

Rx 500

90386

10

28.6 +04 11

4903325

-00.8

0 00 +002 AG-103

-0004 -0138 ZU

-0012 -011 60

-002 -011 565
5 400 -

[-001 -007]

41

Σ(14)
-8.6 ± 0.0

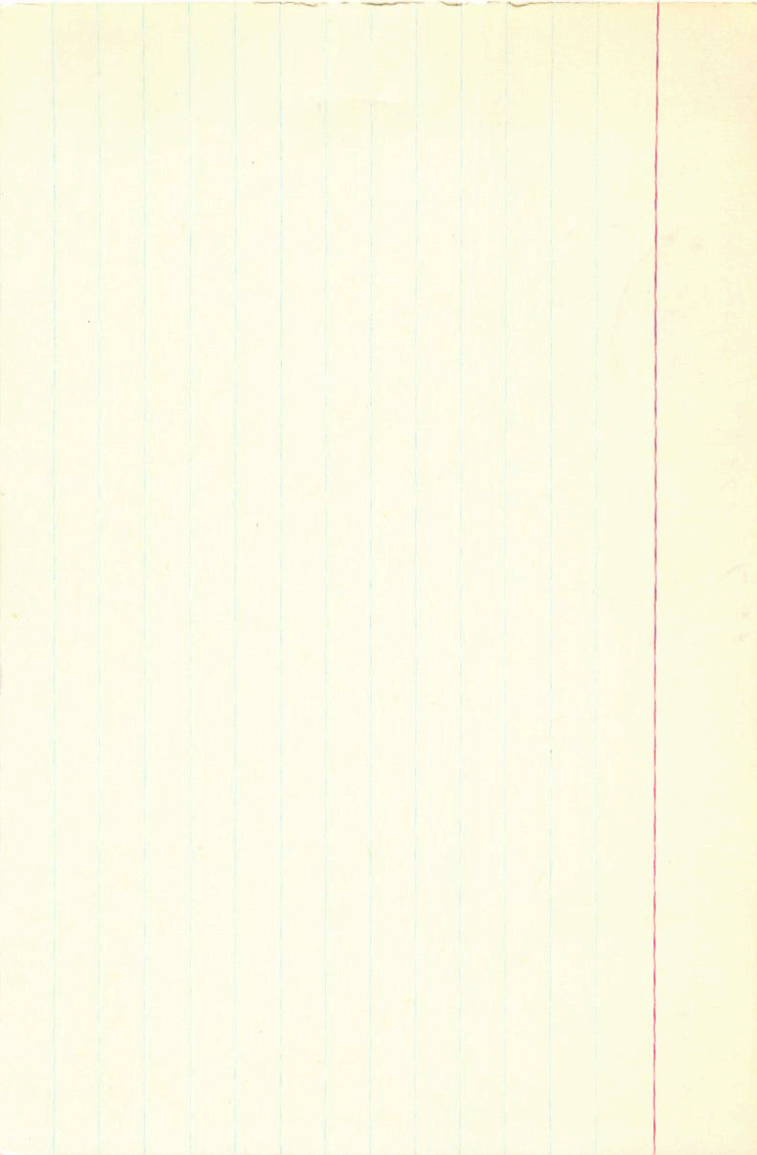
-0014 ± 8.7 -025 ± 8.0

90519 10 24.1 -45 17 782 +1.38 N11II

14334

4.573 1899.7 -45 16 36.35 1897.1

1



90520 10 24.1 -45

14335

~~8.17 + 1123.11~~

-0090 ± 8.0 +060 ± 7.5
-0089 +070
19 7.5-1 +62 G-34 +17.6 ± 0.3

4.594 1898.5 -45

18 32.30 1895.2

464
5.058

-3.29
35.89

18
+69
2.60

855

42.8

1929.30

55.98

129.70

-36.92

1324

3015

18
+69
2.60

47.3

466.26

32.90

411

-45

33.35

1789

18
+69
2.60

-39

32.20

43.4

48.2

1956.20

18
+69
2.60

1954.20

32.43

1957.0

30.64

540

18
+69
2.60

30.98

30.64

