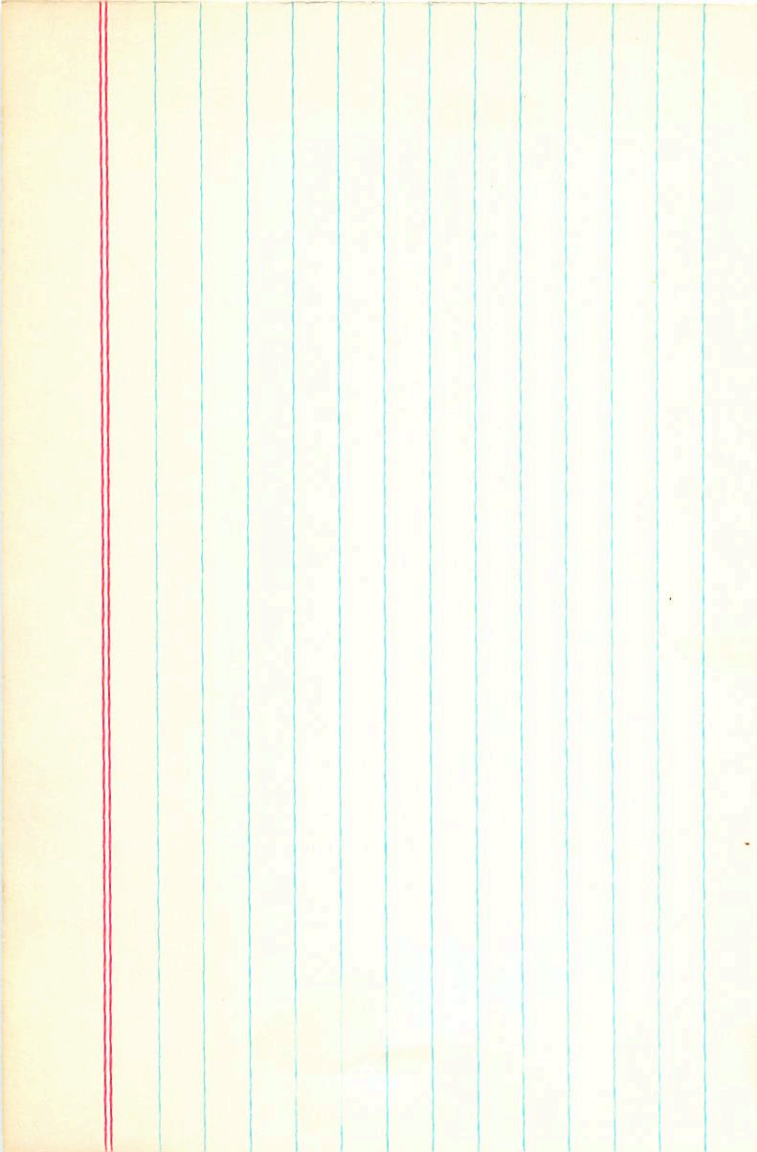
322
58.970
58.548

1.22
33
34

25876
32.962
58.835
433

50.83
8555
388
35.24
35.24

1927.27



209661 22 03.0 ⁺⁶⁰⁵⁸ -44 13 6.93 +1.04 (2.08)
 30841 -0274.55
 -042
 110 III -36.3 to 75 (14)

5-8.570 1907.1 -44 12 34.56 19049

$$\begin{array}{r}
 -322 \\
 \underline{.548}
 \end{array}$$

$$\begin{array}{r}
 25.874 \\
 32.462
 \end{array}$$

$$\begin{array}{r}
 58.825 \\
 \underline{-17.13} \\
 41.695
 \end{array}$$

$$\begin{array}{r}
 58.841 \\
 \underline{-26.10}
 \end{array}$$

(34.1)

$$\begin{array}{r}
 1493 \\
 \underline{+196}
 \end{array}$$

$$\begin{array}{r}
 1.22
 \end{array}$$

$$\begin{array}{r}
 33.34
 \end{array}$$

$$\begin{array}{r}
 50.83 \\
 15.53 \\
 \hline
 66.36
 \end{array}$$

$$\begin{array}{r}
 35.21 \\
 \underline{34.57} \\
 0.64
 \end{array}$$

$$\begin{array}{r}
 34.44 \\
 \underline{34.44} \\
 0
 \end{array}$$

$$\begin{array}{r}
 97r \\
 \underline{34.82} \\
 62.18
 \end{array}$$

$$\begin{array}{r}
 35.14 \\
 \underline{-19.526} \\
 15.614
 \end{array}$$

~~844~~
~~41.2~~
 (26.3)

8414

342 Aspen

30896

13879

22

3.214

- 0°

34'

