

+0023±3.4 -075±3.4
+0022 -079

217303

22 57.4 -25 26 5.8 g 100 -34.98

32049

14430

23.520 1406.4 -25 25 53.96 1403.1

-100

23.420

2.307

21.222

23.529
53

1436

15

461

23.542

-229

519

970

485

+065

30.0

352

50.44

55.18

1933.79

172

53.46

+24

53.22

311

36.6

33.5

53.11

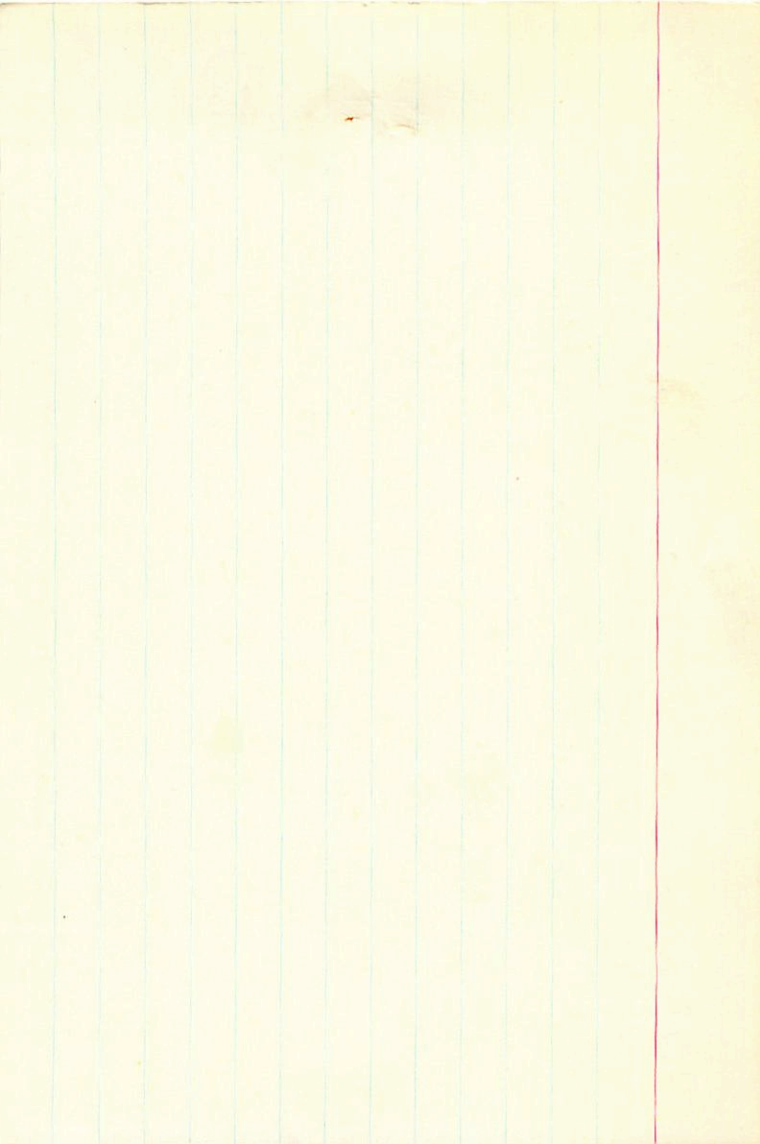
14

52.97

1934.32

53.10

-2.66



217357

22

57.6

-22

48

8.1 dmi +16.68

32054

14431

38.193 18975

-22

47

37.81

1895.9

125 ± 6

3465
41,658

-993
+64
+17.1

-3.41
41.22

18.602
20.648

39.200
47

153
20
133

457
228

39.337
13
324

2,430

36.6

41.56
1.90
41.54

193457

39.68
40

39.00
24

38.76

39.20
14
39.06

1782
38.91 +2.31

1933.64

821

34.1

38.2

1

49

22.950
-22.800
-993.000
65.000
-0.500
8
17.100

0.858
0.379
-0.346
-3606.913
-34.573

-0.300
0.918
0.261
1583.045
17.043

-0.417
0.120
-0.901
1845.670
-0.746

ya

3 yr
 217364 22 57.9 -53 01 4.2 568 -1.18
 32061

-0074 ± 2.8 -012 ± 2.5 $+1.1M$ $318?$
 -0083 -018

14432 56.296 1909.0 -53 1 22.00 1903.0

$\frac{303}{.599}$

$\frac{L56}{21.44}$

56.464

$\frac{-73}{391}$

$\frac{556}{278}$

$\frac{-321}{}$

38.7

22.01 1939.70

$\frac{-7}{21.94}$

$\frac{22.26}{-82}$

9541
 47.7
 44.7

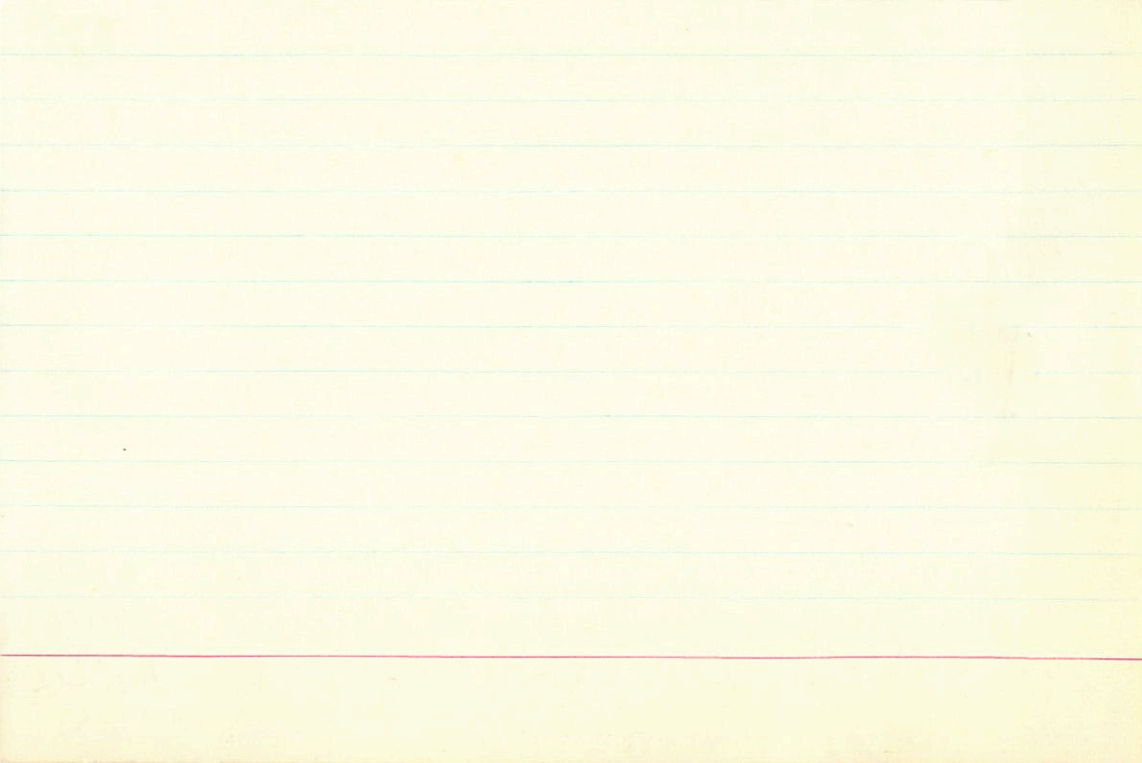
56.238

$\frac{-73}{.145}$

22.35

$\frac{-24}{22.59}$

1955.71



3Pac
47428
32065
14434

22 58-1 -00 05 6.4 g 64 -15.86

+0028³⁶ +019³⁴ N30
+0025^{31.8} +019^{31.6} GC → N30

217403 22 58.2 -51 13 8.30 1939.52 +7.81

32068

14436 11.729 1912.8 -51 13 8.30 1939.52

$\frac{-290}{439}$

5.67 + 1.42

$\frac{17}{13}$

8.13

11.714
 $\frac{-73}{643}$

34.7

8.00 1939.52

$\frac{-7}{8.07}$

9493

$\frac{8.22}{09}$

10810
1081-004

47.5
40.7

11.863
 $\frac{-61}{602}$

8.15 1955.41
 $\frac{-7.38}{8.15}$

+283

1445
 $\frac{722}{11}$

913
46

50

217403.000*

22.000*

58.200*

-51.000*

-13.000*

0.081*

-0.004*

5.000*

5.28
113.7

100.000

7.800

0.327

-0.482

433

28.896

-0.134

-0.208

-168

-15.010

-0.152

-0.851

-24

-21.869

81 Agv

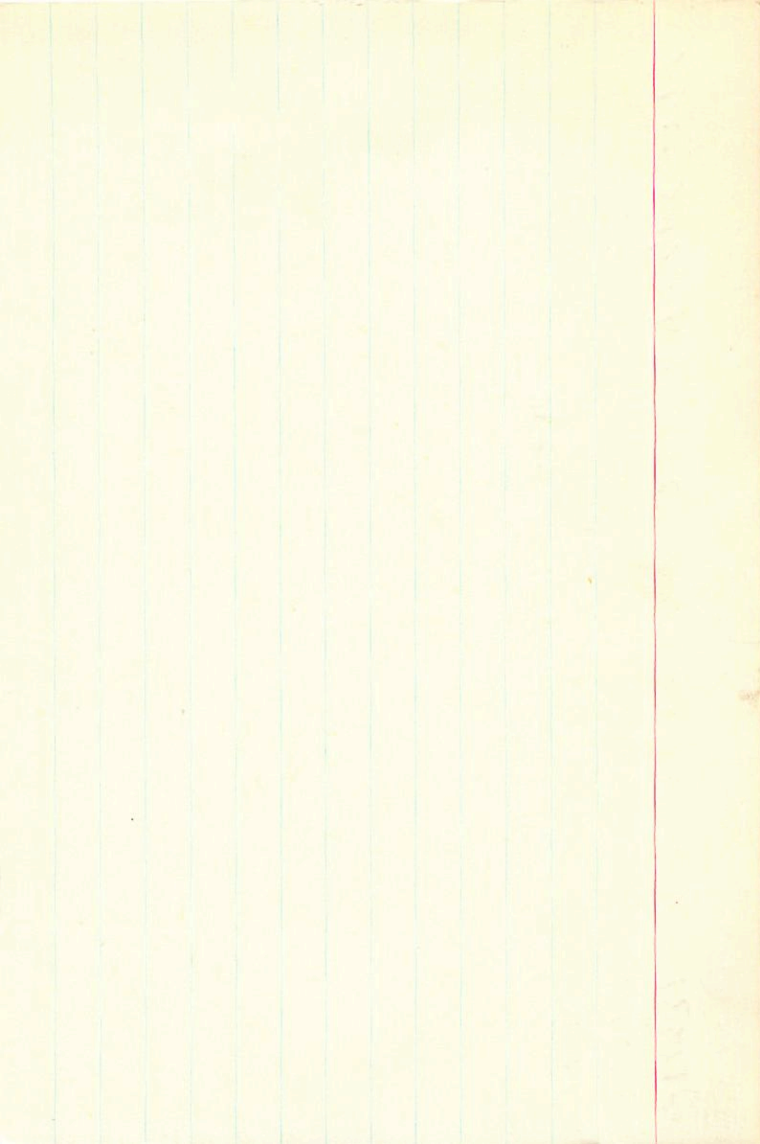
217531 22 58.8 -07 20 6.4 gms -2.16

32079

-0011 32 -007 32 N30

14440

-0012 ± 1.9 -007 ± 1.8 0.0 → N30



-6006 ± 3.4 -005 ± 3.1 6.5 -0.16 0.0
-0011 -002

217673 22 59.4 +56 50 19172 -5.58

32091

14444 23.400 1892.4 +56 50 11.37 1890.2

$$\frac{035}{433}$$

$$\frac{30}{11.67}$$

$$\begin{array}{r} 20.01 \\ 3300 \\ 23.315 \\ \frac{391}{396} \end{array}$$

44.1

8.1 1928.2

$$\begin{array}{r} 810 \\ 11.20 \\ \frac{1148}{22} \\ 11.71 \end{array}$$

$$\frac{7293}{36.5}$$

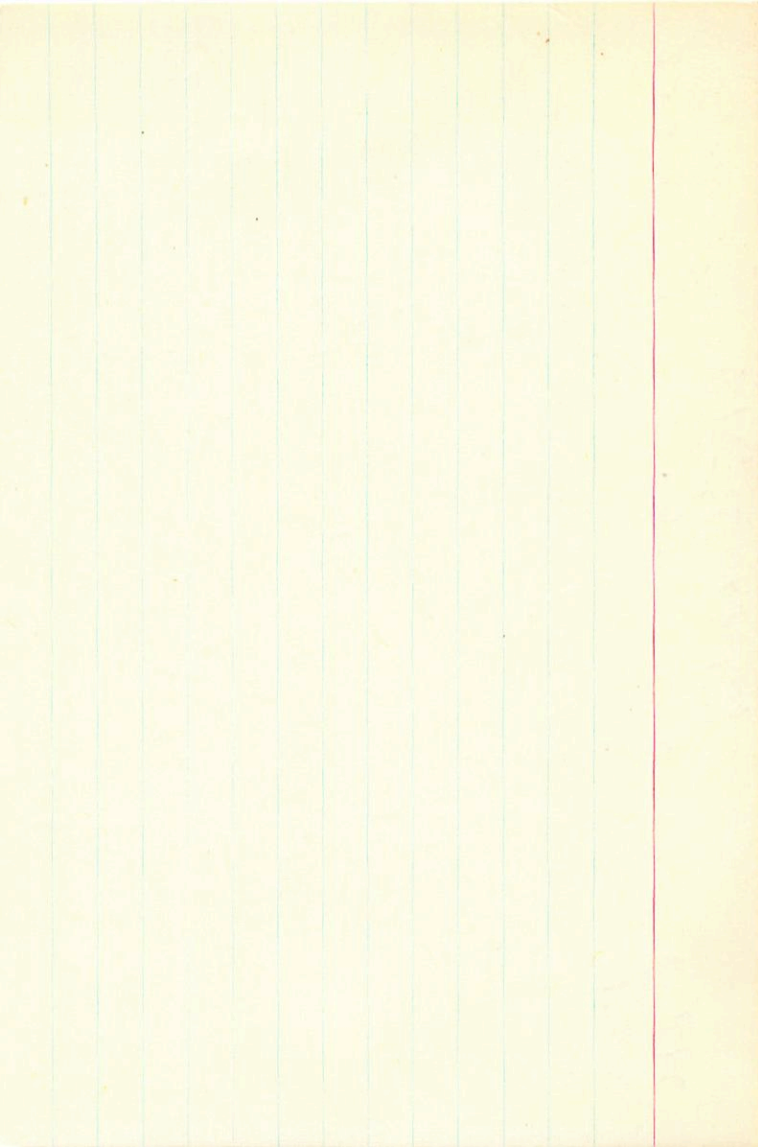
46.3

$$\begin{array}{r} 23.368 \\ \frac{10}{376} \end{array}$$

11.69 1144.73

$$\begin{array}{r} 11.69 \\ -28 \\ \hline 11.41 \end{array}$$

$$\frac{11.56}{-11}$$



-0015 ± 6.7 -006 ± 4.9
-0025 -075

H0217595

22

59.6 -45

34

+20.5 ± 0.3 C, (1)