30.98

30.98

30.98

18
+69
2.60

10.40000

4.20000

-1.00000

-7.00000

6.00000

158

0.000

-0.825

0.461

0.328

-11.389

-1.805

0.211

0.789

-0.577

-27.176

-4.307

0.525

0.407

0.748

-15.970

-2.531

41

26 Sep
 90473 10 24.1 -00 44 6.8 gms +4.08
 -0033 52.3 +001 2.1
 -0033 +007

14333

6555 3.748 1897.2 -0 43 59.80 1891.9
 174
 922

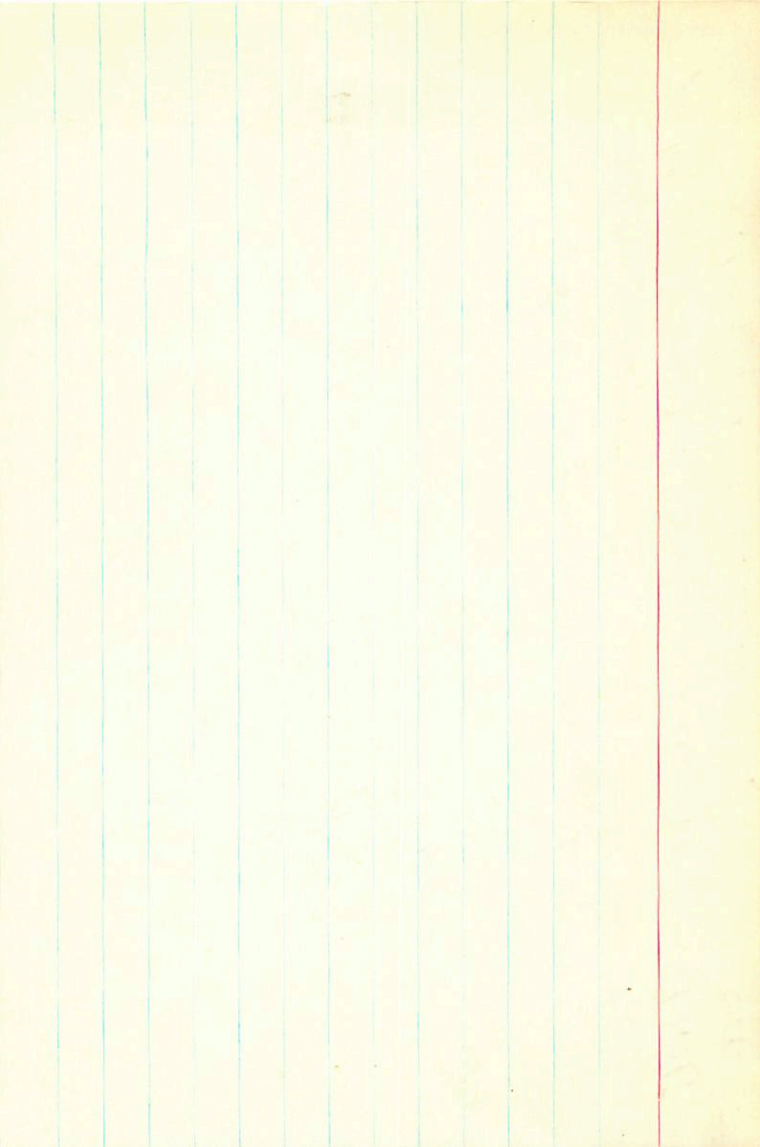
-00341 +0037
 -057
 -044 +004
 47.131
 14.686
 3.819
 807
 413

388
 36.9
 45.0

1585
 792
 -130
 8187 - 9905
 498 - 1378
 772

22.31 1934.10
 -36.70
 599.01
 59.55
 59.56 +0.31
 +21 5
 59.35
 59.93 1939.78
 +22
 59.70

0496
 -0012
 -044
 0060
 6.13



$^{2(4)}$
 $+15.3 \pm 0.6$

90559 10 243 -43 09 8.17 +1.23 NIII - $\overline{12}$

13³"

