

+29.3029

17 23.7 +29 31

61

Y 3975

+29

17 25.5
27.4229

+29 26.58

AUS 10585

9.5 } 0.5
9.9 }

60 M(8)

46 YK(8)

48 S(7)

93

Binary

W10114

-195 284 L

-106 276.8623

-213 285 Y

-176 M

8.03

79.7

79.5

9.0

100W

-7.784W

dmo

9.01 + 1.14 + 10.64 (5)

AD

M

8.31 + 1048 (3)

bin 232 m
922 m
922 m

-230

285

Bin 50 38 42

6.0
0.60

-9.0

-202 -283 Y

-10 -6

-1 +4

-0.200 -0.285

1.95

-9.0

9580 -6288 347
6121635 -7776 4068
2222

-195 -278

12 37.7
1.80

61.000*

17.000*

27.400*

29.000*

27.000*

-0.211*

-0.285*

1.950*

24.547

2.2

-492 4W

NR6578

17 376 -2 08

AD160471

GC23953

W0206 160

~~0488~~ 453-891
634 758 323
-896 409 256

+0015 -0236
-0557 -0395
+0882 -0245

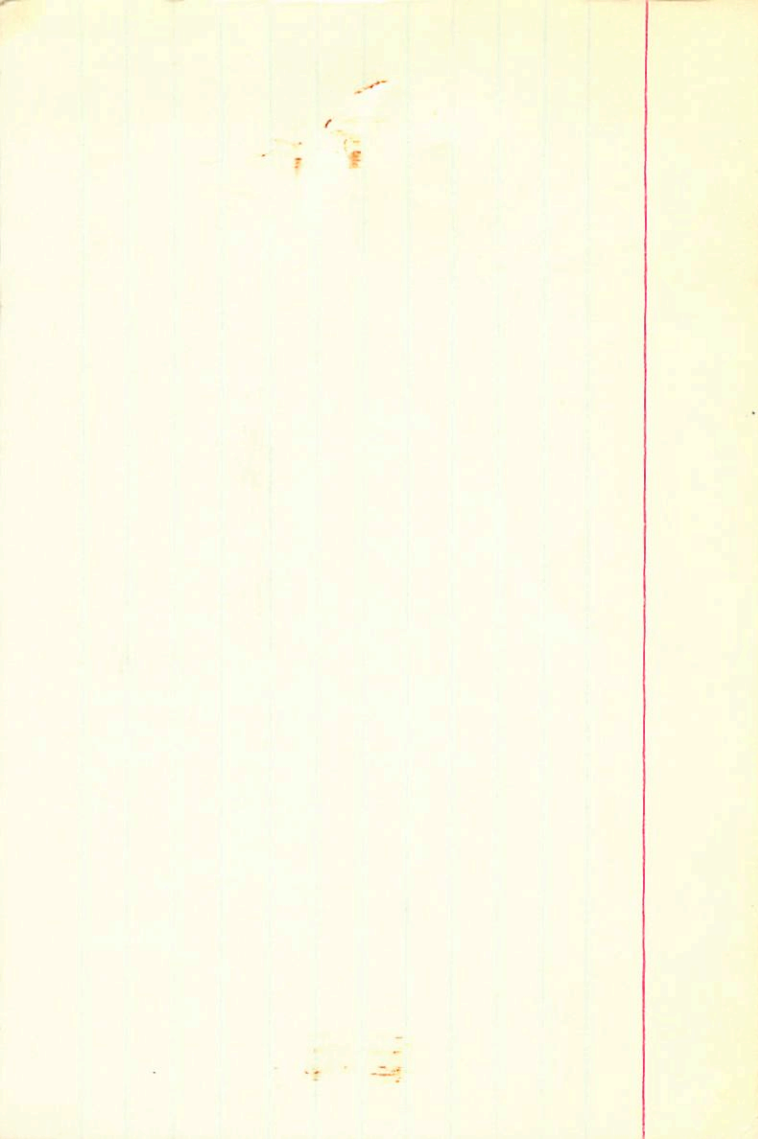
-0017 ±3.8 -021 ±0.7
-012 36.44 1408.2

064
727
-0017 -016
-0015 -011
-022 -011
45.56 1504.14

35.743
-4
739
51.75
3731
793

35.95 1933.96
-4
36.01

-3.9 +43.6 +40 35.17
-17.1 -18.3 -35
35.84
+11.5 -12.5 -1
35.71
-30



6194/5

14 38.1 .74 18

A5 / A0

109 1026

15039/5

22428/30

5.5
5.11

10008 10004

10001 10001

10001 10001

13/0

16.6
9.7
14
17

10001 10001

2.5
2.10

5.78

-0.1 -0.8

141 141 141 141

5.80

150.1 150.1

143 143 143 143

6.93

1.025 1.025

143 143 143 143

6.94

155 155 155 155

145 145 145 145

550

381

486

948.2

641

868

9=2

181

5.10

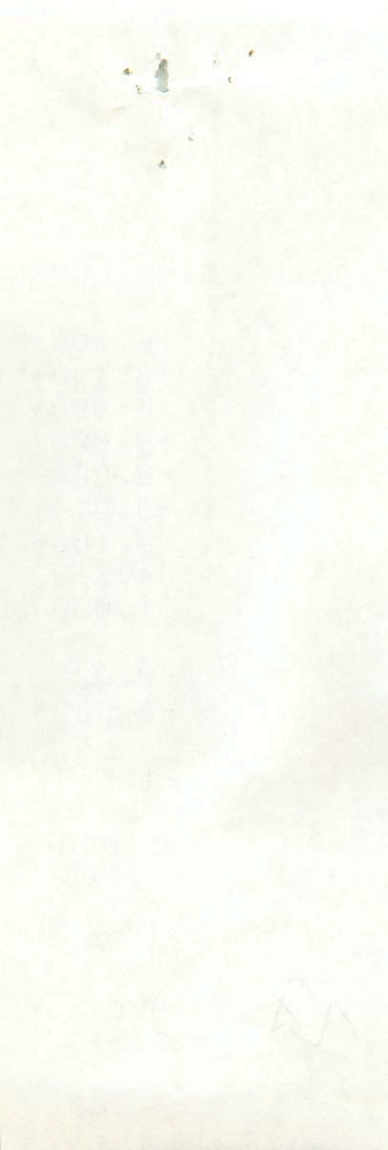
1470

1470

1470

1470

27



6195.880*

16.000*

38.100*

4.000*

18.000*

-0.004*

-0.014*

5.100*

104.713

-31.000

-0.032

-0.802

21.568

-0.060

0.305

-15.703

-0.014

0.513

-17.363





Handwritten signature or initials in the bottom right corner.

14.600

4.300

1.000

-8.000

5.200

110

-31.000

