

u. lib  
-2004305  
9058

15 39.1

139867 15 38.5 -29 08 7.28 +1.72 M4 M5

6621082

+0014 #005  
-0007 ±5.4 -0.12 ±6.3

28.514 1892.5

23.65 1893.3

+0004 -008  
+0008 +000

22.97

674  
174  
474  
0

56.660

31.882

28.542

.608

612

+065

31.56 1933.98

52.88

24.44

1.38

23.06 #.22

-13

23.19

CPO 44.7548

-065 173

Rayley

139961

15

39.4

-44

47

AOE

8.90 + 0.095 + 0.175 (5)

647 6.34

AI ↓

+146.0' f

S

1566

-0172 -088 Y+L FR4

-44.8

-0145 -074 C(II)

2140

-0160 -082

82.5

-0156 -078

7.4

-015

-0172 -088 Y+O

147

-1666

-0173 -086 CO

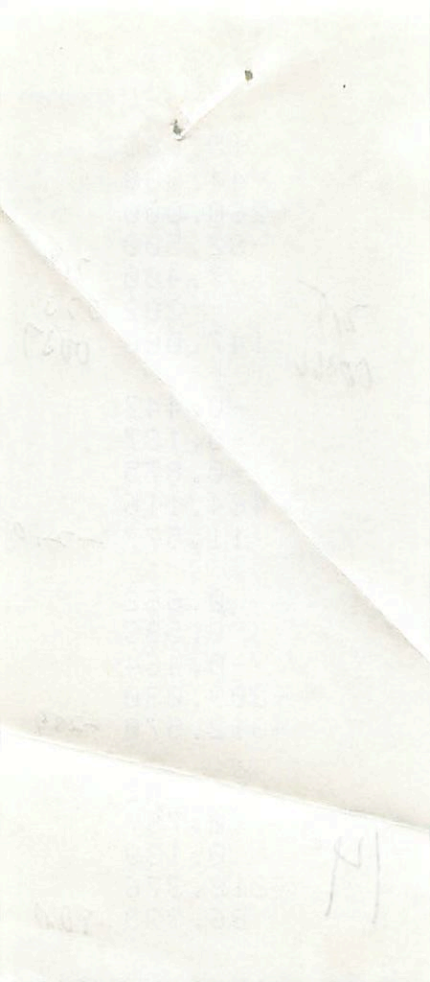
-168 -076

-0172.5 -085

-183.6

-185 -082.5

14



15.568  
- 44.888  
- 268.888  
- 82.588  
7.488  
382  
147.888

215  
00366

215  
273  
0037

- 8.447  
- 8.187  
- 8.875  
464.116  
11.577

-200

8.662  
8.588  
- 8.464  
- 899.838  
- 312.578

-289

8.682  
8.787  
8.139  
218.376  
86.393

14

+50.0

+3902401  
0021108

RRGB

15 09.6 +08 43 7.15 gmi -500

SR(60)

