

215724 22 449 -35 29 GOME +27.1 40

F=01083

6.70 +0.45 16.1

1498041

6.753

Sting 1968

-0052 -077 030

~~-0052~~ -074 00 →

-0053 -076

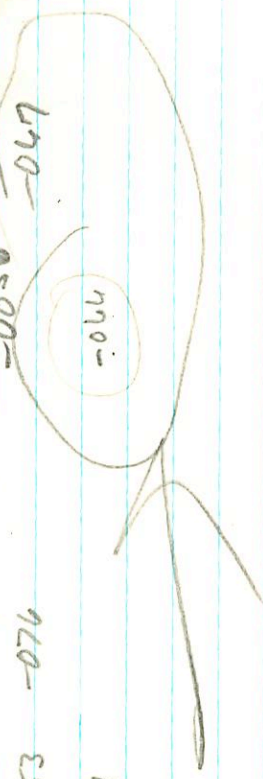
-0062 -066

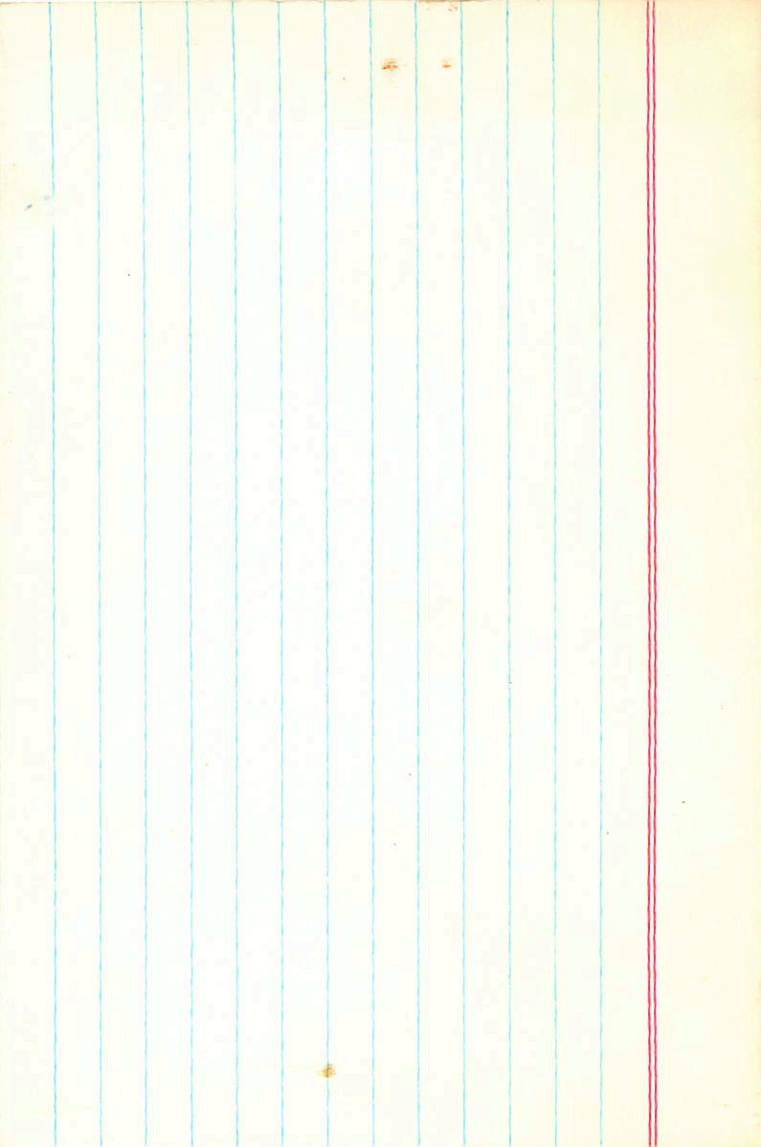
+1/2

-0056 -047

-061

-064





215812

G-C31808(90)

W14318(70)

Y5523

-405757

A0516270

Dm = 0.3"

22 453 -04 29

dB3 -22.6 to 15)

dB3 -25 CA(15)

6.66 + 0.65 + 0.12 6.5 ER

S = 07

4670

S_m = 0.27

B

-206 ¹² -300 ¹²⁰⁰

A

-203 ¹⁵ -279 ¹⁵⁰⁰

-205 -290

-31 -33 +14.04

-44 -41 +13.03

334(14)

154(12)

