

7256

8.26

+0.525

+0.04

F8V -22.2

139007

+25° 29' 32"

$$\begin{array}{r}
 +.028 \\
 -.004 \\
 \hline
 +.024 \\
 -.003 \\
 \hline
 +.021
 \end{array}$$

$$\begin{array}{r}
 -.121 \\
 -.004 \\
 \hline
 -.125 \\
 +.005 \\
 \hline
 -.120
 \end{array}$$

$$\begin{array}{r}
 15^h 32^m 40.390 \\
 \hline
 40.402 \\
 \hline
 40.400 \\
 .001 \\
 \hline
 401
 \end{array}$$

$$\begin{array}{r}
 +25^{\circ} 10' 1.85 \\
 \hline
 1.64 \\
 +25^{\circ} 10' 1.50 \\
 \hline
 .31 \\
 \hline
 .19
 \end{array}$$

1928.38

1930.2

139007

15

32.6

+25 10

8.5

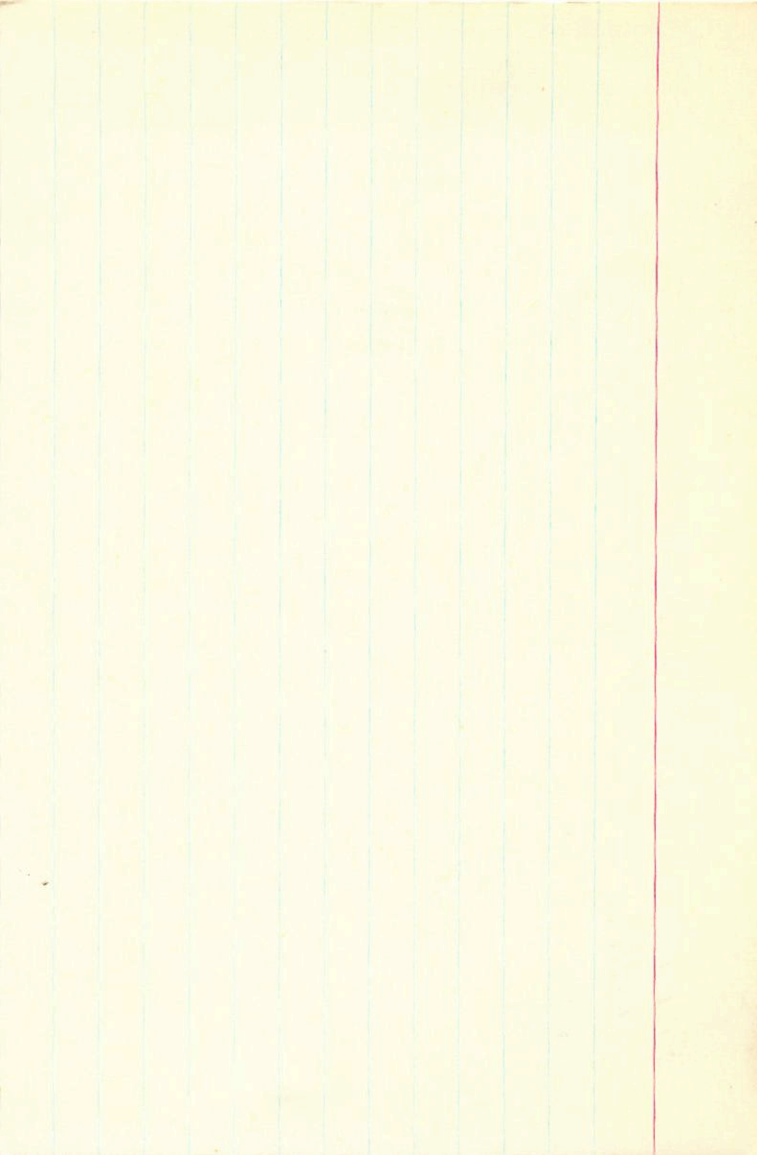
F8V

-2226

+2502932

8991

+028 "121 Y



8 Jul

138905 15 32.7 -14 37 4.0966 -27.52

20949

85

26.24

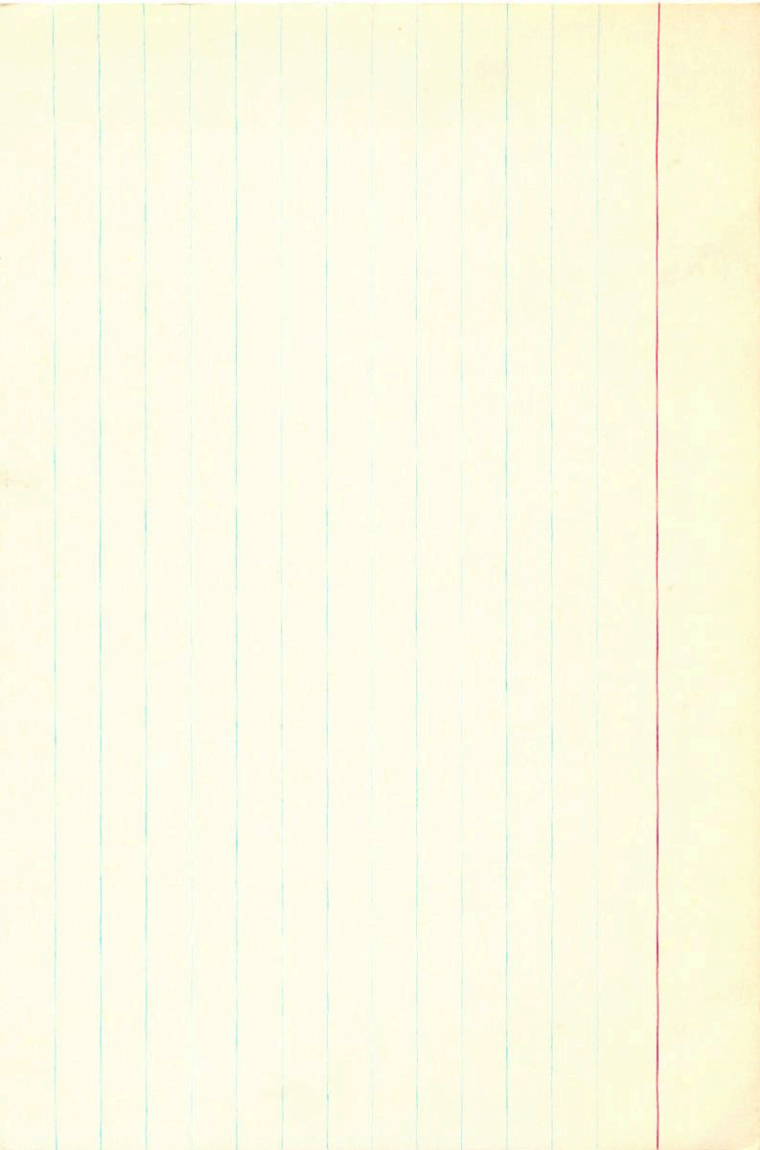
8992

+0043 +00484N30

+00454.0 +00241.06c → N30

11  
Aug 20  
New York

Analysis



Qumc

139669

20952

8994

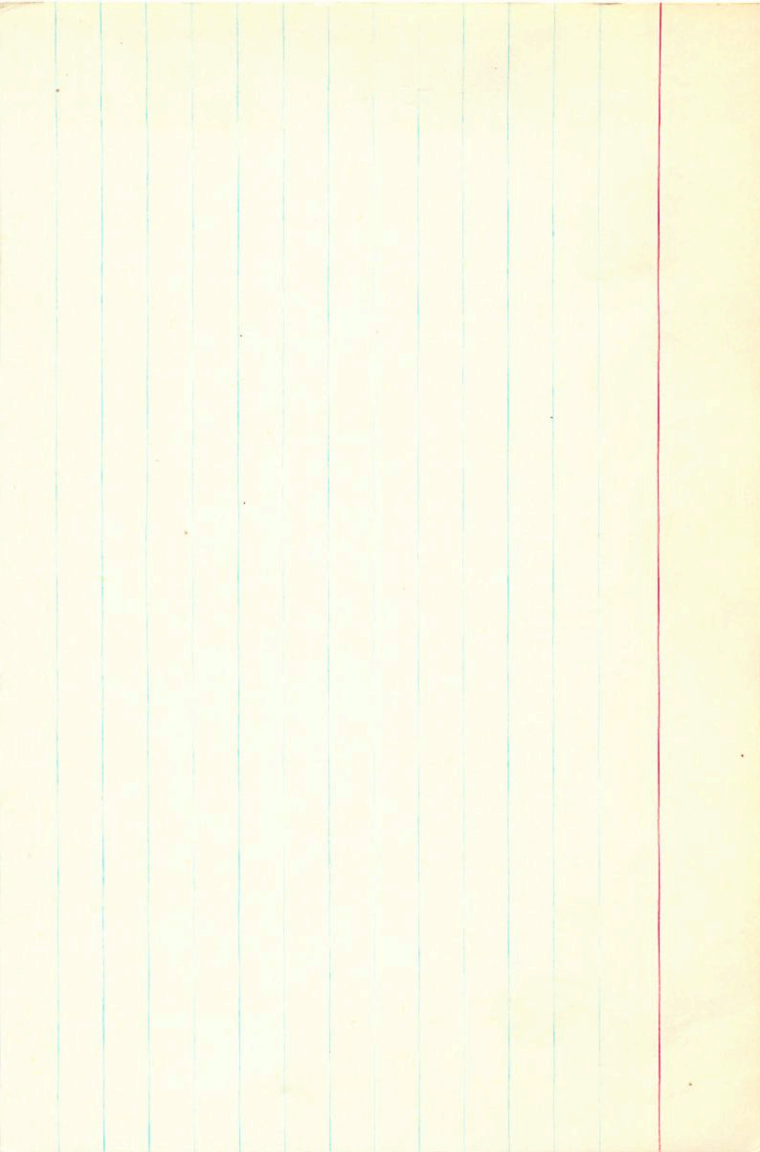
15 32.9 +77 31

-0154 41 +011 45 N30

-0158 ± 1.5 J011 ± 1.2 GC → #30

5.3 9124 -25.0a

-26128



7th Dec 1640 1077 15 231 164 04 AS 4th Dec 1642

139319

+2.8

pp 110  