-0.250

0.545

-0.000

-21.852

22.410

0.621

0.724

0.299

-24.525

-11.950

-0.742

0.422

0.520

-19.527

-10.259

27

+9 +4 +114

159964 17 38.3

23471

2.125-0.6

+0007±8.7 +108±6.0
+0018 +109

-72 12

+0.6
000

+

F8E +35.0±0.3
+0.46 1.60 5.4

18.346
-035
1.311

1899.9 -72

11 59.27

1892.5

-6.21

000 +109

05.48

+018 +110

-607

18.079

1.85

18.260

1.84

.3-2)

363

18.388
-1.46
16.928

+0012 +1085

+00155

+00070 +1147.4

+0126

009 +109

10.84

53.90

4.74

4.27

3.47

1.31

1.16

1529.3

59.5
0.5
59.45

NO

10215 17 38.8 731 19 6.440 -6.16

23989

6.34 + 1.05 + 88

B058115

113'

-0056 ± 43 -077 ± 3.6
-0053

48.100 1902.7 1901.2
245
.365
46.76
376
5052

-072 -075

48.20

+19

679

= 146

48.5 1900.9

-34

48.16

-2.36

10215.000*

17.000*

38.800*

31.000*

19.000*

-0.072*

-0.075*

6.000*

158.489

-6.100

-0.304

-0.496

-45.125

-0.333

0.731

-57.289

0.199

0.468

28.620

28

28

第 一 章

第 一 章

第 二 章

第 二 章

第 三 章

第 三 章

第 四 章

第 四 章



ADS 10715
 160835 17 390
 23999
 10219

-0017 + 2.2
 -0021
 +24 32
 16" / 8.8
 14" / 8.8
 2.146 1897.0 +24 32 121.22 1891.9

090
 236
 2.155
 159
 150
 2.159 -077
 +3
 102

36.9
 0019 +0505
 -00165 +0875
 -225
 -019 +058
 10.79 1928.41
 -23 47.75
 10.56 33.9
 11.07
 11.99

11.85 1939.31
 -27
 11.58
 10.79 1928.41
 -23 47.75
 10.56 33.9
 11.07
 11.99

11.99
 11.99
 11.99
 11.99

37.5
 430
 32.21
 25C

14" / 8.8
 14" / 8.8

16.85 1939.31
 -27
 11.58

10.79 1928.41
 -23 47.75
 10.56 33.9
 11.07
 11.99

10.79 1928.41
 -23 47.75
 10.56 33.9
 11.07
 11.99

11.99

$$-0006 \pm 4.2 \quad -013 \pm 4.1$$

160781

$$17 \quad 39.1 \quad +0001 \quad +06 \quad 20 \quad 6.0 \quad 967 \quad -31.08$$