2450

-0138 ± 20
-0144
-300 ± 1.8
-308

31509) 15.519 1591.2 -4 29 19.72 18845

$$\begin{array}{r} 811 \\ \underline{16.330} \end{array}$$

$$\begin{array}{r} 19.65 \\ \underline{0.07} \end{array}$$

$$15.612$$

$$\begin{array}{r} -13 \\ \underline{599} \end{array}$$

$$\begin{array}{r} 605 \\ \underline{\quad} \end{array}$$

$$\begin{array}{r} 44.577 \\ -925 \\ \hline \end{array}$$

$$31073$$

$$15652$$

$$\begin{array}{r} -37 \\ \hline \end{array}$$

$$611$$

50.5

$$18.22 \quad 1942.10$$

$$29$$

$$17.93$$

$$27.15 \quad 1941.22$$

$$332$$

$$41.7$$

$$\begin{array}{r} 972 \\ \underline{17.43} \\ 17.68 \end{array}$$

$$17.43$$

$$17.68$$

57.2

$$\begin{array}{r} -7 \\ \underline{17.43} \\ -17.61 \end{array}$$

-0050447 -058#3.8

-0041 -59

215443 22 45.9 +37 09 6.0 968-25.18

31824

14325

-59

968-25.18

53.307 1897.4 +379 11.33 1842.2

262

.549

44.73

8643

53.423

476

476

476
-123

30.1

3.35

4.68

17.7 1425.6

5435

12.05

12.37

12.42

12.57

12.8 1429.7

-19

12.67

27.7

35.5

12.54

12.09

-2.09

53.43

D



70 Apr

215874

31822

14324

4476
22

14

52.375

$\frac{-100}{275}$

33.461

18.910

$\frac{52.371}{25}$

346

-14

$\frac{330}{330}$

52.372

$\frac{-16}{356}$

+0020 ±1.6

+0020

45.9

+0020 +010

+0021

+034

+032 +006

33.5

343

$\frac{+068}{343}$

+006 ±1.7

+014

-10

49

6.2 dfo -5.86

6.208

0.166

0.184

0.914

2.763

-10

49

12.71

1898.5

2.784

$\frac{-31}{13.02}$

13.02

2.55 1928.47

54.22

$\frac{13.33}{44}$

12.89

38

$\frac{12.51}{12.79}$

22

12.57

12.54

$\frac{+48}{12.54}$

1938.81

12.54

$\frac{+48}{12.54}$

6728

33.6

35.1

31808

Carl II

-0136 ± 47 -27935.2
-0136 -269

15.297 1892.5 -4 49 19.00 1890.2

782

16,079

57.980

17.700

15.580

565

10

555

958

479

15.416

13

403

600

44.0

16.68

2.32

8.82 1930.98

56.30

12.52

45

12.07 2956

36

14.78

11.71

12.46

18.14 1942.10

29

17.85

7308

36.5

46.3

ff

120

1.2

11+

2

Handwritten signature

19

22.750

-10.800

33.000

6.000

5.4 5.500

120.22 126

125.4

-5.800

0.848

0.434

-0.304

142.642

+19

19.720

-0.268

0.846

0.461

-17.128

-5

-4.830

-0.457

0.389

-0.834

38

-61.457

-2

-2.991

+0025 ± 11.3
+0028
-016

215953 22 46.0 +49 19 7.2 9MY-55.16

31825

14326 58.557 19073 +49 19 6.71 1905.7

$-\frac{35}{6.36}$

$-\frac{149}{408}$

11.1 1925.24

54.04 58.410

20.1

54.41

4.370

27.9

64

5.35

474

5.21
6.111
60/35

473

464
4056

21.7

5.90

464

58.410

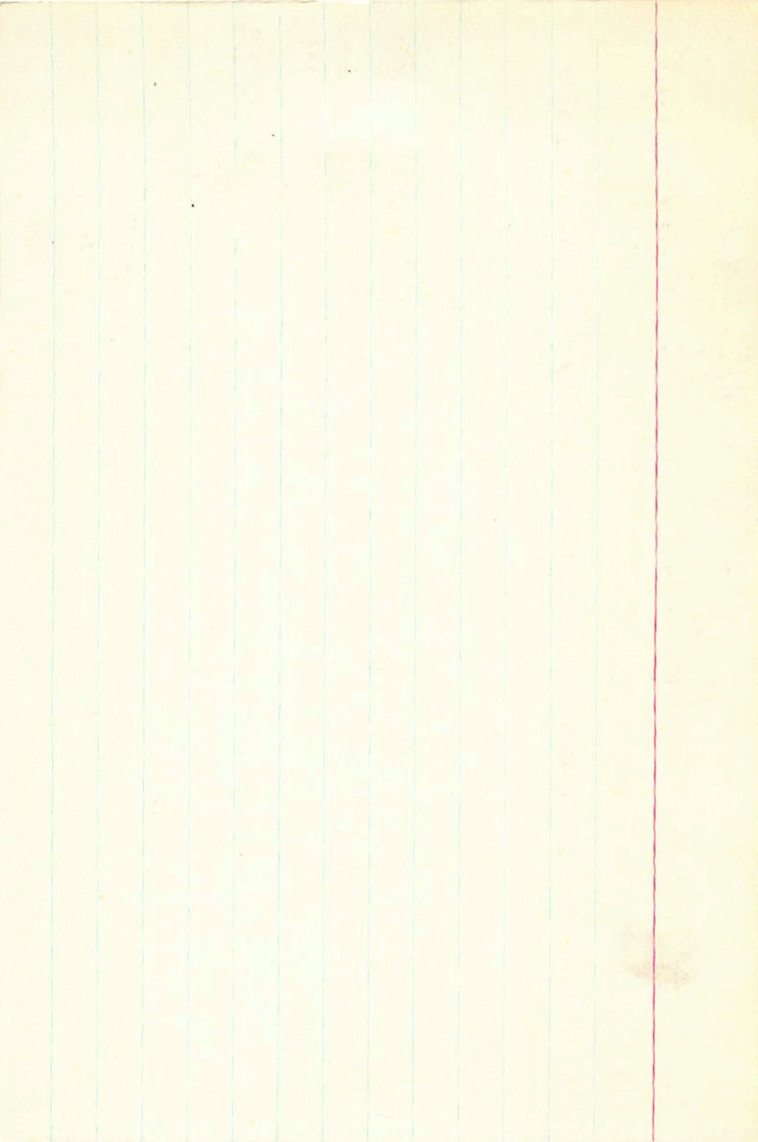
4056

~~49 1925.6~~

454

6.1 1929.6

592



① 5/14

Age 22 46.9 -13 51

g mo +1.0a

HR8679

4.07 +1.59 days

-015 -031 FAB

216032

-017 -034 GC

31986

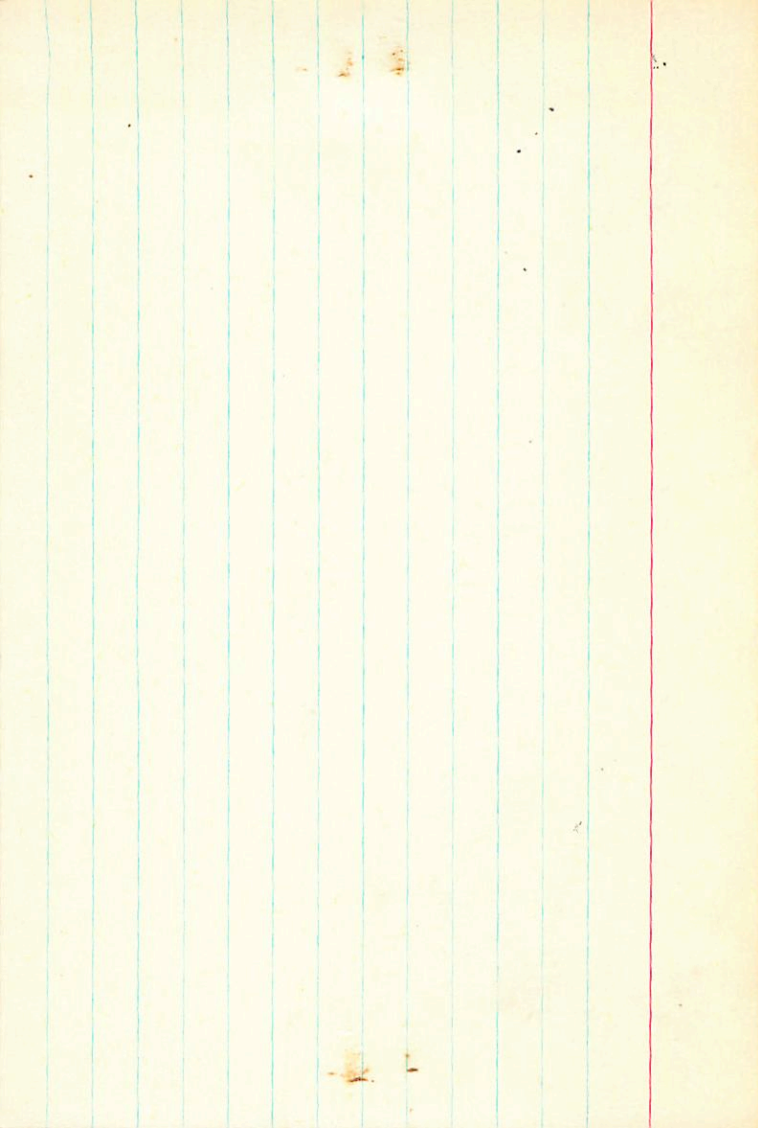
-000962 -03162 N30

-013 -031 N30

14333

-0009±10 -035±1.66 → N30

-015 -032



8683

22 46.9

+62

41 603.00

-26.68

$$\begin{array}{r} +006-048 \\ -\underline{3} \\ +003 \end{array}$$

39

216174

31854

14340

22 47.7 + 55

38 5.6 100 - 3

+ 0096 ± 2.9
+ 0098

42.086 1892.5 + 55 - 38 14.20 18

$$\frac{-552}{41,534}$$

$$\frac{-2.35}{11.85}$$

40.25
1530

41.872 3931
881 41.965

42.039 + 431
9 048

17.1 1927.8

$$\frac{55.65}{78}$$