3.1960

pink

FD0111 -0044

plus 0.6
FD0111 ①

4.7 ①
7.5 ②
7.5 ③ + 7.5 a

70196
70196

0.794	0.480	-0.373
-0.152	0.752	0.642
-0.588	0.452	-0.670

2 Blue

209688

22

03-1

-0022
-39

47

4.6

MO

+3882

-002429

+04772.6
+042

20892

6.472

1906.5

-39

47

D.71

15040

445 + 139 + 2455

13877

104

1576

-2.16

9.87

6.44 1940.41

6.529

-32

497

413

6.90

16.86

803

+1.84

95.68

47.8

43.5

6.489 - 091

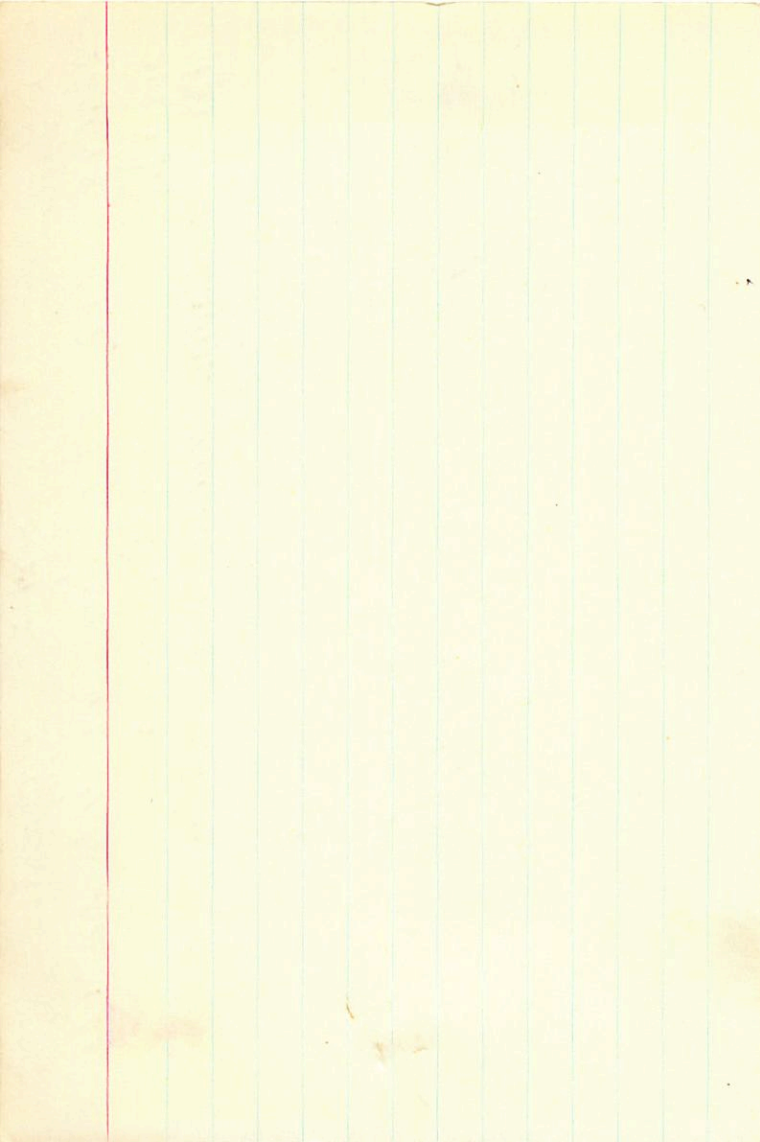
485

9.04

1555.27

-16
473

-12
9.16



8411

217
12085
624
78
624
624

22 03.1 -09 48 102 177

209688

38892

4.46 + 137 + 1.66
4.46 + 136 + 1.65 C
4.44 + 137 + 1.6449

252 1204
84 235

384 + 565 5(11)
3.81 + 51.5(12)
3.82 + 54 ;

Keep
long

-60169 -1166 1-114 138.800

L 16 + 18

2.70
2.25
505

~~50152 1149~~
~~74 39~~

0022-120

-0153 -00197 -1224

-623-126

-0105

-1222

230
126

-017 246

-019-190

114
13

-0024± 2g - 720±2.0

6.472 6.5

$\frac{104}{576}$

-0023

771 40

-0019

$\frac{515}{2.15}$

729

-0023

716
715

6.484 70.32
-12
732

10.61
 $\frac{10}{1.74}$

6.489 55.55

9.3
 $\frac{11}{9.22}$

6.529
 $\frac{132}{29}$

90.11

6.64
 $\frac{24}{3}$
6"

55



55

-22,446
-0,888
-53,624
-0,023
-0,545
-37,950
-0,592
-0,141
35,800
100,000
3,000*
-0,119*
-0,017*
-40,000*
-35,000*
3,100*
22,000*-21,0

55

11,000*
-0,800
-53,225
-0,023
-0,545
-33,215
-0,592
-0,149
35,800
102,329
5,000*
-0,120*
-43,019*
-33,000*
3,100*
22,000*
841

W.P. ^{mm}

22 03.2 704 49 GRS -14.47 SB

209727

4.85 +1.42 +1.81 K4(1)

-17.2 L(5)

G-C 30544

-19.5 W(4)

W 13878

+6064 32 +107 35 N30

W(HOLD)

-7.9 V(3)

W 5331

+0070 522 +105 51.9

1400 (27)

+404500

-191 (1)

-191 (2)

+65 +16 +11 .010

+103 GC

+48 +6 +10 .015

+086

+107

N30

13A(12)

13M(7)

1Y(12)