+0021±4.4

-0.40 ± 4.2  
-0.89

26.180 1913.7

0.75 1511.6

$\frac{76}{1.14}$

+16 -38  
-1.0 -1.0  
+0.4 +0.6  
+0.3 +0.5

$\frac{1.53}{2.28}$

36.27  
005  
275

+0016 -038

0.3 1940.0  
 $-\frac{11}{0.19}$

$\frac{-001}{82.6}$   
 $-\frac{44.2}{-42.3}$

Block

+019 -038

36.15  
 $\frac{23}{193}$

1.9  
 $\frac{2.75}{1.5}$

-96.6 +140  
-17.4 -268  
-22.4 -398

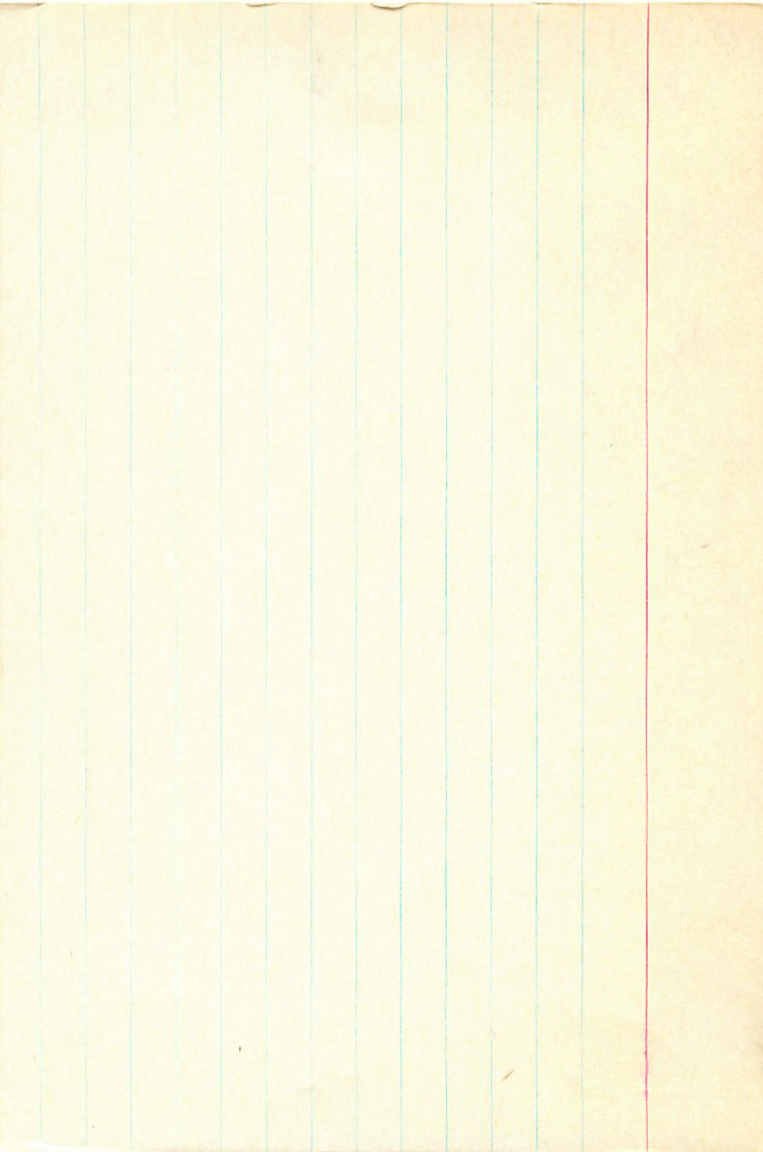
coups.

+446 +950 -241  
+662 +524 +534  
-603 -053 +796

+940.4  
-0402 -1531  
+0596 -0944  
-0543 +0095 -0448

0  
 $\frac{0.045}{0.002}$   
 $\frac{0.000}{0.000}$

-1923  
-0348  
-0448



140611

15

40.1 466 00

9.2

dgw

-20.46

400

C2105

(56.10)

9066

43561

4660916

$$\begin{array}{r}
 +05322 \\
 - \quad 3 \\
 \hline
 0507
 \end{array}$$

$$\begin{array}{r}
 -178 \div 0 \text{ GR} \\
 \quad 12 \\
 \hline
 -179/81
 \end{array}$$

$$\begin{array}{r}
 +043 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 -150 \text{ GP} \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 +047 \\
 +8 \\
 \hline
 +055
 \end{array}$$

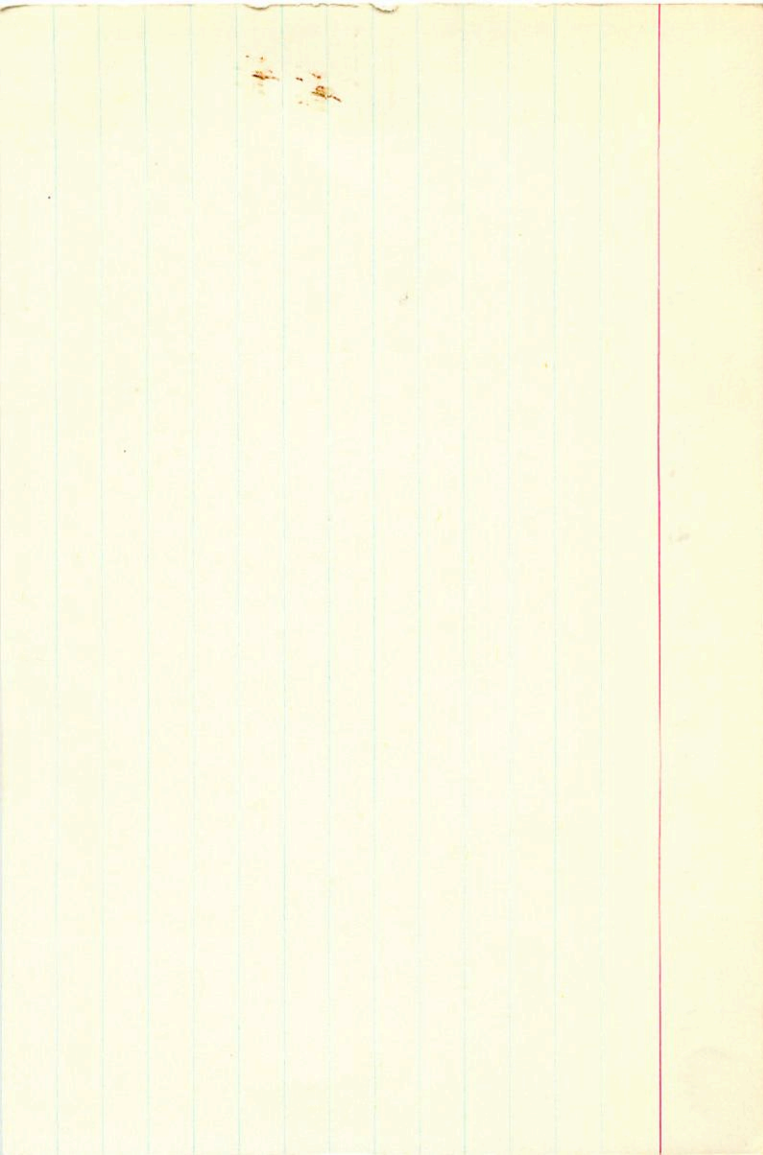
$$\begin{array}{r}
 -185 \\
 \quad 12 \\
 \hline
 -183
 \end{array}$$