$$\frac{12.32}{10}$$

13.10 751
13.23 13.76

18.33 + 1.91

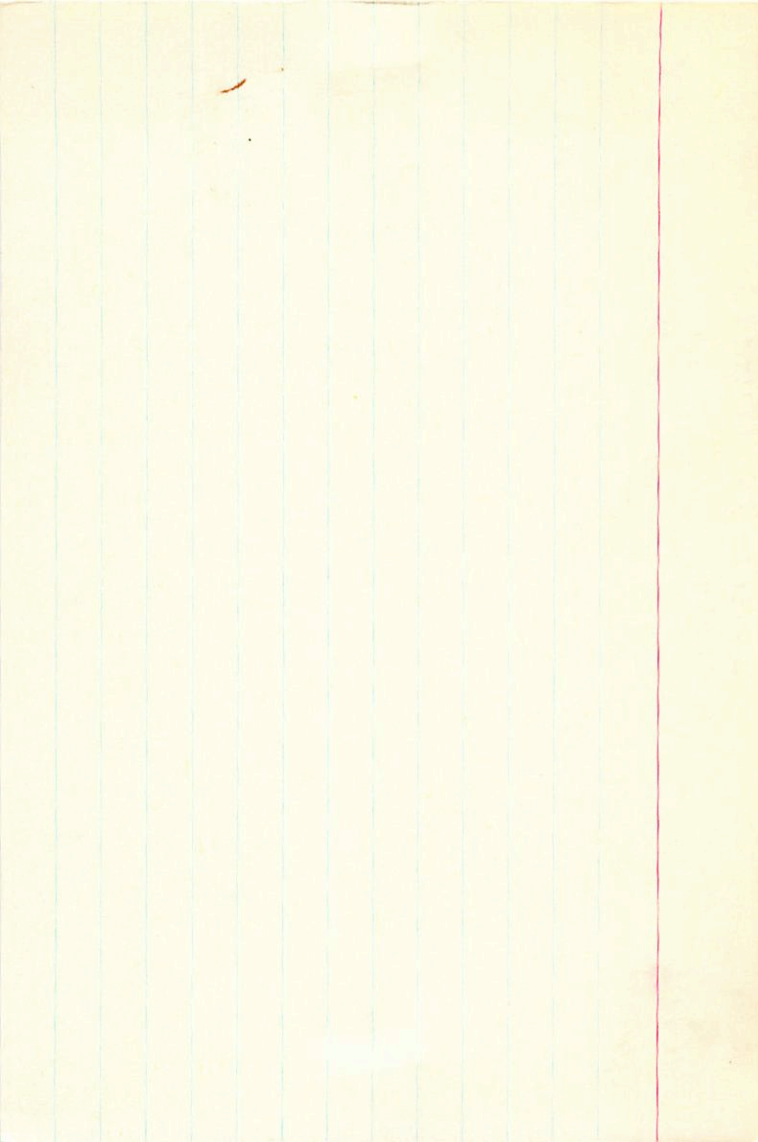
14.50 1945.00

$$\frac{-32}{14.18}$$

728

36.7

39.8



Lup 0.356 18.65 18.65 / -2.04 15.5

216228 22 47.9 +65 56 3.7 9.11 -12.44

31857 [0.07] 16.10 24.7 348 353 7.14 +2.557 -123 40.59

14343 [0.03] 0.53 1 80 -121 24.130 40.57

80.64
FRS

-0.118 ± 0.8 -122 ± 0.8 66 → 1130
-0.656 -1248

36 ± 6 MP FLY 2535g
1.200 9.07 2.18

Δ = 0.05f -0.1686 -1150

C_n = 0.22/mv -0.665

0.1123
-0.665

0.1123
-0.665

9359 -4228 1409
-3414 -4040
1350 -0.226
-0.322

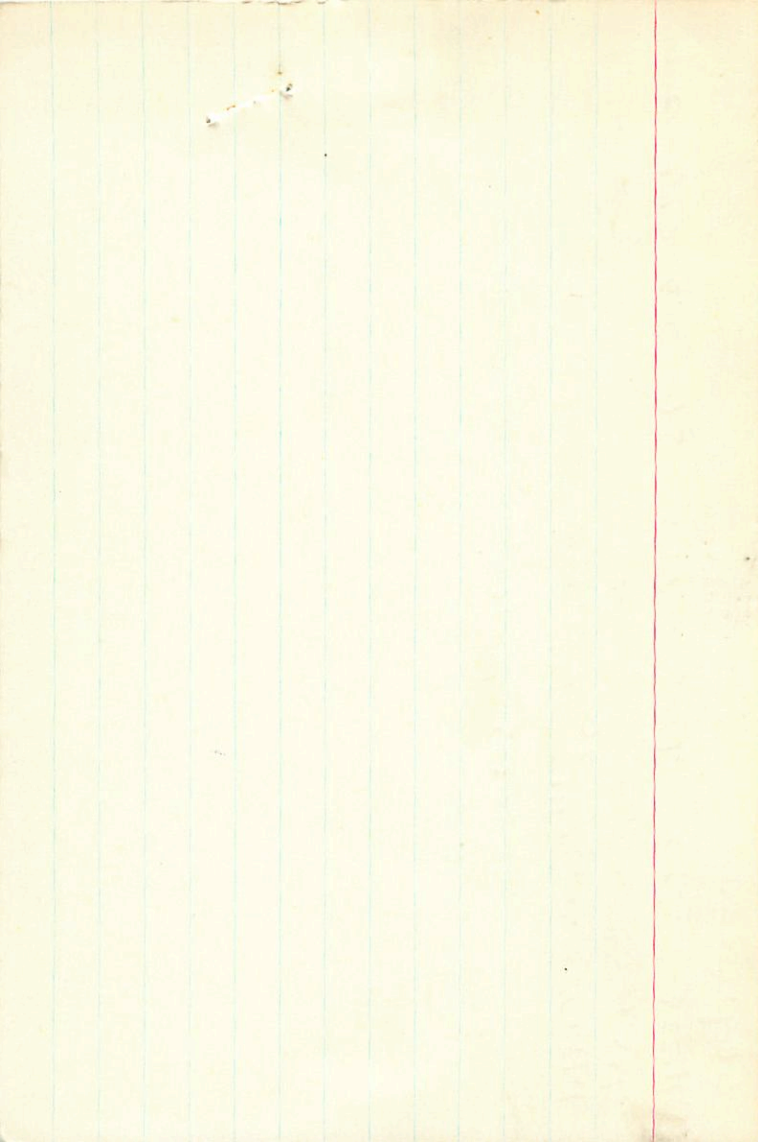
0.132
632

0.322

0.132
632
0.132

0.132
0.322
0.132
0.322

0.132
0.322



14346 22 48.2 -39 25 110 +27.36

474
32
48
42
92
142
151

42

+60279 -0.13

+1030 -106

+1028 -009

+032

525

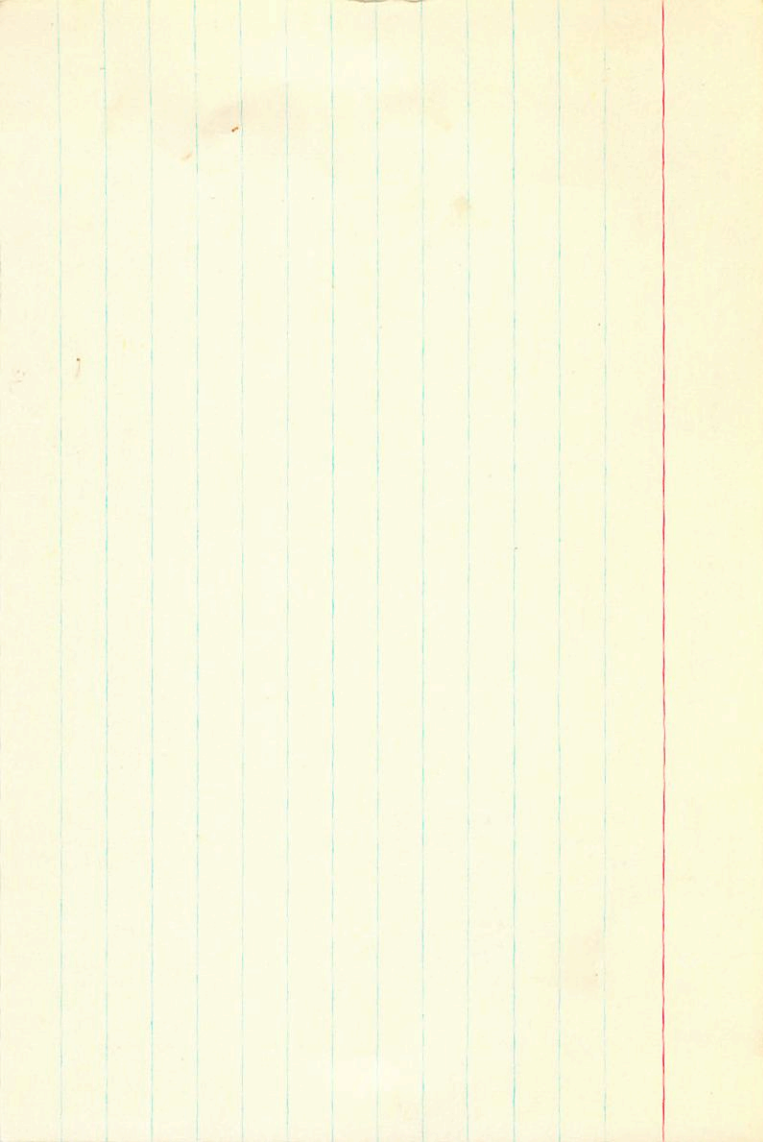
6748 93

8946 180

825 300 -425 +1250 -0.128 +1122 +20.4 -11.6

-281 953 110 -0426 -0405 -0831 -14.9 +3.0

-441 -026 -847 -0670 +0011 -0659 -53 -245



NEWEST
916219

1034 + 14 1204

518- 44 C14 h:88 -eC
22
@as

10032 + 010

10026 + 018 44050

1048 + 2
-3 + 8
10034 X 100
10034 X 100

228

+172

+45

+14

70

5.1

10967

1041

1093 + 014

525

1049 009

9898 9656
9898 9656
10000
2951
SELL
11311

-1.1
+18.1
-13.4

+2.6
-2.5

23.17
~~19.2~~

+41.8 23.3
-11.1 ~~19.2~~
-4.2 -23

222
+17.9
-15.7

40

RAD. VEL. : -8.200
 MODULUS : 251.1
 DISTANCE : 7.000
 PM. DEC. : 14.000
 PM. R.A. : 45.000
 DEC. : 17.750
 R.A. : 22.000

p1 (U) : 0.851
 p2 (U) : 0.523
 p3 (U) : -0.049
 pU : 207.523
 U : 22.549

p1 (V) : -0.270
 p2 (V) : 0.224
 p3 (V) : 0.000
 pV : -21.313
 V : -12.203

p1 (W) : -0.447
 p2 (W) : 0.272
 p3 (W) : -0.290
 pW : -40.259
 W : -0.004

Handwritten mark resembling a stylized 'M' or 'W'.

R.A. : 22.800
DEC. : 17.750
PM. R.A. : 45.000
PM. DEC. : 14.000
DISTANCE : 7.000
MODULUS : 251.14
RAD. VEL. : -8.500

q1 (U) : 0.851
q2 (U) : 0.523
q3 (U) : -0.049
dU : 207.553
U : 52.549

q1 (V) : -0.276
q2 (V) : 0.524
q3 (V) : 0.806
dV : -21.313
V : -12.203

40 q1 (W) : -0.447
q2 (W) : 0.672
q3 (W) : -0.590
dW : -46.259
W : -6.604

216380
31884
14354

22 45.4
6.1

+0148 ± 2.6
+1372
+047 ± 1.8
+048
26 9 63 +1.88

004
45
4

1600 2450
2.21 2.11

25.141 1881.8
20137 +047
50.15 1884.9

+106 +017 6c
+114 +040 6c(2)
+116 +043

also 11 m 40 / 1009
55 + 24.132

A0516317

6

id on 5.10.11
11.05.11
26.6.0
55.07.5
24.6.7.5
17.5.4
7.60
+628
24.6.4
2/9

51.9
56.60
48.80
49.26
49.36

1929.5

A 6814-14
B 6814

49.22
49.23

+099 +047

22.27
49.2 1929.7
12
49.06

29.6
49.17

-304553 875 479 110+043 +15 038 +2 099

033 012 005 036 -014 554 +0.9 +1 0 012

-9 +46 +10

+44 -16 +6

013

-9 +44 +9

+42 -16 +5

014

-9 +40 +9

+35 -14

≡

J Page
216385

22 49.9 +09 34 5.3 dFS +116a

31899

124362

+0350³² +043³⁵ N30

B

(866) 11"

+0350±1.4 +049±1.366 → N30

39±3

13" N14
20" 11"

R

+03532 +0430 FMSump

12.24

2.1

22.8
+96

10.16

524
524 +039

531

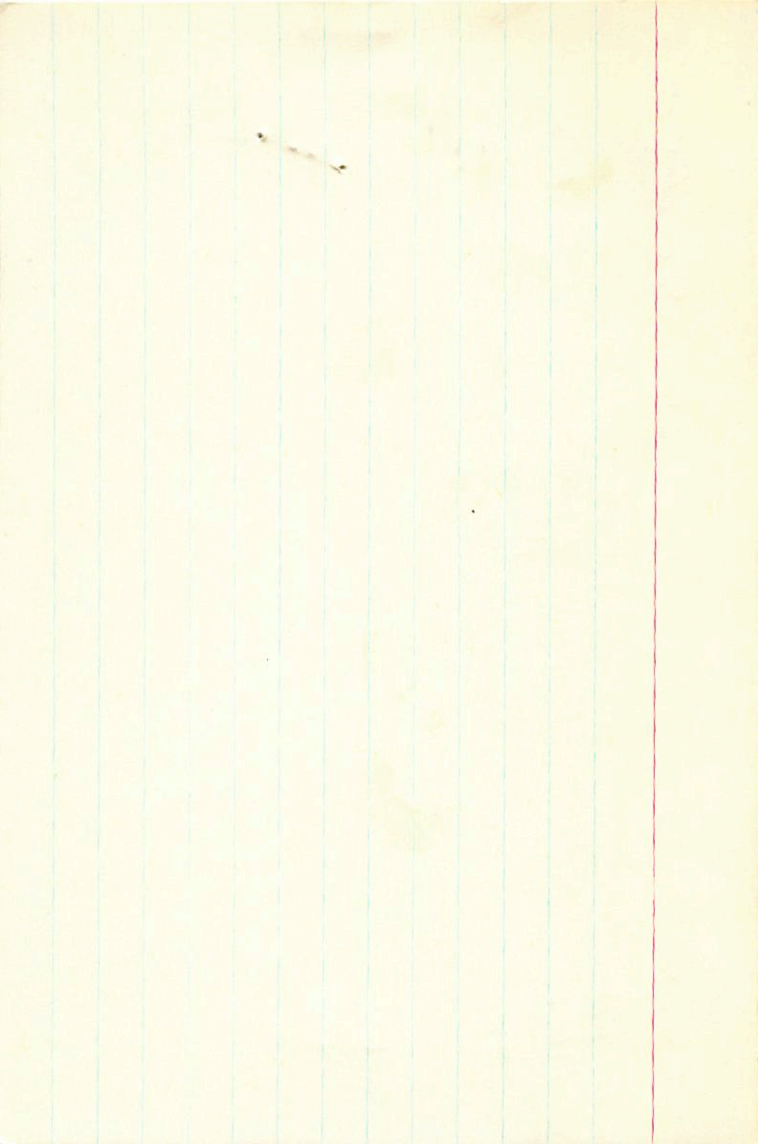
39
11.5

9247

10.51

4.45

11.6



216385 22 45.9 +9 34 F7 D ¹¹¹³ 286

HN 8697

GC 31859

49 (5) Neg

5.14 + 47 - 4 3 E 99

.321 .149 .433 ④ 502 - 2.63 /
④ out

250
174

207

369

250"