32093

7.22 + 0.43 F5

-0.018 -0.008 1+

36.439 1909.1 -45 34 22.80 1904.4

061
1500

340

27
22.53

10.674

26.58 1930.56

25.945

300
23.58
23.40
23.18

28
43.1

36.619
114

415
-085

38.7

1500
-355
445

22 91 1955.72

36.40
-38
304

14
23.07
23.12
-49

-259 566 -707 707 -015 -008 +20.5 006 -14.5 -025

-005 002 -017 006 -052 -071 +14.5 +14.0 -3.5 025

+10.9 -6.6 -15.6

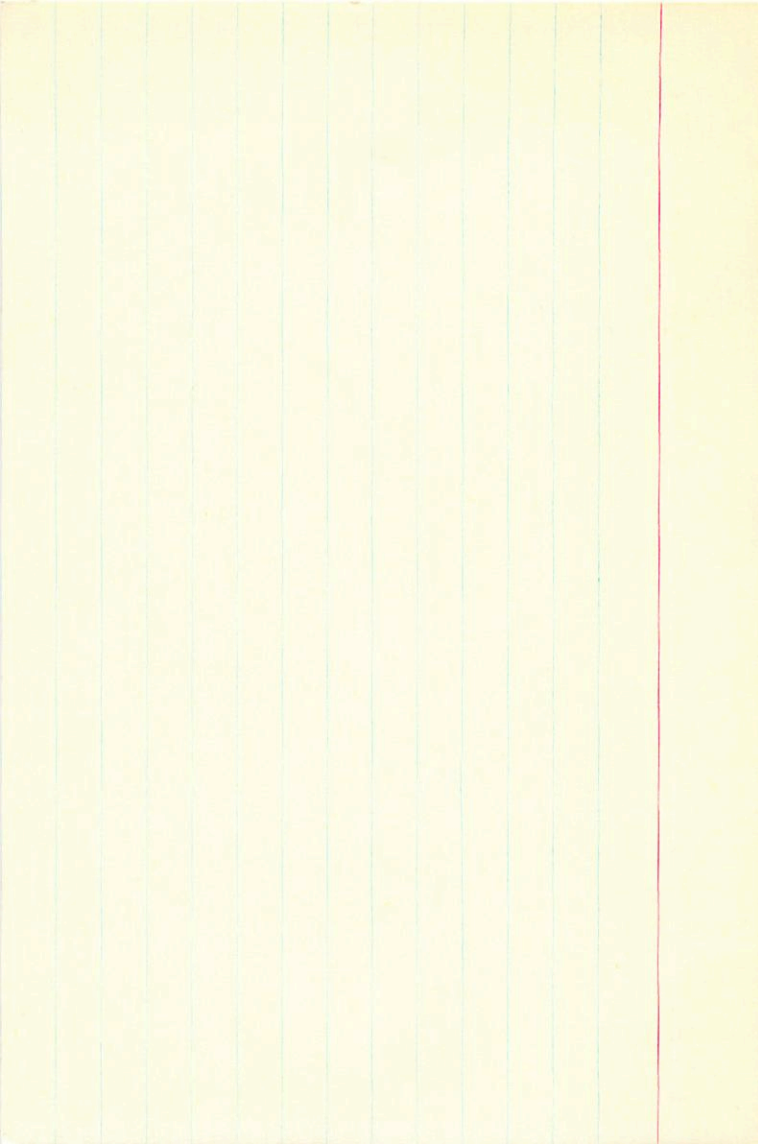
-12.1 -2.9 -16.6

+11.4 -7.2 -15.9 02

-12.7 -3.2 -15.1

VYA and 22 59.6 +45 37 9.65 PF -7C

14445



217694 22 59.6 +50 34 7.4 84111 -81.28

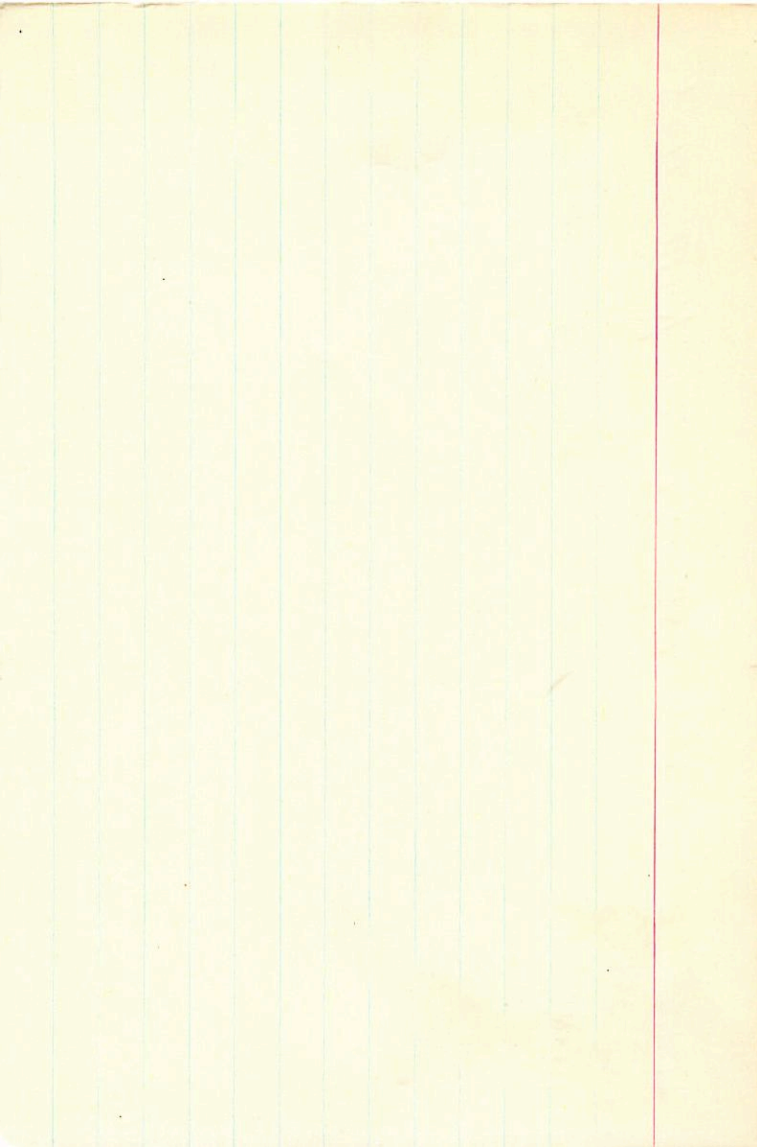
+50°39N

14448

-0040

+5034

0



GL 33335
POS 17180

22 59.9

33" South

-0032 -12%

24

23 59.9 +10 30

8.74 +0

5m - 0.4

-055 -10% Yale

+905314 -035 -100% Total

1405.55 240 0.33 3A

1416.21 236 0.34 2A

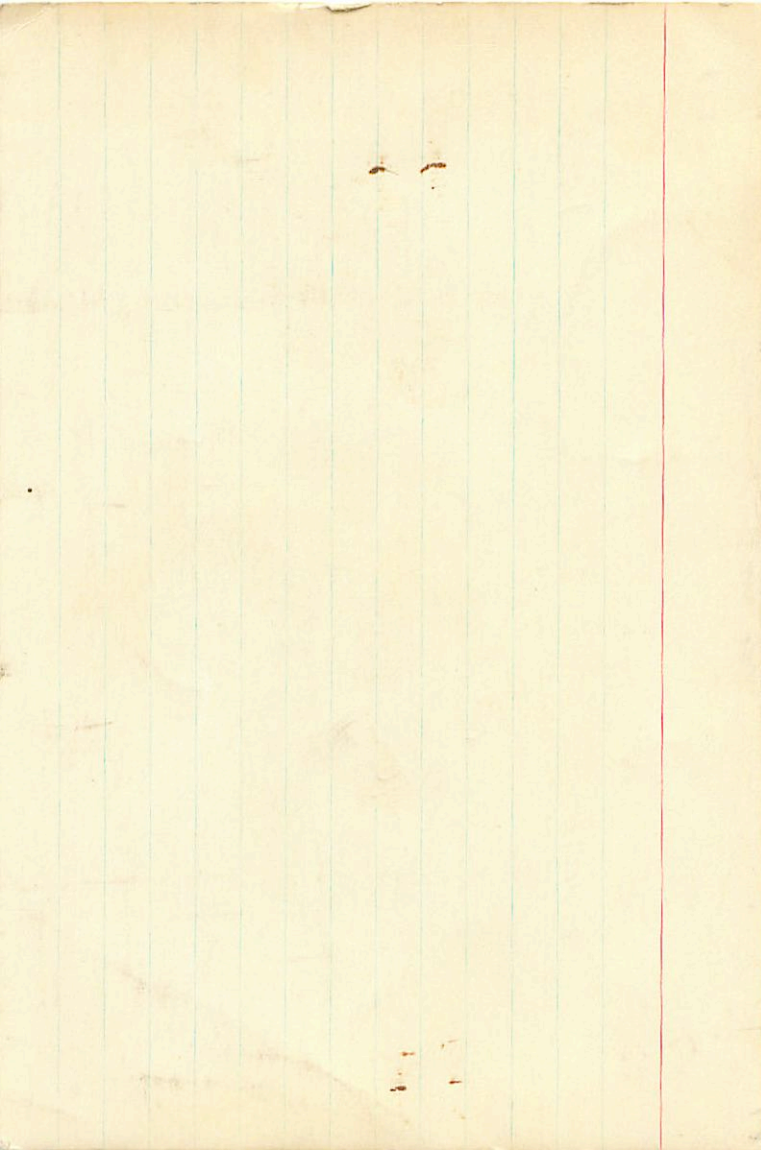
1433.73 240 0.17 2A

1451.79 250 0.18 2VB

1454.78 250 0.19 3VB

1458.61 245 0.28 3B

1461.69 247 0.27 4B



217703

23 00.1 -21 08 K0 III-12 +24.5 4C

FD1292

5.97+0.44 2.03

-0037 -133 N30

-0040 -157 60

-0038 -140

-.052

217703.000*

23.000*

0.100*

-21.000*

-0.000*

-0.052*

-0.140*

5.000*

100.000

24.500

-0.473

-0.324

-55.236

-0.527

0.284

-45.716

0.004

-0.902

-21.697

51

51

W 1455

23 803 + 42 29

726

2 A m

53A (116)
46 (16) (M)
507

A 0 217782

56 3210

- 8 010 + 90

+ 17 714

+ 21 22

A 516467

+ 0.0047 - 002 00

(sum)

