

t:7 ~~3~~ 3 Nov

156846 17 17.6 15 17 03TD

HR6441 +6
-124 +3.5

GL23420 -0.07 -124
+124 6.50 +58 +10 (2)
-0.0004 +3
-0.5396 -1506 -150 -121 -69.26

15.4
18.4
25.0

19.2
+3.0

1368 · 200.452 = 2.628 (2) 5,193

[200] 266 +1

[61] 378 95
+46 / 188

" 47
+67.3 -25.4 -5.5 -147 -69.2
-24 -830 +279 -112

3.48 +66 -47 +2
0 -8 +3

1596
 544
 4
 8
 4
 3
 4
 6

6441.000*

17.000*
 17.600*
 -13.000*
 -17.000*
 -3.150*
 -3.121*
 3.500*
 53.119
 -69.200

 -3.030
 -3.981

 65.404

 -3.873
 3.086

 -43.732

 3.267
 3.173

 1.393

81.2

6

156968

17 17.8 + 0.9 31 220

~~-(2.38)~~
-12.38 w(4)

GC23422

7.97 + 0.60 + 0.0660 ± R

w 10008

Σ = .07

136-31

73938

1903364

-0019 -309

-028-309

20

-030 -314

-28

-029 ± 8 -314 ± 7 4

-309

5.00

123

7.94 381

176 349

3

7.94 381

165

352

370

9318

4418

-194(16)

354(8)

317(12)

9 ± 5

1
1
1
1
1

156968

17 17.8 +09 31 d60 -12.38 w/14)

G(23422

w10008

7.97 +0.60 +0.06 G O U R

Y3938

S=07

+9°3366

-25 -49 -24 .025

-35 -59 -29 .020

-79 -116 -54 .010

-030^{±7} -314^{±7} 60
-029^{±8} -314^{±7} Y

1009 638001

-19A(16)

35-MIT)

3LY(12)

9±5

01722 + 570101

-00204 6.7 -31446.5
-0024 -308

48925 1302.3 + 9 30 52.75 14001

7

$$\begin{array}{r} 49,020 \\ \underline{095} \end{array}$$

$$\begin{array}{r} 15.67 \\ \underline{8.42} \end{array}$$

$$48.931$$

(33.1)

$$56.13 \quad 1989.42$$

$$\begin{array}{r} 938 \\ \underline{7} \end{array}$$

$$\begin{array}{r} 56.08 \\ \underline{5} \end{array}$$

$$\begin{array}{r} 533 \\ \underline{57.62} \end{array}$$

$$\begin{array}{r} 934 \\ \underline{001} \end{array}$$

$$\begin{array}{r} 52.34 \\ \underline{2} \end{array}$$

$$59.6 \quad 15314, 10.76$$

$$\begin{array}{r} 982 \\ \underline{11} \end{array}$$

$$48931$$

$$-001$$

$$940$$

$$\begin{array}{r} 59.25 \\ \underline{35} \end{array}$$

$$\begin{array}{r} 08 \\ \underline{35.4} \end{array}$$

(35.3)

17,300	:	P. A.
9,500	:	DEC.
-38,000	:	P. A.
-309,000	:	DEC.
2,000	:	ANCE
100	:	PLUS
-12,300	:	VEL.
0.000	:	(U)
0.021	:	(U)
-0.779	:	(U)
-0.000.710	:	DU
-0.000.004	:	U
0.000.0	:	(U)
0.070	:	(U)
0.471	:	(U)
-100.400.440	:	DU
0.000.000	:	U
0.010.0	:	(M)
0.000.0	:	(M)
0.410	:	(M)
-1474.000	:	DM
-0.000.000	:	M