63

1644 1648 AG 12

00000

+008 7021

1649 1646 P  
9.2 3.0



6

10

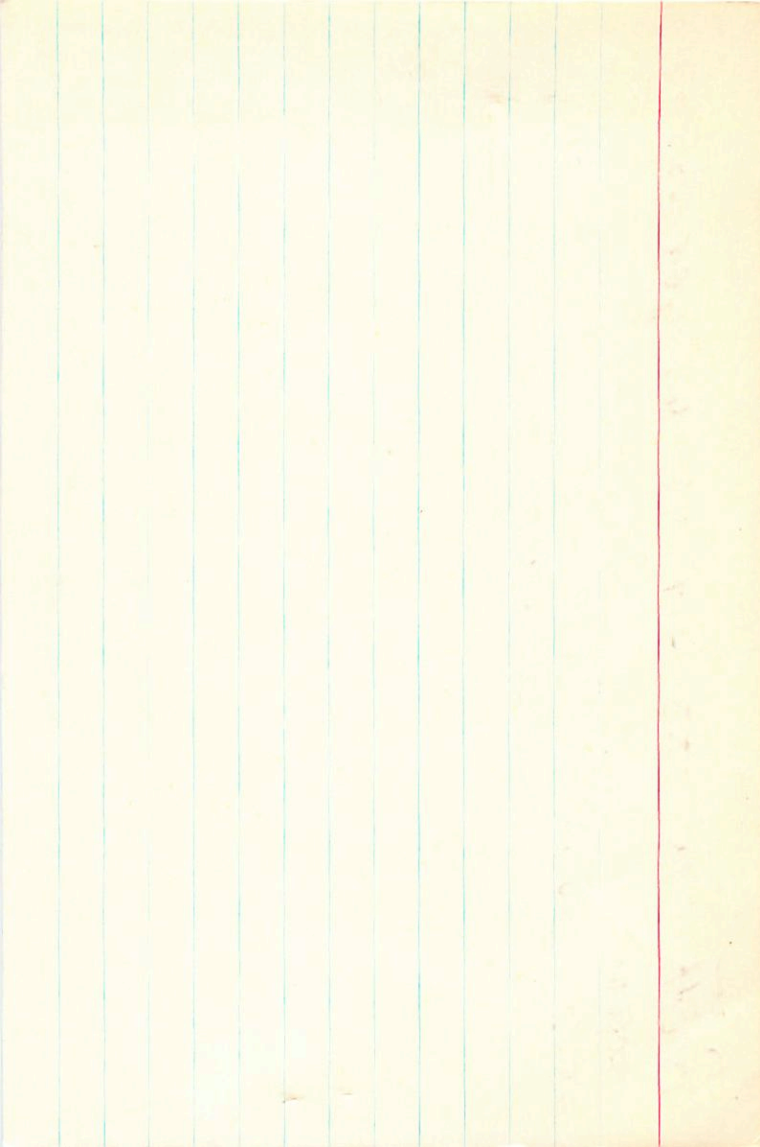
15 Sun  
139074

15 33.3 +17 49 6.1 908 -22.30

20962

8996

-0053<sup>23</sup> -018<sup>23</sup> N30  
-005752.4 -016±2460 → N30



139087

8.744

15 33.5 +11 25 6.0 9100

$$\begin{array}{r} 108 \\ 30.348 \\ \hline 506 \end{array}$$

12.9

$$\begin{array}{r} -0029 \pm 5.7 \\ 0007 \\ -0005 \\ \hline 0005 \end{array}$$

50.20 10.7

~~$$\begin{array}{r} -043 -019 00 \\ 0 +6 \\ -013 \\ \hline -260 \end{array}$$~~

$$\begin{array}{r} 30.453 \\ +11 \\ \hline 464 \end{array}$$

(70.66)

$$\begin{array}{r} 50.24 \\ -38 \\ \hline 49.86 \end{array}$$

$$\begin{array}{r} 30.471 \\ +8 \\ \hline 479 \end{array}$$

66.74

$$\begin{array}{r} 50.23 \\ -89 \\ \hline 49.83 \end{array}$$

$$\begin{array}{r} 20.464 \\ +11 \\ \hline 475 \end{array}$$

(11.80)

$$\begin{array}{r} 50.54 \\ -85 \\ \hline 50.16 \end{array}$$

$$-020.2 -01115$$

13.125

10



5796.000\*

15.000\*  
33.500\*  
11.000\*  
25.000\*  
-0.043\*  
-0.013\*  
5.000\*  
100.000  
-26.000