13.52 + 1.65 + 1.32 m4 595

2.00 + 5.42 - 5.8 - 32.3
+ 2209 - 564 - 570

115
135
145
155
165
175
185
195
205

115
134
153
172
191
210
229
248
267
286

255
275
295

32

29.600
9.600
531.000
39.600
1.500
20
11.600

0.851
0.511
-0.122
2295.774
42.598

-0.276
0.633
0.723
-568.858
-2.942

-0.447
0.582
-0.679
-1002.445
-27.883



B3

$\rho = 0.64$

BHP ay

22 50.5

+15 31

wt)
-260d

$$V = 10.059 - 10.79$$

$$-0.3059 - 0.7749$$

-299 954 268 864 -030 -071 -260 -019 -70 -332

-009 -006 -029 -018 043 -166 -250.6 -239 +75 001

-196 -91 -392

-280 -345 +2

004

-235 -86 -363

+266 -345 +48

0011

12R8713

216489

22

50.6

-0017 ± 30
-0012
-039

Sp. B. P = 24.65
5.7 gwt - 12.38

31908

018.3-023.7 PIC 5

-12.9 Submit

14366

34.431

+16

34 31.31

18993

85
576

-0013
+ 9
+ 3

1.32

5.64 + 12.079

34.476

-0.019 -0.24

31.37 1933.6

N/II - 289

481

36.8

14
31.51

(412)
(100)

34.457

FLY
+ m. con.

31.51 1940.10

-14
413

31.52

Weight 0.10
Kupferstein

462
-044
8987

31.52

1549

4480

1561

-1459

1054

8672

112

737

36.8

37.5

43

1085

22 512 -70 20

-10(4) (6)

216437

-01

-3 4 5

6631926

6.04 +66 1.78 6470 -2

ednd

508
96

-0055 +068 1250

-0057 +068 06 →

12.544 19084

0084 ± 3.3 +067 ± 3.0

29.24 19067

-0056 +068

00768 +0781 F104

-028

-0387

-2.0

-039 +069

2.55

44



1950

1951

1952

1953

1954

1955

1956

1957

1958

1959

1960

1961

1962

MA

216437.000*

22.000*

51.200*

-70.000*

-20.000*

-0.039*

0.069*

2.550*

32.359

-2.000

-0.164

-0.521

-4.277

0.321

-0.498

11.368

-0.107

-0.694

-2.067

44

+75⁰855

22 51.2 +75 46 9.3 d111 +38.88

31927

14371

G

+811 298₁₅

+108 → 20

+293 ± 000 +1114 003 GP

+783 +288

+114 GP

+0744 ± 8

+113 ± 8 new

+0744 ± 8

+148 ± 11 6-6

+079952.5
+0796
+148510.6
+113

13.952 1505.8
425 45 38.20 1909.5

3.532
10.420
- 599
32.21

347 1929.9

12.30
38

-18

334
3452

$P=0.32$

Surface 22 51.4 +37 40 63+63 -22.58

216598

+071 +03 Hyd.

14372

+049 MCR

743

057

10073

1010

+085

MCR

M

W

18.8

5.35

210

51.22243

+37 40 18.8

1929.7

22.429

18.61

52.5

+854 +501 6142

+3522 +0237

3759 +19.7

416

-3.2

-285

+221 +932

-1175 +0105

-1070 -5.6

-27

-21.0

-436

+937

-1798 +0397

-1401

-7.4

0

+7.4

-231

-245 956 602 751 +07 +03 -22.5 018 -14 114
 026 1 083 + 804 -39
 021 005 067 017 019 341 -17.8 -17 +5
 057 007 004 026
 -15 +39 -3 01

$$\begin{array}{r}
 -14 +48 \quad 0 \quad 008 \\
 \boxed{+41 -25 +4} \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 -17 +45 -11 \\
 \hline
 010
 \end{array}$$

40516345

22

514

441

29

412 C

5.6

150 (P)
150 P

.0206

407000

-022-011 H

-255 956 707 707 -022-011 412 -008 45.5 -038
-006-002 -021-008 009 -105 78.5 48.1-2.5 015
48.7-2.7 46.0

75 Agv
 216567
 31931
 14375

+0030 = 2.6 -044 = 2.3
 +0028 -038

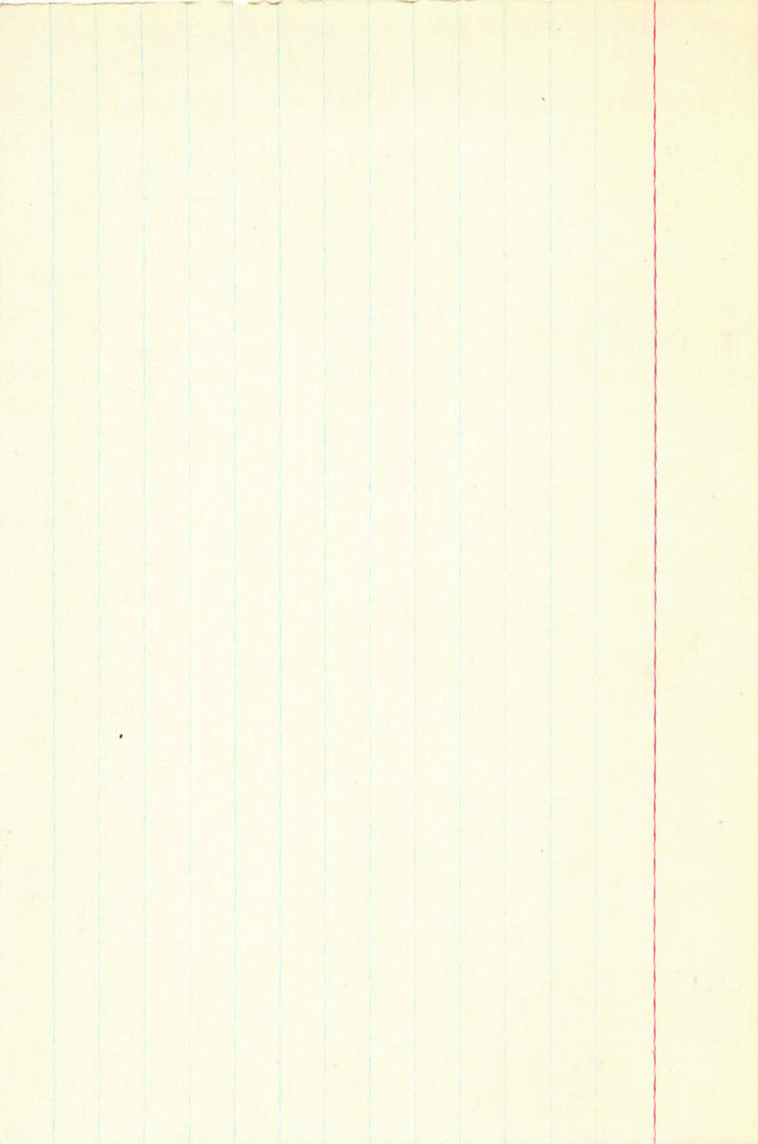
22 51.5 -12 27 7.2 g102 +4.88

28.935 1898.9 -12 27 23.09 1894.9
 $\frac{-153}{.782}$ $\frac{242}{20.67}$

9.851
 19.058
 28.909
 .882
 -16
 .866
 +100
 882
 163
 28.913
 -16
 .897

35.3

20.81 1928.80
 58.02
 22.79
 42
 37
 27 38
 38
 20.99 -1.50
 22.57 1929.53
 22
 22.35
 334 4833
 22.17 34.2
 39.3



H18714 22 52.1 +16 41 55.1

H0216672

6.28

6.28 6.3 +1.78 +1.86 (3)

R R-I

4.55 +1.60 (2)