954



20 Sep

20960

22

03.5

462

32

5.4

GRS-2092

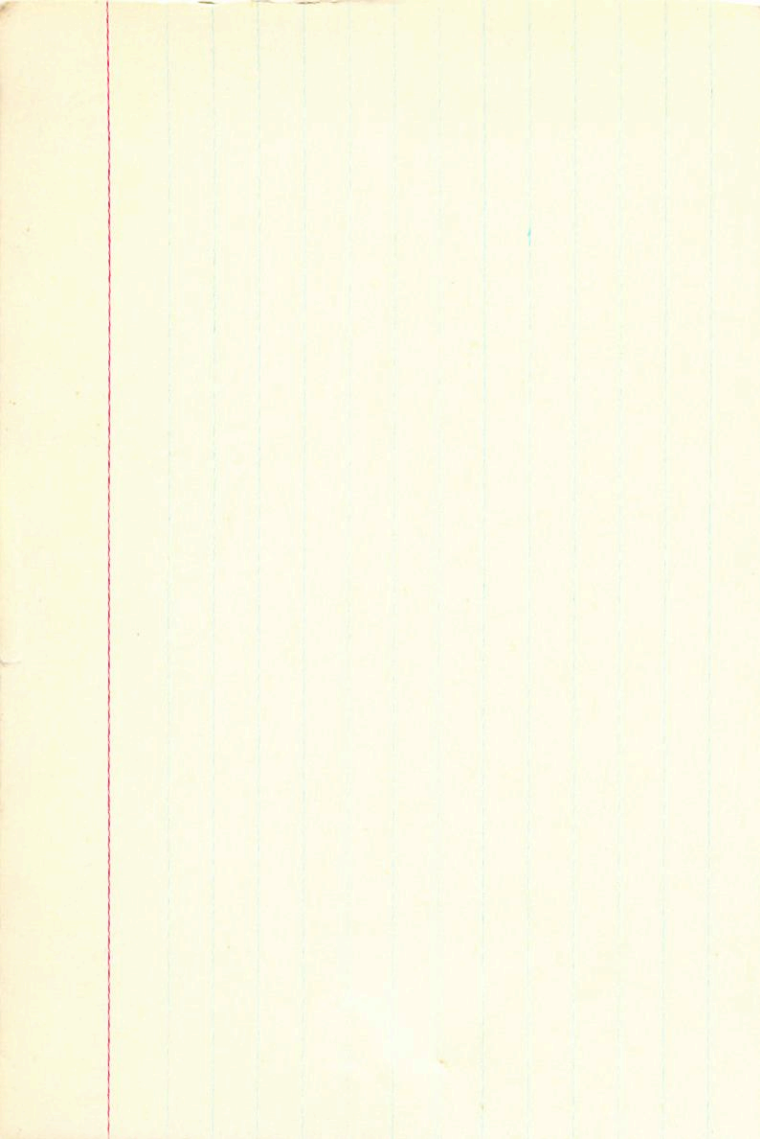
30504

+0015'41 +062⁵⁵N30

-2227 (3)

13552

+0016'51.5 +061'51.5 GCR 2130



7384

8424

22 04.0

+44 46

185 11

20945

20945

5.10 4 +1.57+1.47 4.23 +0.69

~~2.5 703 503 462~~

4.10 104
2.70 066
2.47 12

-0205 -0108 ±2.5

-356 964 -302 071

-146 -22.8 0814 -4533 -0717

2.9
3.0
5.9

+47
-0053

-001 -015

~~996 276 071
894 250 2 -0015~~

+13
+34

W. C. C. C.
P. C. C. C.
205780

21 341

28

Leaving allowance HKSP 24 79

W 13843 22 04.1 45-3 23 2165

40209992

Gc30923

+520310Y

8086 1501.1

~~024~~

~~8.059~~

8.024

8.08

-11C012)

500

4022 -0068

+0015 -0034

70006 -013

45.57 15005

~~42.1~~

46.41 1546.48

~~-32~~
~~46.15~~

-0004

45.9

~~17~~

~~73~~

45.73

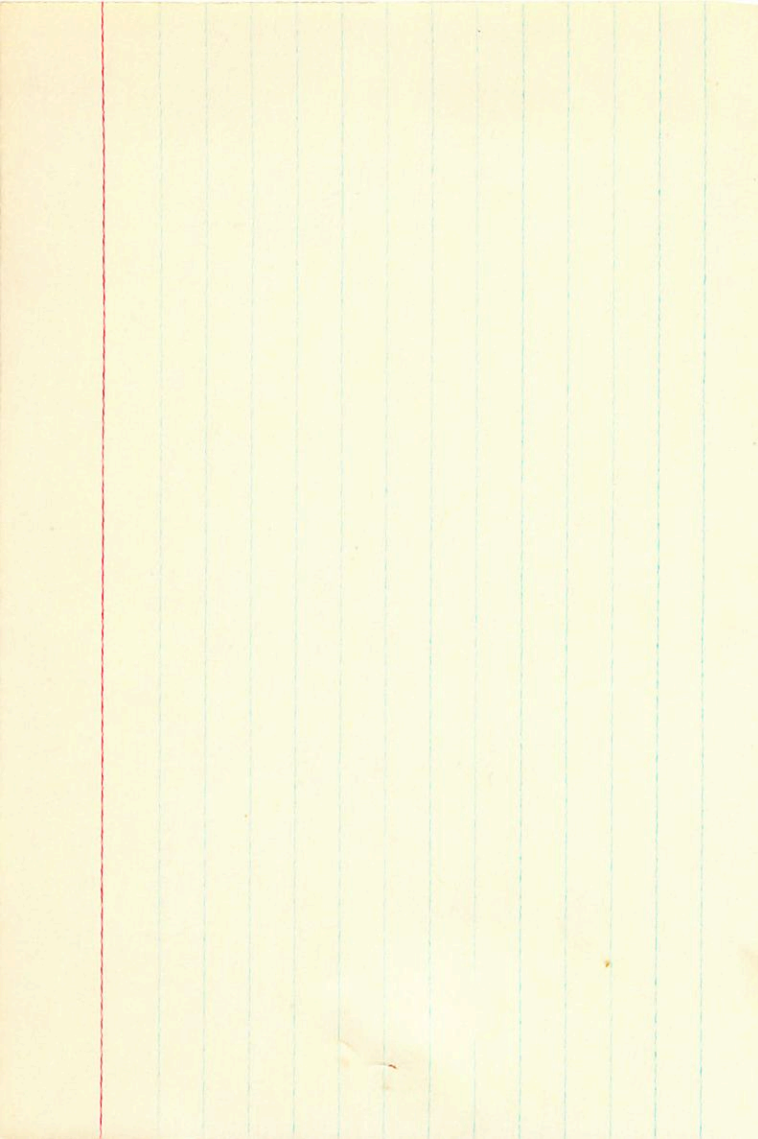
+794 +578 +174

-158 -024 +84

-582 +912 -025

-

-11



LDS 772

22

04.85.