0.057  
-0.630

22.074

-0.180  
0.214

-23.503

10

0.099  
0.747

-9.475

0.469  
0.876  
0.112  
69.769  
17.839

0.664  
0.266  
0.699  
51.218  
14.821

-0.582  
-0.402  
0.707  
-11.695  
-13.518

9

-0015 ± 4.2  
-8017  
+001

139357 15 33.9 +54 05 6.0 g 114 -9.98

20977

9003 56.671 1897.9 +54 5 12.53 1593.4

078  
749

16.97

39.712

~~56.685~~

706

713

138 202.3

~~692~~  
678

~~657~~  
671

427

+62  
13,15

712.3 1928.0

59.32

12.98 961

12.60

13.58

73.44

13.29 1945.30

12.95

13.20

+0.5

12059

unc

40.2

46.8

1447.24

13.40

16  
22

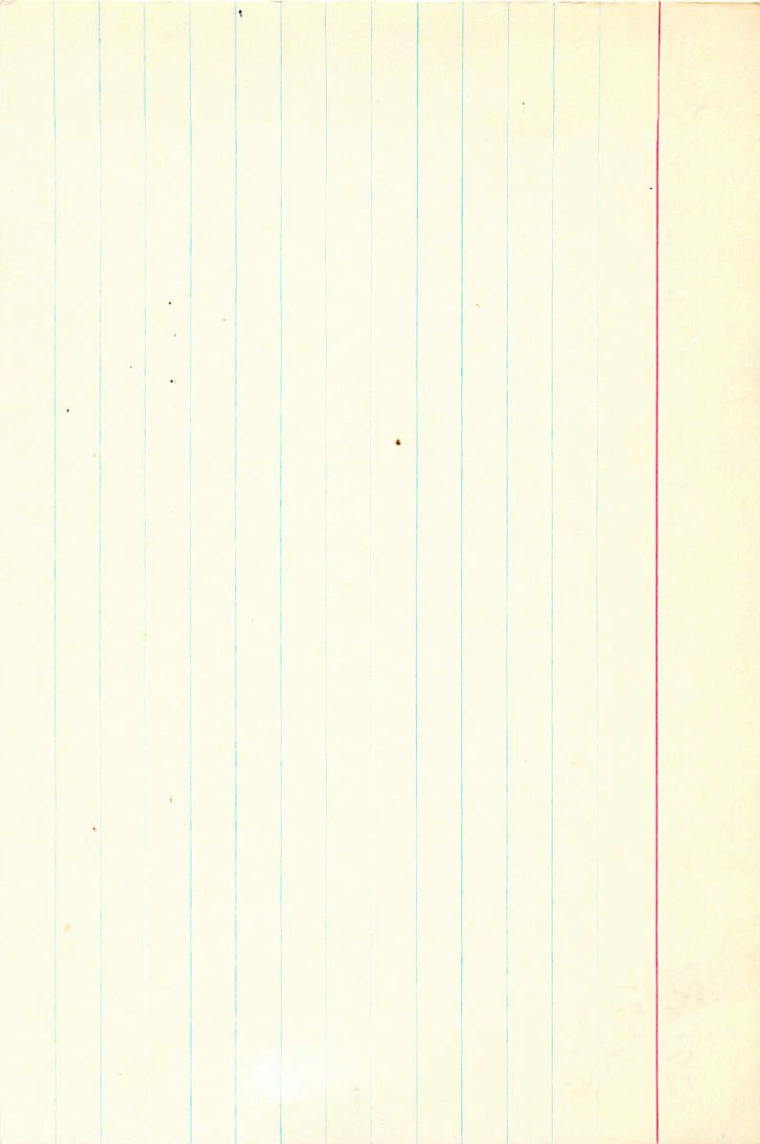
56.649

670

54.624

640





25 bit

139063

15

34.0

-27

58

3.8

gms

-24.9a

20979

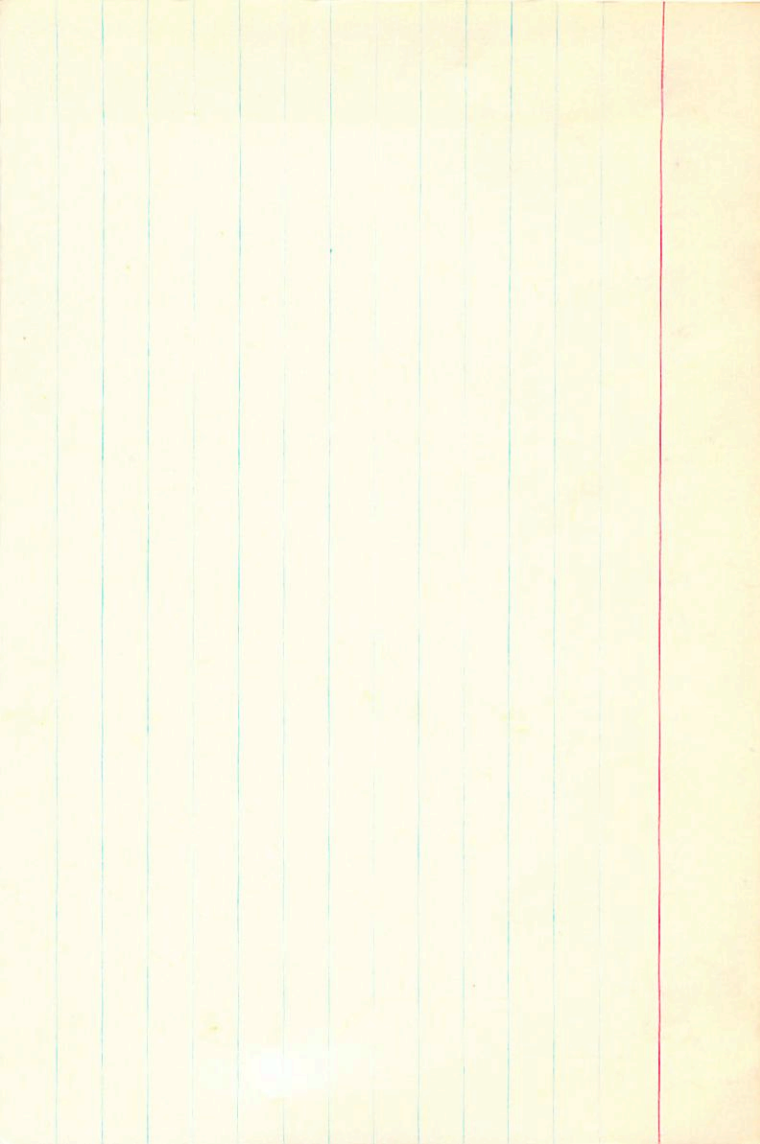
9005

-0010<sup>41</sup> 000<sup>44</sup> N30

-0008±2.~ -001±1.96c → N30

37<sup>±7</sup>

12<sub>m3</sub>''



