

90861 10 27.1 +28 50 6.9 110 +28.6

14409 45 +28.2 (2)

6580 +6005 -1001 N30 +37.5 (2) 86

+0010 -003 = 4.0 (2) → N30
±5.0

91056 10

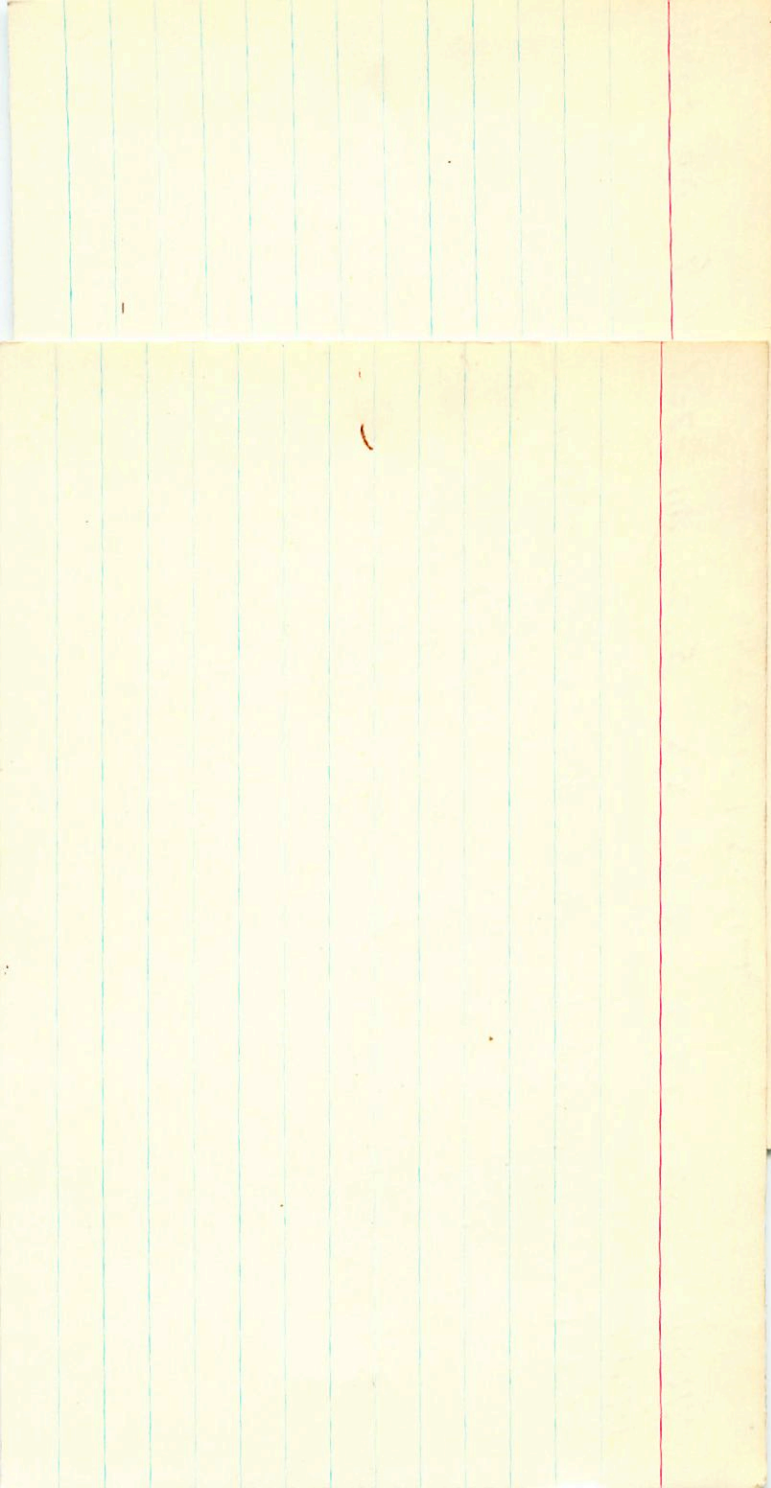
14419

6584 12.66

05
723

12.606

23
629



+56.1458

Y 2457

cp. to 364 MA

and +570.266

10

¹⁰
10

21.1

24.0

27.315.7

+56

44

+56³⁰

+56 14.86

300

90 M(6)

A 4.82 +51.00 F8V

+9.2a

(2) B 8.69 +1.36 +1.26 ~~7.7~~ JM

+12d 2ml

7.84 +0.555 (2)

Yale -165 -058

8.6 MO

Common prof. met. with No. 2459, 123" distant.