-51

21

325-125

10.54 + 1.15 + 1.15

9.85 + 0.92

(2) (2)

304

CR

12.60 + 0.95 + 1.15

11.50 + 1.09

(2) (2)

13.50 + 1.50 -

12.85 + 1.25

(2) (2)

25

22.100
-51.350
520.000
-125.000
24 3.600
30. 52
0.000

0.799
0.023
-0.601
1216.460
37 53.841

-0.161
0.971
-0.177
-822.657
-25 -43.174

-0.580
-0.238
-0.779
-751.225
-23 -39.425

57

Sy. N. P. - 109

L Page
210027

22 047 +25 06 40 dks 4.02

30932

13895

+0216 83 +029 77 M30

+021650.9 +02751.0 Gc 9M20

7455

+02199 +0216

+02201 +0223

2950

332

301 P20

20
0.35

-43



210007 22 4.7 +25 6 FS II

HR8430 3.76 +44 -3 J

GC30932 SB 10 888

24 Aug 1296 .159 .446 (S) SDC

(ii) J 34 136 28 3.670

[m] 212 +13 28 469 (10) G4

[L] 387 +17

0.60 fl.2 L.2 -7.9

+1192 -173 736

89

Handwritten scribbles or symbols.

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210144

22 84.5 +52 53 4100-36.18

(13)

GC30839

R 12.51

7.78 +0.80 +0.41 GPEP

Y5349

S=02

R5203112

-540 -334 CC

-81 -24 +4 .040

414(28)

1M(17)

414(10)