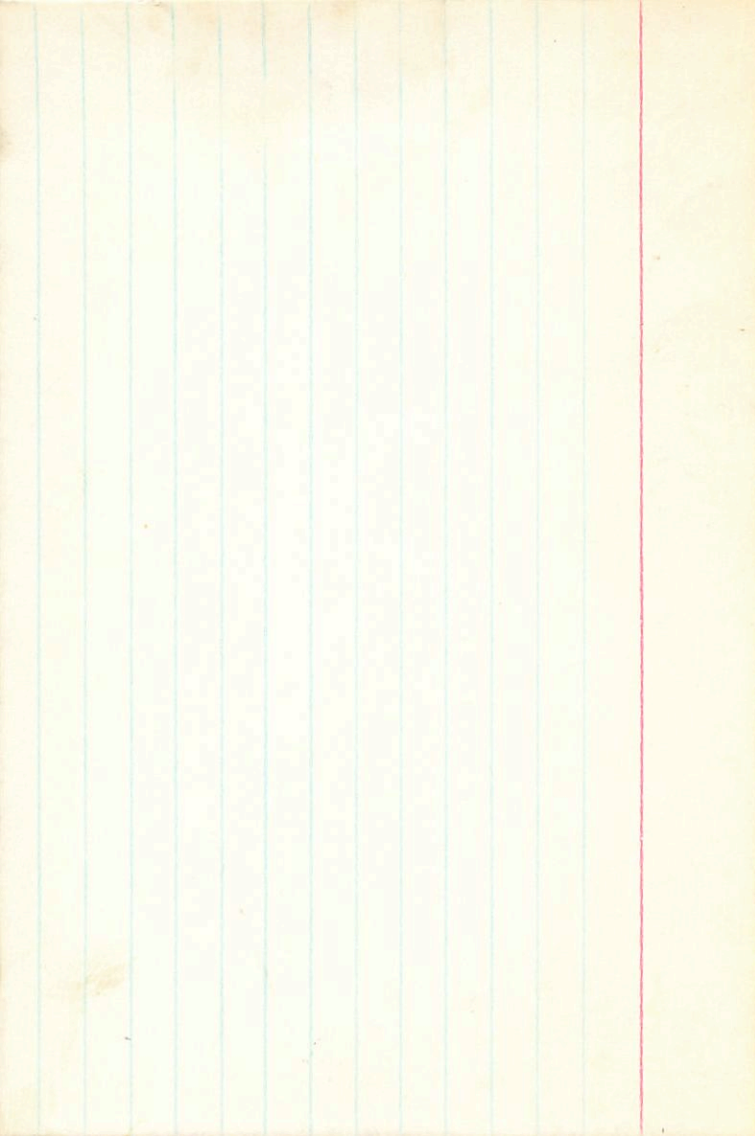
+11.0
" +0.007 "0006

2 out

+2.9 -6.9 -27.7

9.0

+13 -25 -33/1000



77 Agl
316640

GC 31544

W/14382

Y 5554

-11970 di-

GC -226 -086

22 52-1 -14 32

g124 -36.36w(5)

14±10 Y(10)

77 Hz

22 52.1 -16 32 5124 -36.38 W(10)

216640

GL 31944

5.56 H.M +1.09 122 II R

W14382
45554

-0152³² -082³³ 030

W(1.8)

-1706619

-0154±1.9 -087±2.2 GL 7130

-226 -086 GL

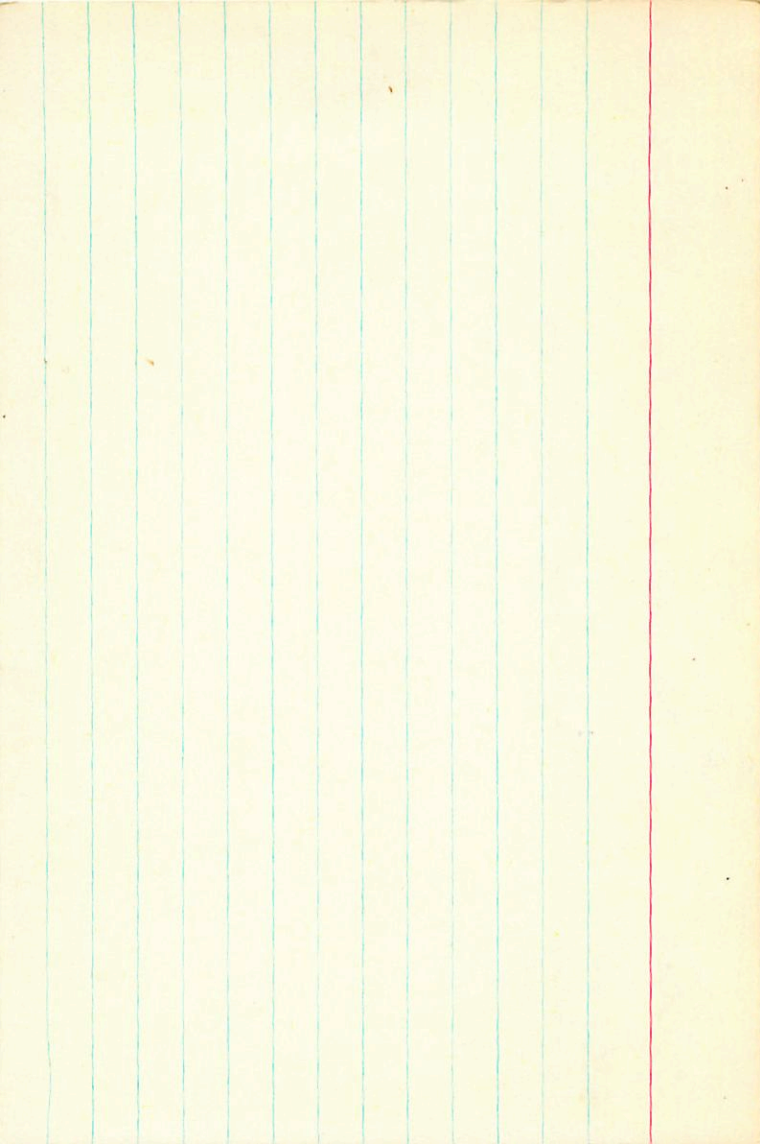
-219 -082 130

-220 -083

-42 -16 +48 .020

-95 -17 +65 .010

14±10 Y(10)



8736

22 5-2.3

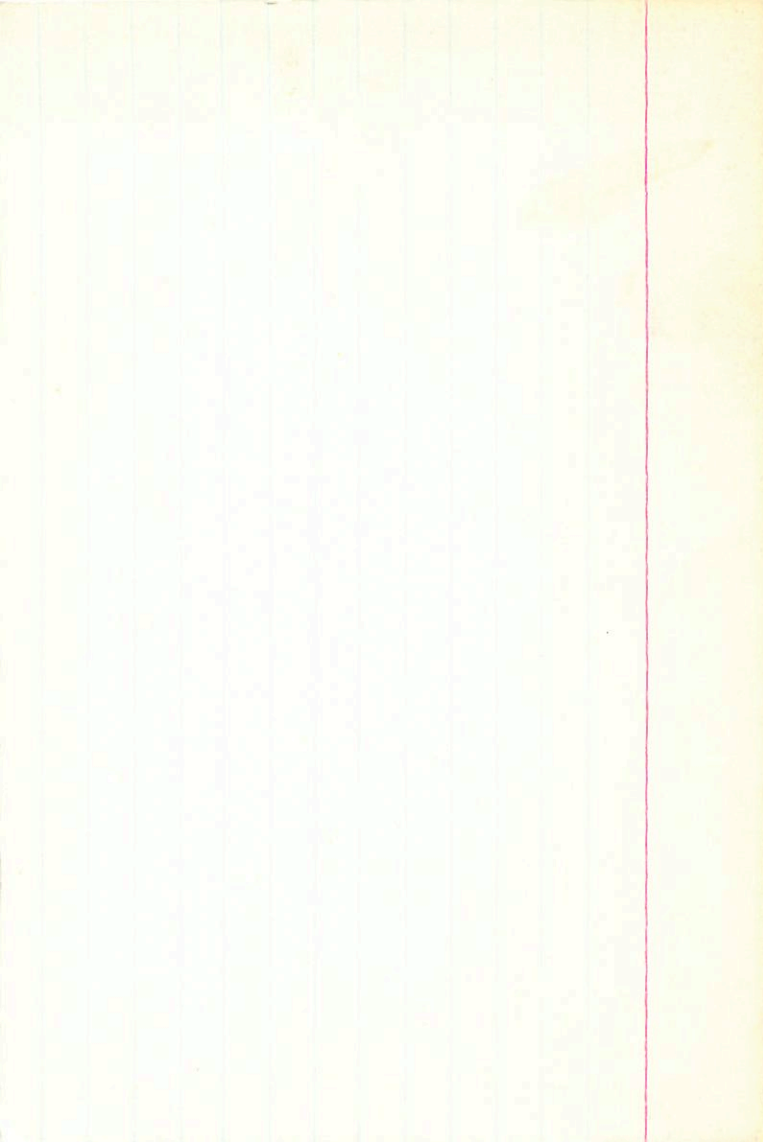
+8506

6.0

NS

+007+112.62

-30d



216656

22 52.4

-48 46

F5

+3 d c (1)

GC31552

-0223 +053

44

B-V

6.67

+0.03

Cape

W18384

-0224 +054

5

B-V

+9.71 S.E.