-0.176 -0.035

+9.2

0.6

7.07

6.91

4.64 +0.16 R

7.84 +0.54 R

30.000*

10.000*

27.300*

56.000*

15.000*

-0.176*

-0.035*

0.600*

13.183

9.200

0.686

0.559

14.178

-0.339

0.269

-1.996

-0.372

0.785

2.315

0977
005

1212

-1.0

134

46

46

+56.1458

10

22.2

+56

15.4

-184 -37

AGN3

+56.1459

10

22.4

+56

14.3

-170 -37

+57.1266

10

20.3

+56

46.5

-204 -64

0.3731

Y=60-0.201-0.41

0.084
14.7
+1.2

Y=60-0.239-0.86

S W350 F84
-0.2050 -0.37

371 172 -331 2615

374 160

31504

91011

6589
14434

~~10 27.9 +0.2 24 24 24 24 -0.78w(3)~~
w(+2.2)

7.1

+0042 ± 2.6 -046 ± 2.2
+0040 -043

56.042 1401.2 +2 24 26.70 1897.6

$\frac{205}{55.837}$

$\frac{2.41}{29.11}$

$\frac{25}{55.946}$
 $\frac{.977}{.977}$

27.24 1934.5 +06756 -0.36568

$\frac{745}{27.30}$ +06352.6 -046 ± 2.2 CC
+063 -044 Z

$\frac{12}{55.993}$
 $\frac{.993}{.993}$

36.0

27.31 1940.00 +063 -045

$\frac{19}{27.50}$ 39.2

$\frac{983}{T.146}$
 $\frac{1.71}{27.40}$ 39.6

391-920 042 599 +063 -045 -0.7-0020 -213 ✓
-025+001-056 002 -128 -270 -0.7 +1 0

-12 -27 -21 0 10

-33 -10 +4

91011 10 27.9 +02 2Y 09110 -0.7w(3)

7.0

w(2.2)

w(2.2)

06756 -03656 Y
06353 -08652 66
0644 -043

-69 -18 +11 .005

391-520 042 599 +064 -043 -0.7 -002 0-264²⁶

-025 0-059 002 -128 -280 +1 0

-22-51-37 0055

-62 -16 +10

-12 -28 -20 01

-37 -9 +4

008

-16 -35 -26

-44 -12 +8

+460/635

66582

W6591

72462

10 28.5 +45 48 4m1 +25e w(3)