X

R.A. : 17.300
DEC. : 9.500
R.A. : -28.000
DEC. : -309.000
DISTANCE : 5.000
MODULUS : 100
VEL. : -12.300

1 (U) : -0.093
2 (U) : 0.621
3 (U) : -0.779
dU : -896.710
U : -80.094

1 (V) : 0.567
2 (V) : 0.676
3 (V) : 0.471
dV : %-1064.440
V : -112.238

1 (W) : -0.819
2 (W) : 0.397
3 (W) : 0.415
dW : -474.622
W : -52.562

7

Carleton

156897

204

17 18.0

-21 03

F2E

HR6445

85-204

6023423

4.39 +38 -05 C

438 +41 -06 J

40(3) 0ph

254 154 501

2.68

670

1/2' 187.2 2.68 222,1

[m] 206 +14

~~no 3472 US. 511 2679 0+~~

[E] 416 +8

264
-217
1251

01750

8518

194E

[C/E-21E]

1.20 +47 -35 -22.5

7083

7074

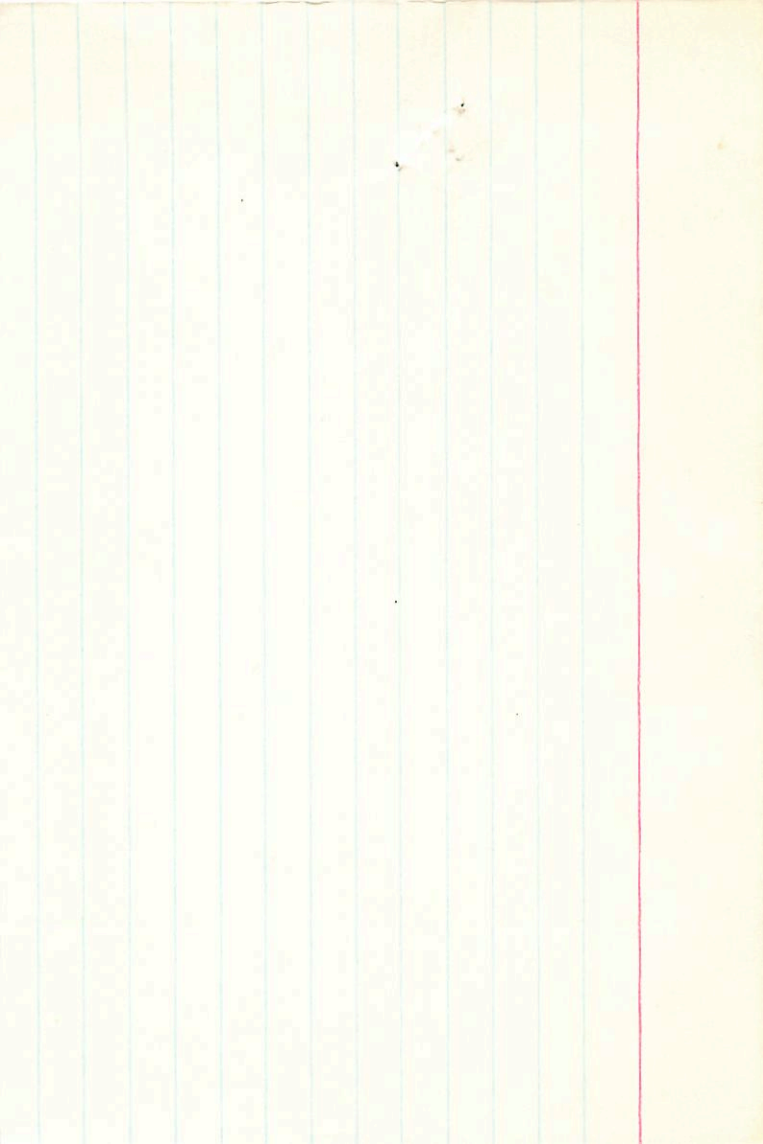
8350

8499

3254

6310

2051-181-1503



30ph

$+0165 \pm 1.2$ -213 ± 1.4
 $+0174$ -224
 17 18.0 ± 0.2 21 04 4.5 $dF2$ $-9.1a$
 0552 -217
 23423 216 $F2E$ $-7.5a$