$$\begin{array}{r}
 +055 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 +6090 \\
 \hline
 \end{array}$$

N 30.





J Nov

15

40.2

-54 50

-31c  
20

-020 -030 Cpa 19

-20 +1

-022 -029

15



0.000\*

15.000\*

40.200\*

54.000\*



A056756

140590 . 15 40.3 +60 09 8.4 d66 +33.26

21119

9068

19.409 1911.1 +60 8 40.59 1900.6  
 1.175  
20.584

51.00  
 29012  
20.012  
 .062  
 071

17.2

24.1 1927.6

47.70

36.40

36.45

36.10

36.75

518

~~28.9~~

~~26.3~~

37.00

37.26

+4.1

1930.2

37.4

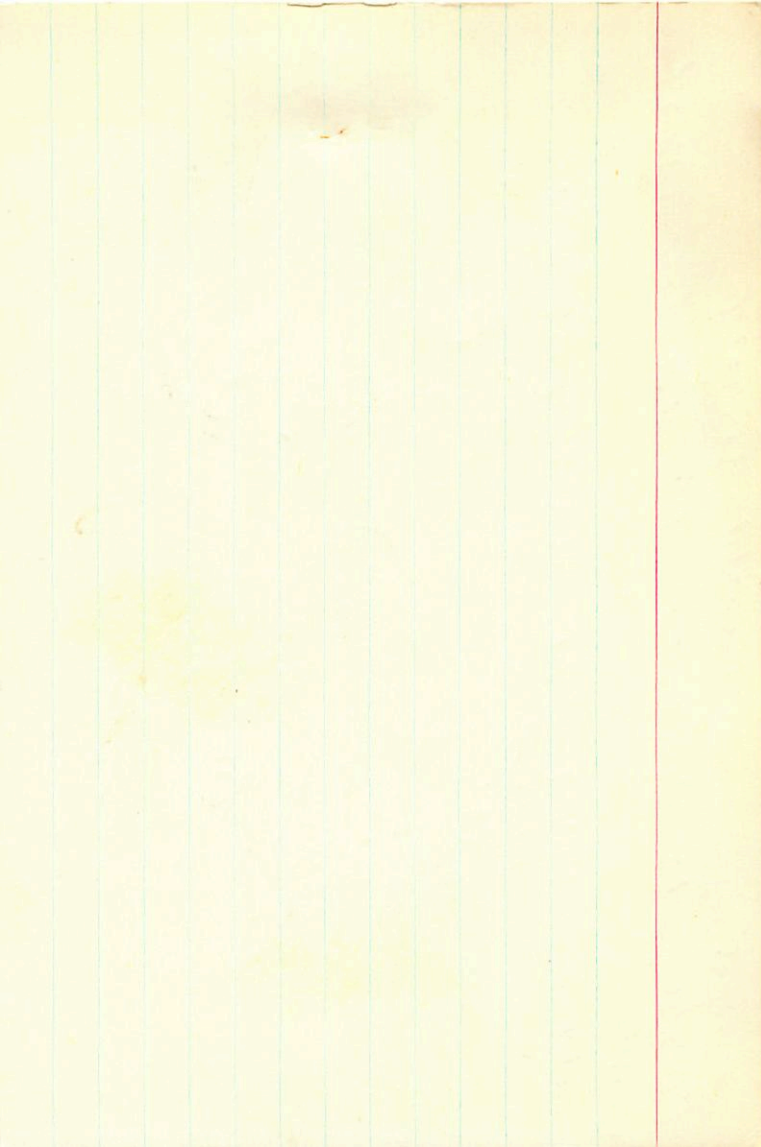
-15

37.25

20.040

20.040

-338





ywb

A059757 15 40.6 +24 27

-10.56

140434

.0201 (3)

21130

A018

-106 +038 6-c

9071

3.93 000 -0.05

-106 +042 N30

A059757

-0078 87 +042 45 N30

-107 +042 F=N3

40-700.5

-0081 ±1.1 +043 ±1.1 6L → N30

-106 +041

2055

-00795 +0425

-010 +173 1008 2.897

alw

-103  
-100 +041

10.5

Spontaneity

-921-571 445-995 -106+041-10.5 018-5-175  
-057 015 061-010 -365 360 -9.4+5+8 0201  
-13+26+4  
+24-15+9 9