139195

15

.341

+10

||

N1-Ba1

+7.8 a

+249

Argue

5.26 + 0.95 + 0.67

+0.24 - 124 G-C+new →

$\pi = .011$

.031

$\pi_{tr} = .030$

wt

$\mu_V = +0.4$

+2.65

= ~~2.65~~

$\gamma$  -45

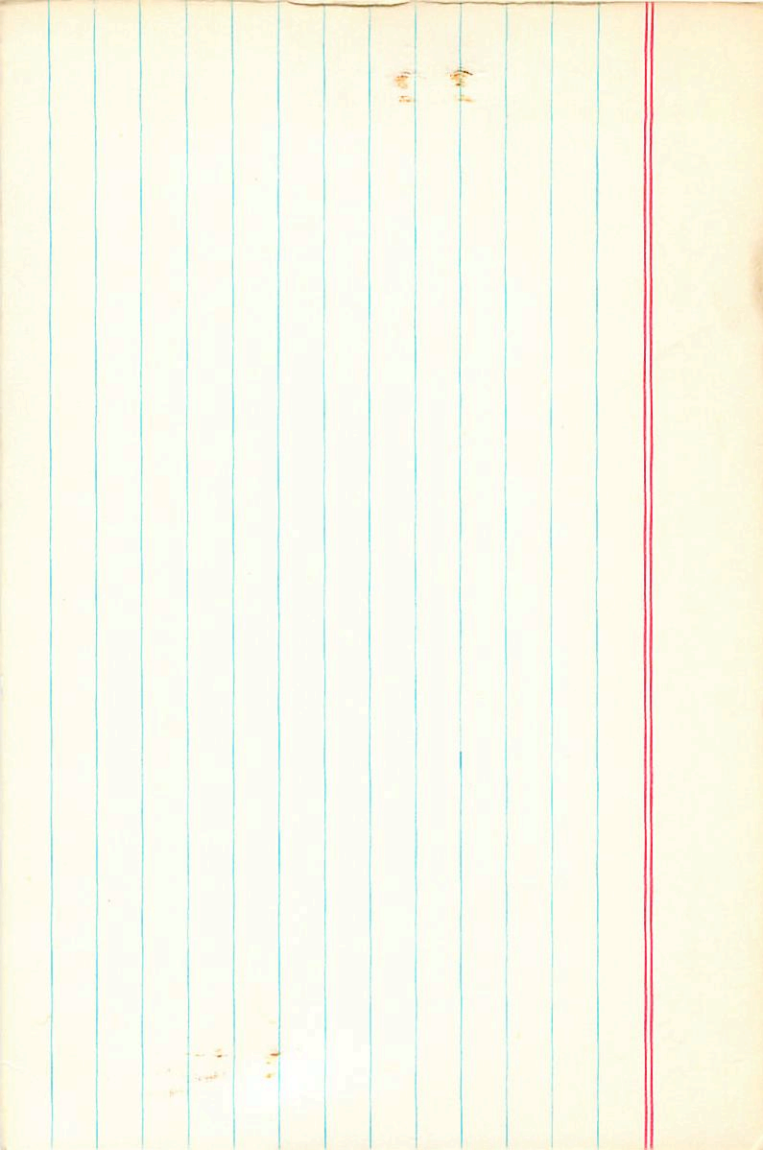
-20

$\nu$  -25

-8

$w$  -21

-3



165m  
 139195 15 34.1 +0028 ± 3.0 -136 ± 2.2  
 +0021 -125  
 +10 11 5.4 ~~10~~ 7 +7.8a

20981 ~~165m~~  
 +0025 -127 →

9007 5.258 1903.1 +10 10 33.62 1400.2

30<sup>47</sup>  
 A(20)

-131  
 157  
 5.196  
 17  
 213  
 5.239 228  
 4  
 243 +071

+037 -127

34.3

260

5.26 +95 +66 4 20 "

487 31  
 453  
 4.08

+6.77  
 40.39

36.60 1934.6

-14  
 36.46 1147

35.21 1940.30

-20  
 35.01  
 35.74

-4.65

+4.90

37.4

37.2

487 31

44  
 4.81  
 4.08 1.47  
 261

11





139195.000\*

15.000\*

34.100\*

10.000\*

11.000\*

0.037\*

-0.127\*

2.600\*

33.113

7.800

147

w sup  
 139127 15 347 24 4.3 MO -7.08  
 2001 4.35 + 1.40 + 1.69 <sup>5.85</sup> 4.36 + 1.44 MO III -6.4 ± 0.4  
 9010 40.567 1407.0 -42 24 17.68 1900.9 -6.2 156.

SD ±  
 +055 ± 3.0  
 +056  
 -0132 ± 4.4  
 -0137

7.9  
 -4.4 104  
 -6.4 6.1

-2.70  
20.38  
 18.05 1980.43  
 -22

1141  
570  
 565

17.03 1956.02  
 -19  
17.22

40.482  
415  
 414

96.45  
48.2  
47.3

17.74  
2.64

139475

45-48  
1304  
5797

129127

21021  
1501

61324 + 0590  
657

+26 + 357003  
-0135 + 0555 mm

139 + 068  
-138  
-1455  
-1474062

42-45  
1496  
m = 353  
15 347

23 584  
-42 24

no 11

433 + 43 + 1725  
432 + 42 + 700

422 + 42 + 1725 + 1711

3.57 + 0.55 = 3.62  
3.62 + 0.5355 = 3.62

3.57 + 0.55 = 3.62  
3.62 + 0.5355 = 3.62

6.5  
324

250  
74  
324

358  
324  
324  
324  
324

713  
-24

5797.000\*

-15.000\*

34.700\*

-42.000\*

-24.000\*

-0.139\*

0.066\*

4.800\*

91.201

-6.500

0.259

-0.875

29.279

-0.245

-0.450

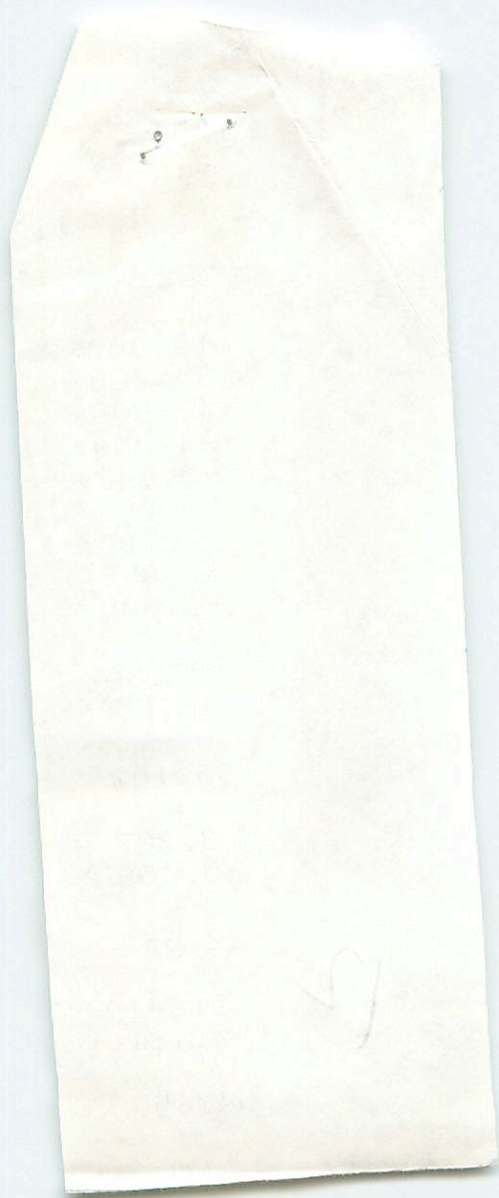
-19.391

0.641

0.181

57.304

V2



5797.000\*

15.000\*

34.700\*

-42.000\*

-24.000\*

-0.147\*

0.062\*

4.700\*

87.096

-6.500

0.280

-0.875

30.103

-0.287

-0.450

-22.059

0.641

0.181

54.658

M

-6025 ± 6.4 +075 ± 6.4  
-0016 +077

139478

15 387 +52

14<sub>6.5</sub> OAF -15.98

HR587

6.5

-023 +075 6c

139478  
21000  
9015

39889 1895.9 +52 13 57.98

135  
40.024

1795.9 -014 +090 6u(2)