10009 0.255 1898.7 -24 3 4007 15591

-546
 $\frac{506.6}{59.409}$
 59.409

0608
 0604
 43.42
 43.35

46.79
 -10.84
 29.17

0.164 0.716 91.0 44.54 37.72 1939.10
 0 -30

-179
 $\frac{149}{149}$

42.4

37.82

5027

24383
 35785
 0.108

145
 61
 $\frac{145}{145}$
 $+739$
 147

1.39 1941.17

37.04
 $\frac{43}{38.34}$

38.22
 -9.17

41.0

-22
 $\frac{38.87}{38.87}$

8

-0107±9.0 -070±7.5

6.8 $\frac{4}{1}$

-1.5±0.5 $\frac{3}{1}$ (4)
+6 $\frac{4}{1}$ (4)

A5 $\frac{1}{1}$

17 18.5 -58 25

15-6751

23436

6.77 ±0.25

6.8.9.4 9.4

27055 1905.6 -55 25 27.13 1503.2

$\frac{475}{530}$

3.28
 $\frac{85}{85}$

23.

32.1

54.09 1929.86
 $\frac{85.00}{85.00}$

17.080
10135

7546
317.7
31.5

27 $\frac{210}{94}$
 $\frac{218}{27}$

29.09
 $\frac{232}{232}$

1463
 $\frac{2732}{347}$

$\frac{281}{249}$

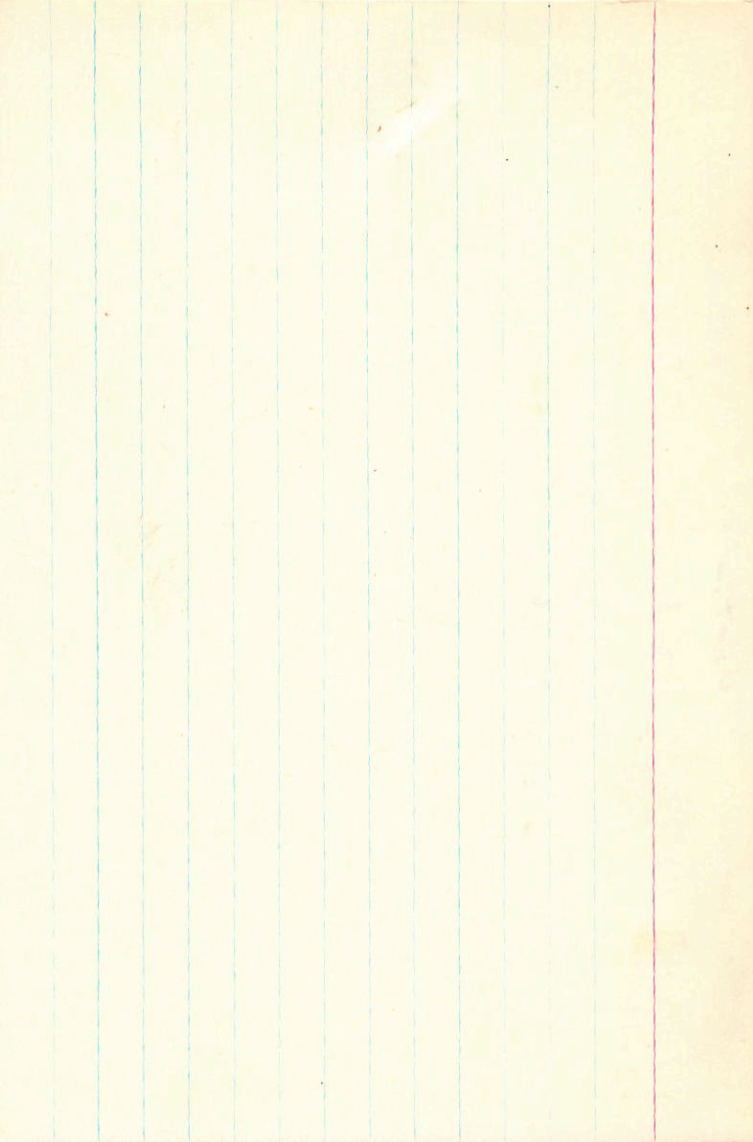
26.20
 $\frac{26.77}{347}$

26.57

1445.4

27.284
 $\frac{284}{284}$

27.56
 $\frac{28.00}{28.00}$



6457 17 19.2 -35 52

157000

+0065 ± 40
+080 52.15 007
415 -5.27

16.280 1.9 +0064
1313