15.650  
26.450  
-112.000  
41.000  
3.000  
40  
-10.500

-0.449  
0.768  
-0.457  
362.592  
19.237

0.662  
0.630  
0.406  
-192.457  
-11.928

-0.600  
0.120  
0.791  
308.501  
3.976

16

4R5850

-0004 ± 12.2  
-0013

+2.0 00D

140438

15 40.8 +13 50 6.4 68

III - IV -9.98

21132

-75 ③

9073

50.334 1906.2 +13 49 32.48 1901.6

A069758  
Damped

$\frac{0.39}{1.373}$

$\frac{1.94}{34.42}$

$D_m = 1.24$

50.320

$\frac{332}{-041}$  81.5

33.14 1934.1

$\frac{17}{337}$

$\frac{332}{-041}$

$\frac{39.00}{-14}$

33.07 1189.93

50.302

+24

326

$\frac{-220}{-85}$

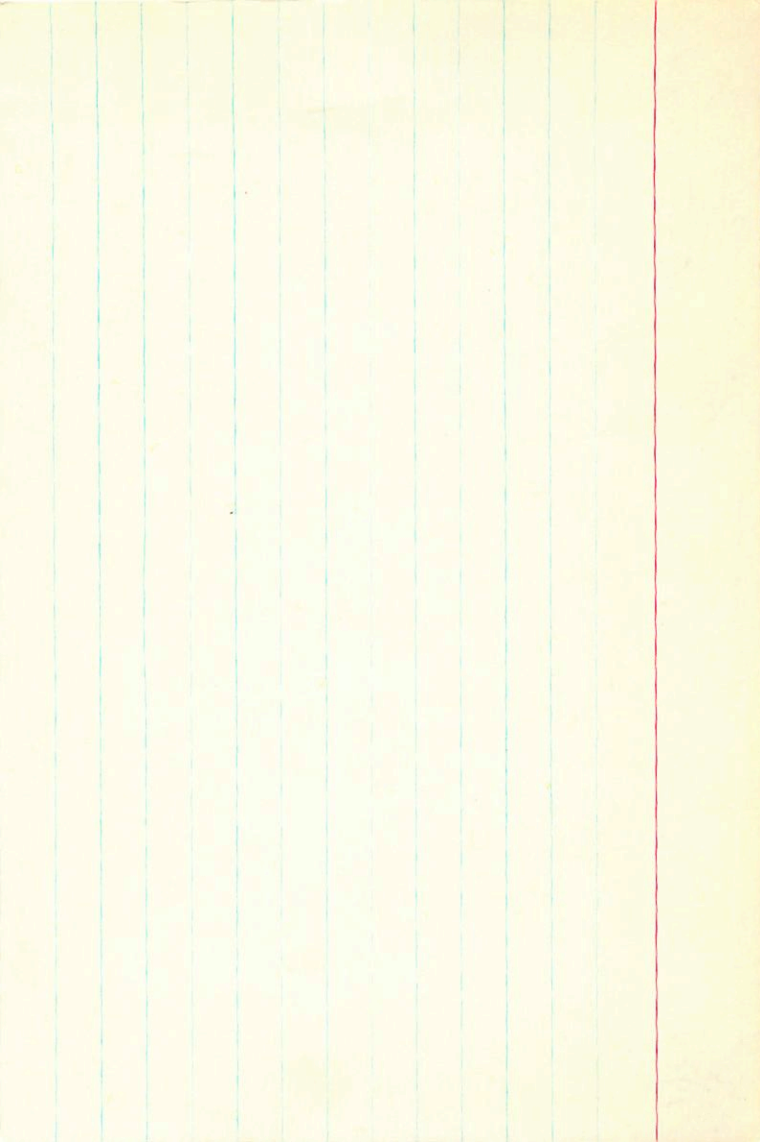
32.8

37.7

36.1

$\frac{32.92}{-1.50}$

1433



F0 III

Cape  
-31.2  
4

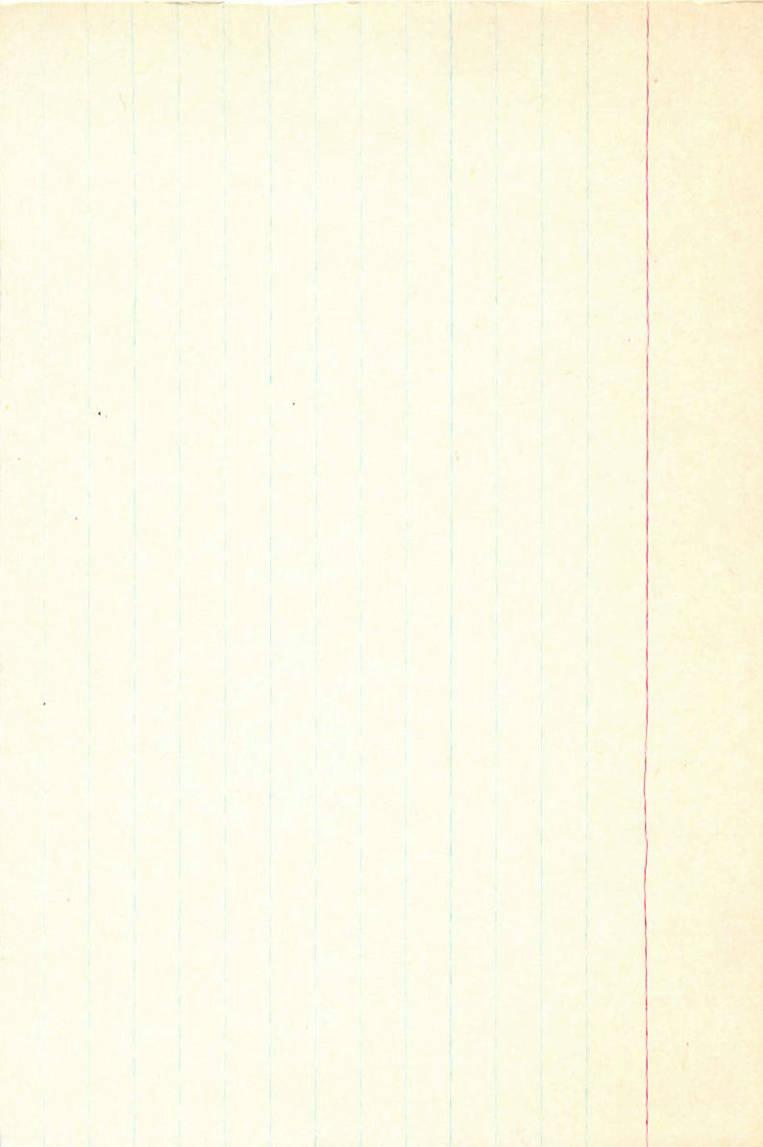
15.4(1.2 -15.31

140417

5.40 +0.24 (1.60)

-00257 -060

-446	265	-855	+0763	-0754	+0004	0	+26.7
642	740	-116	-1133	-2104	-3237	-140	+3.6
-603	615	505	+1032	-1756	-0726	-32	-15.8