-4.06  
53.92

-015 +088

57.98

42.0525 1426.6

39.652

54.1

58.15 1927.3

55.95

21.88

43.9

56.55

57.29

119.52

955

39.932

57.97 1144.93

39.8

955

-89

+3.37

43.9

39.938

1847.29

955

58.18

57.9



~~-806-552-750~~ 413 -015 +088 -15.9 070 -13 256

-012056009-041 137 395 -9.7 +6 +5 005

+23 +16 1.9

139254  
21005

15 34.9 -22 59 5.8 9100 +7.18

-0017 ± 5.1 -088 ± 5.1  
-0023 -091

9019

51.362 1406.5 -22 58 39.53 1406.2

074  
51.436

23.194  
28.138

57.332  
55  
38

372  
064

51.369  
-12  
357

27.6

3.85  
34.68

39.78 1127.69  
59.15

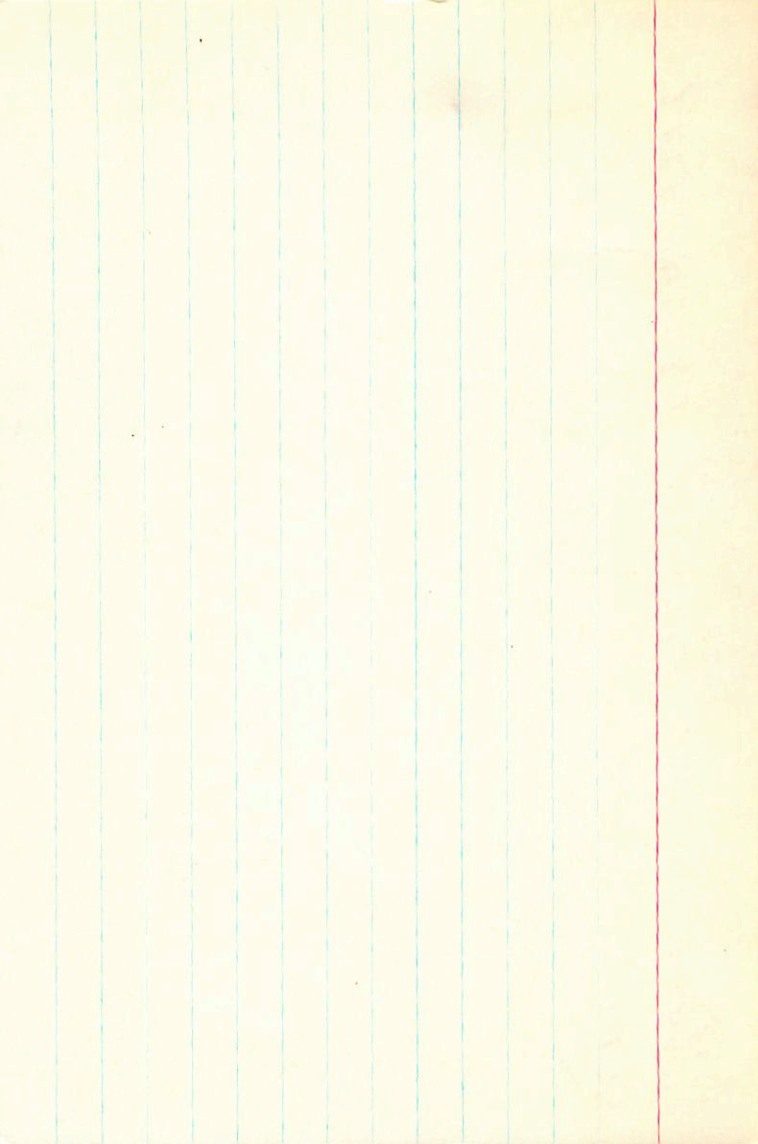
37.93  
130  
36.63

37.55  
-27  
37.82

37.22  
2.54

445 6823  
34.1

1940.54 27.9



+0096 11.3 -370 ± 9.5

139487 15 35.6 +10 24 dF7 +38.28 WS(6)

6621020 7.10 +0.50 -0.06 F6E

+102586  $\delta = 0.6$

+3532 34.869 / 899.8 +10 24 26.5718969 +11.12 -370 G-U

W9024 -482 +19.65 +153 = 368.88

19A128 387 46.22

34.659

-800 -600 150 583 +145 -320 +35.2 -067 +7.1725

116-053-087040 360 ÷ 640 -23 -30 -55 025

1 -48-236

5 24-41

9 9-226

-10 -54 +69

-78 -22 -81

-13 -49 +54

-64 -16 -11

035

7 -43-20

-6 22-82

11 4-20

5902

139211

15 35.8

-59 45 F8E

-215-46

F0975

621027

302

5.95 + 0.48 (1.62)

-0.144

-0.166 ± 5.8

-220  
-225 ± 4.3

50.056 19048-0172

27.21 1844.6

750

11.34

(69.5)