1967

17.3

-35.9

9.9

5.9

2.45

-6

57.52

33.24

35.616

40.705

5.24

1.20

5.01

52.16

+1.80

50.36

50.36

50.13

50.13

0806
080099

56.56

170

547.2

19.55

19.55

10064-1095

10063-1098

1.20

1.94

1.20

1.94

237 186 286 2.6.34
245 146

9

17.300

- 35.900

99.000

99.000

2.450

31

- 6.000

- 8.093

- 0.119

- 8.989

- 91.104

3.116

0.567

0.810

- 0.151

595.523

19.307

- 0.819

0.574

0.000

- 41.817

- 1.342

9

+0198 -010

+0188 ± 15.0 -027 ± 10.6
+0203 -006

4V

157373 17 14.2 +48 14 6.3 dF2 +30.97

23461

+0192 -009

10025 12.542 1510.5 +48 14 13.32 1508.5

~~743~~

+192

11.799

12.663

1448 195417 17.444

32.112
39.983

+464

13.99

44.1926.7

28.5
18.0

12.114
11.12
12.2

328

-45

30.18

13.92

17.1

164
65
+3

149
4

14.54

12.119
17
20

14.67 1930.4

-35

14.48 195417
49
13.99

~~12.663~~ 14.35

12.663
19
1.684

46.8 mo.

4.192-009

+309

-086 971	-224	-0741	-0414	-1205	-5.6	-6.9	-12.5
563 232	753	+5177	-6049	+5078	+23.8	+24.5	+48.3
-522 058	567	-7554	-0025	-7584	-35.5	+17.5	-18.0