284

860 465 208

- 308 145 940

- 400 872 - 271

1981 - 0044

- 0710 - 0014

- 0935 - 0053

1937 + 136

- 0724 - 14

- 1018 - 19

272

504

+ 1.5

- 0.5

15m = 2m

~~1889.54 318 0.28 3B~~

1935.18 13 0.20 21A

~~1948.70 359 0.45 31B~~

1952.63 4 0.44 2 VB

1957.62 19 0.84 3B

1958.65 not run 3B

1958.72 25 0.46 1B

1961.92 not run 4B

1962.63 not run 1B

1890.63 318 0.26 9B

1893.23 321 0.45± 5 Sp

1898.79 330 0.36 2A

1900.70 332 0.35 3A

1902.70 339 0.39 1A

1905.69 339 0.47 1A

1912.61 345 0.45 3A

1914-1918-1921 not run 3A

240174

23

00.4

+56

50

8.6 dg 5

-38.76

3W

+5602933

14457

-0124 4024 Y

0

$\frac{+1}{+025}$

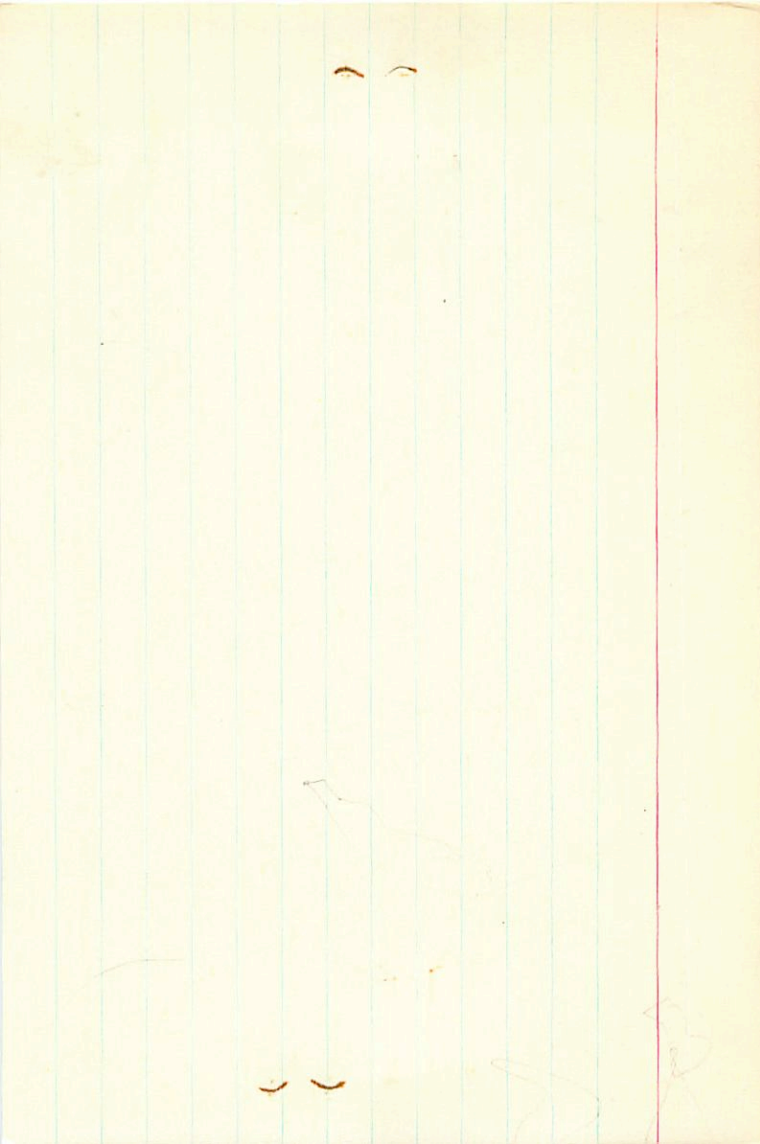
S=00

8.65 +0.725

+0.30

5.36

3.30



71486

8778 23 01.2 158 18 62705

+065+0196-
3 +1
+062-+020

52



8778.000*

23.000*

1.200*

58.000*

18.000*

0.062*

0.020*

5.000*

100.000

14.000

0.290

0.329

33.851

-0.100

217906
32135

202 1466 23 0 1.3 +27 49

M20-111 9 M2 +8.79

9773

2.30 +1.66H

M2111

+188 +143 FR3

+141 N30

WB -1.6 +141⁷N30 +186

+0140 29 +141

+141 N30

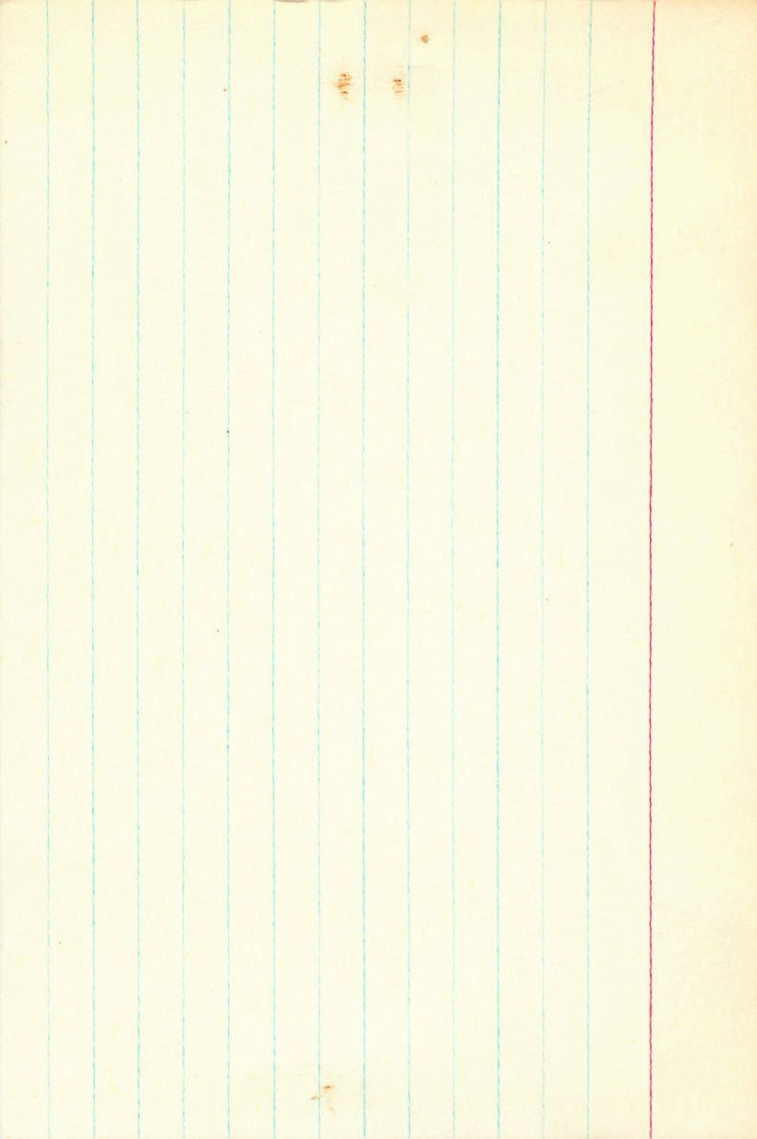
+187

60 → N30

+0141 ±1.0 +143 ±0.8

+134 +7 +2 083

+153 +7 +5 021



(15) 1-8

23 01.6 +66 56 5.5 9.13 -7.06

1447

AR8779

478 - 8 0 474

2094

$\frac{192}{374}$
 $\frac{183}{413}$

$\frac{284}{274} + 023$

HD211029

+003 +016 66 → 2736

695

1018 170

5695

861 320 385

+0235 +0250

+0985 +16.7 → 2.7

-314 -250 915

-0267 -0189

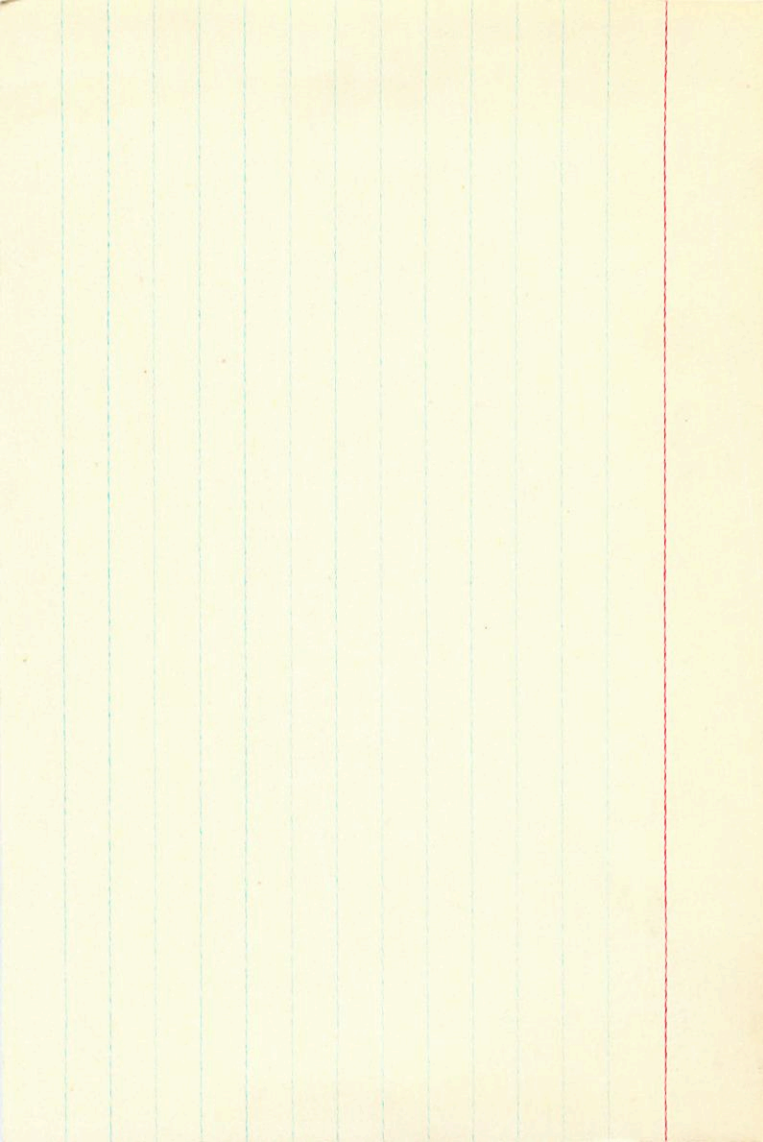
-0456 -7.2 → 6.4

-398 910 113

-0339 +0688

+0349 +55 -0.8

191



2180M

23 02.6

-13

21

144

8783

-048.5 +038.4

6118 994 488 104 108 5.1 4 P

6259 -3654 } 0622
0794 -6435 } -0014

218101 23 02.6 +12 18 d69 -27.480(3)

GC32158

W14481 6.44 +0.83 +0.55 68ER R

Y5590 $\delta = -05$

H1504760

6.09 +2.5 2st

28 +8
-150 -153 60
-183 15 -202 164

-4p 30 +9 .030
-61 -34 +1 .020

31 ± 11 418)