3345

100
820.55
55.020

-0597±4.6
-0589
-334±4.0
-337

53323 1895.2 +52 53 27.07 1892.0

3272
56.996

19.37
46.44

1946.08

53.601

28.82
-37
28.45

607

51.3

1144

53.536

28.77 1946.84

537

-34
28.39 .92
46.5

572

53.5

+3.023

28.42
-18.02

8431

114
-12
22 65.4 -33 15 A24

1.00

210049

30554

+00 024

-0308 (F) 4.50 105 105 C

448
10044

+0200
~~4080-031~~

→ 024 172 1.8848 2.970 11 62.5

43

+081 -026
+11.6

11.1V
37

176
252
1079

2790
045=2
070=2

+024

Bank 51

96
21

1431
1475

10.4
3.9

448

+116

448

59

q1 (M) : -0.580
 q2 (M) : 0.016
 q3 (M) : -0.815
 MP : -220.606
 M : -24.574



q1 (V) : -0.161
 q2 (V) : 0.978
 q3 (V) : 0.134
 DV : -204.197
 V : -12.448

q1 (U) : 0.799
 q2 (U) : 0.208
 q3 (U) : -0.564
 DU : 270.262
 U : 11.982

R.A. : 22.100
 DEC. : -33.250
 R.A. : 95.000
 DEC. : -31.000
 STANCE : 4.180
 MODULUS : 69
 VEL. : 11.600

8435

22

051

118 14

210874

582

109109

521.91 8698

16.39 ± 0.02

8698

9416

1272

7940

3363

10064

M

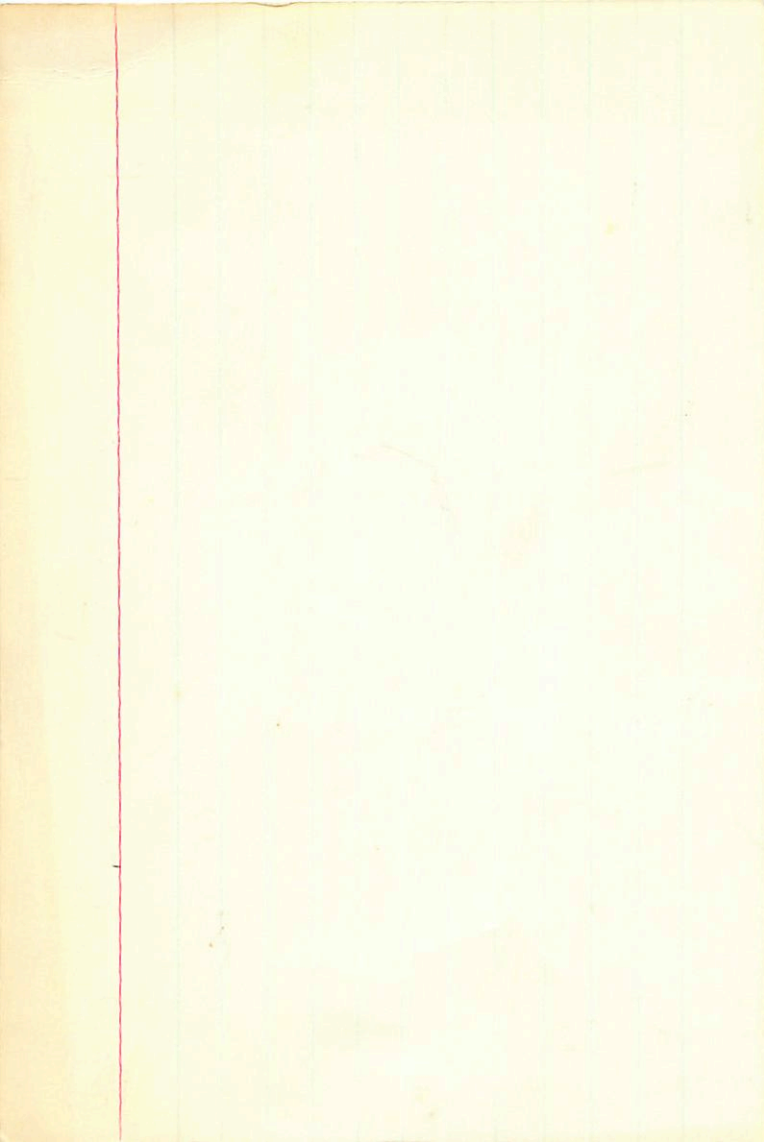
22 05.5 f21 27 B7b

25 Aug

GC30956

S. 28 - 0.10 - 0.41 Roman

E 24b.05



NRDA

210049 22 05.5' -33 14 4.6 Azm 116.8

30954 4.51 +0.07 +1.53 5