6464

17

200

740 07

15749 ✓

AS 107, 1579

15994

1000 059

717

157

0216

154

450 5107



10

4304

15723

23497

10031

$$\begin{array}{r} 12585 \\ \underline{610} \\ 12075 \end{array}$$

12.601

$$\begin{array}{r} 544 \\ \underline{604} \\ 1024 \end{array}$$

1024

35.4

$$\begin{array}{r} 47.87 \\ \underline{12.47} \\ 35.40 \end{array}$$

$$\begin{array}{r} 46.21 \\ \underline{10.87} \\ 35.34 \end{array}$$

$$\begin{array}{r} 46.34 \\ \underline{10.94} \\ 35.40 \end{array}$$

$$\begin{array}{r} 46.19 \\ \underline{10.79} \\ 35.40 \end{array}$$

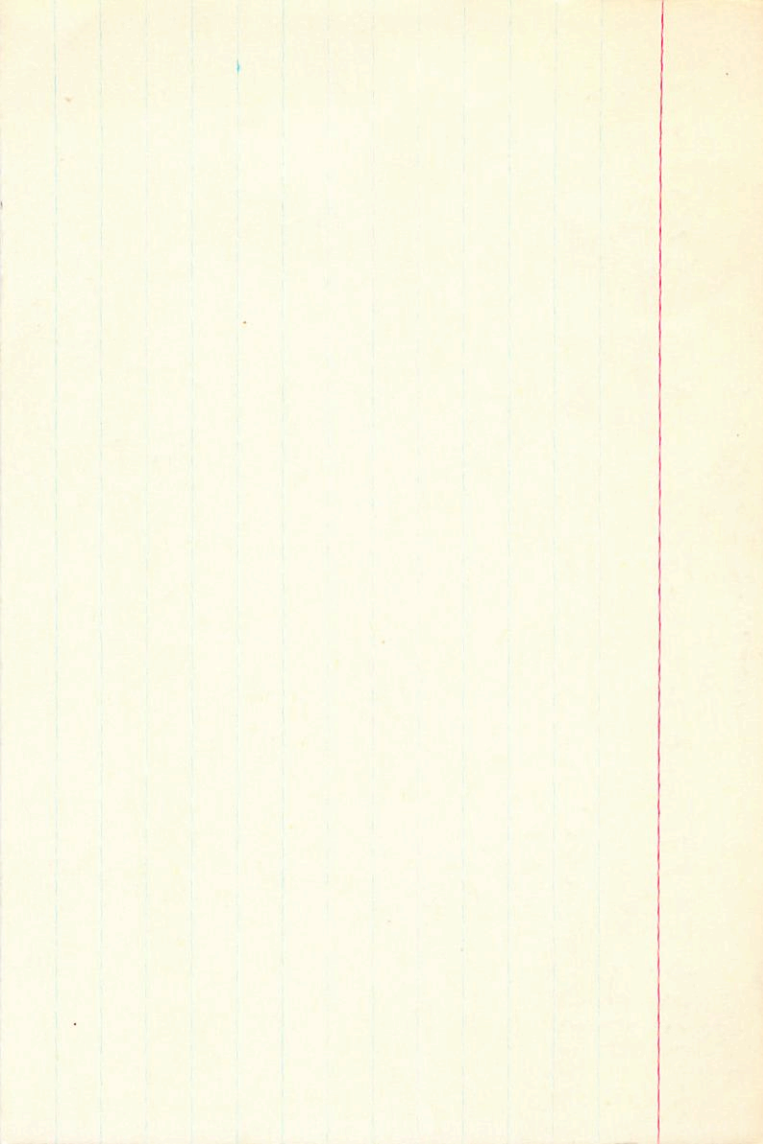
$$\begin{array}{r} 46.34 \\ \underline{10.94} \\ 35.40 \end{array}$$