-45.889

ART 921

18

44

413

-45

86 34.9

F75

141145  
65541

-0123-063  
-01106-058

18994

113

-115-056

163 404 2.650

130 503  
122-490  
256 181

+3.7

8.000

0.69

18-547

37  
4



140728

15 41.5 752 31 5.5

Aug -16-16

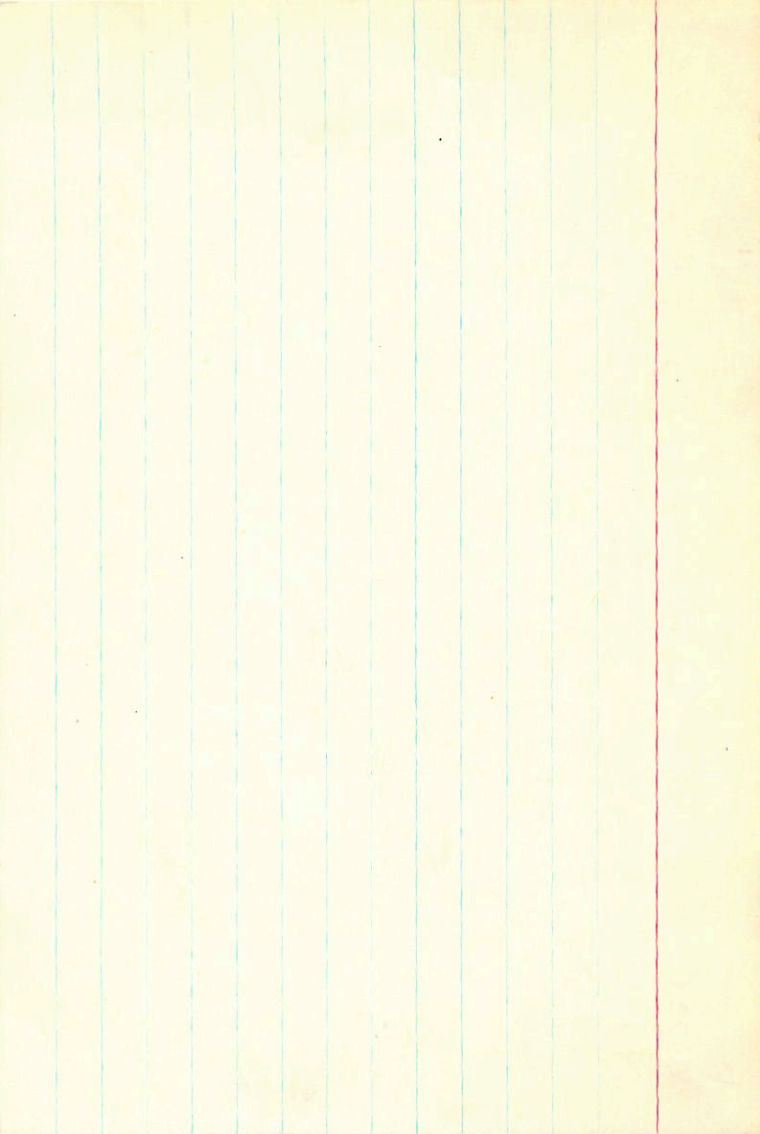
21154

-0076<sup>25</sup> + 028<sup>28</sup> N30

9077

-0074<sup>21</sup> + 029<sup>21</sup> 1.56-c → N30

-15.5 (9)



149039

15 43.0 + 03 08 26 L

+53.1806

2.27 400 181 369 ①

25 Ser

S.O. 1 = 349

W 9091

15 43.5 -01 39

5.4 -12.19

H 140873

-0020 ± 2.7

-043 ± 2.3

-0002

-029

0621187

15 43 30.285 1500.5 -1 38 5-6.59 1900.0

99  
334

2.15  
54.44

42 59.260 -004

37 3.17 1940.77

31.043

-1 52.81

43 3 0.303 4

38 55.98  
+ 19

307  
21 330

55.79  
26

228  
-006  
0001

55.53 55.62  
- 1.18

30.291

-0011 -036

55.74 1939.99

294

55.72

43 30.296  
40

38 47.18 1934.26  
234

5364/330

54.82  
54.50

-152-175-40

15 441 -40 02 (42+83 (1.53))