13904 28.275 - 1905.5 -33 14 0.61 19047

-267
1008
1.68

28.244
-2.1
223
59.59 1940.43

42.4

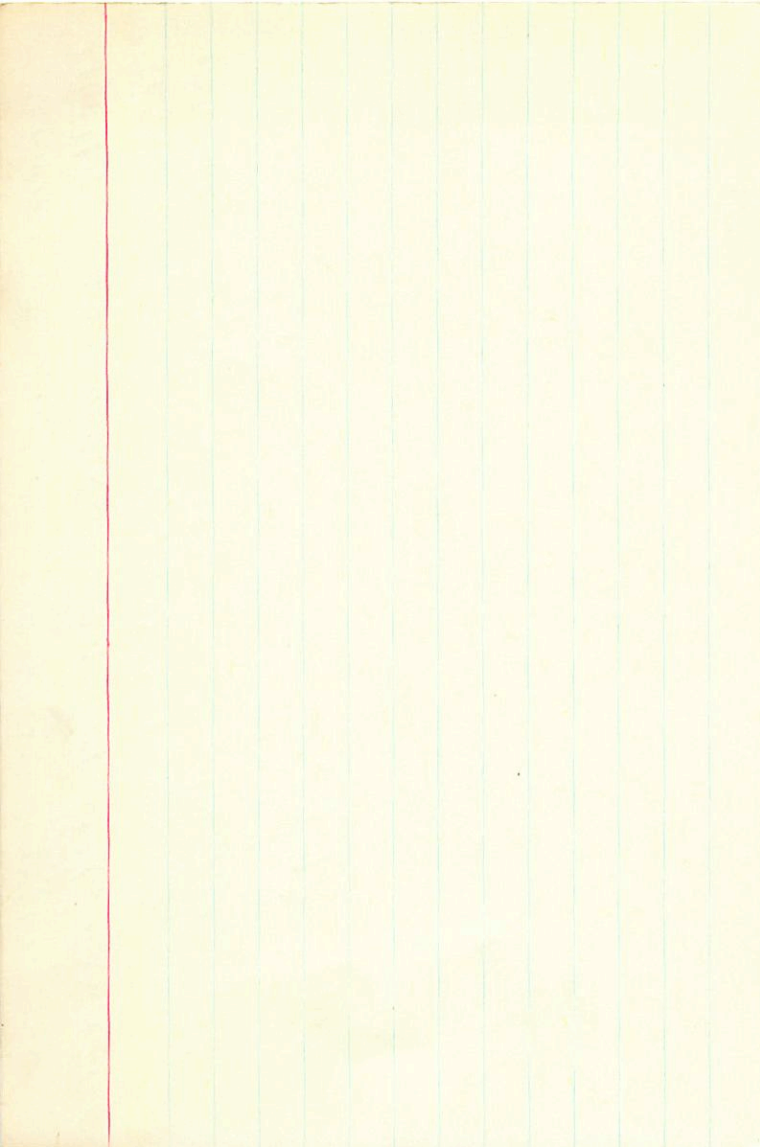
528
264

59.92 95.88
59.96 47.9
1.03 43.2

28.319 +256
59.58 1955.45

-14
305
59.59

+0060±3.2
+060 -037±3.2
-33 14 4.6
-024



210221
30958

22

05.6

+53

04

6.5

A3p -25.56

13909

34.244

1897.5

+53

3

94.96

1845.4

052

1,296

38.75

55.452

34.2340

272

274

260

34.239

-036

245

-0010 ± 4.4
-0010

-008 ± 3.7
-006

37.9

44
45.30

25.8

1925.6

18.922

44.746

7134

35.7

45.18
45.19

45.05
-0.25

40.3

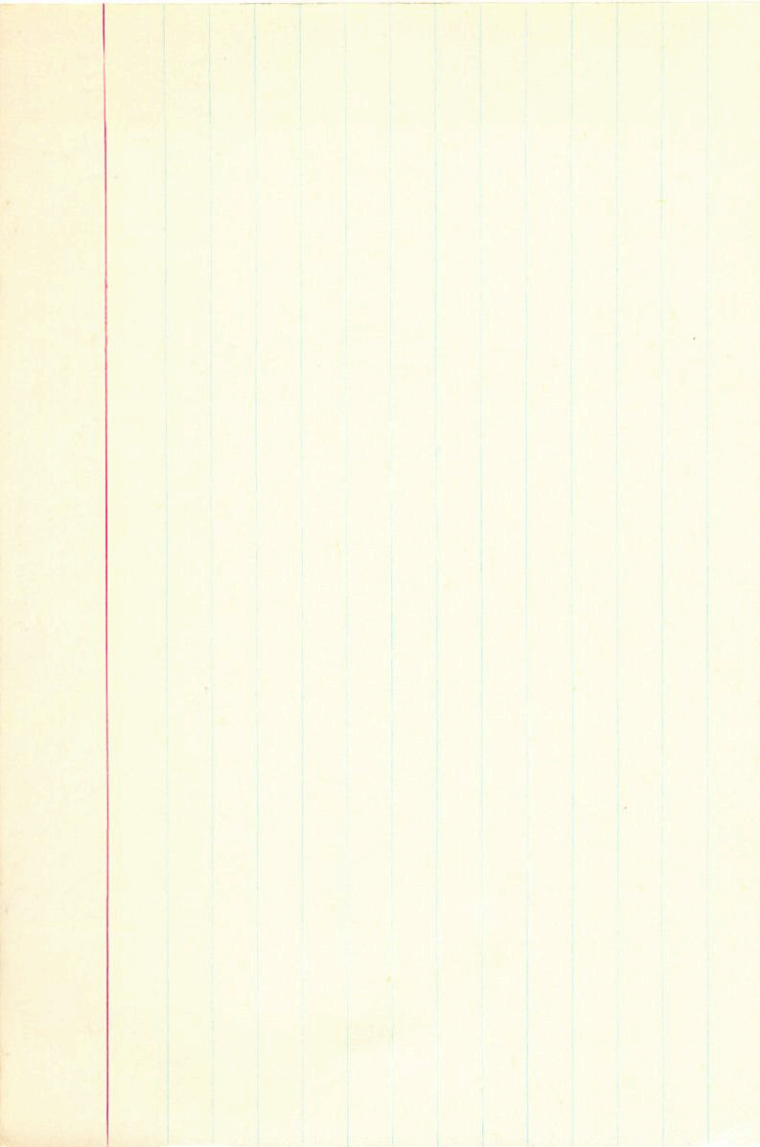
45.37

45.10

1945.74

-37

44.73



~~0030±4.8~~ -036±46

210210

22 06.0 +25 18 6.0 A9 +2.0 B

~~30968~~

~~13912~~

58.548 1915.5 +25 19 55.15 1910.5

$$\begin{array}{r} 104 \\ \hline 1652 \end{array}$$

$$\begin{array}{r} 1.42 \\ \hline 56.57 \end{array}$$

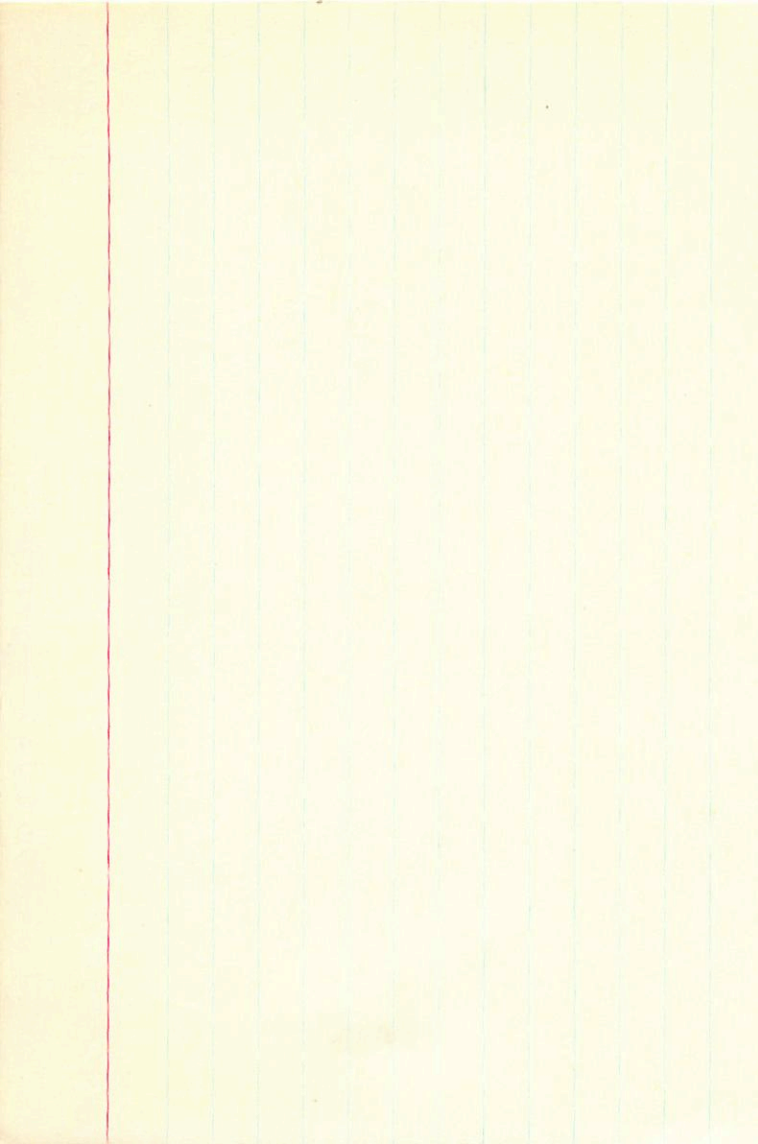
~~58.628~~

$$\begin{array}{r} -1 \\ \hline 627 \end{array}$$

~~-025~~

56.02 1927.86

$$\begin{array}{r} -10 \\ \hline 55.92 \end{array}$$



210693 22 06.6 -41 28 787 +65 916

30983

+0170+15.0 -055+13.0
+0132
GSE +80±0.8

32.662 1503.1 -41 48 10.39 1902.2

-797

263

31, 865