23991

10220

$$5.904 \quad 1892.1 \quad +6 \quad 20 \quad 12.50 \quad 1893.3$$

$$\begin{array}{r} 035 \\ \hline \end{array}$$

$$\begin{array}{r} 939 \\ \hline \end{array}$$

$$5.932$$

$$\begin{array}{r} 11 \\ \hline 943 \end{array}$$

$$\begin{array}{r} \hline 942 \end{array}$$

$$5.923 \quad +003$$

$$\begin{array}{r} 18 \\ \hline 941 \end{array}$$

$$\begin{array}{r} +74 \\ \hline \end{array}$$

$$\begin{array}{r} 13.24 \\ \hline \end{array}$$

$$13.23$$

$$1933.1$$

$$\begin{array}{r} -13 \\ \hline 13.10 \end{array}$$

$$13.53 \quad 1936.38$$

$$-13$$

$$\begin{array}{r} 13.40 \\ \hline \end{array}$$

$$\begin{array}{r} 13.25 \\ \hline \end{array}$$

$$000$$

160950

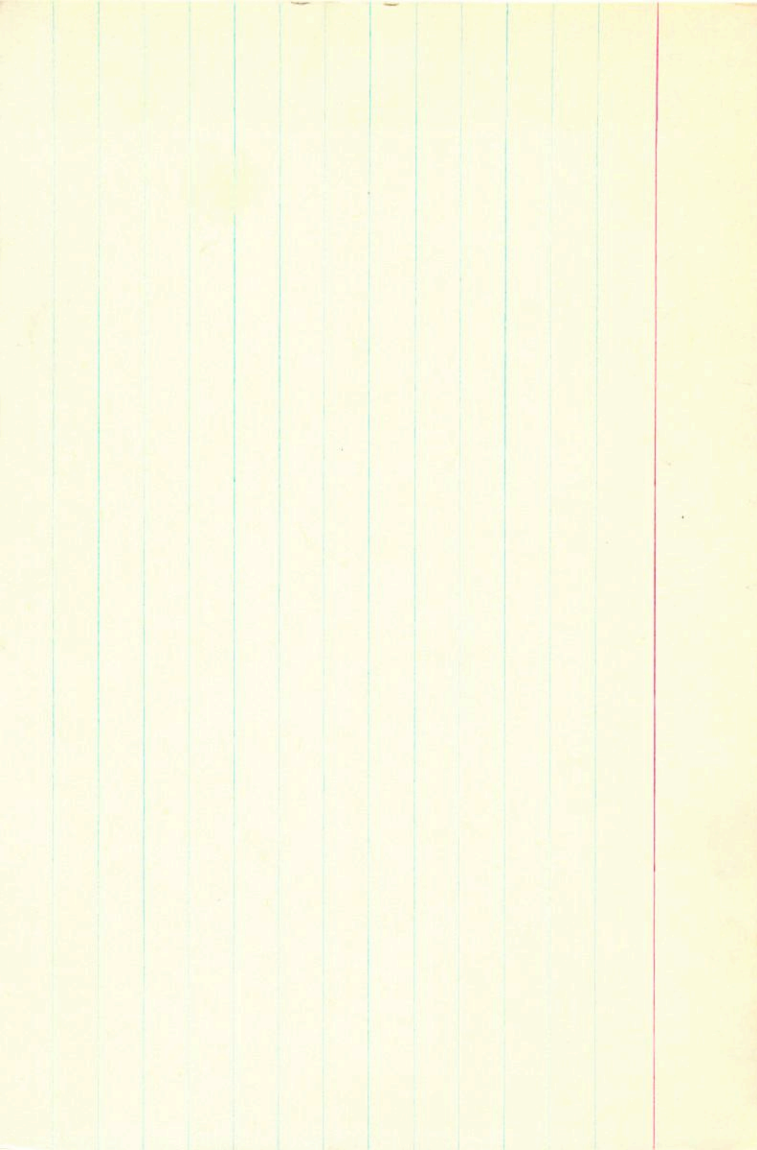
17 39.1 +43 30 6.7 112 -29.28

23993

+0050" +058" N30

10222

+0046±4.0 +061±3.0 GC → N3.0



V703500 17 34.0 -32 30 -53 0.115

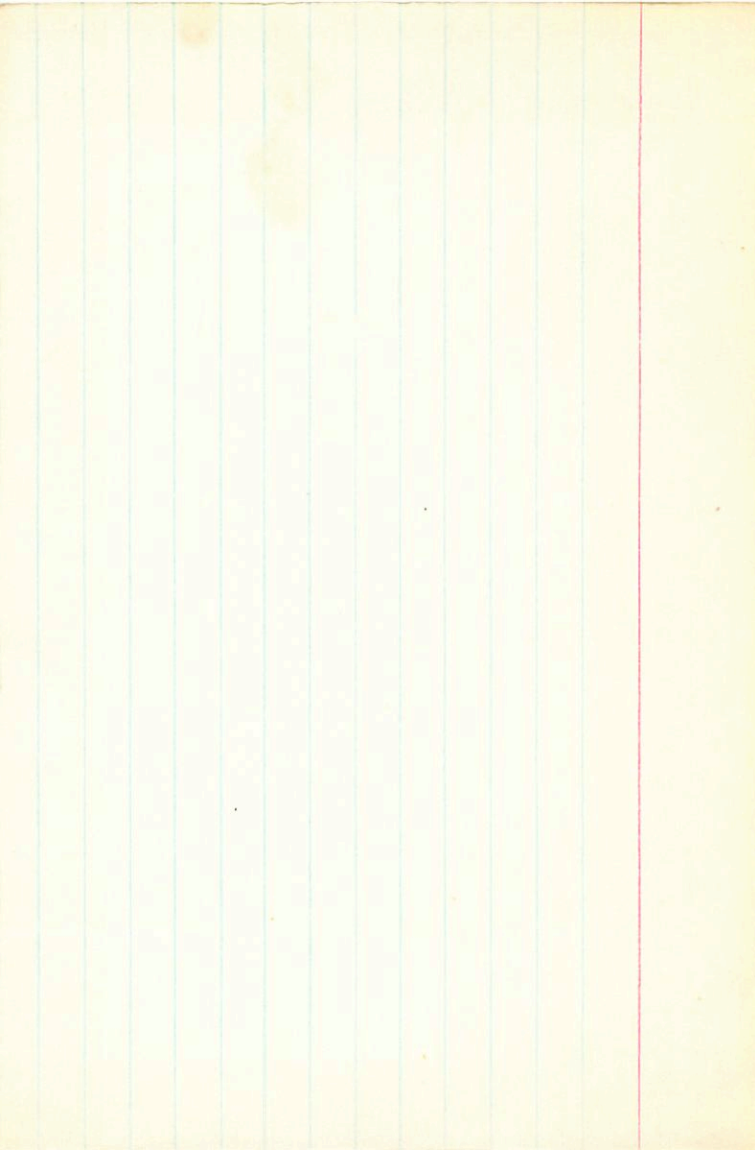
160509

132.4754V

7.8 +0.36 +0.07

0.115

.224 · 159.869 2.752^② 10,7,28,8



3.4

MRM 19

17 39.7 +15 58 d=1

160910

HR6594

GC24009

5.55 +38-05 3595

1258 .55 .541 @SFC 2680

Dist

205
TMM +112 hmdt
TMM +112 hmdt

6

[m] 20/17
19/h
lit

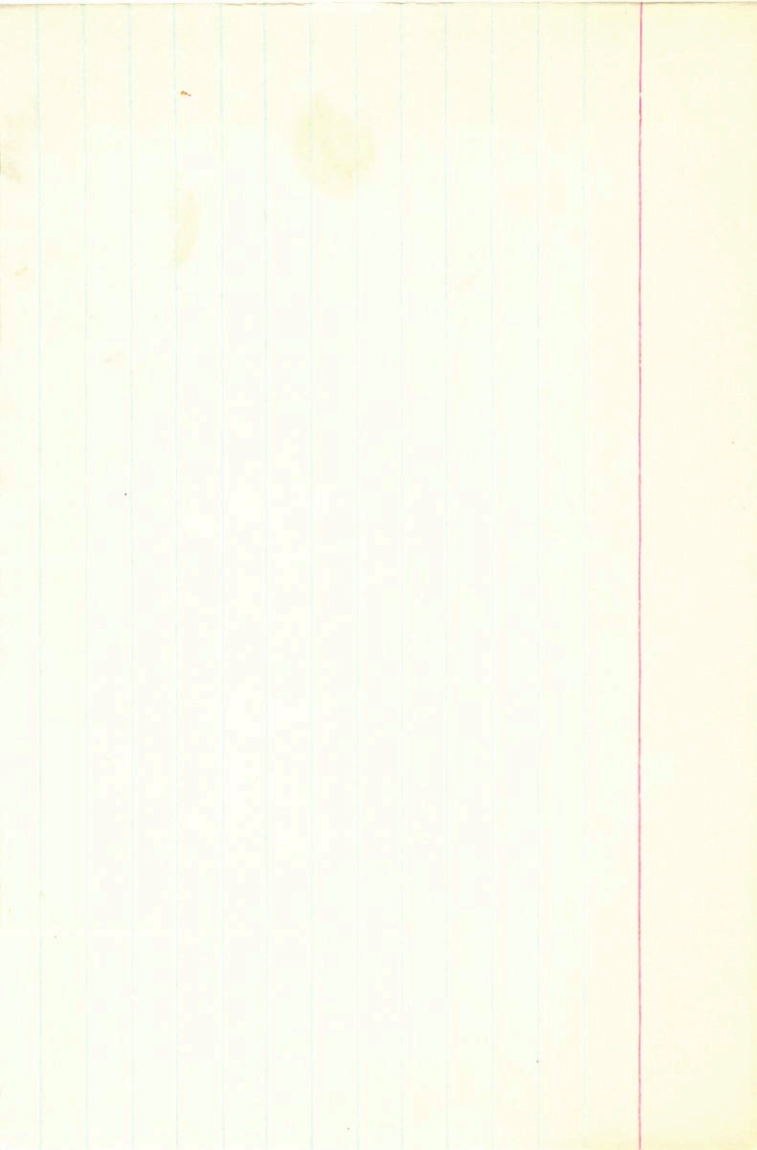
[C] 489
2.50
1283/

+42.2 -15.6 -11.9 1000+

011

+355 +324 +148

6506-
9236-936h
8892



A0510723
11^m 11^q

+0004±2.1
+0005

+096±1.9
+107 (5.6)