F.D. 10.20

Glaxo 1202

GS III-IV -275-42

-0155  
-0154 7100 -0417.65  
22.90 1894.6

5.457 1503.6 -0156

7.187  
730

2.07  
20.93

-0158 +8  
-044 +10

22.90 1894.6

40.79 1524.52

-0150

-0150

43.08

84

23.06

23.74 / 23.74

22.8 1985.3

22.86

25.780  
39.570  
5.920  
5.780

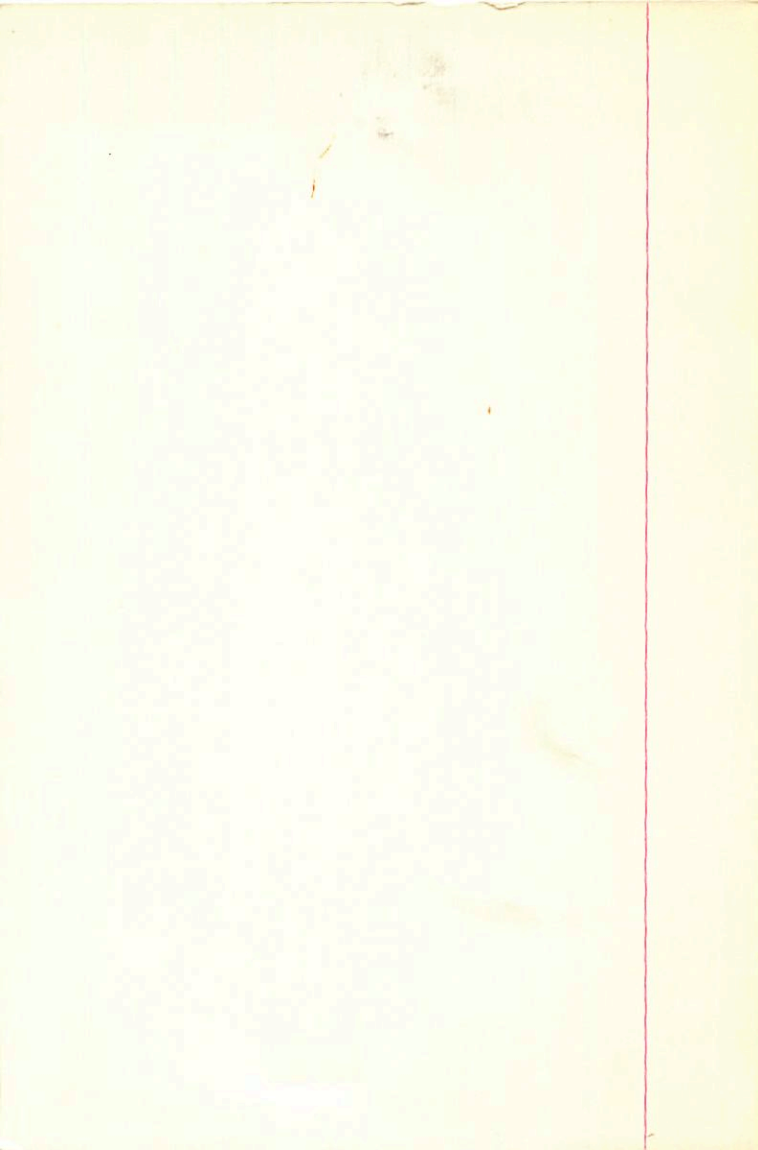
-0172

5.145

30  
710

17

140882 15 445 -49 35 745 +1.58 1244#  
-154





-0043±2.4 +031±2.2  
-0042 +039

0040±058

141187  
21224

45.0±0.3 +14 16 40 -3428

0041  
9100

5.72 +0.09 +0.06 A2E -063 +031 CC

HR5570

52.851 1910.3 +14 16 5.15 1506.2

W9100

971E  
58,022E

-1.36  
3.79

57.925

26.5

1820  
910

4.82 1934.2 X

57.887  
876 -112

-14  
4.68 1939.43 36.8

13.63

5.40 1939.43 36.8  
-128 996  
5.2 4.98

30.0

57.77  
+5.77  
774

-00430 +0330

-00400 +0315

+1.19 2491 -9250 073  
-6619 3810 0182

-0610  
60 059 +0474 474





15.750  
14.250  
-60.000  
42.000  
4.790  
91  
-34.200

90.75  
94.38  
95.05

-0.429  
0.656  
-0.620  