-013257.8
-0133
-1937.80
-199

372.917 1897.4 +16 17 44.47 1897.5

694
38,611

10.13
54.60

38.099

10
47.04 1934.5

103

166
~~47.04~~

083
39.8

46.04 1939.86

38.055
063
-528

19
46.23 637 436

46.68
37.2

-7.92
39.7

+0020±6.4 -023±5.8
+0019 -018

-0.90D

218103 23 027 +01 02 6.4 6.9 11.1 -12.4 Y

321622

14485

44.064 1901.8 +1 2 12.91 1500.5

-0.96

968

43.968

44.018

11

029

1.14

15.05

14.25

1934.8

17

14.42

44.036

0

032

14.41 1936.5

0

14.42

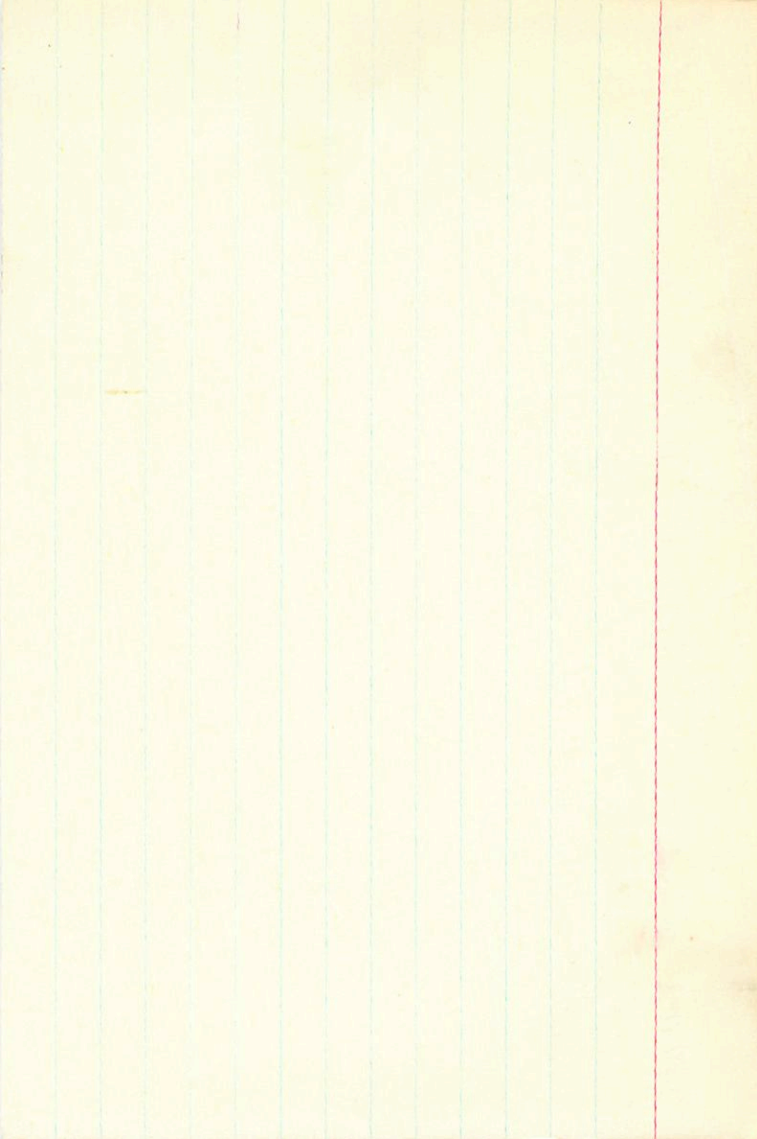
35.7

-63

13

35.2

+064



86 Agn
218240

+0046 ± 2.6
+0043
-002 ± 2.5 +15.60
+21.0 (Σ)
-24 04.0 1 4.8 969 +15.22

32152

14496 59.868 1904.6 -24 0 49.30 1903.7

A0511511 -209
1.659
49.24
09
579

193364

46.54 54.59 193331

59.787
-13
774
39.320
20.530 23.275
59.850
49
801
-156
786 +1933
49.30
-09

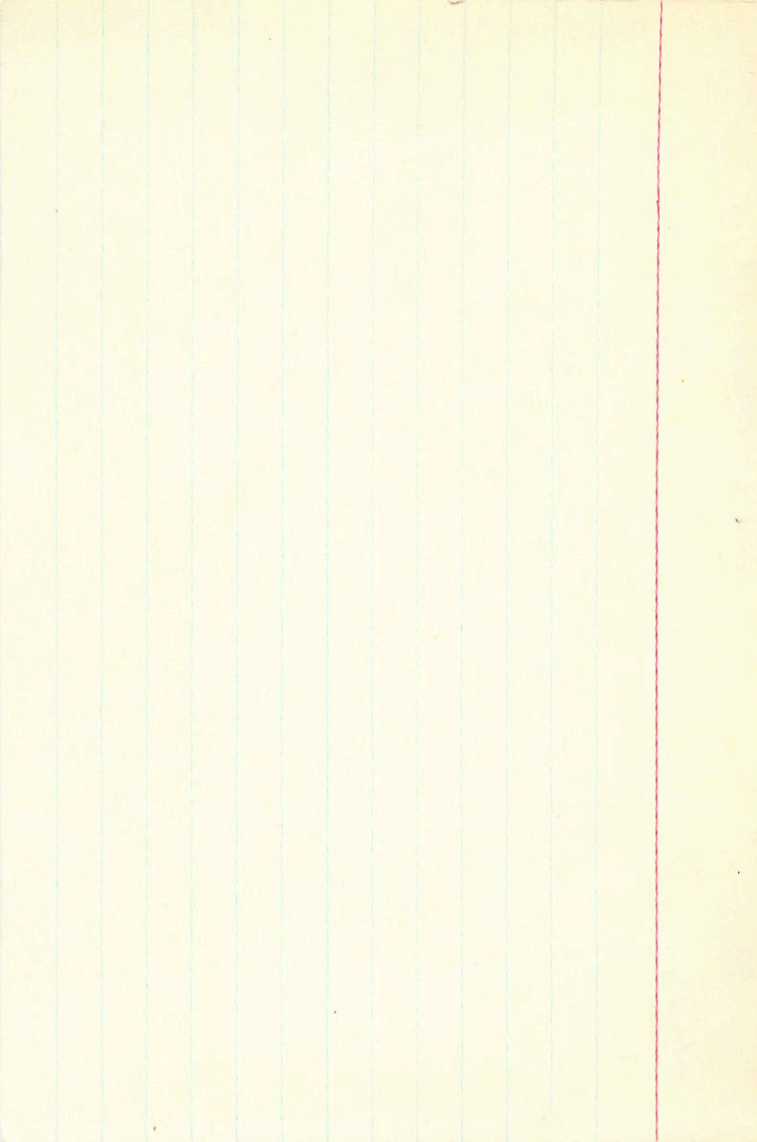
~~315~~

~~48.22~~
~~48.49~~
177
48.85
+ 25

65
51
4
49.44 19884
7215
3677

44, 2.3 49.0
214
36.2
32.5

59.840
-23
815
35.3
30.7



218329
32196

550g 14505 23 04.5 109 08

9 m2 -5.49

HR7795

4.50 +1.56 +1.81

1.25E -00

+10006 52 -00951 N30

+007 -012 6-C

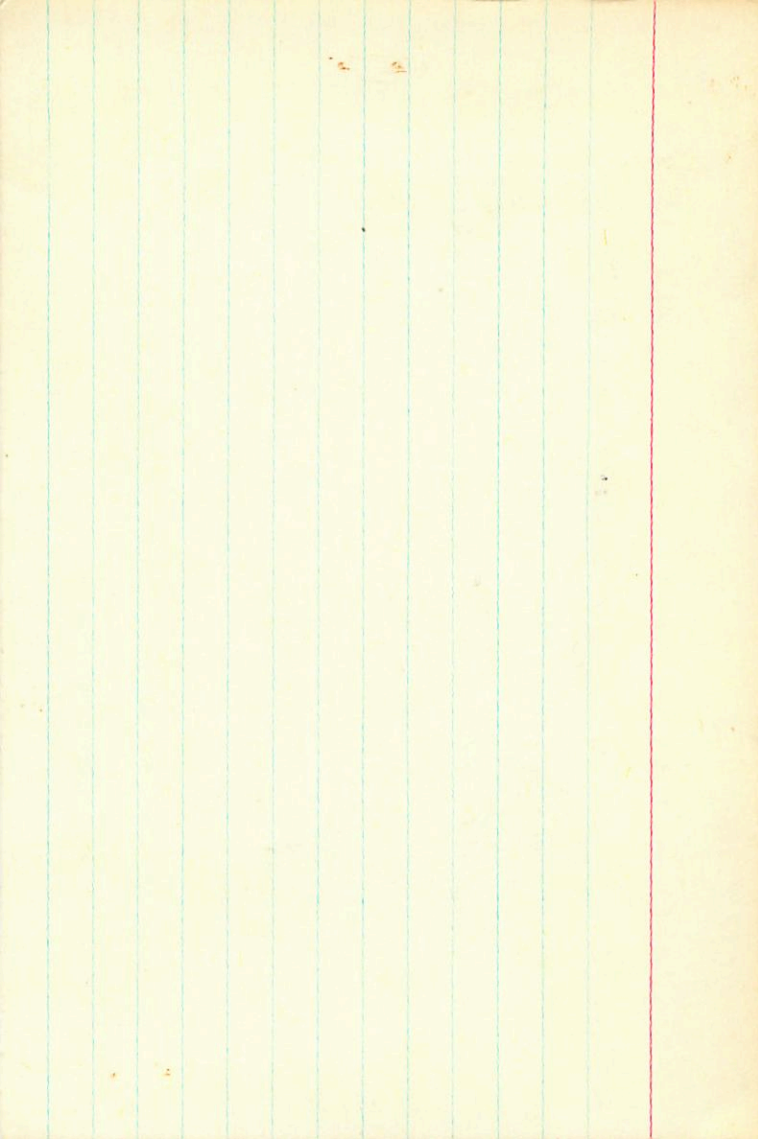
+008 -009 N30

+0005 ±1.6 -010 ±1.36 ± N30

+004 -009 F

+007 -010

40110 -0140
F135



41504764

218347

23 04.6 116 00 dF6 -22.5 8413

6C32199

8.90 + 0.51 10.02 F7BR

W14507

$\delta = 0.2$

168

-0076 ± 8 -041 ± 9 GC

-0065 ± 6 -071 ± 6 NW -110 -041 GC

-0077 ± 6 -056 ± 6 Y → GC

-0072 -060

$$\begin{array}{r} -0076 \pm 8.0 \\ -0065 \end{array} \quad \begin{array}{r} -041 \pm 8.7 \\ -071 \end{array}$$