160910 17 39.7 +15 58 dF1 -43.78

24009
10229

43.917 1907.1

+15 58 25.69 19042

-017
900

-4.40
21.29

43.928
929

24.52 1933.5
24.50

±13

29.3

43.909

25.27 1939.32

-9
900
914

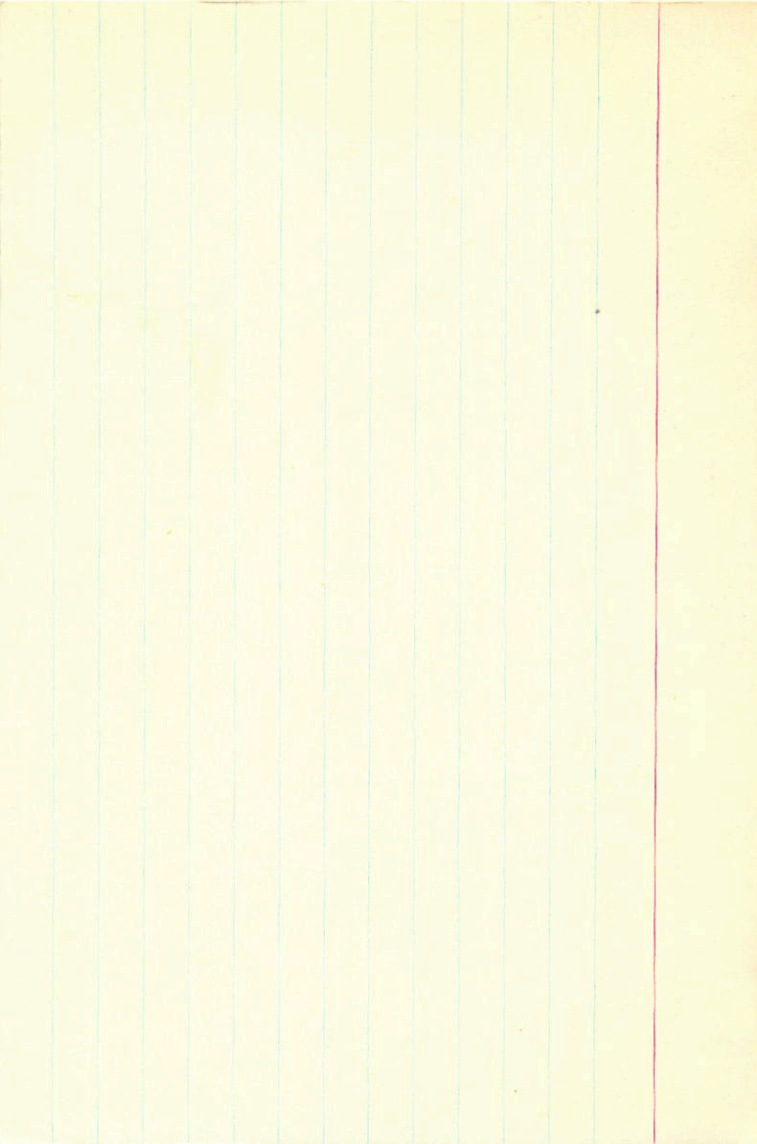
-29
24.98
36.4

+014

24.74

2.82
32.2

+3.45



160935
24005
10224

+0013 ± 6.0 -134 ± 5.6
+0009 -122
17 39.7 +21 32 6.7 F8 -27.28

40.144 1901.6 +21 31 35.08 1900.6
-063
081

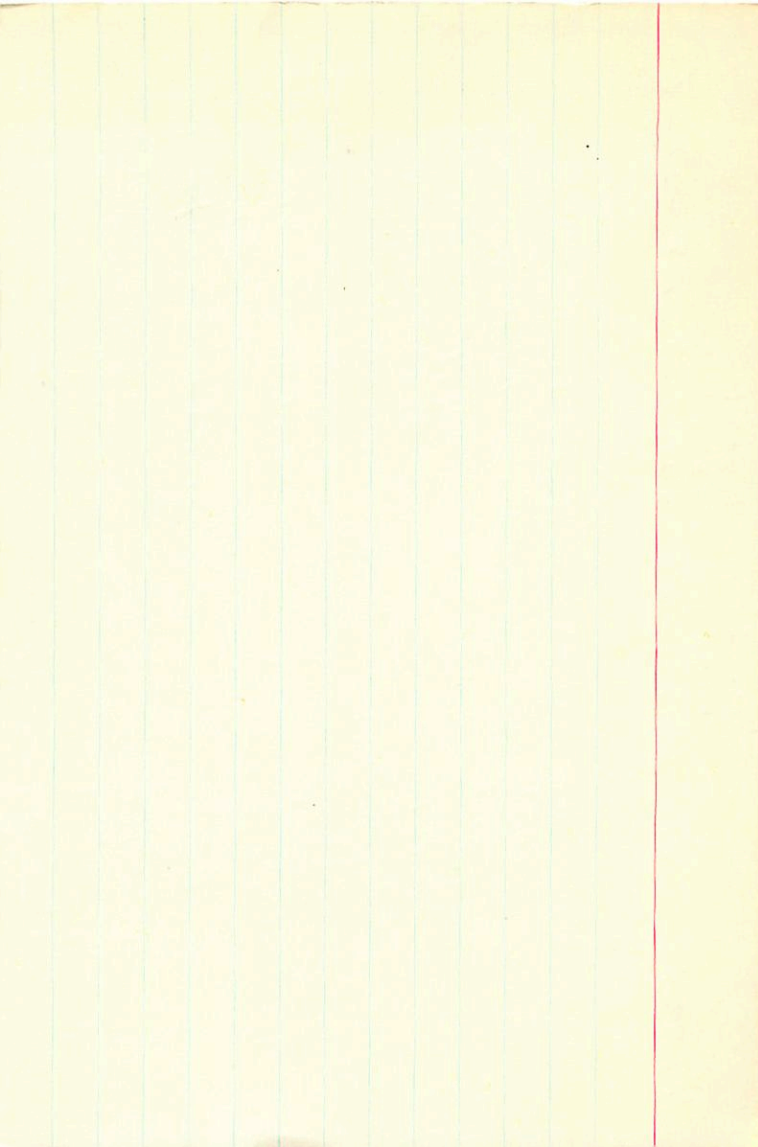
40.124
1
125
~~39.905~~
40.088 246
3
091