8.86 +1.33 +1.29 K7V R

+41	-43	+9	.072
+43	-48	+9	.064

-60 -58 cin

75m(5)
718+(2)
71-(10)
<hr/> 64±8

427
2025
5.05

91280 10 29.5 -28 00 4F5

HR4130

GC14465

6.01 +0.51 +0.015 2595

[m] 219 +20

[C] 437 +122

327.160 .502 2.68 548.4

1.50

+5.6 +14.3 -12.2 -081 -18.1
+255 -101 -226 -004

+225

3.75

47

408

4133.000*

13.000*

23.500*

-23.000*

0.000*

-3.081*

-3.009*

3.750*

55.234

-13.100

3.20

3.295

3.015

10.348

91280

10 29.5 -27 59 F8V -18.1^{4C}

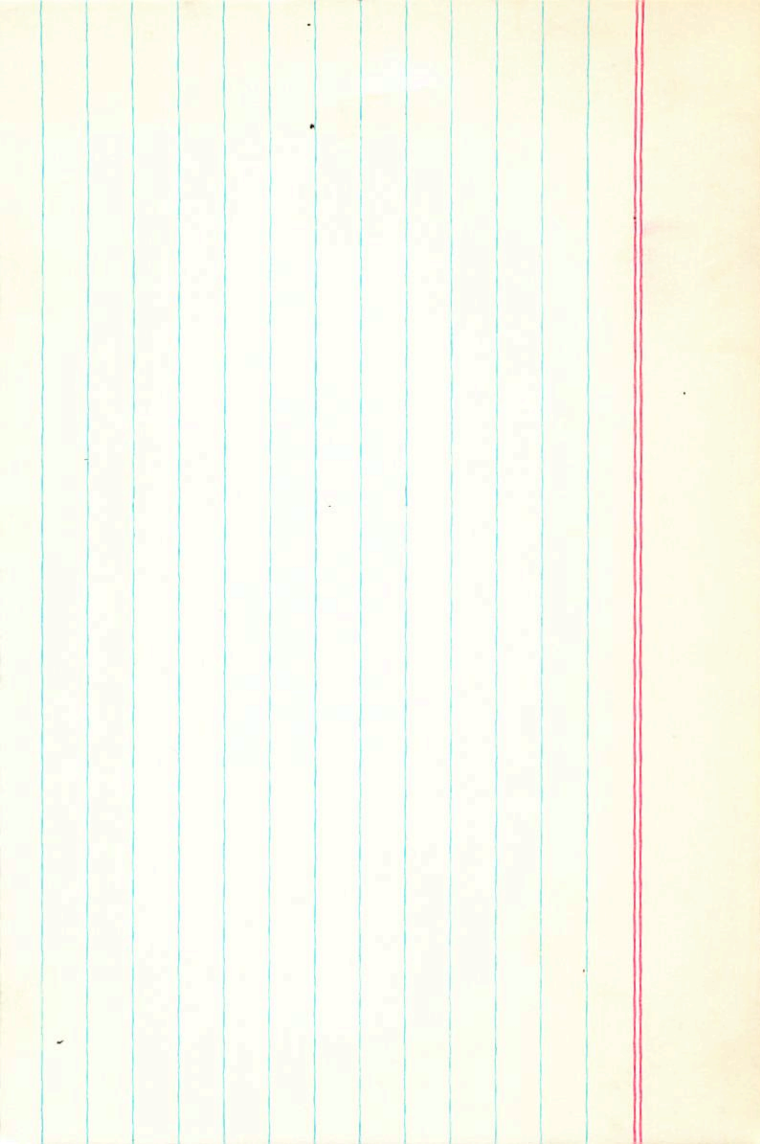
F201175

-20.7 (9)

4130

6.04 +0.51 (1.65)

-0.81 -0.09



HRV142

10 29.9 -72 5F 8 M 411.20
-0024 ± 5.1 -008 63.9 →
-0044 -003 → -011 -008 60

14450

9494
9415

4.91 +1.69 Cope

14480
660

52.243 1900.7 -72 57 51.33 1906.1
 $\frac{94}{52.243}$
337
1034 005
+35
 $\frac{35}{50.98}$

474
0

52.174 1015 51.12 1940.80
 $\frac{21}{52.174}$
204 .133
51.13

0237
0204

-832-402-383 +0590 -0095 +0495 +7.5 -4.3 +5.8
228-382-896 -0162 +0090 -0072 -1.1 -9.8
506 832-227 -0359 -0198 -0557 8.3 -2.5

5
-1089 1310.80

91312

10 30.3 +40 41 AYH

79
58 58
P

HR4132

4.78 +0.19"

A7L

-136 -008 G

-136 -002 N

-139 -004 P

-137 -005

57

22" 11.7

-832	186	523	+5403	-0044	53.59	+4.7
228	974	015	-1481	-0231	-1712	
506	131	852	-3286	+0031	-3255	+2.6

10.5

+14.6 L(9)

-2.0 V(3)

+350(2)