$$-105 \pm 5 \quad -064 \pm 6 \quad Y$$

$$\begin{array}{r} 311 \\ 59 \end{array} \quad \begin{array}{r} +0056 \\ 58.79 \end{array}$$

38.065

1903.1

+15

1902.2

$$\begin{array}{r} 356 \\ 38.724 \end{array}$$

$$\begin{array}{r} 1.96 \\ 0.75 \end{array}$$

38.187

$$\begin{array}{r} 8 \\ 195 \end{array}$$

$$\begin{array}{r} 434 \\ 217 \end{array}$$

32.0

57.95 1939.86

$$\begin{array}{r} 19 \\ 58.14 \end{array}$$

~~39.18~~

$$\begin{array}{r} 38.25 \\ 239 \end{array}$$

$$\begin{array}{r} +605 \\ 217 \\ -207 \end{array}$$

58.9 1930.4

$$\begin{array}{r} -21 \\ 58.69 \\ 83 \\ 58.42 \\ -2.33 \end{array}$$

$$\begin{array}{r} 026 \\ 35.1 \end{array}$$

32.9

218416

23

04.9

+52

33

62

110111

+4.76

+0011 ±4.6

+0012

+007 ±3.9

+015

-0.8 00

32205

14511

56.741

1897.4

+52

32

44.29

1894.7

$\begin{array}{r} -0.58 \\ \hline 683 \end{array}$

$\begin{array}{r} -39 \\ \hline 43.90 \end{array}$

50.36

6.292

56.652

.734

0

38.8

37.8

1926.4

6.15

43.95

43.27

22

47.22

44.44

7239

36.2

41.5

56.715

0

721

728

7075

44.97

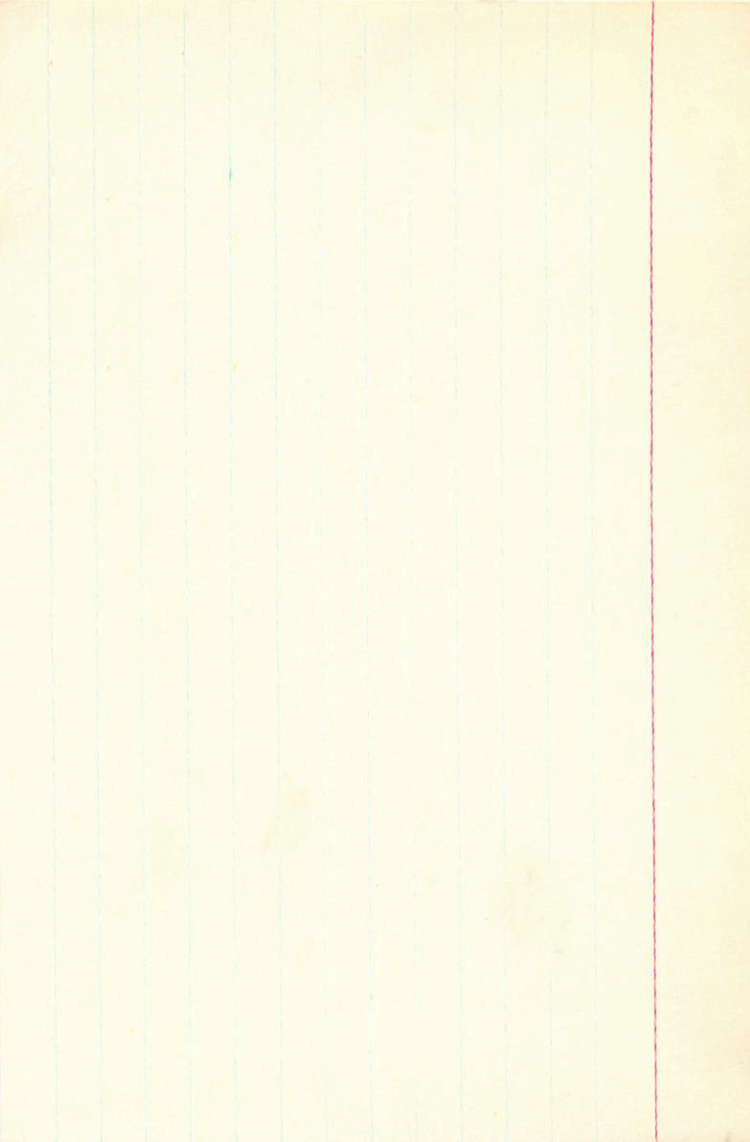
1945.99

-37

44.60

44.52

+62



4 And
218452 23 05.4 +46 07 5.6 gms -6.2 b
32216

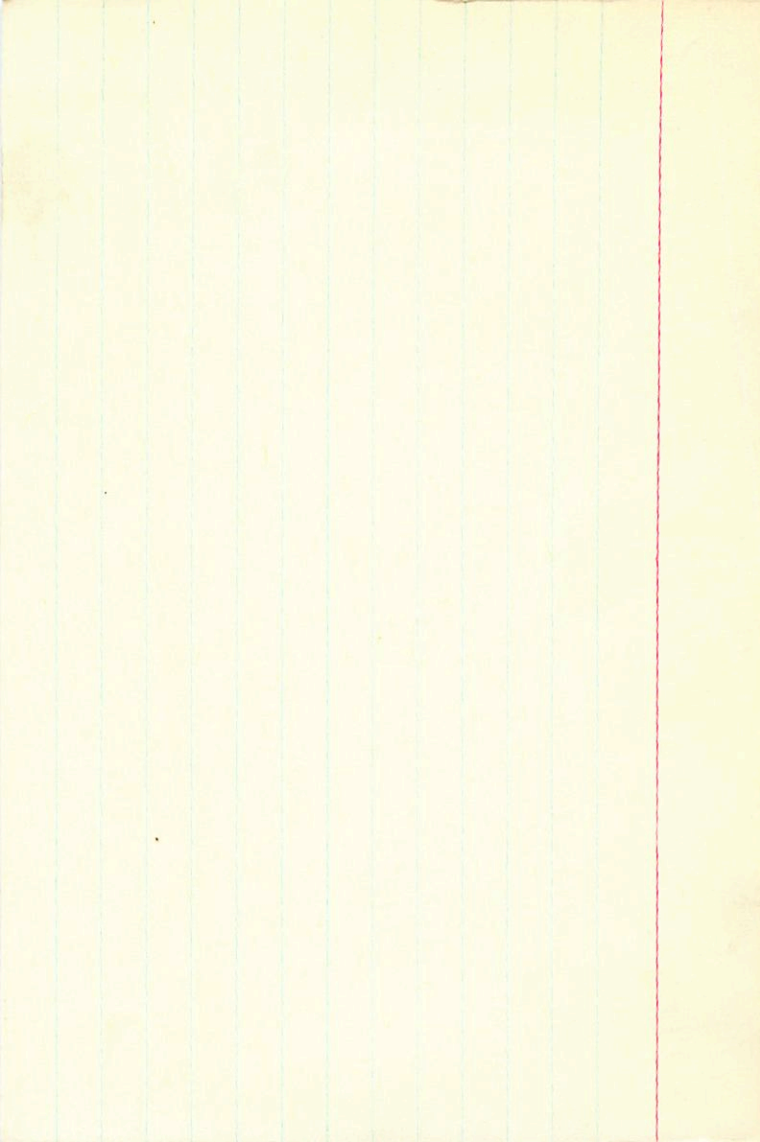
-11.5 (9)

-0016 ± 1.9 -0.30 ± 1.8

14519 21.697 190.7 +46 7 0.50 18983

A0516526 22 24
-0021 ~~1.9~~ -0.28 ~~1.9~~ N30

-0019 ± 1.9 -0.28 ± 1.8



4A and

23 05.4 146 07 gms - 6.26

HR9804

5.33 1.41 1.72

-017 -03066

W14519

NS III

-022 - 0288
-020 -029

~~-236 972 721 493 -020-029 -6.2 -021-4.5 -09.54~~
~~-007 -005 -028 -020 062 -7.56 -4.3 -4.2 +1.0~~ 01