248.989  
43.821

0.660  
0.697  
0.281  
-43.160  
-13.524

-0.617  
0.289  
0.732  
227.501  
-4.391

8

-0147 I 4.6  
+070 ± 3.4  
-0143  
+072

141472 15 45.4 +55 38 5.9 9103 -4.08

21233

9103 22.923 1897.8 +55 37 32.91 1901.6

767  
23,696

47.17  
36.118  
23.232

1276 9293  
276 23.091  
23.990  
20 23.0105  
23.01

27.956  
27.291

-3.39  
37.52

14.8 19278  
38.80  
36.00  
56  
36.56

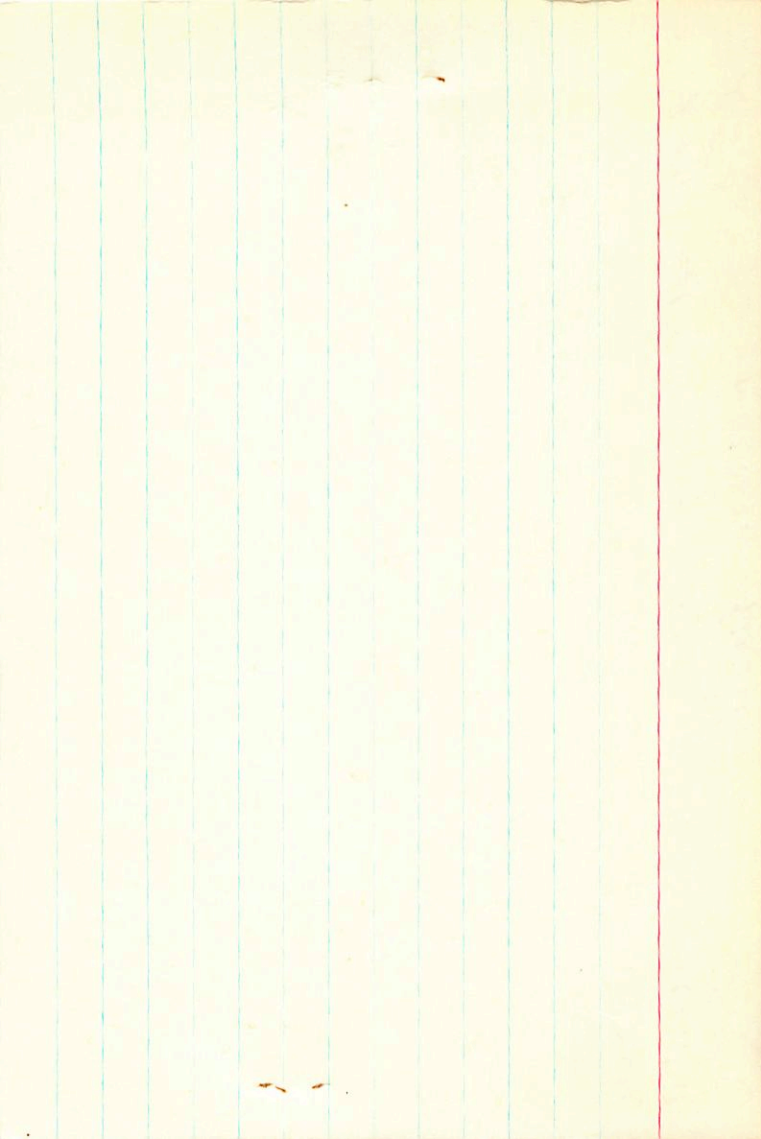
42.2

21.88  
37.29  
+2.77

36.42 1944.74  
37.86  
-34

37.522 1947.29  
37.827  
-33 37.94

11.983  
40.0  
38.4



1956

638 125

+31 52

15 46.0

5877

1028-05066

-2 75

1026 044

19





5877.000\*

15.000\*

46.000\*

31.000\*

52.000\*

0.026\*

-0.045\*

6.500\*

199.526

-19.500

-0.226

-0.394

-37.445

-0.042

0.481

-17.751

15

305m

141378

15 463 -3 40 5.6 A3 -16.4b

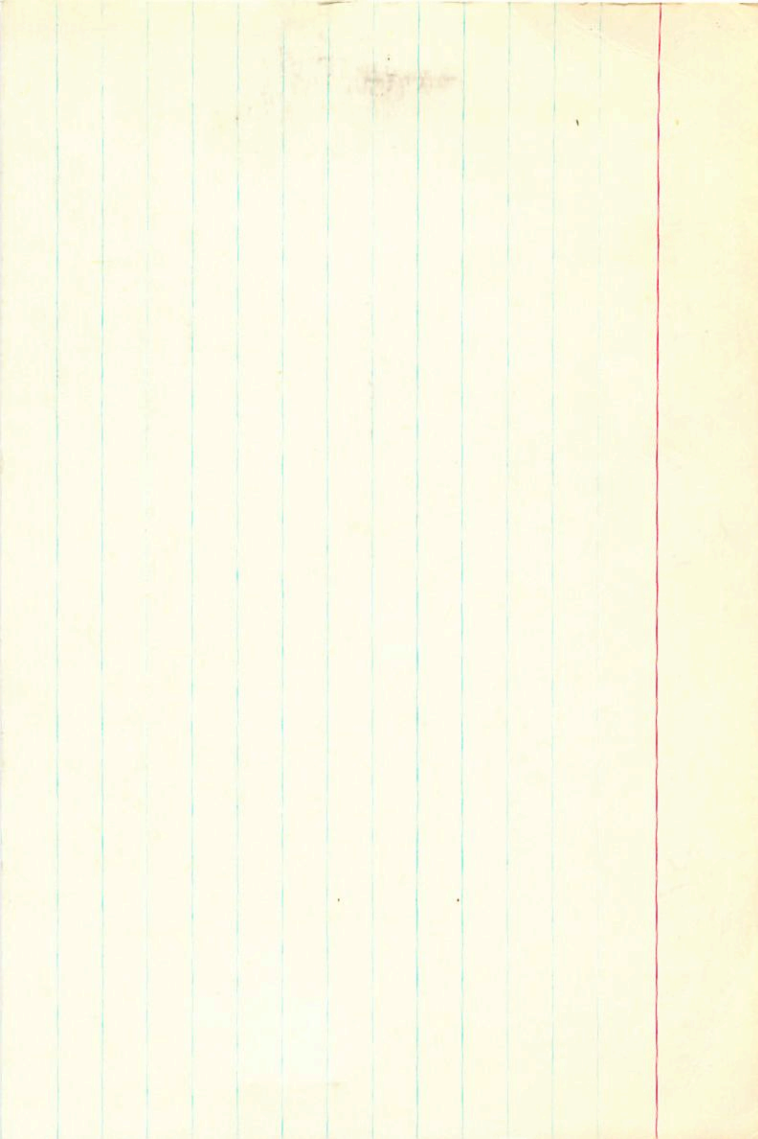
21251

0015<sup>29</sup> 1007 30 N30

9112

-0023±2.2 1007±2.166 7030

6456 93.9  
-9949  
8801 1088  
-9666