+48

-14

391-924 652 758 -137-005 114-003+9 -019

052 001 127 003 232 606 +10.6 110 +4

+2 +34 +0

02

+6 +44 +5

0.5

~~91190~~

91190

10 30.9 +75 58 5.0 967 +16.66

14507

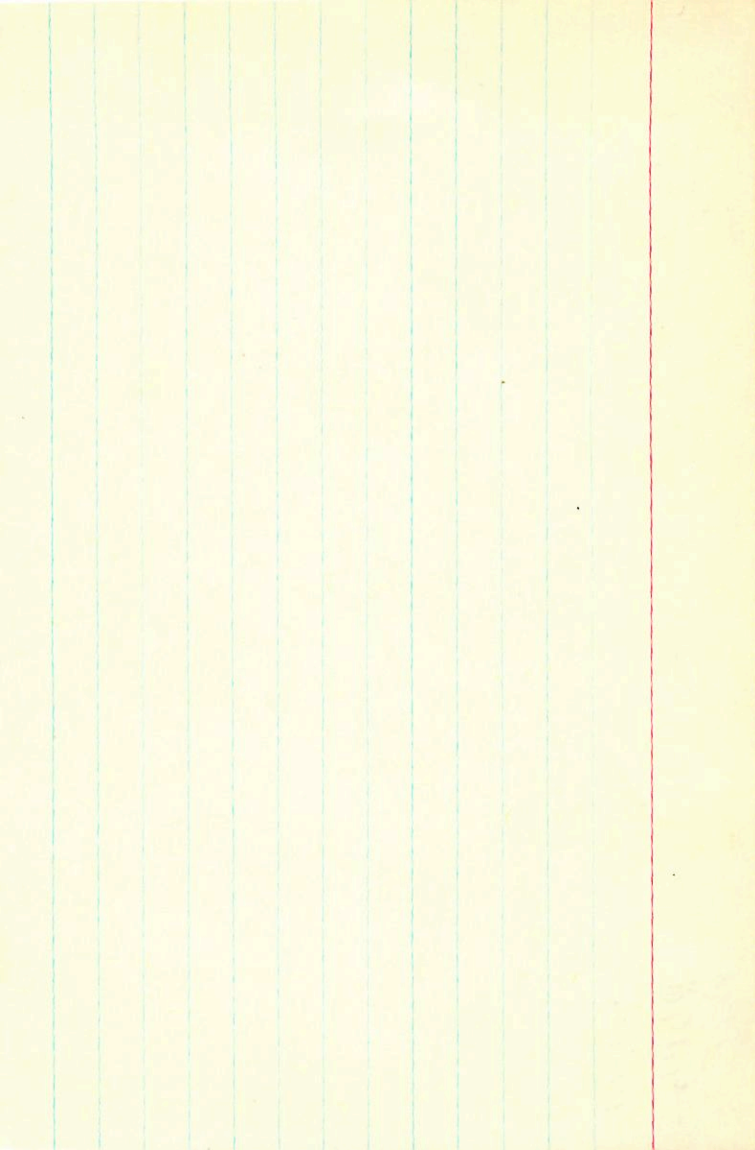
79

6610

-0076

000 N30

-0083 ± 0.9 -008 ± 1.0



441490

9155

1452

6613

A05783

91538

F0913

GC14514

+27 -38

10 31.3 -39 59

+11.604

6.68 + 0.52 (1.98) 6.84

+0022 ± 7.8 -0.41 ± 63
-0.38

18.294 1500.9 + 0020

$\frac{-110}{184}$

+0021 -0.39
+0023 -0.39

47.23 1898.2

+2.14
45 -0.09

+0.62

2.91 1929.07 - 1.29

12.013

$\frac{6.248}{263}$
18.240

43.15

$\frac{46.06}{46.22}$

1935.8

46.05

$\frac{246}{31}$

46.3

46.16

46.36 1982.4

$\frac{18.249}{2}$
9.1245

46.57

7 x Leo

4148

10

324

8+

55

A2

SB July?

91626

14541

TRV do

15274 15.5y
7105 0.19y

48.510 +25-160
+91-52+
+197-47-150

494
522
+502
+747

110-353-011
110-353-011
110-353-011
110-353-011
110-353-011

→ 035 162 1072 2887

034 161 1070 2880

032
632
173
171
178
346
1064
1067
2870
2880
304
304
304
304

181

1571
1408
1408
1408

+0.85
58.85

959 - 9620
- 2732

46.7

1186

0520
0520

48



8/9

4143.000*

13.000*

32.400*

3.000*

55.000*

-3.050*

-3.011*

4.550*

81.200

15.700

3.187

3.335

23.791

-3.102

-3.502

-13.594

-3.143

3.797

1.692

48

365⁰⁰ M6

110⁰

10 33.0

-29 18 8.8-9.7

U Ant

Numbers

273 5.42 + 2.46 - 3.70 + 1.05
 275 5.40 + 2.87 - 3.61 + 1.03
 791 5.27 + 2.83 - 3.55 + 1.02
 843 5.40 + 2.85 - 3.70 + 1.08

2440340

3.79 + 1.02

47 5.44 + 3.63 -

50 5.51 + 3.16 -

3.93 + 1.06

84

3.87 + 1.06

403

4.07 + 1.015

404

3.83 + 1.135

406

4.12 + 1.015

409

3.95 + 1.045

4484 (2)

R R-1

May 350 + 1.00

2.50

3.05

5.85

Q = 4370

"

-0.0317

-0.004

LAB

2440340

m-m 5.85

147pa.