+4.8 -2.3 -8.1 007

-26.8 -1.8 -9.1

+3.6 -18.5 -16.5 008

-23.7 -2.4 -7.8

+2.0 -14.6 -13.5

+0.9 -12.0 -12.5

-16.3 -8.65

-0.1 -9.4

0075

+0.6 -11.0 -11.8

-15.2 -8.7 -4.1

012

015

013

5 And

218470 23 05.5 749 01 5.8 dF=3 -2.08

32220

14521

+0152 46 +134 50 N30

8806

+0146 ± 22 +134 ± 17 CL → N30

W350

+0150 +1341

23.1

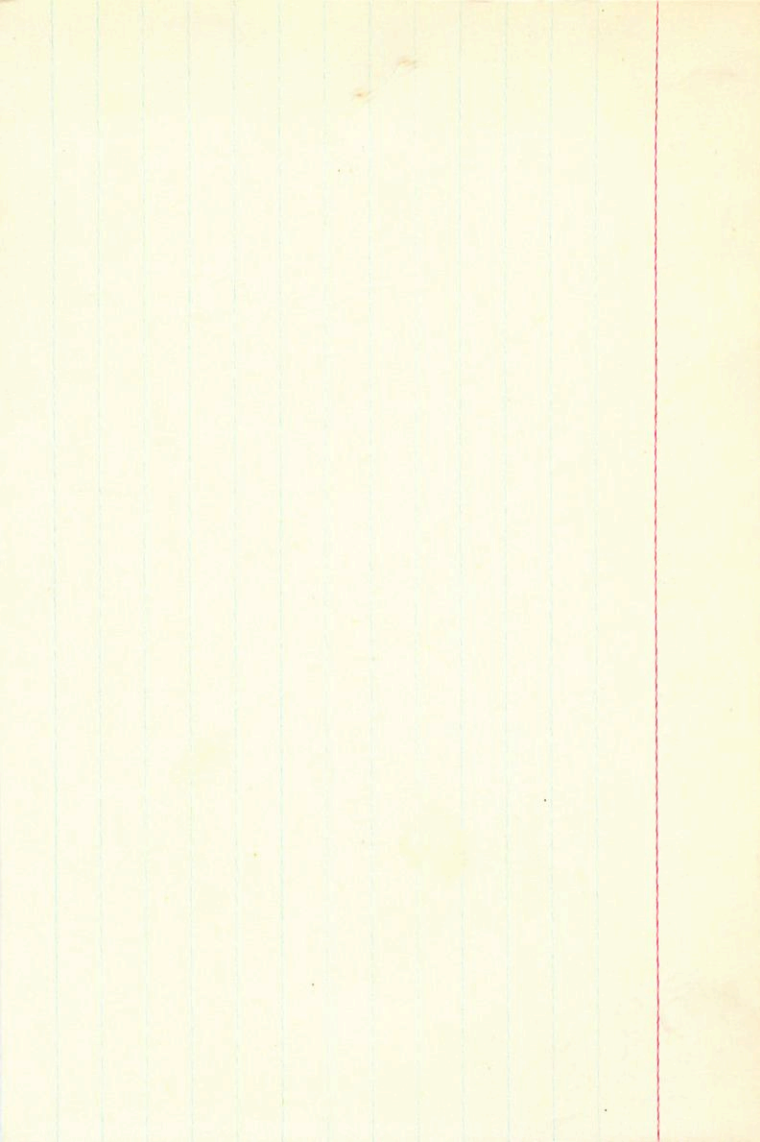
01541 +1324

+46

1536
156 ± 125

238
+124

-2.0



355

+12
+5

218470 23 5.5 +49 1 F5U

HP8805

#2.0 N30

GC3220

~~101440 +11110~~

5.63 +42 -3 1 egg

S Mand

101543 +1066 F14

1153-1132

1455 ② SPC

772 +12
23 15 +12
+1519

1286 152

2.672 ③

76 -204 294

Calc

207 +118
438 +56
75

2070 +258 -8.8 +10.4
+874 -58 +298

130

$$\begin{array}{r} 231\bar{7} \\ 654 \\ \hline 0990 \end{array}$$

$$\begin{array}{r} 345 \\ 1575 \\ 11904 \\ 13486 \\ \hline 13518 \end{array}$$

53



8888.8888

23.000*

5.500*

49.000*

1.000*

3.153*

3.132*

2.650*

33.884

- 2.000

3.881

3.273

23.657

- 3.204

3.946

- 3.803

3.285

- 3.176

13.015

53

TT Cap
218654

23 06.3 775 07 4.6 g 61 -18.6a

Sp.O.P =

32287

14530

ADS1654

47-7.0 0.5

+ 0013 ± 1.1 - 0.25 ± 1.1 Gc → 1130

17.7 Dukt

$$0.85 \quad a^3 = .62$$

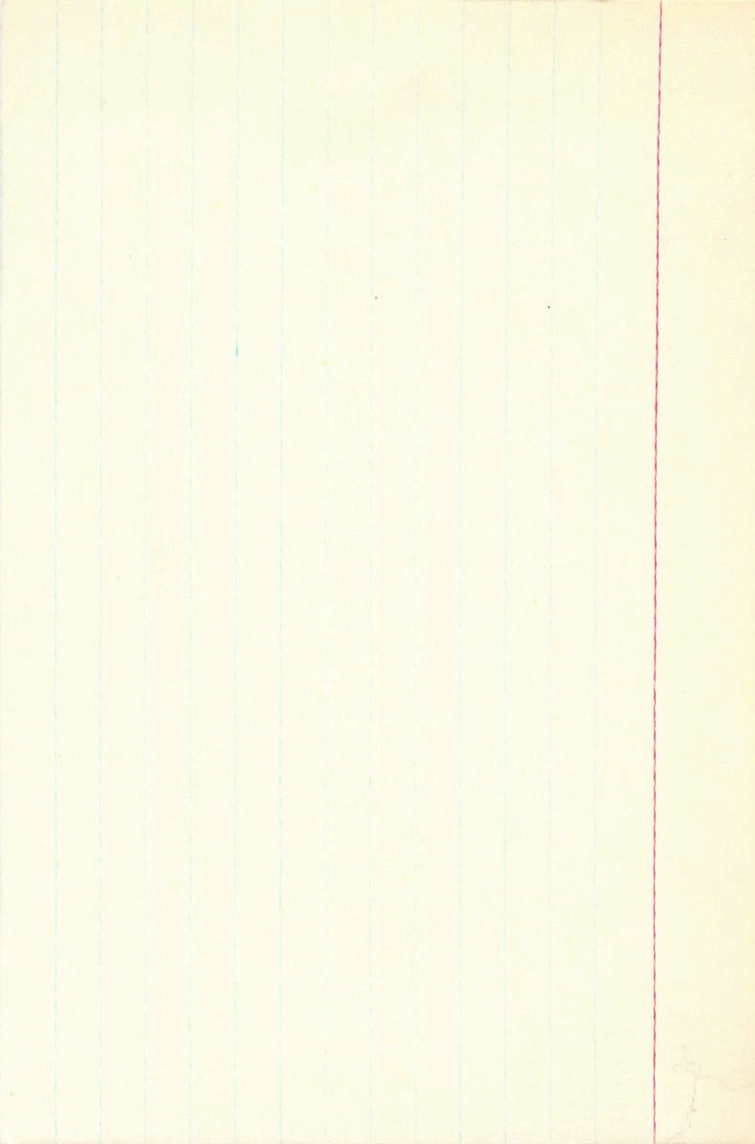
$$\frac{a^3}{\rho^2} =$$

$$\rho^2 = 2.24 \times 10^4$$

$$= 2.27 \times 10^{-6}$$

$$1 \times 10^{-6}$$

$$0.1 \times 10^{-6}$$



AOS 16638

23 063

+25 07

-18.602

1.4p

6189

+010-025 66

+008-021 F

-232 523 966 257 +009 -023 +8.6 -022 -18.0 -025
002 -005 009 -021 109 019 -4.7 -4 +1 0189

+2 +2 -19

-7	-14	-11
----	-----	-----

16.53
ADD 1.1

17.63

28 060 + 10 41
30 56.3 25

535
1000 010

16.85 0.1
14.76 9.72
+ 52
5.09

16.763
+ 5
765

10030 000 1490 338
10033 10023 + 10
10476 15.10

9533 9809 0442
-3220 9946 0118

1050.5 - 002

16.839
11.11
5.729
55.15
15.14
6.11
55.15
60.5

+ 5 + 9 Areas

6-54
11-24
11-52

11 01 +

28 01.3
+ 1004187

23 06.6 -0.2 32 32 -40.886(4)

3~

8.62 +1.02 +2.08

218566
6632241
W14533
Y5602
-3°5577

me km
egg (2)