27 SW
-0032 ± 2.6 -002 ± 2.4
-0027 -006

90485 10 24.3 -4 08 6.6 967 +6.08

14338

6557 15.264 1902.2 -4 7 59.65 1896.4
153
417
+11
59.54

15.285
13
298

323
794
34.2

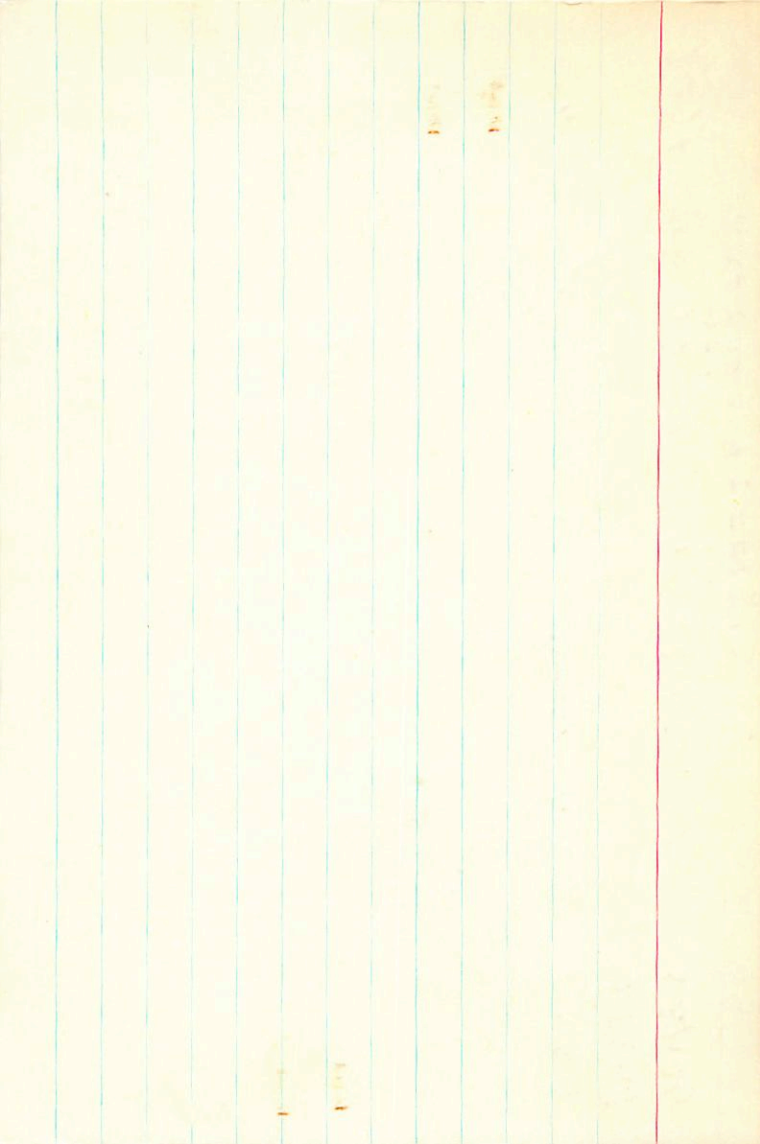
59.488
15.858
15.344
342
36
348

60.08 1939.30

+39 161 285
59.69

22.69 1933.55 36.4
36.90
59.54
40.0

59.54
10.12
59.9
59.50
-26.6



90572 10 24.9 +03 49 490 +45C 45J

6614355 2.4

W6564

AD5

A057779 DM=1.5

1" April 009

-0072 -026 GC → 430
-0093 -030 2mm

-0082 -028

+39 -43 +11 0.15 ?
+43 -47 +7 -0.13 !
+55 -59 +7 -0.09

-12547 -02656Y
-10847 -02246GC

| | | |
|-------------|-------|------------|
| +4808 -0613 | +4195 | +40.0 4x.5 |
| -1830 -1044 | -2874 | -28.7 2.61 |
| -3042 -0543 | -3585 | -35.8 7.37 |

-825 +462 +323
+214 +747 -574
+522 +409 +746

100 PA
+56.5
-54.6
-2.1

-6072 + 6.9 -02745.9
-0093 -031

55.305 1895.8 + 3 49 9.21 1891.2

$$\begin{array}{r} 55.305 \\ \underline{390} \\ 55.695 \end{array}$$

$$\begin{array}{r} 1.59 \\ \underline{10.80} \end{array}$$

$$\begin{array}{r} 55.289 \\ \underline{25} \\ 55.314 \end{array}$$

$$\begin{array}{r} 9.49 \\ \underline{4} \\ 9.53 \end{array}$$

$$\begin{array}{r} 31 \\ \underline{4} \end{array}$$

$$\begin{array}{r} 9.53 \\ \underline{4} \end{array}$$

114
35.3

$$\begin{array}{r} 55.311 \\ \underline{21} \\ 55.332 \\ \underline{372} \\ 323 \end{array}$$