$$\begin{array}{r} 35.1 \\ \underline{0.18} \\ 35.28 \end{array}$$

36.9

1939.06

$$\begin{array}{r} 46.34 \\ \underline{1.10} \\ 45.24 \end{array}$$



-0025 = 4.8
-0015
-010 = 3.2
-010

157498 17 21.2 -9 19 7.8 dg-1-37.78

23519

-0015
-0014
-010
-010

pc = -48.7

10046 13.275 102 1909.2 -9 18 46.25 1803.6

909546
 $\frac{102}{377}$

7.89 + 62 + 46 + 46
320'' 48.79

51131

22200

13.331

346

-14

330

-041

13.292

46.40

4.97

8.64

500

335

330

-041

13.292

46.40

4.97

-0017 -014

-0016 -00946

-0226
-022.5 -1055

2984 -9943

-4612 -1070

0233

0040

27.8

1934.56

20.13

2735

47.78

1.50

45.94

45.17

45.1

46.35

46.43

Agenda
Touche
Wassert

402

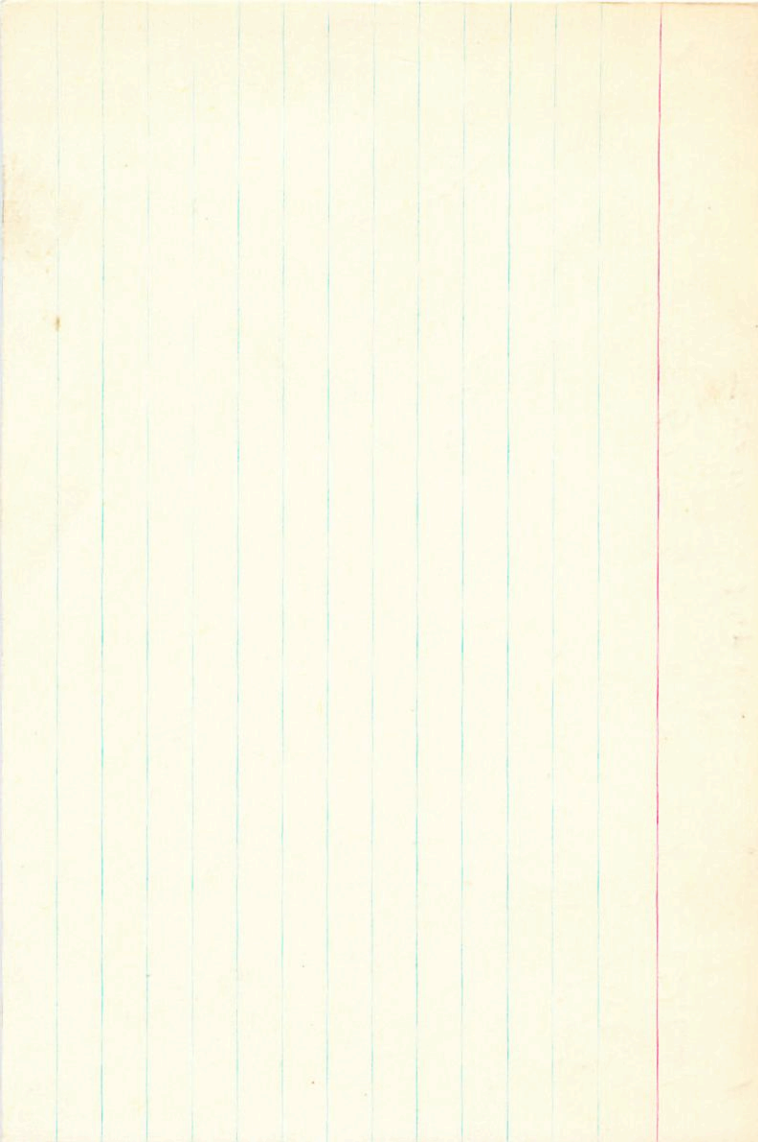
37.0

33.4

1939.46

46.12

-0.33



6.64 253 16.700

157935 17 23.4 716 26 6.7 F2 -51.98

23603

10075 -0010²³ +034²⁵ N30 -494

-0013²⁴ +034²⁵ E3.66-2 SW30

100
P, 71

0376

104
-012-1052

0023

71.7

4154 3778 0342
5094 9225 0034

0094

8.12

-1.86

-4551

96 -11.11 0086

8904

5.34

26594 8.7

-688

-0712 544 +0224 536

-0009

+0224
+0224
3464 9.0

0011

+0224
3119

0014

+0227

3347

0012

3407

334

-00105 +0315

-01
3406

26579

+11
540

6676

3554

-47

3507

26613

-5
604

-0151
-015 +0322

3414

4034

-29

3238



165341.000*

18.000*

2.900*

2.000*

31.000*

0.261*

-1.096*

-1.400*

5.248

-7.200

-2.612

-0.850

-7.589

-3.158

0.489

-20.092

-3.424

0.197

-19.392

6461

17 21.2 9

- 55° 28'