228M1

23.1
-2.5
+630
-700
2044
-409

44M(6)
30Y(10)
570(3)
5517
28±4

-378

94 2.23

GC +625 -09Y

Y 658±4 -119±6

613±9 -080 Cap. volume

632 -098

+43 -56 +1 .040

+58 -53 +5 .045

+51 -56 +7 .05

+48 -48 +4 .055

+

37.175

1507.3

40417.8-0
+0430
+0421
-2

-09477.8
-104
-100
31 50.17 1403.7

-1.781

4.34

32,394

45,78

50

3.015

30.872

33.887

14.41

1941.28

3.77

49.43

-2

33.688

45.45

33.552

49.35

1933.6

528

35.130

30.1

52.12

44.11

49.28

33.7

.007

52.34

3.56

488

10

MS
D

23.100
-2.500
630.000
-100.000
2.440
31
-40.900

0.864
0.477
-0.160
2352.355
78.887

-0.323
0.769
0.551
-1327.921
-63.393

BM

-0.386
0.425
-0.819
-1352.112
-8.897

88 Ag₂

218594

32246

14535 ✓

23 06.8

-21

27

3.8

N 2 II

g 111 +21.1a

+22.0

72

+0042

+035

72

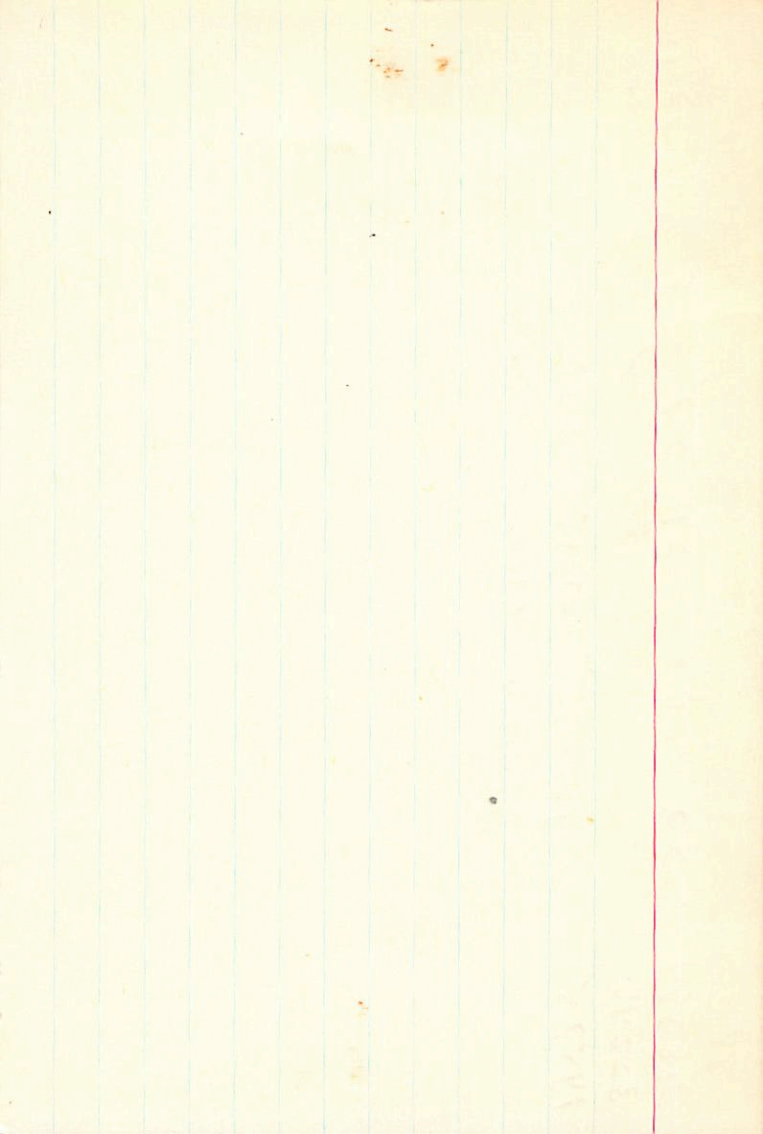
N30

+1060

+0041±14

+036±15

G₂ → N30



89 Apr HO GORER

+0016 ± 2.5 -00752.5
+0024 -006

11 June?

218640
32262

23 07.2 -22
+0023 -007

4.9 4.9 62-4.82
-0.24
-10.2

14541

14.767 1902.5 -22 43 44.13 19070

+0023 -0.13
+000.2 TOTAL
-100.25 -0.13
-0.374
-0.375

+865 +383-311
-326 +912+205

-076
691
+7.4 +1.5
-5.0 -1.2
-3.8 +44

51.90 1933.07

-380 +110-418 5-4.707

20-11.29
14.819
774
773

7.22
44.67
44.32
44.24
44.17

+1304 -0130 41174
+0491 -0303 -0794
-0573 -0030 -0604

14.8125
-2.5
58

73.67
36.8
35.8

+0023
+0023-013
+0024-014

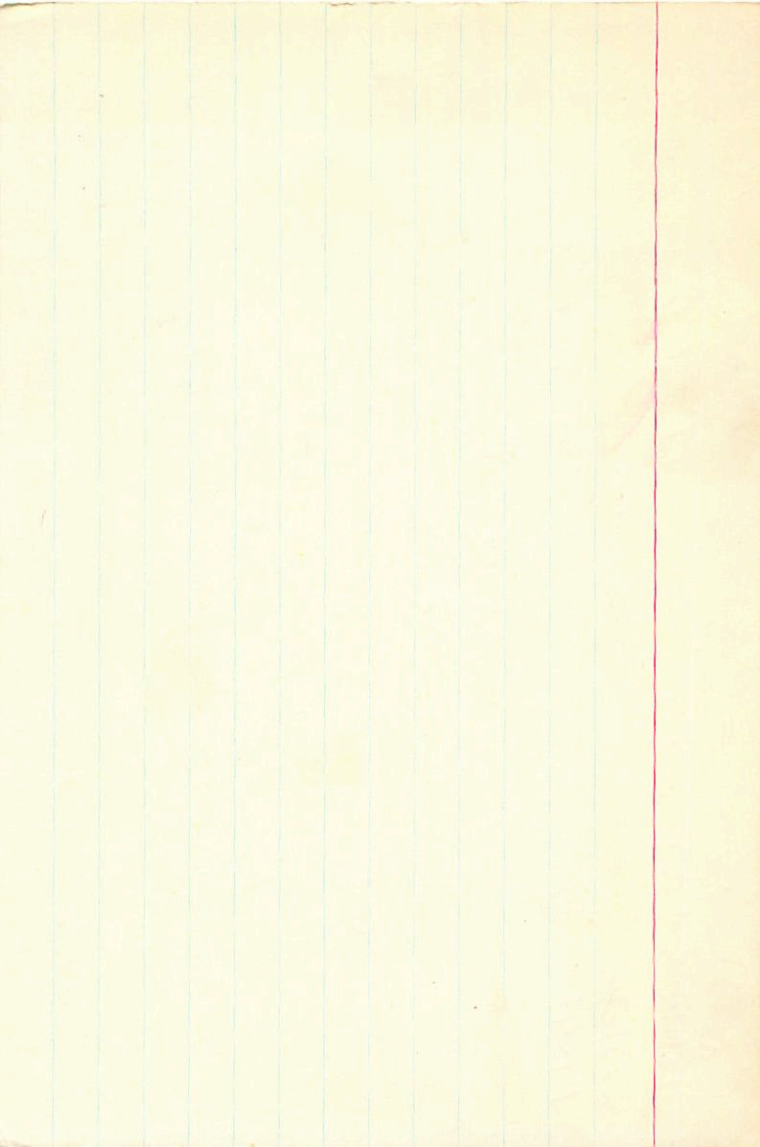
14.85
-1.74
5.74
14.83
-2.1
5.27

9369
-3496.2-0255

4165
1.70
44.67
44.32
44.17

9369
-3496.2-0255

9997
-0255



F82

218630 23 7.2-43 8 FGV

H18814

600000

682 +49 -2 C

QFD

307, 155, 418, 2.636, 3, 72, 152

315

J646

318 101 422

508

446

-0292 = -320

-016 +12.5

210 f20

357 f12

250

-5.4

-1.0

-11.2

-13470 39.1

15231 +9.4

5955 +3.7

-13272 -018

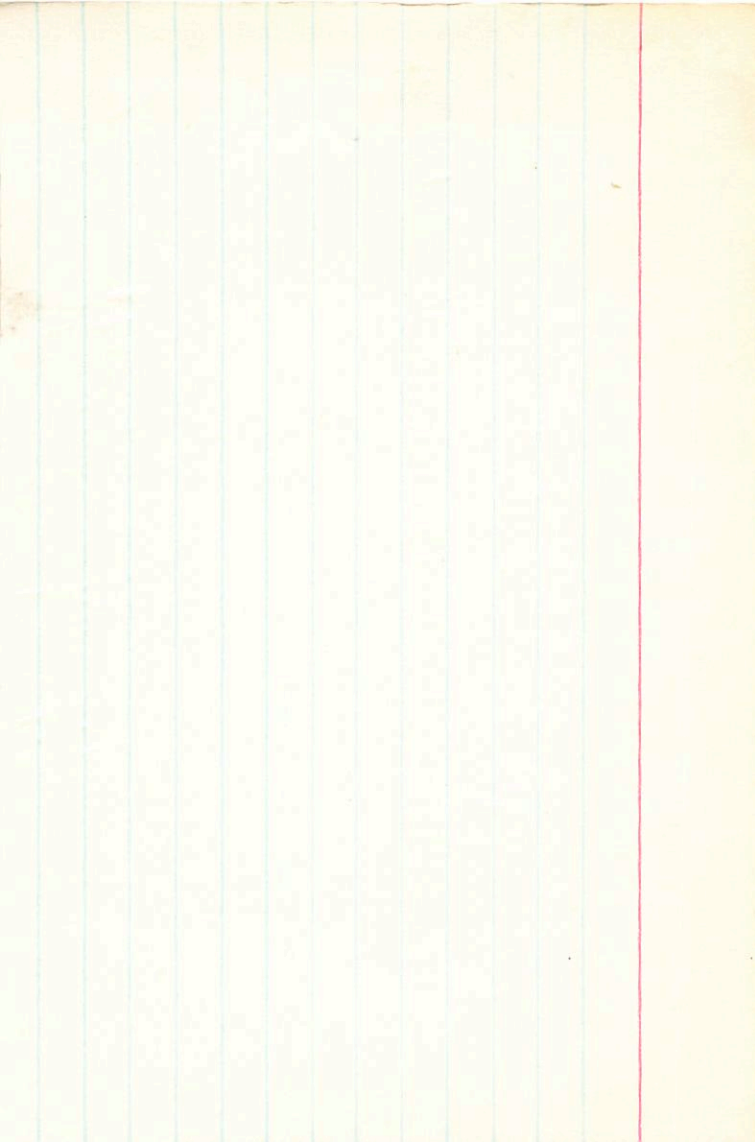
4545 -0714

5524 0161

86522-48-84-292518

-326 512-292518

-812-292518



218630 23 07.2 -43 08 F8E +10.2 4C

F01089

+140 1056
+12.8

5.80 +48 1.62

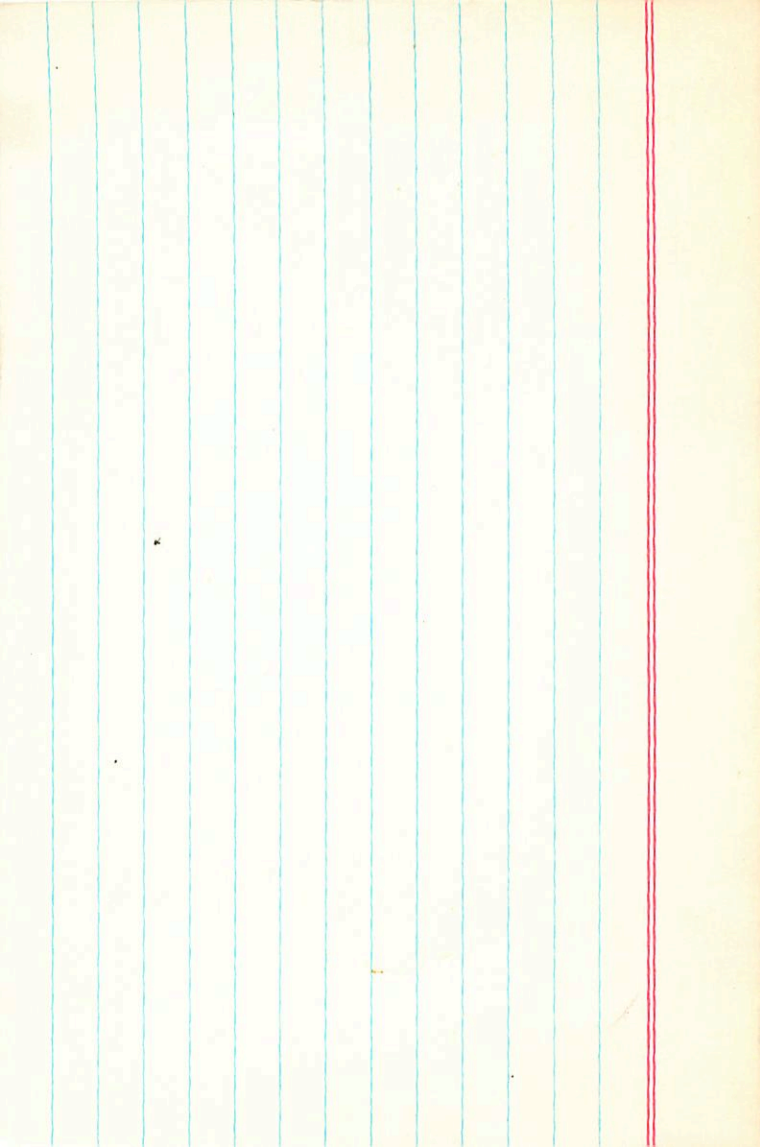
6.9 }
8.5 } 1"