108
+ 027

29.4

6.62
41.70
37.77 1933.5
+4
37.81

38.40 1928.44
-23
35.17
41.94
30.0
37.99
30.4
-3.71



161193

17

40.2

+51

50

6.19

120

-8.78

-003474.1
-0030

-02043.9
-013

24025

10232

12.831 1898.4

+51

50

28.85

1896.4

175

13.006

38.46

34.452

12.913

625

524

12.839

860

-126

2641
880

41.6

1.67

29.52

73.3

44.41

28.85

29.49

24.39

29.77

-34

29.43

24.55

29.27

1927.5 12013

40.0

43.0

109

29.36

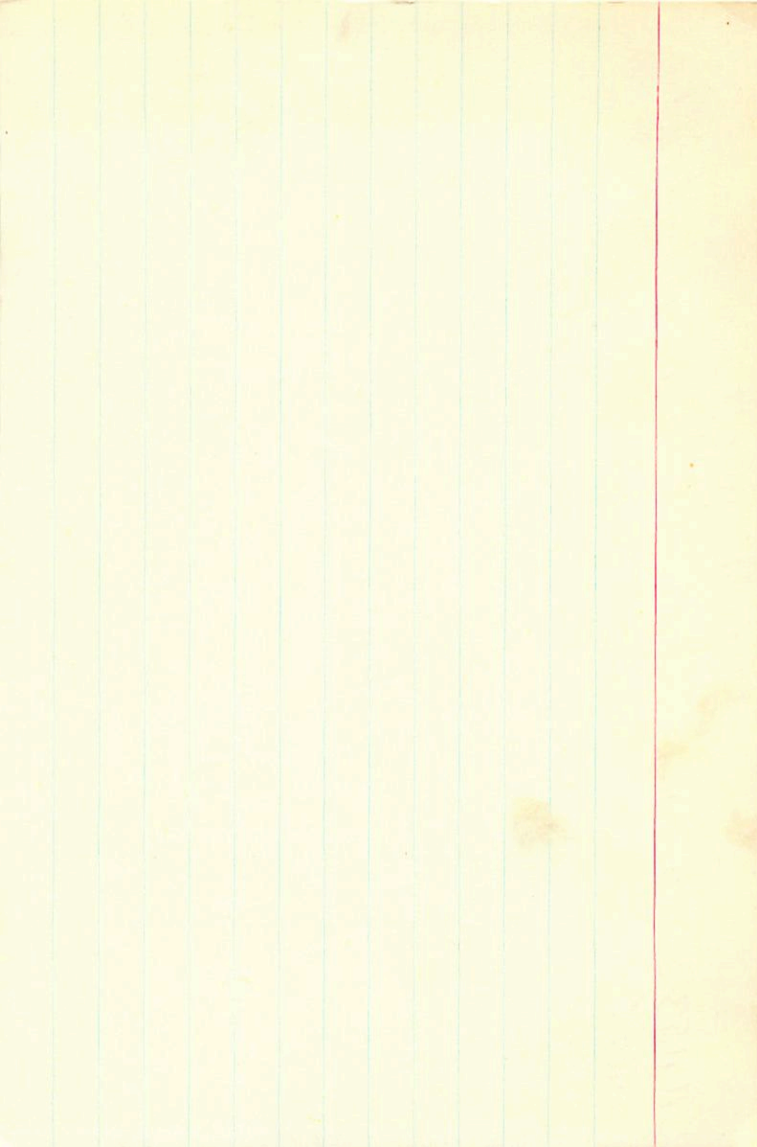
56

1945.24

1947.39

12.534

452



161096 17 41.0 +04 35 2.9 gKI -12.000

24048

10239

$-0029^{108} +160^{104} N30$

$-0024^{20.7} +159^{20.8} 00 \rightarrow N30$

2355

2-78 +1.16 +1.24 122 III



84 Her

-0087 ± 2.0 +067 ± 1.7

-0084 +072

161239 17 41.3 +24 21 5.7 g 69 -25.66
24059 -22.4 (1)