2.80 Ma

13 Ave

23515

177

- 55.5

175

10044

24

- 0.40

+0.505 +8.5 +0.4

-0.816 -14.3 +0.1

-0.610 -10.6 0

630

+0001 -0.24 N30

-0013 -0.33 GC

+ 16 + 8

+0003 -0.25

+0002 -0.245

1002

+004

16.58

2 Ana 16007-012 N30

- 0.082 -0.444 -0.892

0.562 0.718 -0.410

- 0.823 0.536 -0.191

+0507 +31.9 -0016 +0379 +0363 +23

-0008 +0516 -0781 -40.0 +0106 -0613 -0507 -32

+0053 -0834 -0156 -0757 -0613

-0078 -0622 0.700

152498 17 21.2 -9 19 dg-1

7.89 +62 +06 3 eggs

[m] 279

[c] 257

.391, 208, 1335, 2.610②, 58, 2

157617

23527

10049

39.127 1889.7

+8 53 51.45

19.97.9

$$\frac{-0.24}{1.03}$$

$$\frac{36}{}$$

34090

$\frac{11}{101}$

51.81

51.48 1933.5

45.2

34100

$$\frac{\frac{15}{118}}{\frac{110}{1007}}$$

$$\frac{-13}{5135} \quad 122$$

52.00 1936.26

$$\frac{13}{51.87} \quad 976$$

51.87

$$\frac{5161}{-20}$$

34.9

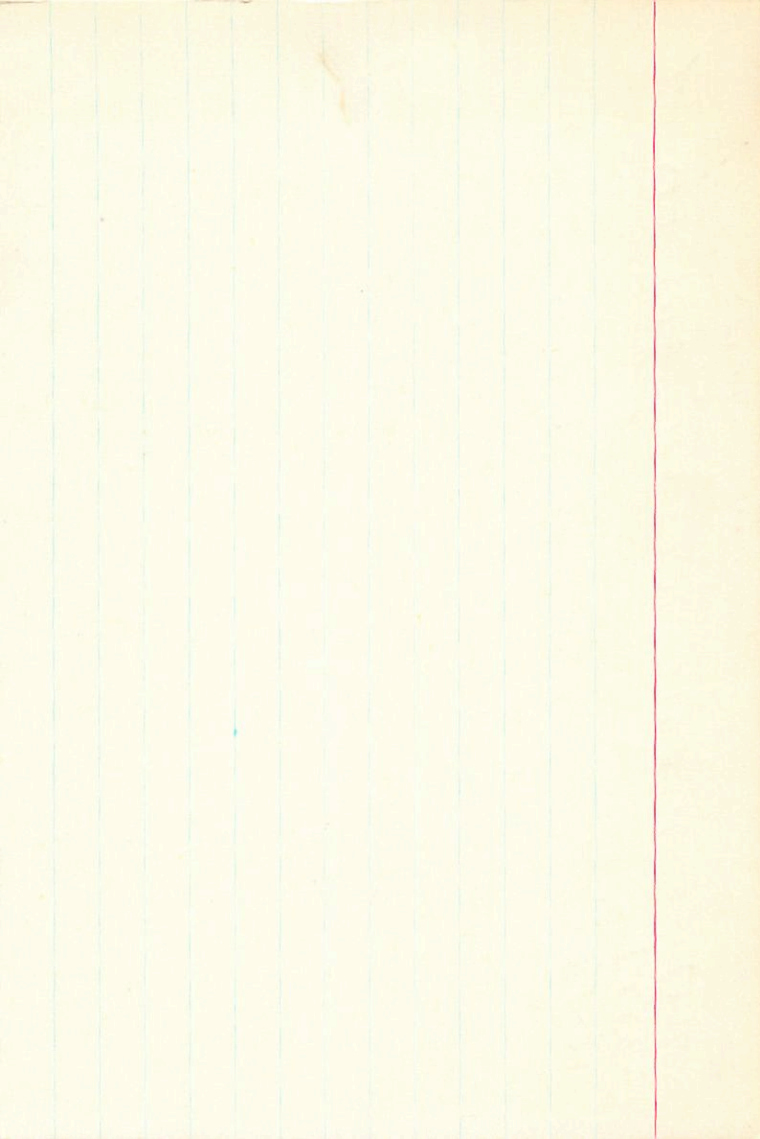
37.0

+0004±4.3 -007±3.0

+0002 -007

17 21.6 +08 54

5.9 9.101 +15.98



AD510522
157527

17 21.7 -21 24 6.0 567 -55.98

23533

10051

37 37 N30

-0013 -027

-0012 ± 2.4 -031 ± 2.6 64-9M30

66
85.5
16

FU

-0087 -0264 FU

-00106 -0236

-80096 -6206

-00125 -029 N30+

-0285

17.33

-214

-14

-20

54.5

-55.9

-0175

-55.9

438

-018-028

-0134

-013-020