+13 -41 -2

3.93 + 1.06

84

3.87 + 1.06

403

4.07 + 1.015

404

3.83 + 1.135

406

4.12 + 1.015

409

3.95 + 1.045

12.7

349 102

-0.31-0.03

-0.29-0.07

+37

3.15

311

133

178

49



179

0.000*

10.000*

33.000*

-39.000*

-18.000*

-0.029*

-0.007*

6.000*

158.489

37.000

0.097

-0.104

11.510

-0.038

-0.955

-41.416

49

-0.096

0.278

-4.851

568 1500 - 0083 - 0008

+37

V Amt

-39 18

33.0

GC14552

-0027 ± 5.5 - 007 ± 4.2
-005

12.97 1405.7

31
12.66

12.88 1938.65 200

248 no.
+26
-47
-59

+07

12.81

1.1 5280

-3.7

-353

-10.4

-0027 ± 5.5 - 0022

-0022 - 004

1509.7

-036 - 008

+1425 - 0205 +1200
-0401 - 0070 - 0471
-0850 - 0311 - 1161

14186

-03599

-09469

59.378
168
486

59.405
018
423
063
-

+12663 - 01288

-02855 - 00444

-92684 - 01514

-0027 - 003
-1 ± 2
-0028 - 005

-032 - 005

-835 541 - 100

235 185 - 954

455 820 281

-0.22

76.

BP (365)

10 83.0 -39 18 +370

255.170 -00275.5 -0074.2

59.378 1909.7 -0022

12.97 (505.7)
+3.7
12.66
12.88 1938.68

~~-0022-006~~

59.405
18
0.23
-0.64

0 -1
-007-000
-020-
120-

1001 16000

16000
+14.0
-41.4
-3.4

838 536 -107 +1231 -0102
241 187 -912 -0354 -0036
450 824 286 -0720 -0456
-4.0
-35.2
+10.6

-13

+1189 +18.0
-0390 -6.2
-0576 -14.50

12.3
345.100
380 1.71

356 mi

10

33.5 + 36 35 - 43 - 23.76

HR4150

6.3

+036-044 66

W6621

+0030±3.1 -044±2.3

+039-041 66(2)

370

+0028 -044

+035 -042

24.637

1841.1 +0029 -044

11.97 150.3

-127
460

2.03

460

460

24.625

+035-044

12.06

1452.65

1009

1035-044

-20

634

11.86

11.86

29 74

9.74

9.74

1452.65

-19.2

-4.7

-16.6

-20.0

+3.6

+13.6

+20.0

-1802

-6.7

+12.5

-19.2

-16.4

-4.7

+1.6

+1.6

+1.6

+1.6

+1.6

+1.6

+1.6

+1.6

+1.6

+0985

+3.6

-20.0

-20.0

+3.6

+13.6

+20.0

-16.6

-4.7

-19.2

-16.4

-1802

-6.7

+12.5

-19.2

-16.4

-4.7

+1.6

+1.6

+1.6

+1.6

+1.6

366-930 593 805 +038-042 -23.7-025-14.1-161

-014 009-030-023 -175-123 -19.1+17.8-7.0 0 1

+0.3-19.3-30.2

+9.1-13.2-22.1

0 2

-21.1-6.3-16.0

+6.1-15.2-24.8

1 5

-24.5-8.8-14.3

Ep-B. Pe. 6. 7. 14 Dep. Lyndhurst + 12 Oct 21
 91816 10 33.6 -11 39 d 123 + 3.58 w (3)

6-614569

1/21/12

66623

8.02 + 0.85 + 1.96 Alex

42482

8.04 + 0.80 + 1.45

-1102916

8.06 + 0.83 + 1.95

LR Paper

Proved 1978

+0054 -264 1055
 60924

+737 -254 ac

141

-1165

+0089

+136
 -5
 +131
 -274

1357

-260

+0112

+165±8

-243±5 CP

-138 -260

+0093±4

-254±10 CC

+ 91

-267 mm

29±12 C (7)