-125 -222

-0.170 / -220  
+10

25887

-59.75

49746 41.01  
-46  
0

47.469 = 49.6

~~1012-5811~~

35.84  
58.459

1928.78

41e -  
-214

Le 1h

2.677  
61.149

-117

39.07  
3422

3.0  
21e

8828 -752  
-1168 -649h

150  
6/4  
150

~~0168-0910~~

3422

01616-0114

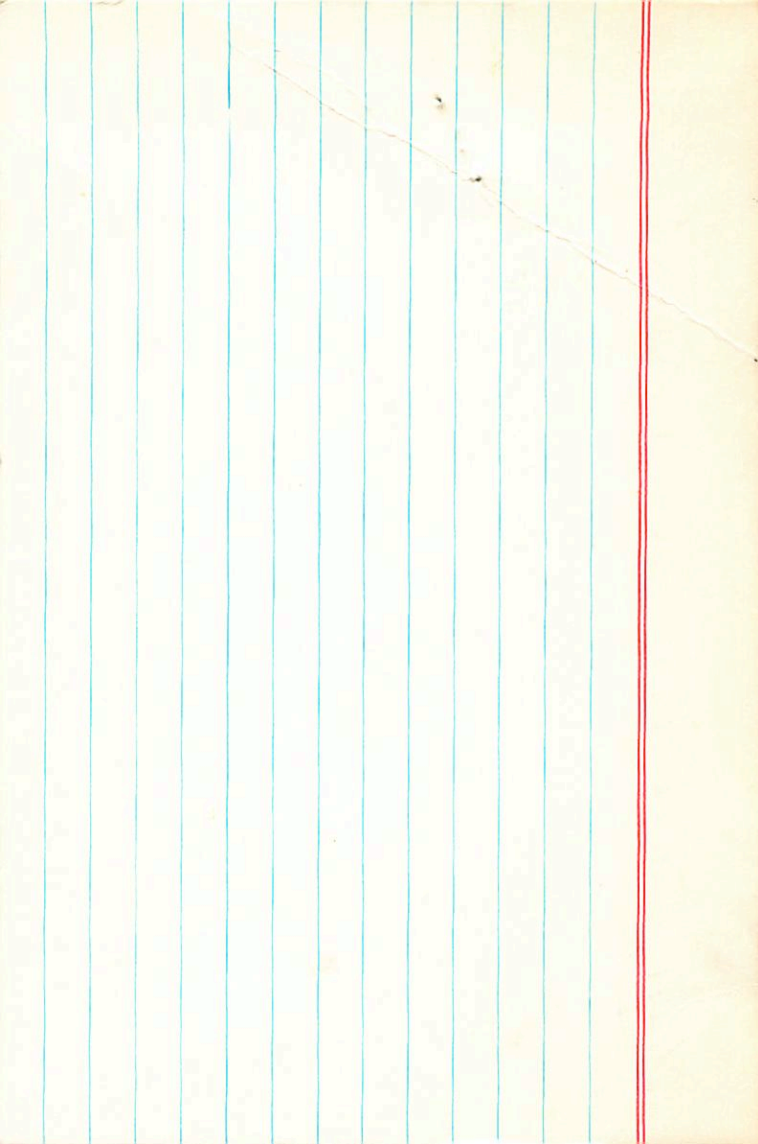
3423

50.272

0200

85.8

124  
21e



7600 Sp.

139211  
HR5803

15 35.8 -59 44 F80

GC21027 4 14 13 5.59 +0.505 -0.01 255L

17A A 7  
17B 5 4 7  
5 4 4 7  
5 4 4 7  
5 4 4 7  
5 4 4 7

.326 .136 .482 2.645 @ 4,10,6,2

[m] 155

-117 -215  
-210

323 147 403 2.645

[5] 417

900'

-462 -402 -280 12562 +4002 +6564 +30.0 +17.0  
-664 434 -609 -3642 -4320 8012 -3.0 +13.1  
-598 806 -060 13261 -8023 4762 -8.2 +1.4



103  
124  
161  
163  
169  
8

13

192.0- : (M) IP  
489.0 : (M) SP  
429.0- : (M) SP  
000.0- : (M) SP

355.0 : (V) IP  
044.0 : (U) SP  
288.0- : (U) SP  
510.008- : (U) SP  
745.002- : U  
V

924.0- : (U) IP  
962.0- : (U) SP  
997.0- : (U) SP  
518.072 : U  
128.00 : U

002.15- : .JEU .DAM  
04 : BUJUDM  
000.0 : ZUMATEID  
3.000 : .DEC : M9  
000.000 : .A.R .M9  
000.005- : .DEC  
000.00 : .A.R  
000.01 : .A.R

R.A. : 15.600  
DEC. : -59.750  
PM. R.A. : -246.000  
PM. DEC. : -214.000  
DISTANCE : 3.000  
MODULUS : 40  
RAD. VEL. : -21.500

q1 (U) : -0.459  
q2 (U) : -0.400  
q3 (U) : -0.793  
dU : 675.612  
U : 43.951

q1 (V) : 0.663  
q2 (V) : 0.440  
q3 (V) : -0.606  
dV : -835.612  
V : -20.247

q1 (W) : -0.591  
q2 (W) : 0.804  
q3 (W) : -0.064

-0017 ± 4.6      +005 ± 3.4

139569    15    35.9    +30    16    8.8    dF6    -2397    -272

21029

9.0    dG-1

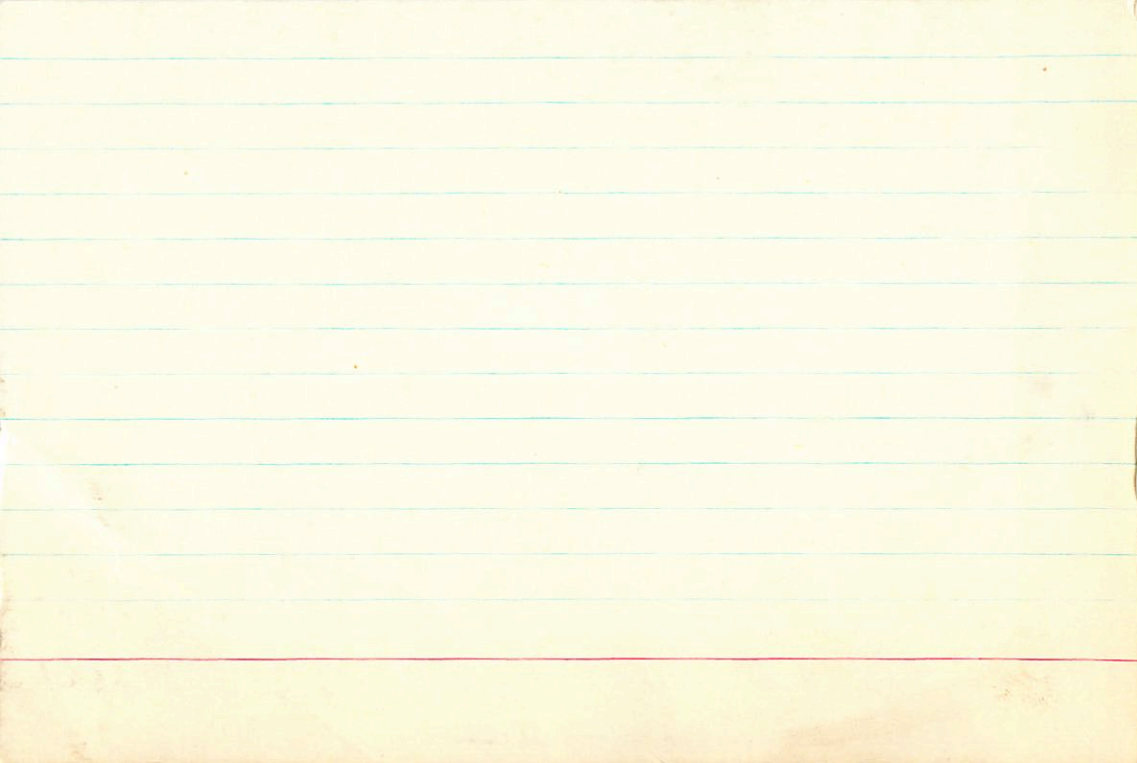
9025    51.682    1897.4    +30    15    53.95    1892.7