7.76

29.1

1.284
31.080

19.28

1929.53

8+3.1

31.12
32.114
2.530

10.78

24.2

42.2

-224

766
383
+518

10.75

-3.44

40.0

32.559

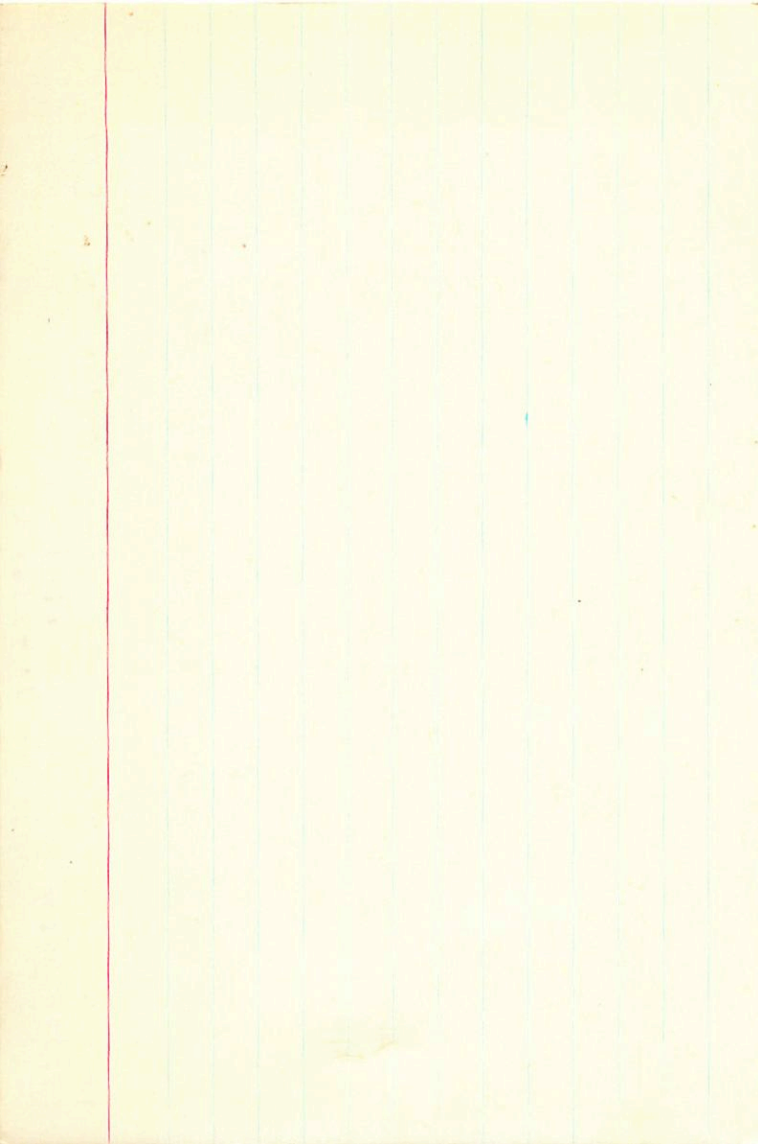
11.55

1554.78

-17

11.09

5.42



AR fac

EB $P=1.95$

210334

22 06.7

+45 30 7.3

$P_0 + 65 - 346a$

~~30988~~

$4.10 + 50 + 30 - 33$ ~~24.8~~

13917

-0056 +044¹⁹ W30

$(P-I) = +0.33$

-0032 ± 6 / +033 ± 5.16c 7 W30

Charluis CR

Percentage 6.75 + 0.92 + 0.55

^{149c} PASP 89762 a m H.25 -

-046 + 065 10000

15275

34430

-0053

+044

45.41

1927.2

W350

$\frac{12c}{58c}$

-0054

+046

-111 / 4450

-00587 + 0587

~~-087 + 046~~

46.17 1551.76

-051

34.923

-18

~~-045 + 055~~

$\frac{4405}{39428}$

48.555

$\frac{128}{128}$

+1.89

-057 +096

-346

860 552-056
-163 060 985
-578 604-144

-2161 +1291 -0870
+0440 +0131 +0571
+1562 +1753 +3315

-33
-34.1
+5.0

19

P

133

134

22.100

45.500

-68.000

55.000

3.750

56

-36

-34.600

0.799

0.594

0.094

-25.654

-4.704

-0.161

0.060

0.985

51.078

-33

-31.171

-0.580

0.802

-0.143

340.079

24.078



36 Apr

210269 22 06.5 +0039±20 +051±2.0
-08 36 +051 2.0 944 -45.78

30989

13919 48.292 18933 -8 25 56.37 18902