Y5553

-0227

5

B-V

-49 01358 617

-0231 +058

5

B-V

S05 6.7:7.0 95"

-22.85

5

B-V

7.6:8.0 0.2

-0229 +056

5

B-V

7.6:8.0 0.2

-0233 +058

5

B-V

GC

-234

+059 B

220

1057

~~239~~ ~~784~~

~~+23~~ ~~+85~~

~~-0223~~ ~~+0.59~~

GC

-224

+055 A

220

1057

~~211~~ ~~+37~~

~~+6.2~~

~~+6.2~~

42.6

-230 +049

A 6.66 +0.46 - Cape

BC 7.02 +0.57 -

22 8 (10)

8 c (17)

14.5

898 -9840

4530 1783

2357

-1072

-0.64 0.29

718

204 260 175 327 (1)

to

July 505 144 422 1

to 29 June

216656(50) 22 52.4 -48 45 65- 46 d C(11)

G-631952(50)

W4384(50)

A 6.67

+0.43 Cape

G-0 73 d C(11)

75553 95"

Under 347 7.02 +57

A -224³⁴ +055³⁴ G-6

B -234³⁹ +059³⁵ G-6

July
-0238 +053 AB

A -226 +069 B

B -222 +075 C

-43 -18 +19 .020

-96 ~~43~~ +39 .010

55 54

-49 -

22 45 217

11 24

Both chambers

nm no

-0237 +063 22.85

-0731 7056

9.6

13-2-22-24

22.4 (6) 100

22.5 (7) 100

ASOT 8CC -

752 660

25

65-80 172 0.28 212 mile

1900.8, 1947 0.45 2I

14.7 1943 0.40 1I

16.8 1962 0.32 3I

26.7 193 0.18 6B

27.9 206 0.14 4B

52.87 155 0.193 30I

52.70 165 0.23 10

48.83 152 0.20 4B

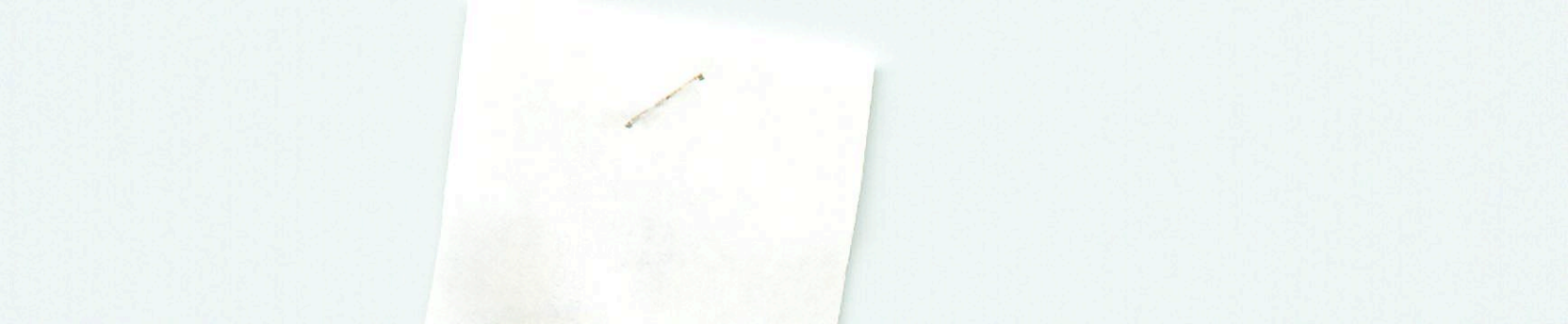
56.88 167 0.23 30

52.87

44.94 320 0.15 3B

48.82 4: 0.12: 2B

56.88 101 0.12 3B 64.90 < 0.11 14(I)



22.85
148.75
1046.00
34.00
2.00
12.00

77.73 349A 0.15 30cmA

216656 22 524 -48 46 6.7 65 +6d1c

75.91 170.5 0.40 2WMB 7.0 60 +3d1c
AB

740.8 185 0.45 2I
14.7 184 0.40 1I
16.8 186± 0.3± 2I

W-M=3.0
4.0
M V W
+34 +21 +31
+55 +34 +20

26.7 193 0.15 6B 44.84 320 0.15 3B
27.9 206 0.14 4B 49.02 4± 0.12 2B

29.75 224 0.14 2B 54.54 2.10 14
30.91 248 0.12 2B 59.55 2.12 14

31-36 Touchdown 3B 56.86 101 0.12 3B
39.74 325 0.16 3B 64.90 114
45.31 332 0.21 2B 64.33 26.1 0.15
48.83 332 0.20 4B 64.65 40.5

52.70 345 0.23 14 6.71 +0.45 -0.05 7.45 +52
54.89 336 0.20 14 0.20 8mpA +12 3.12
56.88 347 0.23 3B 15.80 1721 7.09 +0.56 +0.01 7.84 +64
59.45 344 0.27 14 64.35 348.4 0.28 B 2- 11.90 29.4

21552 21.760 1605.1
-022667.3 405555.6
-0234 4056

1.015
22.775

2.21
36.74

-34.13 1602.5
3.653

1.164
23.043

-0236290 405955.3
-0240 4056
-0.48 1792.8

-337
3.85

22.004
-50

(429)

24.54 1440.62

14
34.90

460.9
48.0

51.346
2812.5

(42.1)

0.52 1629.34

58.52
2.08

21.9
54

1539
70

33.80
-21

(45.5)

1.59
1.50

21.636
-51

9177
905

3401
-21

1455.41

3.51
3.35

00.30 1456.10

565
565

~~5005~~
11005

2420
2.54

21.765
-51

714
4065

22.032
-1.0

208
1.04

8549
42.7
(44.9)

1 Pac

216701

22

52.4 +00

48

6.0 A3 +12.88

31954

14384

25.954 1898.6

+0

47 52.48

14333

$$\begin{array}{r} -062 \\ \hline 892 \end{array}$$

$$\begin{array}{r} -28 \\ \hline 52.20 \end{array}$$

$$\begin{array}{r} 25.930 \\ \hline 945 \\ \hline 15 \end{array}$$

$$52.35 \quad 19344$$

38.8

$$\begin{array}{r} 25.953 \\ \hline 944 \\ \hline 944 \\ \hline +052 \end{array}$$

$$52.51$$

$$52.41 \quad 1940.38$$

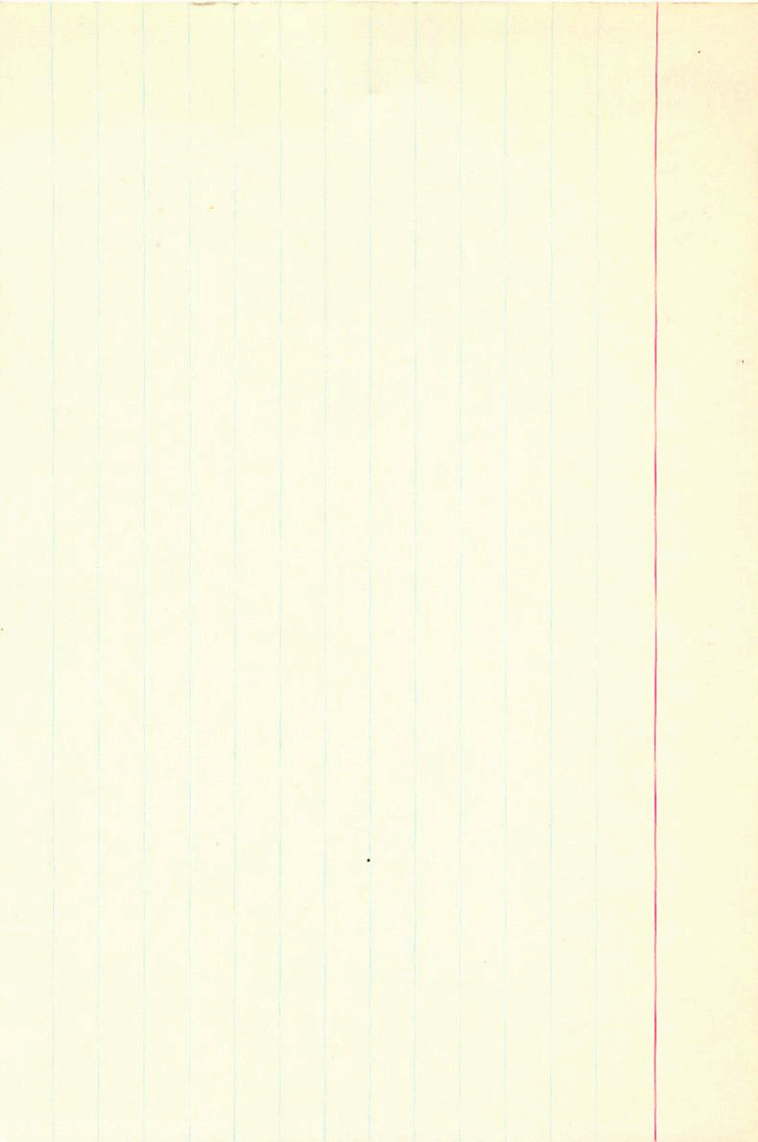
$$478$$

$$52.59$$

$$57.4$$

44.1

$$\begin{array}{r} 52.55 \\ \hline +135 \end{array}$$



216718

22

$+0019 \pm 2.9$ -00.1 ± 2.5 -51 (3)
 $+0017$ -004
 52.4 -05 15 5.9 967 -886

31960

14390

35381

18993

-5

15

16.68

1400)