-032
-034
-029
-0208

42.429 42
-0017 03078222 873

$\frac{64}{998}$
-0012
-0014
46.70

-0014 -0324

-00137 -0273

25.78

42.424
-17
437

4265 -0191
-10
4729

3134 -0422
-9566 -6702
019 -027

42.420
70.6

48.07

0.1.911

49.13
-29
46

42.411
-4
407

48.56
-43

==

17.330
-21.400
-14.000
-20.000
5.450
123
-55.900

-0.006
0.132
-0.987
-7.214
54.310

0.564
0.824
0.061
-112.916
-17.300

-0.821
0.551
0.146
-1.521
-8.335

//

-0032=2.2 -045=1.9
-0030 -044

17 22.0 +23 00 5.7 AY -19.78

23546
10055

0.944 1894.0 +23 0 19.16 1893.1

$\frac{179}{1123}$

1.011
 $\frac{1}{0123010}$

0.977
 $\frac{04}{978}$

$\frac{1.003}{1.017}$ -120

$\frac{10.17}{102.0}$

$\frac{256}{2172}$

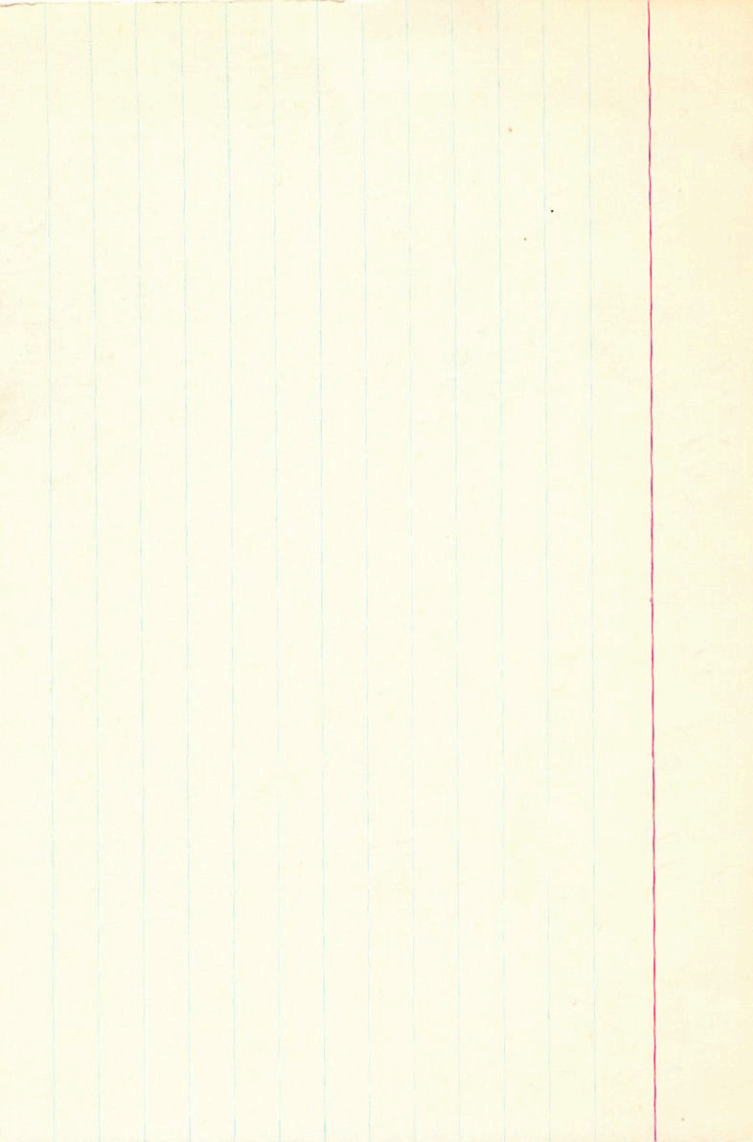
398

425

19.72 1933.4 1914.6
19.76 5982

19.99 1039.53 -40.7
-50981 0.92

$\frac{20.68}{7234}$ 1928.44
 $\frac{38.45}{19.94}$ 1.78



1596

944

44

63

4

638

4

636

2

193

66

8

2

15

6

✓

Fig ~~8~~ 5 New

156846 17 176 19 17 0377

HR644 +v -124³¹ +3.5

GL23420 -0107 -1219 6.50 +58 +10 (2) 454
-0107⁵³ -1219⁵³ 184

19.2 (15) +3.0

-1506 -121 -69.26

any 266 +1 1368 .200 .452 2628 (2) 5,1193

GL17 378 95 47
+56 1.88 467.3 -25.4 -5.5 -147
" " " " " " " "

v -24 -830 +279 -112 -65.2

3.48 +66 -47 +2
0 -8 +3