$$\frac{-221}{1071}$$

$$\frac{-3.05}{59.42}$$

29.073

19.228

48.301

17.74 1933.79

1485

57.67

309

36.5

43.2

46.3

$$\frac{296}{221} \frac{420}{210} + 189$$

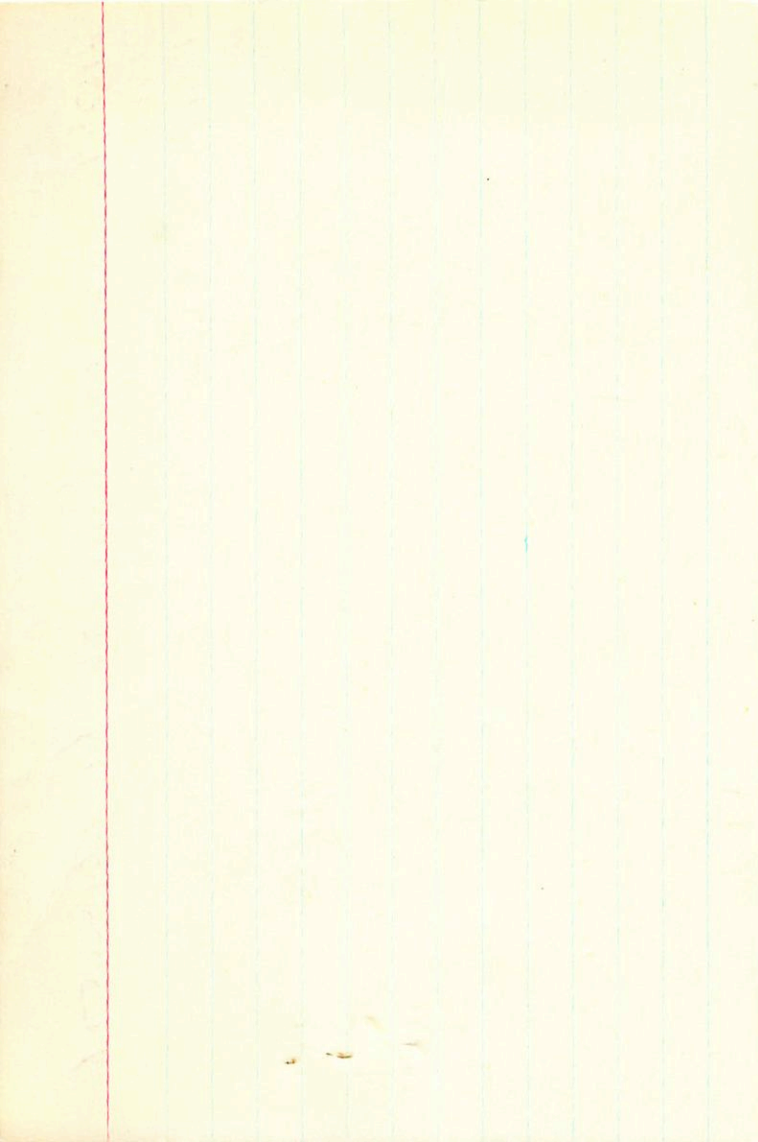
$$\frac{57.23}{23} \frac{57.065}{49}$$

$$\frac{57.065}{23} + 2.36$$

$$\frac{48.270}{245}$$

$$\frac{57.39}{27} + 2.12$$

1939.30



Autonulli d'ad K K 1525

8450 22 076 45 57 425

210418 ²⁷ 871111 ¹³ 836 9799

310131 ¹³ 3.53 408 409 C-5190 2293

2763 4024 051 153 1.053 @ SPV 215

7568 9959 3043 142 430 2836 5615

40311 1124 324 430 076=a 146

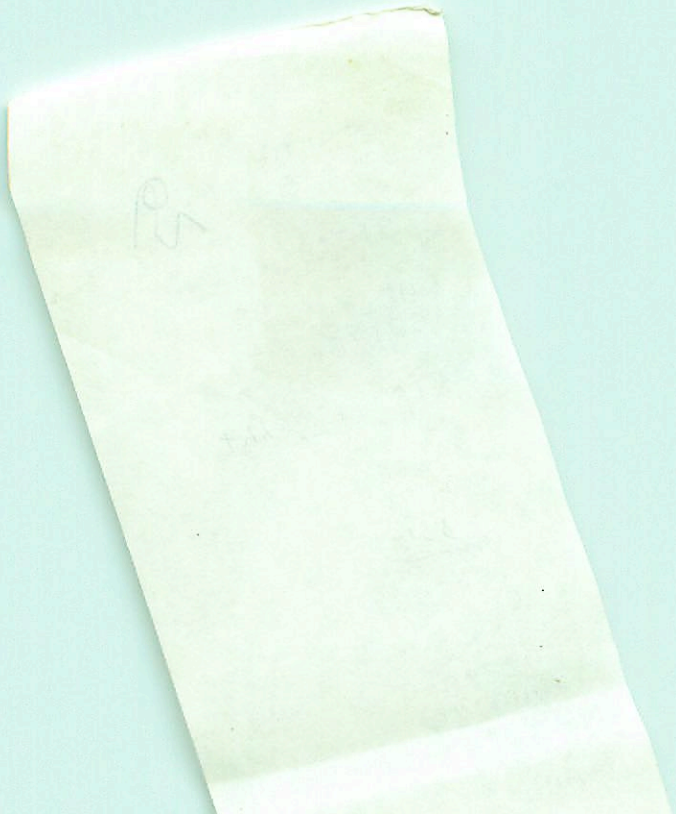
401834 40322 1407 068=2

1032 1032 1.561 40.8

4976 4025 2790 20510 2790 1341 1.30

277X

29



-17-736

-0.656
-0.628

29

-10.216

-0.109
0.720

41.817

744

-0.300
1.104

-158
-0.300

35.461
35.750*

0.032*
0.270*
0.000*

57.000*
5.000*
7.000*
22.000*

5

10

TO: 580

321

11

12

13

total

TO: 580

321

11

12

13

30

40



22.100

5.950

029

277.000

28.000

3.1

2.750

41.000

35.400

~~20.000~~

-16.2

236

6

1424

209

0.799

0.513

-0.306

1,112.118

52

+44

45.570

-0.161

0.673

0.722

-120.426

-18.705

-16

-15.3

-0.580

0.527

-0.621

-686.816

-19

-15

-11.944