AD59727    689  
              771

529  
5366

51308

5672    1931.4



-0045 ± 3.3 -022 ± 2.5  
-0057 -023

139778 15 36.2 +54 40 6.0 9181 -22.86

21036

5032 14.708 1898.5 +54 40 18.16 1902.2

$\frac{232}{940}$

$\frac{+1.05}{79.21}$

36.120  
~~36.120~~  
149.44  
746

37.6

43.6 1925.4

$\frac{1107.26}{39.1}$   
36.9

72  $\frac{724}{716}$

18.54 107

14691

+212  
71

18.90

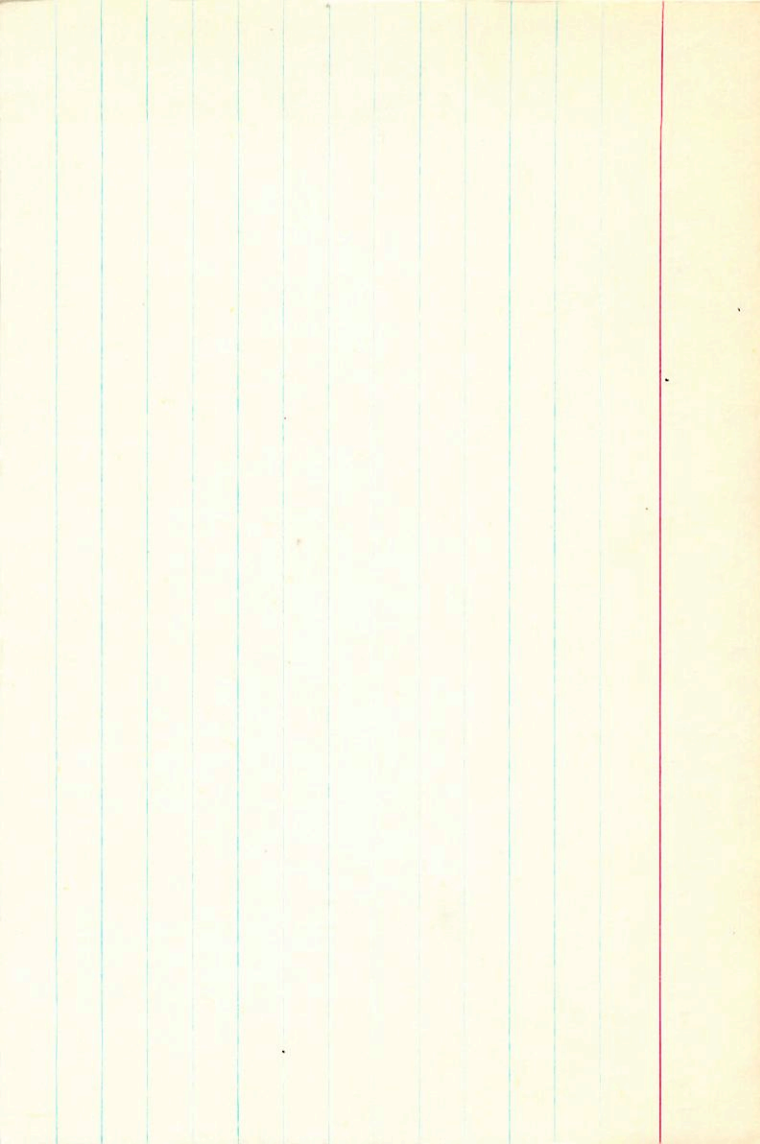
18.36  
85

146700  
714

18.45 1944.57

-37  
18.08 1947.29

18.27  
18.09



139590 15 36.5 -00 09 dF9 -27.58

-201 -100 Y

<sup>s</sup>-031 -083 Gm 50



1120  
-810 - 556 0 1 | -200 -100 -27.5 0 0 -425  
-162 0 117 0 -765 5-54 -27.5 +16 +22 03  
-10

+0010±2.5  
+0008  
-021

139521 15 36.6 -34 15 4.6 0.5 -23.1a

21042

9036 35.039 1899.8 -34 15 0.65 1899.7

$\frac{-0.50}{34.989}$

$\frac{+40}{0.25}$

35.030  
-16

014

0.97 1939.52  
 $\frac{-22}{1.19}$

$\frac{0.27}{0.38}$   
+ 0

47.9

9534

$\frac{2.49}{1.24}$   
 $\frac{-0.99}{-0.99}$

47.7

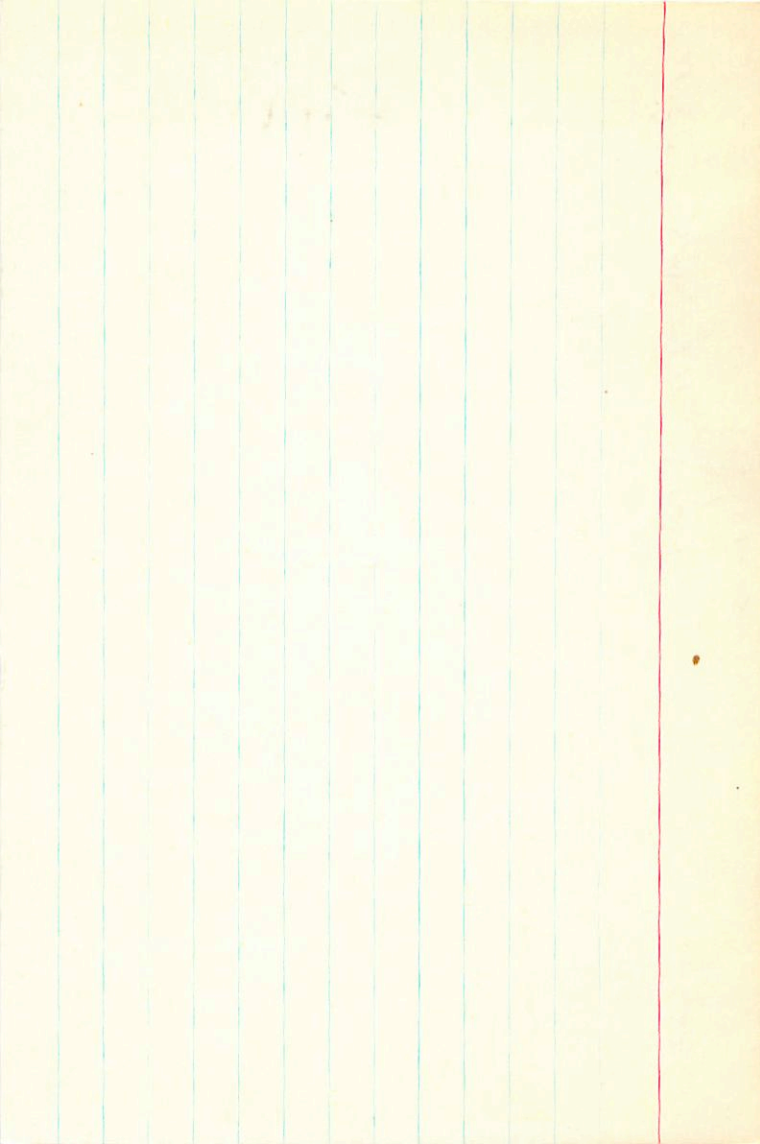
48.0

35.037

$\frac{2.40}{0}$

01.07 1955.82

$\frac{-27}{1.30}$



$$\begin{array}{r}
 -0005 \pm 13.0 \\
 0 \\
 -092 \pm 15.0 \\
 -076 \\
 \hline
 -44 \ 52 \ 14 \ 11 \\
 -22.1 \pm 0.5
 \end{array}$$

c, 14j

$$139465 \quad 15 \ 36.7$$

$$21047$$

$$2.40 + 1.25$$

$$\begin{array}{r}
 41.109 \quad 1902.9 \\
 024 \\
 \hline
 .133
 \end{array}$$

$$-44 \ 51 \ 34.11 \quad 1903.4$$

$$\begin{array}{r}
 4.29 \\
 \hline
 29.82
 \end{array}$$

$$\begin{array}{r}
 57.465 \\
 43550 \\
 \hline
 41.015 \\
 41.117 \\
 \hline
 1302 \\
 \hline
 122
 \end{array}$$