11675  
 +0012 ±3.2 +003 ±3.2 0.0 (P)  
 +0011 -001  
 HRS87 21253 15 46.4 555 32 Am -2.48.

910

5.70 10.10

0.18

1010 1003 6.2

10m 11

25.210 1892.1 +55 31 44.69 1890.1

AD5971

-069

2.17

44.51

AD5973

49.05

36.148

5.198

230

236

48.6

196

265

1054

25.259

20

25.285

25.250

25.272

119.18  
39.7

49.6

20.8 1927.0

36.92

43.87

44.56

44.74

44.30

44.96 1944.89

-24

44.62

138

44.46

-05

44.79 1947.29

-32

44.46

-520 -570 824 564 +010 +003 -2.4 002-2 009  
008 002 -006 -001 043 -015 +1 +1 014

$$\begin{bmatrix} +4 & 0 & -1 \\ 0 & +1 & -3 \end{bmatrix}$$

$$+5 \quad -6 \quad -1$$

$$\begin{bmatrix} -1 & +1 & -4 \end{bmatrix}$$

012



(280) 1523

474 850

-011

①

254  
248  
220  
245  
245  
214  
214

30.707 64

-0204 ± 24  
-0005  
-0004

-022 ± 2.0  
-021 31.178

3.5

21  
228

-0004

102  
3290

-33

301685  
617

64454

11

3244  
3212

301644

67.11

31.50

15.75  
+153

+5  
701

-34  
21.56

-2

-0205

-0004

-005

74  
9.5  
107

-002 -014