~~AD516365~~
 6-8 0.4

-096
 \hline
 $.285$

05
 \hline
 16.63

17.619

17.750

35.369
 \hline
 15

$.354$
 \hline
 -16

328
 \hline

35.364

-14
 \hline
 350

344
 \hline
 $+059$

35.6

16.39 1929.27

5878

1761
 \hline
 40

17.21
 \hline
 25

16.83
 \hline

16.96
 \hline
 29

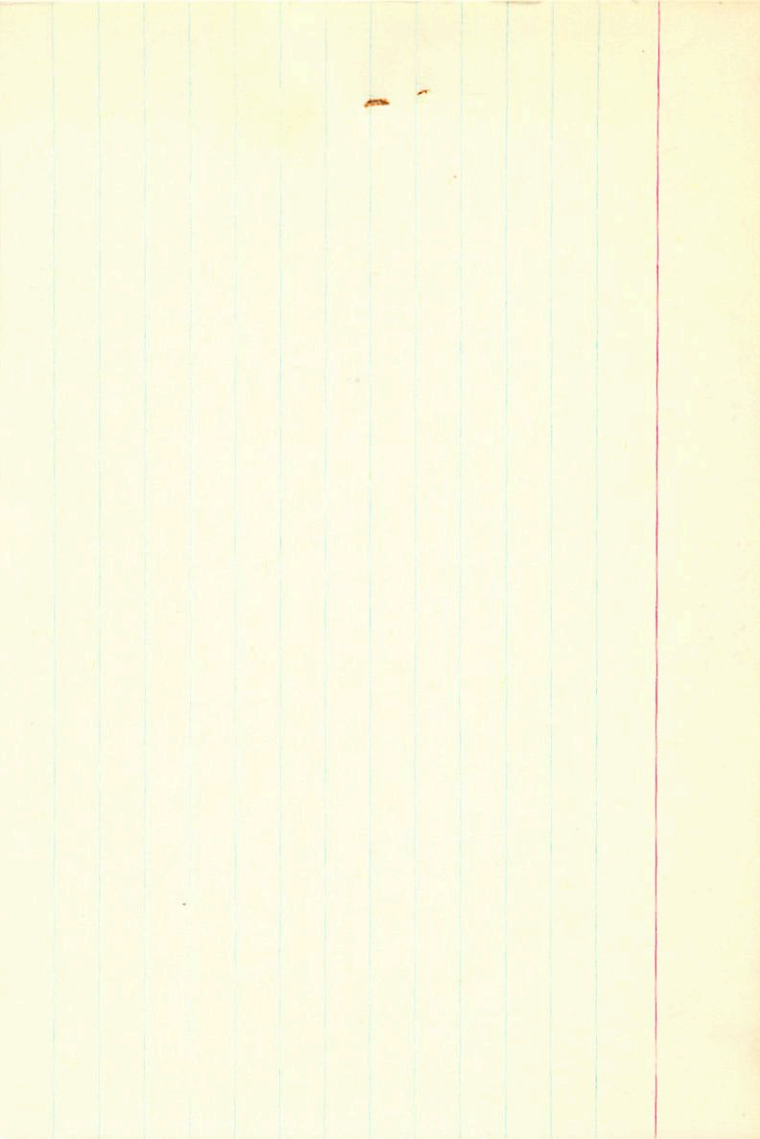
16.69
 \hline

1940.67

14.76
 \hline
 -1.13

6989
 \hline
 34.9

34.8



216756 22 52.7 +36 49 6.0 123-27.56

31964

14392

(678)