+0093 ± 10.6
+6091
-254 ± 5.5
-267
-264

33.057 1904.0
-128
34 0.82 1902.3

32, 629
32, 629
48.70
+12.12

32.898
-8
5-6.86 1933.2
56.94

33.244 2005 2015
18
2006

6.53
-75
6.78

OS

33.244
210
6.53
6.78

R.A. :
DEC. : 10.250
PM. R.A. : -11.250
PM. DEC. : 141.000
DISTANCE : -250.000
MODULUS : 2.700
RAD. VEL. : 32
1.500

d1 (U) :
d2 (U) : -0.002
d3 (U) : 0.250
qU : 0.128
U : X-1192.50
-41.243

d1 (V) :
d2 (V) : 0.230
d3 (V) : 0.003
qV : -0.792
V : -282.028
-51.338

d1 (M) :
d2 (M) : 0.490
d3 (M) : 0.292
qM : 0.628
M : -41.243

20

R.A. : 10.550
DEC. : -11.650
PM. R.A. : 141.000
PM. DEC. : -260.000
DISTANCE : 2.700
MODULUS : 35
RAD. VEL. : 1.200

q1 (U) : -0.835
q2 (U) : 0.526
q3 (U) : 0.158
dU : % -1195.50
U : -41.263

q1 (V) : 0.236
q2 (V) : 0.603
q3 (V) : -0.762
dV : -589.028
V : -21.338

50
q1 (W) : 0.496
q2 (W) : 0.599
q3 (W) : 0.628
dW : -413
W :

HR 4159

14520

91942
14570
6624

10 33.7

-0024 ± 3.8
-0030

4.43
-0.17
+ 1.66 Cape

-57 18 940 ± 9.9e

-0.10 ± 3.5

-0.19 - 0.10e

39.737
111
848

1903.9

-57

17 54.15 1900.5

39.761

1576
1466

733
-115

38.7

39.68
+10
690

53.94 1938.3

53.65
-21
54.15

53.9 1946.3

-24

54.69 79

54.40
-75

6573

42.6

42.1

ADD 2546 4157 10 337

+0006 + 9.0 -069 + 8.3 -21000
-0008 -26 25 -074 -2158 -23.96
-21000 -23.96

91581
14571
p=2114

0205

6.28 + 45 FLE

+003 -082 7
+007 -069 60

42.928 1598.2

-26 24 52.96 15963

+007 -071

-031
897

3.71

49,25

6.78 153003

7.24

32.158
10.676

45.08

33.6

42.838
+28

870
-027
35.2

51.86
-45

52.03
-2.78

37.3

478

52.31
-17

-2.78

52.174

1433.24

42.552
961

52.10
182

519

348 -930 -415 896 +007 -069 -23.9031 +11 -294
-003 -011 ⁻⁰⁰⁷ 064 -029 123 -055 -214 +20 -5 0205

+26 -12 -4

$\boxed{-11 +15 -23}$

91858

10

33.5

70 19

-035 / 22.8 ± 2.4
-038 ± 6.4 (3)

14541

+0210 ± 6.4

92108

58.6 +0015

24.56 96.1

48.015
-57
96.4

205
225

47.964

34.20

35.64

33416

-45.08

14522

+00225 -0365

23.72

47997

+00110

24.25

48105

+38

13

23.

015

91810

605584

10 372 + 54 40

-0443

[-05000K]

-0056843

-01483.3

10.240714

-0061
-0057

-009 228398x
-1111
22

$\frac{222}{2}$

$\frac{25.55}{2}$

10.750

4412

28.32

-2

-0058-0109

$\frac{-18}{2814}$

$\frac{249}{2}$

10.669

5772

28.88

+20

$\frac{689}{2}$

-00599 -0089

$\frac{-17}{96}$
27.

$$\begin{array}{r}
 -0106 \pm 12.2 \\
 -0130 \\
 \hline
 5012 \\
 -47 \quad 35 \\
 \hline
 6014 \quad +31.0 \pm 0.7
 \end{array}$$

$$+005 \pm 9.0 \quad (17)$$

$$9981 \quad 10 \quad 84.2$$

$$14585$$

$$7.29 + 58(1.66)$$

$$1122''$$

$$11.084 \quad 1903.9$$

$$-47 \quad 35 \quad 26.98 \quad 1899.1$$

$$\begin{array}{r}
 489 \\
 \hline
 11.573
 \end{array}$$

$$\begin{array}{r}
 -25 \\
 \hline
 27.23
 \end{array}$$

$$7.833$$

$$40.84 \quad 1928.54$$

$$3.348$$

$$45.51$$

$$\begin{array}{r}
 11.784 \\
 \hline
 11.735
 \end{array}$$

$$\begin{array}{r}
 2 \quad 144 \\
 \hline
 11.072 \\
 \hline
 -501
 \end{array}$$