-0240 -014 N30
-0292 -004 6C
-0291 -009

-0302 -018 Shy 1965
+10 +2
-0242 -016

→ 315

020



218089

23 2.5 + 15 09

+ 24 00

6.55 605

1082-089

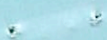
118-811

123
88

2

+ 24

35



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 97
 98
 99
 100

R.A. : 23.100

DEC. : 15.150

R.A. : -123.000

DEC. : -89.000

STANCE : 2.000

ODULUS : 25

VEL. : 2.900

q1 (U) : 0.864

q2 (U) : 0.503

q3 (U) : -0.007

DU : -698.560

U : -17.569

q1 (U) : -0.323

SS

218739

23 07.77 + 47

41

260

-7.98

+0112 24.0

+0146

+005 43.2

+001

32277
14546
KOS1657

PKL
KOS14 2002

{6.9
6.0

+113 24 + 005 24
- 24
G

+162 24 + 005 16m(2)
24

$\Delta m = 0.51$

1544

1352

+003

$\Delta = 0.42$

40.468 1895.8

+47 41 17.29

-33 1883.7

Ver. Dubel

39.867

16.96

19.272

26.4

31.50

320

9.3

7.555

16.25

PKL: 9

8.375

17.10

17.00
+04

40.275

20

17.30
16.59
1929.7

350
547

PKL 6

PKL 6

324

16.70

9902

9458

7355

9247

-226 574 740 673 ¹³⁵+113 +003 -7.9 002 -6 009

031 0 134 0 147 635 -5.3 -5 +1 015

$$\boxed{+5 \quad +48 \quad -5}$$

$$\boxed{+37 \quad -20 \quad -13}$$

$$+6 \quad +50 \quad -5 \quad 013$$

$$\boxed{+43 \quad -22 \quad -15}$$

0199

525812

23

~~275~~
1.00

- 81 -

11

110.00

Eggs

to us - us

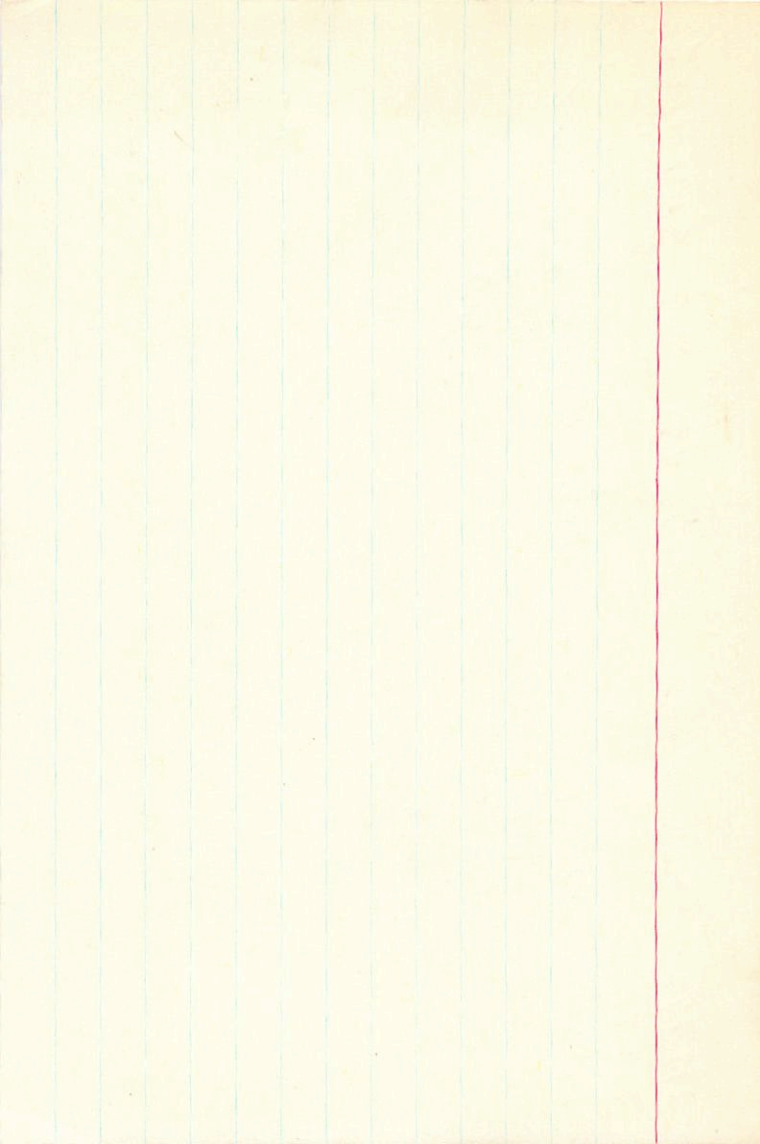
218792
 32291
 14550
 13.346
 23
 08.2
 $+17$
 19
 5.9
 9144
 $+1.88$
 $+0012 \pm 2.6$
 $+0019$
 -028 ± 2.5
 -020
 $+28$
 $+2.8$

1908.8
 $+17$
 19
 22.79
 1908.4
 -0.49
 $\underline{297}$
 1.14
 $\underline{23.93}$

13.383
 $\frac{7}{337}$
 27.4

23.04
 $\frac{10}{23.14}$
 23.66
 1939.64
 $\frac{244}{36.2}$
 $\underline{26.8}$

13.377
 $\frac{-14}{363}$
 $+0.53$



B67-49

23 08.3 +18 38

-24.9

+1805118

8.56 +695

-244.6

GC32292

2.20

~~1.11~~

260.13
-32.14

-208 -202
-3 +8

-211 -194

-0.167 ± 8.3 -182 ± 90

-183

-18 ± 3

+18 38 23.84 ± 1902.5

8.43

-0.150 -179

32.49

15.303

798

16.101

15.543

+8

551

+18

38

25.34

1934.86

+19

15.3 0.04

26.52

5.97

35.1

32.9

1256

628

473

15.71

-5

705

27.7

-19

27.51

1930.3

5.97

32.6

-1

-213 -179

→

218853

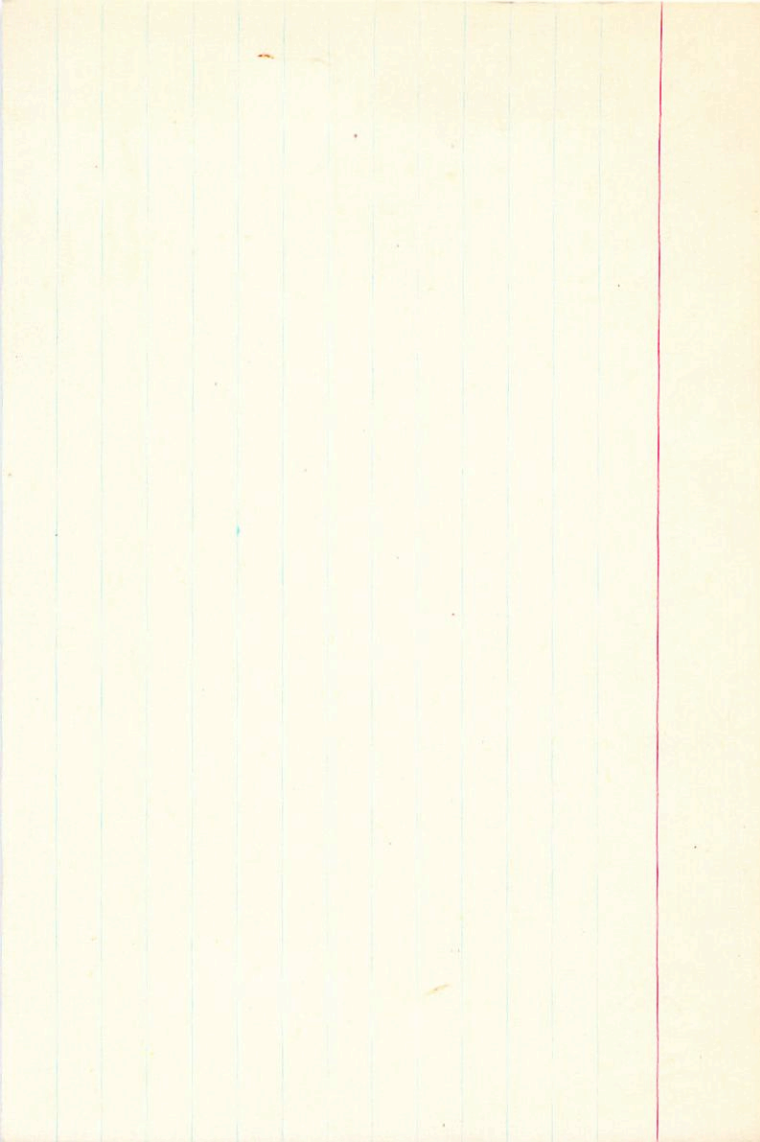
23 08.7 +4 44 6.9 gms -6.28

32299

14553

-000613 +00713 1130

+000454.1 -00323.9



810518

23 07.5

199614

23 10.1 + 2 25

+396
Sub

60 32317

+077-143 Yolo

23.15

+24

+77

-143

40

340

56

R.A. : 23.120
DEC. : 2.400
PM. R.A. : 27.000
PM. DEC. : -143.000
DISTANCE : 4.000
MODULUS : 63
RAD. VEL. : 34.000

d1 (U) : 0.625
d2 (U) : 0.488
d3 (U) : -0.107
d4 : -12.274
U : -4.623

d1 (U) : 0.330
d2 (U) : 0.720
d3 (U) : 0.210
d4 : 0.210

R.A. : 23.150
DEC. : 2.400
PM. R.A. : 77.000
PM. DEC. : -143.000
DISTANCE : 4.000
MODULUS : 63
RAD. VEL. : 34.600

q1 (U) : 0.866
q2 (U) : 0.488
q3 (U) : -0.107
dU : -15.274
U : -4.663

q1 (V) : -0.330
q2 (V) : 0.720
q3 (V) : 0.611
dV : -

17/6/62 23 08.8 -16 31 775 (P)

2985M Cullby 05/5 W(LK)

1035 103

8.95 0.73 12.03
8.96 0.70

1030 103

8.92 479 564 534

-52
-103
656
178

8.59 505 069 324 TMMW

Handwritten signature

-41.15

R.A. : 23.150
 DEC. : -16.500
 PM. R.A. : -52.000
 PM. DEC. : -103.000
 DISTANCE : 6.950
 MODULUS : 245
 RAD. VEL. : -175.000

q1 (U) : 0.866
 q2 (U) : 0.427
 q3 (U) : -0.259
 dU : -413.371
 U : -56.081

q1 (V) : -0.330
 q2 (V) : 0.879
 q3 (V) : 0.345
 dV : -350.868
 V : -146.435

q1 (W) : -0.375
 q2 (W) : 0.213
 q3 (W) : -0.902
 dW : -15.181
 W : 154.159

57

57

23 10.7 439 43

16599 A 7.59 +0.28 +0.18 2 60 4A8

B 9.65 +0.47 +0.02 2 60

+46 -16 -14

$\rho = +0.163W$

17 (3)

150

150 p.p.

E = +0.14

7.47 9.53

+0.24 +0.43

+0.15 -0.01

S (-0.4) +0.01

+1.6 (+3.6)

+0068 +003 G₂ → 1030
 +0055 +013 2000
 +0062 +008

150 p.p.

+867 +451 +214 +2988 +0171 3109 +46.0

-333 +202 +921 -1128 +0076 -1052 -15.7

-372 +870 -324 -1262 -10330 -0932 -13.9

PC32324

43,929 1894.4

$\frac{L-359}{.570}$

+0071 44.1
+0058
+39 43 49.57
0

500 43.1
+010

1890.6

49.57

43.74

$\frac{L-742}{.742}$

286

50.2

$\frac{-20}{50.00}$

1929.7

159

28.0

37.1

1924.2

$\frac{737}{+167}$

32.89
10.788

$\frac{43.661}{.737}$
 $\frac{-732}{.737}$

$\frac{49.97}{+40}$

40.5
9.02
49.52

$\frac{49.714}{+49.94}$