+006339 +009411130

+0070536 +01253.3 66 → 1130

W35D

+00644 +0109

+00649 +0101

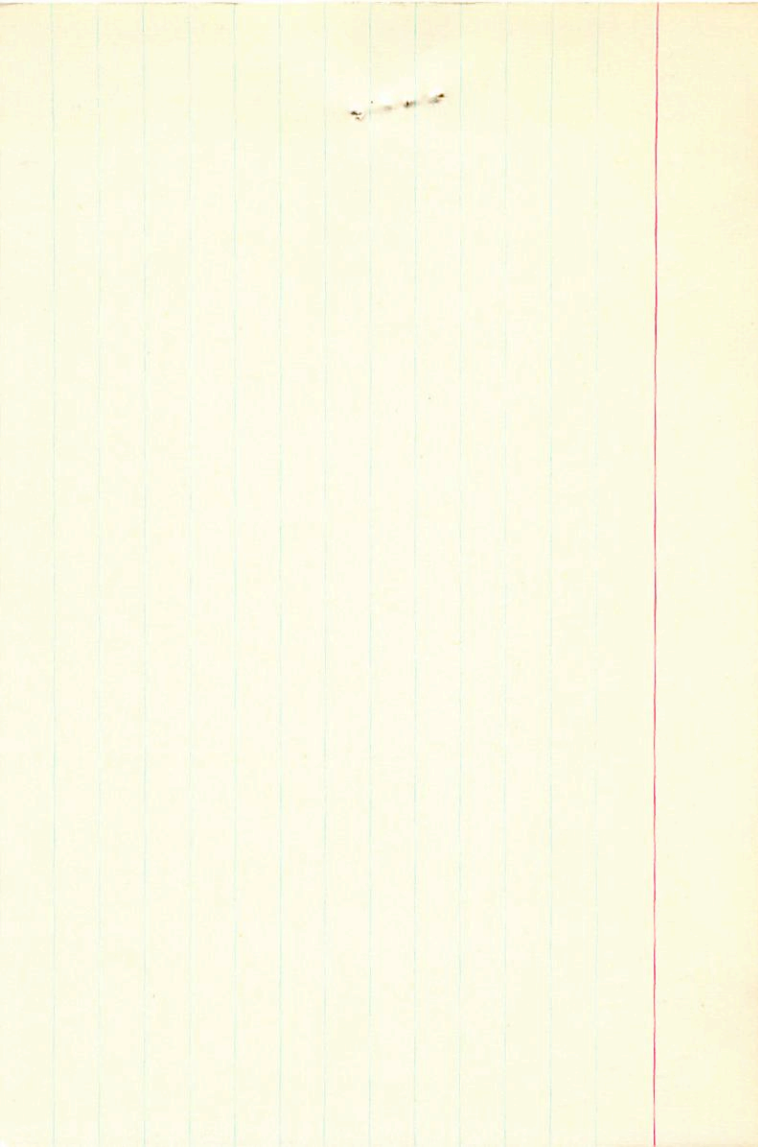
22.9
+36.8

110

+6
3.2

-27.5

0980
080 +006



22 52.7 +36 49 F3

216756

4178718

6231564

585 +37-5 3546

75

49

132

+33

1 69

175 ~~11~~ 11

⁴⁹
273 138

87

956

530 3506 2.674

(4) 6+

3.00: +10.1-25.7 +3.9

~~101-104~~ -140

012
345
678
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99
100

276

AD. VEL. : -27.200
 MODULUS : 44
 DISTANCE : 3.200
 PM. DEC. : 0.000
 PM. R.A. : 100.000
 DEC. : 30.000
 R.A. : 25.200

U : 10.375
 Ub : 338.274
 p1 (U) : 0.829
 p2 (U) : 0.497
 p3 (U) : 0.143

U : -30.037
 Ub : -104.042
 p1 (V) : -0.292
 p2 (V) : 0.237
 p3 (V) : 0.227

W : 3.250
 Wb : -138.339
 p1 (W) : -0.427
 p2 (W) : 0.332
 p3 (W) : -0.348

R.A. : 22.900
DEC. : 36.800
M. R.A. : 100.000
M. DEC. : 6.000
DISTANCE : 3.200
MODULUS : 44
D. VEL. : -27.500

q1 (U) : 0.856
q2 (U) : 0.497
q3 (U) : 0.143
dU : 338.974
U : 10.875

q1 (V) : -0.292
q2 (V) : 0.237
q3 (V) : 0.927
dV : -104.042
46 V : -30.027

q1 (W) : -0.427
q2 (W) : 0.835
q3 (W) : -0.348
dW : -138.339
W : 3.520

9723

22 53.4

+36 05

87 11

216831

3.28

5.73 05 -39 +10 30

000 090 624 2.714

$\frac{180}{509}$

5.45

+0.9

$\frac{-1.1}{6.55}$

3104
+019 +009

8104 +022 +005

47

4002
4005
05

-00146 2.7
-0015 -05

216553

22

54.7

-54

37

36996

41.885 1859.1

14406

071
956

39.94

1927.79

24257

17.6629

41.914

936

91

900

-056

41.609

1.66

369

52.00

1223

39.79

39.76

39.71

40.76

40.10

40.58

40.38

39.1

39.92

39.6

39.72

+ 2

1941.40

10.591

36.0

193.672

10.591

36.0

140.6



0.135

20.754

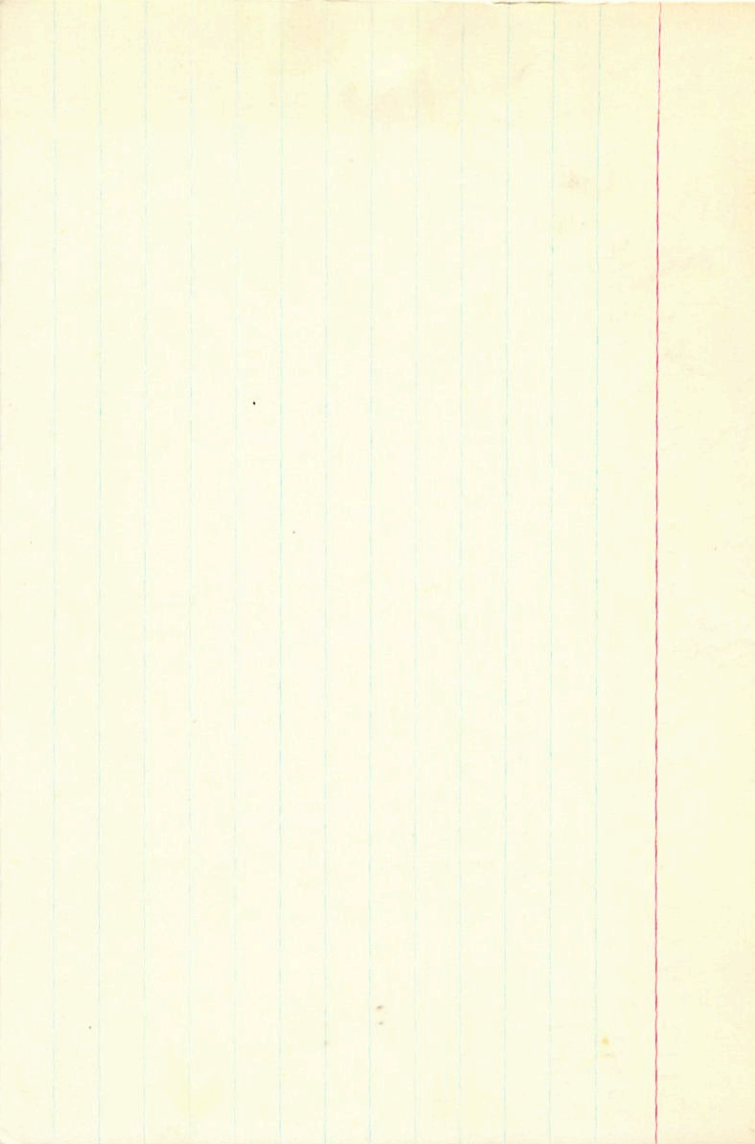
24
24

150

0.025

0.357

-5.442

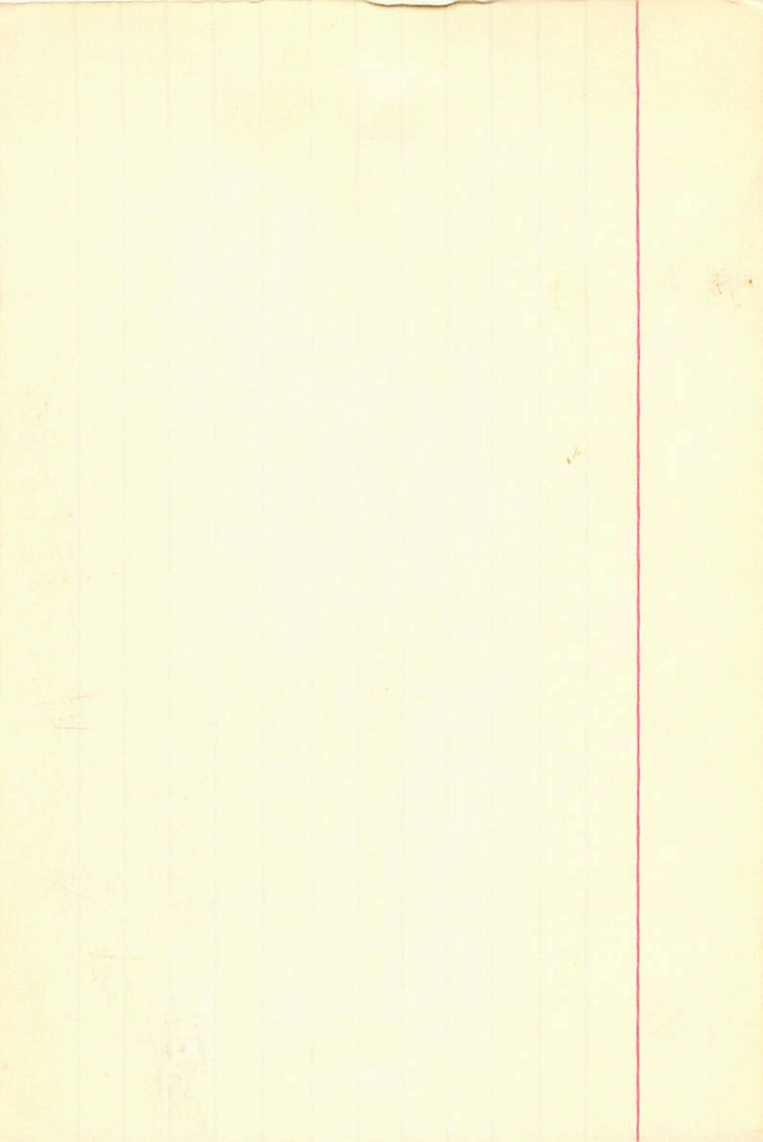


TPX 22 56 - 95 22 00 0.5
0

"
" 0.192 - 0.019

1000000000

857 239 - 457	20867	5550	9245 + 724
- 294 956 - 053	- 2882 -	9120 -	- 5091 - 80.9
- 424 - 181 - 888	- 3889	+ 0418	- 3441 - 34.



2 Pac

217264

32037

14424

10616431

$+0054 \pm 23$
 $+60$
 22 56.9 +00 42

5.6 gNI - 12.78
 -176.5

53.623 1897.6 +0 41 43.69 1898.9
 -283

$\frac{340}{.}$

3.42

$\frac{4711}{}$

+94
 -66

53.550

$+15$
 $\frac{565}{}$

$\frac{574}{}$
 $\frac{574}{}$

53.595

-15
 $\frac{582}{}$

$+23$
 $\frac{4}{}$

$\frac{28.8}{}$

44.62 1933.8

$\frac{16}{}$
 $\frac{44.78}{}$

44.89 1939.13

129

$\frac{23}{}$
 $\frac{44.62}{}$

$\frac{44.70}{}$
 $\frac{44.70}{}$

$\frac{2.41}{}$

36.4

37.5



+27.56

8744

22 57.0 +52 23 626.12

$$\begin{array}{r} -034 +0286-6 \\ -3 \\ \hline -037 +030 \end{array}$$

48.

1

Hydro

1

8744.000*

22.000*

57.000*

52.000*

23.000*

-0.037*

0.030*

6.000*

158.489

27.506

-0.089

0.278

-6.485

0.050

0.954

34.156

0.201

-0.114

28.777

48

-0010 ± 2.9
-0009

+004 ± 2.6
-001

217251

22 57.0 -13 20

6.3 gms + 12.7 g

32038

14425

57.732
 $\frac{0.51}{783}$

1899.4 -13 20 21.36 1895.9

$\frac{-22}{21.58}$

38.752
19.038
57.790
 $\frac{766}{746}$

35.9
 $\frac{36.5}{36.5}$

23.74 1926.97

150
 $\frac{29}{22.37}$
85

751
 $\frac{751}{-032}$

34.40
 $\frac{12.71}{22.13}$
 $\frac{2.6}{+5}$

21.4
 $\frac{21.62}{-04}$

26.189

31.602

57.794

$\frac{-37}{750}$

57.773

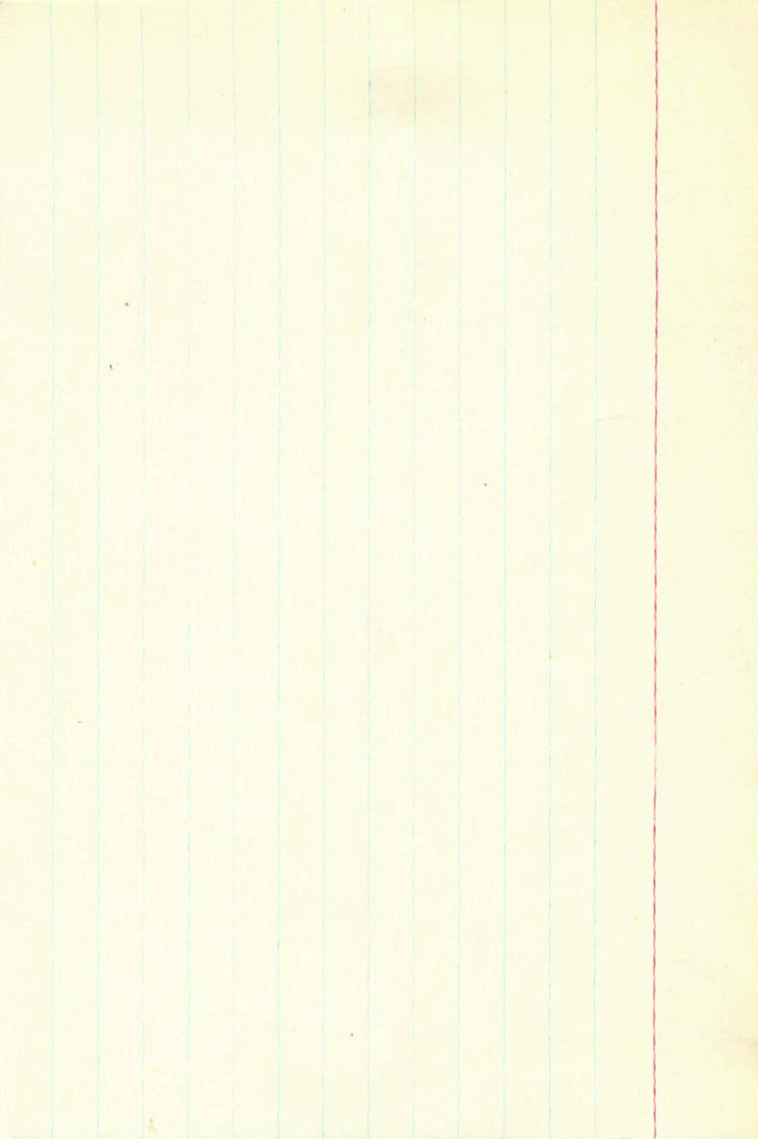
21.59
 $\frac{22}{21.37}$

1939.44

35.7
 $\frac{39.8}{39.8}$

1941.17

21.37 1940.7



+6801345
22 57.0 +68 45 dno 240w(3)

GC32040
W14127
75574
+6801345
8.74 + 0.78 + 0.42 KOV R

$\delta = -03$

241-02

+135 -83 +6 .020
+709 -75 +5 .024
+86 -65 +3 .030

+1084 ± 9.0
+1085
+1083
+589 ± 4
+583 ± 0.00
+5
588
+299 ± 15.0 GC
+299 ± 4 GP
+292 ± 3 GR
-1
+291

+589 +299 GC
+580 +294 Gms
Astr.

+27 A(28)
+9M(8)
-16(4)

18 ± 5

0.891 1908.8

~~4.466~~

~~5.357~~

56.425

58.56

33

6188

2572

+ 1084590

+ 1042

+ 299515.0

+ 68 45 2950 19049

- 13.48

16.32

23.65

- 1.55

23.1

1529.8



11

8723.000*

22.000*

53.400*

36.000*

5.000*

0.022*

0.005*

6.550*

204.174

-576 ~~0.900~~

0.101

0.135

20.754

-0.024

0.924

47

-4.150

-0.025

-0.357

-5.442

216953

31996

14406

-00146 2.7
+0015
-0015
05 54.7 -05

05 6.4 966 -8.78

41.885 1899.1 -5 4 39.56 1895.4

$\frac{071}{956}$

$\frac{-38}{39.97}$

24.257

17.6429

41.944

935

917

41.906
14
-562

900
-056

10.657

31071

41.928

$\frac{-38}{888}$

36.9

52.00

1223

39.77

+6
39.71

40.76

$\frac{60.10}{40.56}$

40.38

$\frac{40.18}{8}$

40.38

39, 193872

39.927

29.65

1927.79

39.72

+2.2

1941.40

10791

36.0

40.6