$$\begin{array}{r}
 26.139 \\
 \hline
 26.40
 \end{array}$$

$$\begin{array}{r}
 46 \\
 \hline
 26.73 \\
 \hline
 +50
 \end{array}$$

$$84 \quad 54$$

$$42.3$$

$$43.2$$

$$38.6$$

$$\begin{array}{r}
 26.78 \\
 \hline
 26.87
 \end{array}$$

$$26.19$$

$$\begin{array}{r}
 10.926 \\
 \hline
 -12 \\
 \hline
 9.806
 \end{array}$$

$$\begin{array}{r}
 -10 \\
 \hline
 26.59
 \end{array}$$

$$1956.00$$

$$-0015 \pm 5.1 -002 \pm 4.9$$

91056

10

27.2

-63

55

5.2

M1

-306

14419

6584

12.664

1412.2

-63

54

57.65

1909.4

$$\begin{array}{r} 057 \\ \hline 723 \end{array}$$

$$\begin{array}{r} + 08 \\ \hline 57.57 \end{array}$$

12.606

23

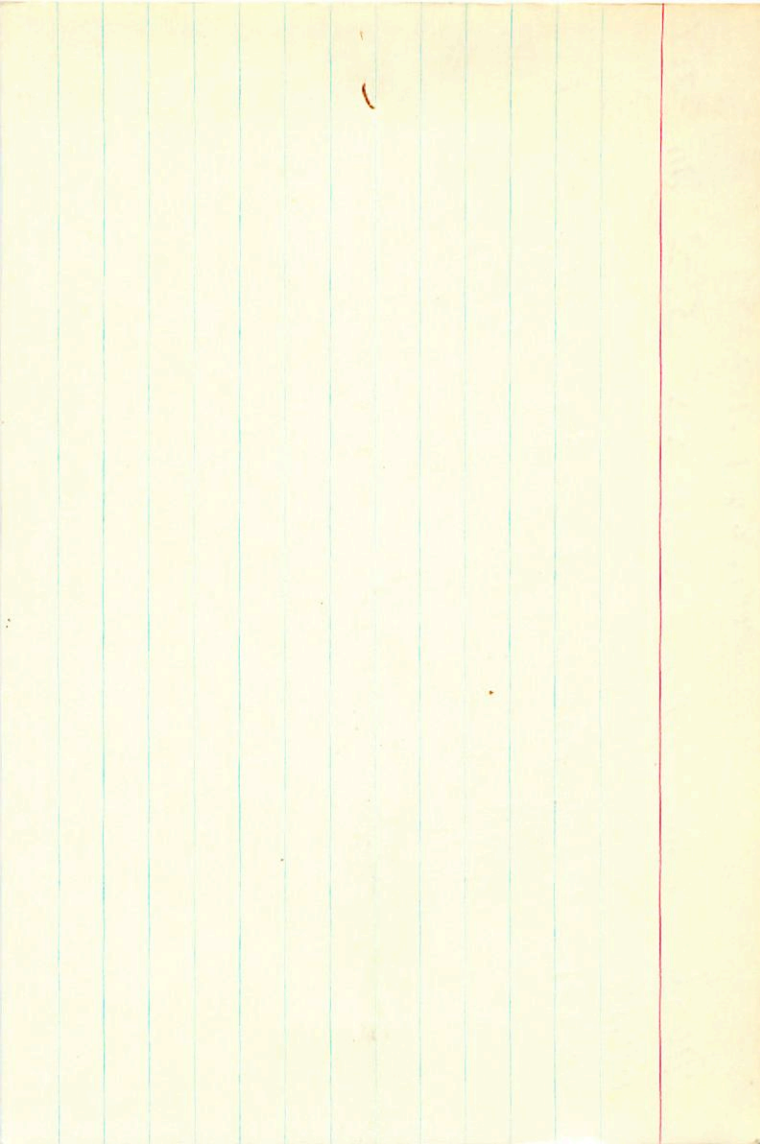
629

57.84

-9

57.93

1941.10



44149a

91550

10 31.6 -23 29 5.3 9144 -3.9a

14524

5.08 +1.61
-0009 54 +019 N30

-5.11 (2)

6613

-0008 ± 1.8 +014 ± 2.0

A057834