(39.4)

$$\begin{array}{r}
 08 \\
 134 \\
 \hline
 0
 \end{array}$$

$$36.93 \quad 1929.27$$

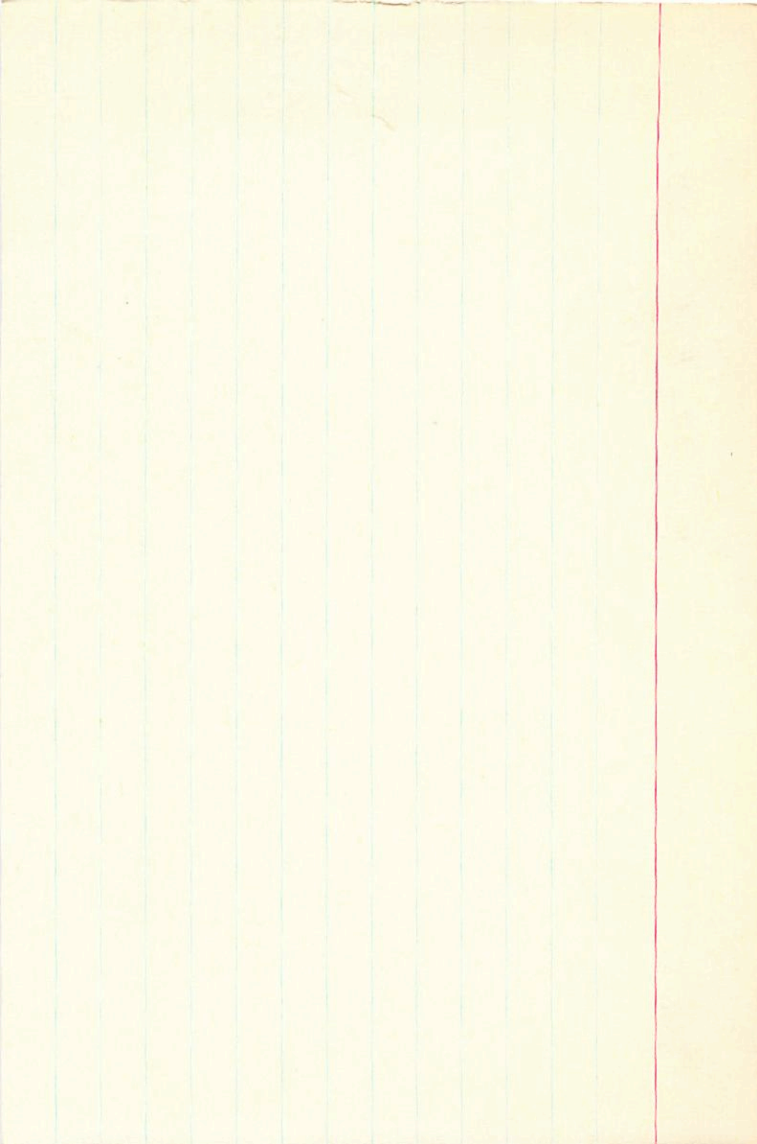
$$\begin{array}{r}
 56.40 \\
 \hline
 33.33
 \end{array}$$

$$\begin{array}{r}
 81.53 \\
 \sqrt{173} \\
 \hline
 384
 \end{array}$$

$$\begin{array}{r}
 557 \\
 3278 \\
 \hline
 3331 \\
 1577 \\
 \hline
 -2.96
 \end{array}$$

$$\begin{array}{r}
 41.158 \\
 512 \\
 \hline
 140
 \end{array}$$

$$\begin{array}{r}
 31. \\
 33.41 \quad 1955.24 \\
 \hline
 -19 \\
 \hline
 380
 \end{array}$$



-0015 ± 1.8  
-0012 -018

4264  
139663  
21057  
9042

15 37.3 -23 39 5.1 @ 104 -21.88

19.178 1898.5 -23 39 25.90 1897.7

$\frac{077}{1255}$

$\frac{50.545}{28.608}$

$\frac{19.153}{19.54}$

$\frac{.209}{.24}$

$\frac{215}{19.224}$   
 $\frac{-12}{212}$

1.24  
 $\frac{27.64}{}$

31.76 1927.51  
 $\frac{5482}{}$

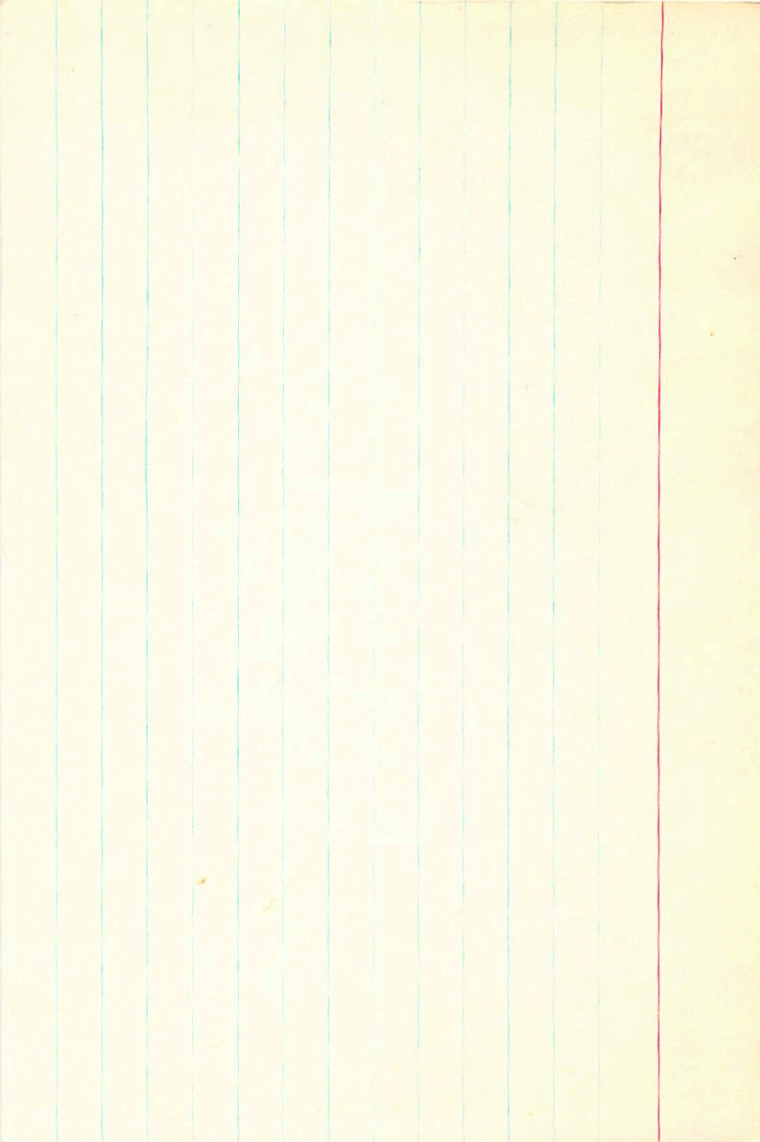
$\frac{214}{-041}$   
34.7

$\frac{26.58}{1320}$   
 $\frac{25.11}{25.15}$

46.66  
 $\frac{83.3}{35.6}$

25.12 1939.11  
 $\frac{-27}{}$

$\frac{25.39}{25.27}$  - .63



5844

$$15 \cdot 37.5 + 69 \cdot 26$$

-2600

40h  
15h  
15h

$$-0.54 + 0.50$$

0.50 + 0.50

9882	6888	0728
<del>1532</del>	8686	0013
	7298	+08

0077

5.57

02-



$$-0007 \pm 7.5 - 015 \pm 6.1$$

139862

15 32.8 +12 13 6.3 965 -2106

21073

-189③

9048

48.400 1895.2 +12 12 48.47 1891.7

ANS9740

$$\frac{038}{438}$$

$$+87$$

$$49.87$$

$$48.358$$

$$49.31 \quad 1954.0$$

$$-9$$

$$49.22$$