10244 18.330 1893.6 +24 20 53.22 1891.5

49/
821

3.92
49.30

18419
420

18524

3
527

474

-344

40.8

53.00 1940.31

-27

52.73

52.26 1928.44

-23

52.03

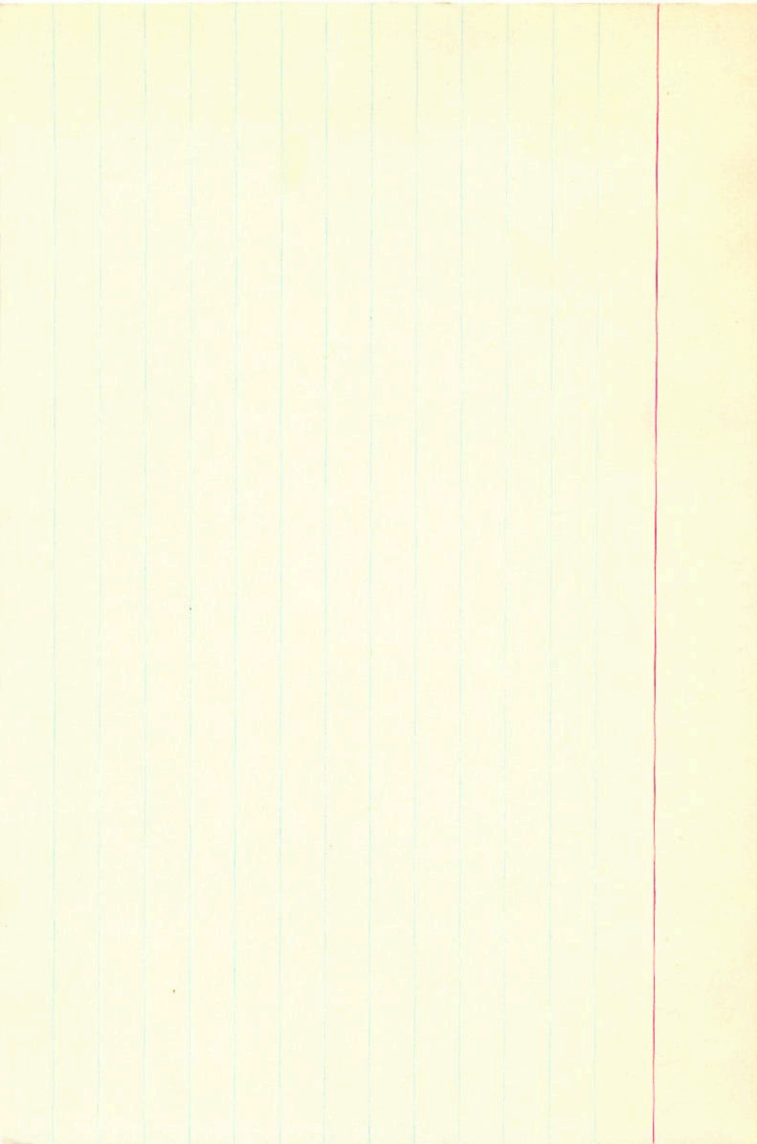
52.38

+3.08

1875

37.4

42.9



161369

17

-0038 ± 4.4
-0037
416

+44

+038 ± 3.3
+032
06

6.6 NY -60.36

24067

10247

36.517
 $\frac{177}{6.94}$

1903.4

+44

6 18.87

1899.0

$\frac{177}{6.94}$

$\frac{-040.170345}{E}$ Figs

$\frac{-1.94}{16.93}$

52.06
44.540
 $\frac{36.608}{6.19}$
 $\frac{6.11}{6.11}$

24.6

58.9 1924.65
41.78
 $\frac{17.12}{5.3}$
 $\frac{17.118}{17.84}$

5305
27.5
 $\frac{28.5}{-}$

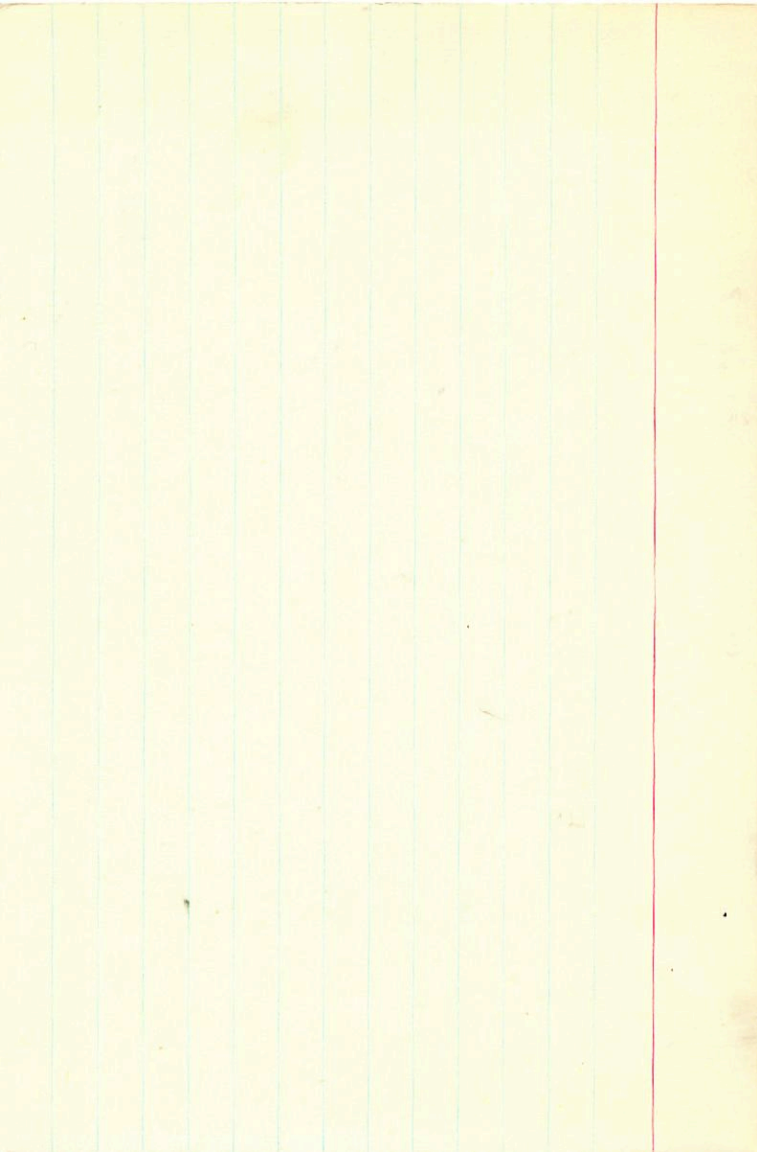
$\frac{6.13}{-0.81}$

$\frac{17.84}{+1.91}$

36.60
 $\frac{15}{6.16}$

4759 ~7049