39.9

9.31 1936.30

44.5

$$\begin{array}{r} 33 \\ \underline{2} \end{array}$$

$$\begin{array}{r} 9.34 \\ \underline{3} \end{array}$$

$$\begin{array}{r} 9.44 \\ \underline{136} \end{array}$$

+20°2488

90494

14346

6561

39+

70 24.5

-0132±5.0
-0144
+20 04

-193±6.9
-181
8.9 d60

+448
3W

28.006 19083 +20 4 15.67 1504.2

550
28.556

8.84
24.51

28.22
24
28.22

~~29.8~~ 1929.8
20.0
-13
19.87

90610 10 24.9 -30 49 4.4 M0 +13.38

4.16 + 1.46 + 2.567 ^{24"}

14352

6563

-0063 -001 N30

-0060 ± 1.8 + 005 ± 1.8 62 → N30

FNS

10749-10104

+21 St

Ant 10 24.9 -30 49 110 +13.3 B

HR4104 4.25 +1.48 *long* -0.77 +0.08 B

W6562 -0.81 -0.01 N
-0.23 +0.15 F

-0.77 +0.07

184(110)

403-915 -512 859 -077 +007 +133-004-7 025
031002070 004 125 345 +1.4 -10 +5
35

+6 +45 -3

008

[+12 -20 -14]

+4 +43 -4

009

[+36 -21 -12]

+24 -20 -13

008.5

1075
587

75 432

(X)

10 249 -30 50 mo II

4104

14852

4.25 + 1.44 + 1.63 ✓
4.25 + 1.45 + 1.63 +

90106

881

Stamps
Val?

294
-0589
48500
40000
+40
-0753 + 0089

+40
-0753 + 0089

-073 + 013

-076
-074 + 011

350 + 0.58 5

349 + 0.57 B

351 + 0.575

313 349 57

235 235 495

187
527

TC = 0187(10)

+15
+9

4104.000*

10.000*

49.400*

-30.000*

-50.000*

-0.074*

0.011*

4.800*

4.75
23.7

91.201

13.300

0.326

-0.075

429

28.715

-0.001

-0.902

-20

-19.383

242

-0.114

0.425

-5

-4.750

1/10

1/11

1/12

4104.000*

10.000*

24.900*

-30.000*

-50.000*

-3.073*

0.013*

4.050*

91.2 93.325

13.300

3.320

3.002

+29 23.930

-3.054

-0.925

-17 -17.300

42 -3.134

9.301

-7 -7.410

ρ f_{me} 44
 368
4100
90537

10 25.0 +36 58 68 III -IV

+69 (20) +71 (3)

AB 4.21 +0.90 +0.65 25 ~~72m~~ 0.5
3.86 +0.32 25 $\Delta m = 1.71$ Miller

3.88 +0.31 5A

3.84 +0.315 5A

-10
+14

3.50 +0.3

305

(3.75)

-0.00946 -0.1055 F124 +5.64

+4
-1193
+40
(-119 -102)

(3.4)

dit!

Y Leo 401.98 thick +1.00 65 1.51 444

4057k 10 17.2 +20 0

8944/5

1.74 +0.43 214

3.04 +0.30 214

23

4100.000*

30.868*
-0.119*
-0.102*
3.400*
47.863
5.600

0.363
0.523

20.320

-0.592
-0.057

-28.660

43

-0.263
0.851

-7.839

β f m

G-8 III-IV +13

A057750

10 25.0 +36 58 +5.6 c

90537

.0217

-120 -109 17

M358

-0096.52 -105

6566

-0100 ± 1.1 -108 ± 1.1

memorandum

DM = 1.71

99.04
+1.21

1957
M. G. A. J. E.
pic

403 -915 601 799 -120 -109 +5.6 -066 +3 -412
048 027 110 060 -057 649 +45 -4 +2 0217

-7 +32 -16

-20 -29 -6

90874

10 25.8 65² 27 46.0 (3)

-65.1357

4115

50.564 70

-0125 ± 39

+015 ± 3.1

-0116

+017 57.63 2.5

-0130

+012

71

64438

1. 102

59.34

50.688

(39.90)

57.53

+34

-17

72.2

57.70

-8711

4910

50.590

424

57.70

-0124 +015

13

-01

-01256 +0186

577

5781

-0787

-076 +023

90853

10 26.0

-0020
-58

29 4.1 F8 +9.3a

14388

-0014

382 +0.30 +1.62 FOII +10.554

6572

2.341

1908.4

-58

29

1.40

1905.6

PMF

079
420

10.4
-58.5
-031

2.358

0.91

1.46 1940.69

0190

+ 15
373

687 +10

-21
1.67

96.69
48.3

0160000

339

39.7

6160
0002

2.297

-0.081

1.22 1956.10

p.s. 0.2

+ 9
305

-30
1.52

42.7

0000000

300

1000

160
69

425
0000
0000

1000

44

MA

10.400
-58.500
-31.000
0.000
6.870
237
10.000

-0.825
0.503
-0.259
63.306
12.390

0.211
-0.151
-0.966
-16.199
-13.490

0.525
0.851
-0.018
-40.306
-9.719

44

90718

14389

6573

8.268 1894.6

$\begin{array}{r} 299 \\ \hline 367 \end{array}$

8.329

$\begin{array}{r} 16 \\ \hline 343 \end{array}$

8.315

$\begin{array}{r} 12 \\ \hline 327 \end{array}$

$\begin{array}{r} 336 \\ \hline 231 \end{array}$

43.0

+14

35

58.90

1892.2

$\begin{array}{r} +75 \\ \hline 59.65 \end{array}$

59.18

1934.9

$\begin{array}{r} 59.22 \\ \hline \end{array}$

0.899 1940.20

$\begin{array}{r} -2 \\ \hline 58.56 \end{array}$

59.09

-0.56

37.0

45.4

-0054 ± 2.5

-0054

26.1

+14

36

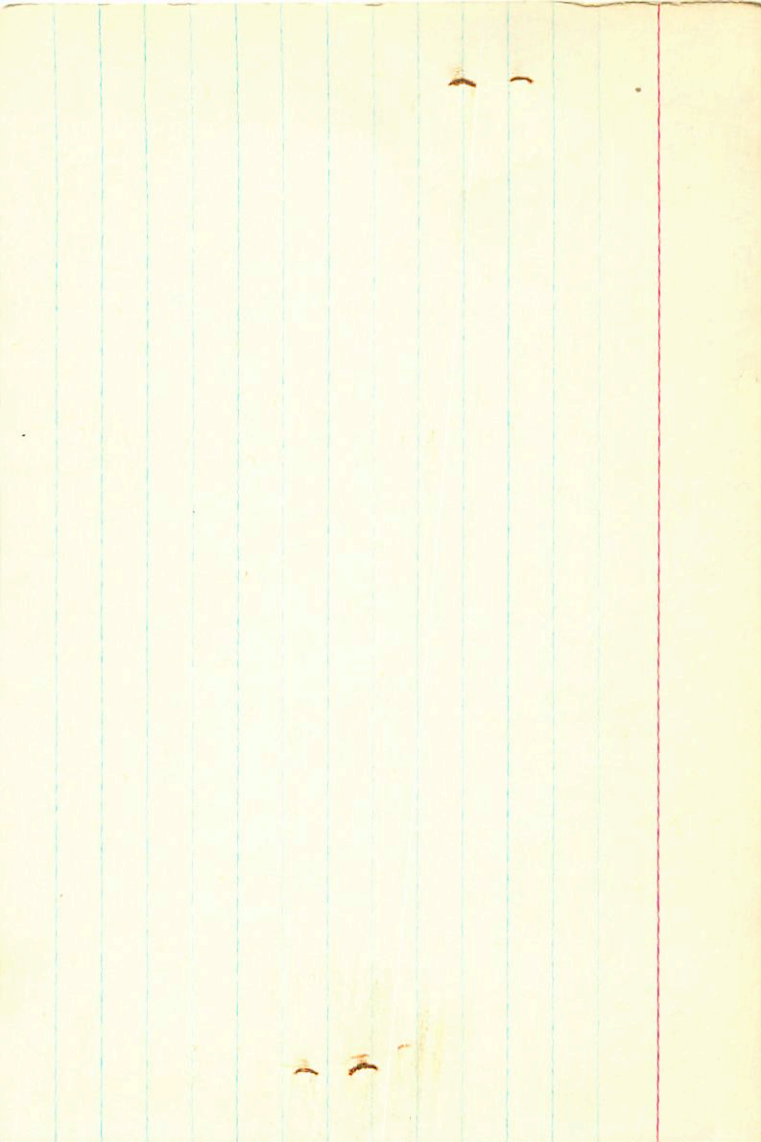
7.1

86.5

+37.98

-013 ± 2.4

-012



4106

~~412~~

10 26.7 165 53 6265 122

-2498
-2588

-001-035
+2
+001

45

1848

1848

1848

-5.041

0.090
0.215

-03.482

0.422
-0.145

-12.864

0.006
0.058

-24.900

158.489

6.000*

-0.000*

0.001*

53.000*

65.000*

26.400*

10.000*

+106.000*

45

+3002022

10 26.6 +29 55 8.5 8.5
GND+102.2

WU577

8.80+1.11 +42 121111 R

+105.9504

GA54-577

10002-004

18-