1544 ~7094
8796

18.2 1930.4
-36
 $\frac{17.86}{17.86}$



-660²¹³³
~~467~~

17 41.6

-6.6 06

11.35

-66.2 ± 7.9

3 Sliding



4720803

34
-17.08

161897 17

42.1 +72

2.6 8.4

dB6

10257 3258-16

-251

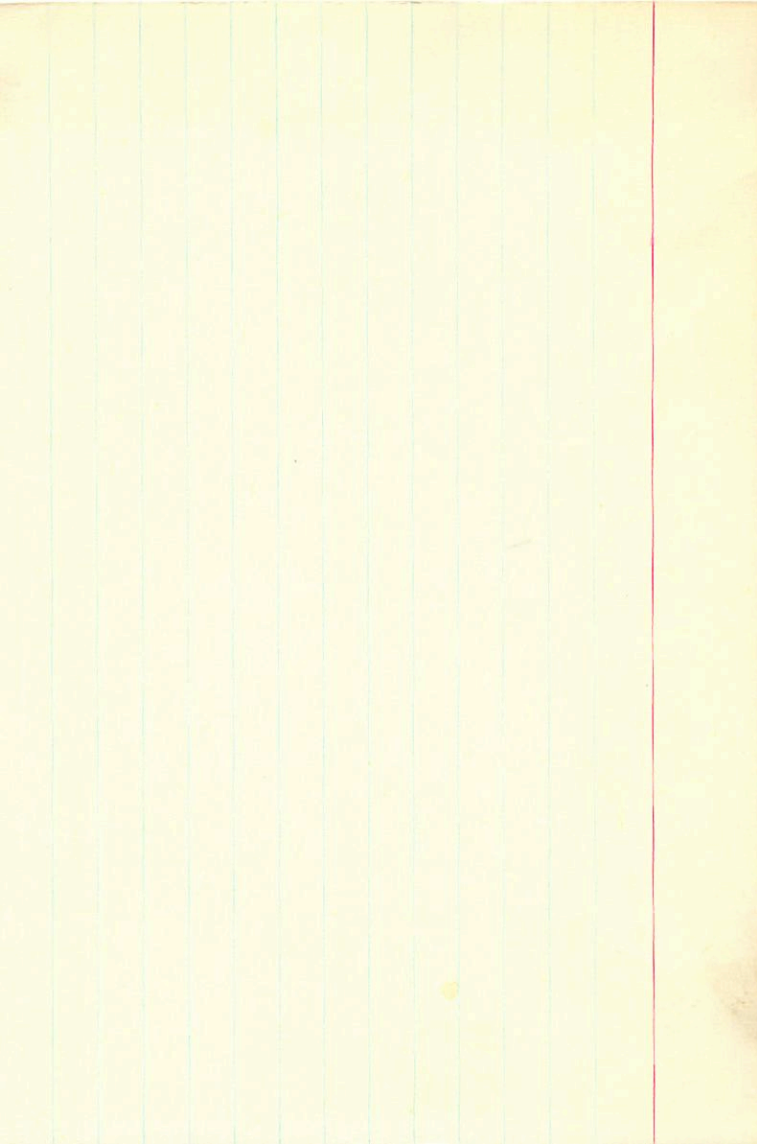
-114 +297

GAZ

3456

-108

+303 G'(H)



161550 17 43.0 +31 09 dFJ -36.86

AFG -37 C

ANS 10765

5" 8.0
5.5

-021 +005

$\sigma_d = 0.10$ $\Delta m = 0.92$

-557-024 518 854 -021+005 -36.8 003 -19 0209

-021003 0010 -055 015 331.5 +2+37 01

-8+39 -17

-0029 ± 6.5 -001 ± 6.1
-0011

161542 17 43.5 +05 56 7.2 A0 -29.56

24105

10269 28.249 1901.0 +5 55 33.72 19013
142
391

28.341
352

34.07 1933.5
-13
33.94

28.336 353
15
354 -038

34.07 193636 986
-13
33.94 34.9
33.94
+19

33.6

