

WY Amt 10 13.8 -2.4 28 +20.8

10.85 +1.5 +4.4 ΔS=6 +0.14 -0.64 C(G-)
+35 0 $\frac{-2}{-66}$

1.53

-813	+581	+0.45	-0.541	-1817	-2358	-235.8	+9.4
+184	+332	-924	+0.223	-1038	-	915	-91.5
+553	+742	+376	+0.267	-2321	-	-1954	-195.4
							+78.6

89090 10 13.8 -28 22 6.1 D

7.21 + 54 (+4) C

[P] 215

1350 .152 .389 2.584 ② 30, 12

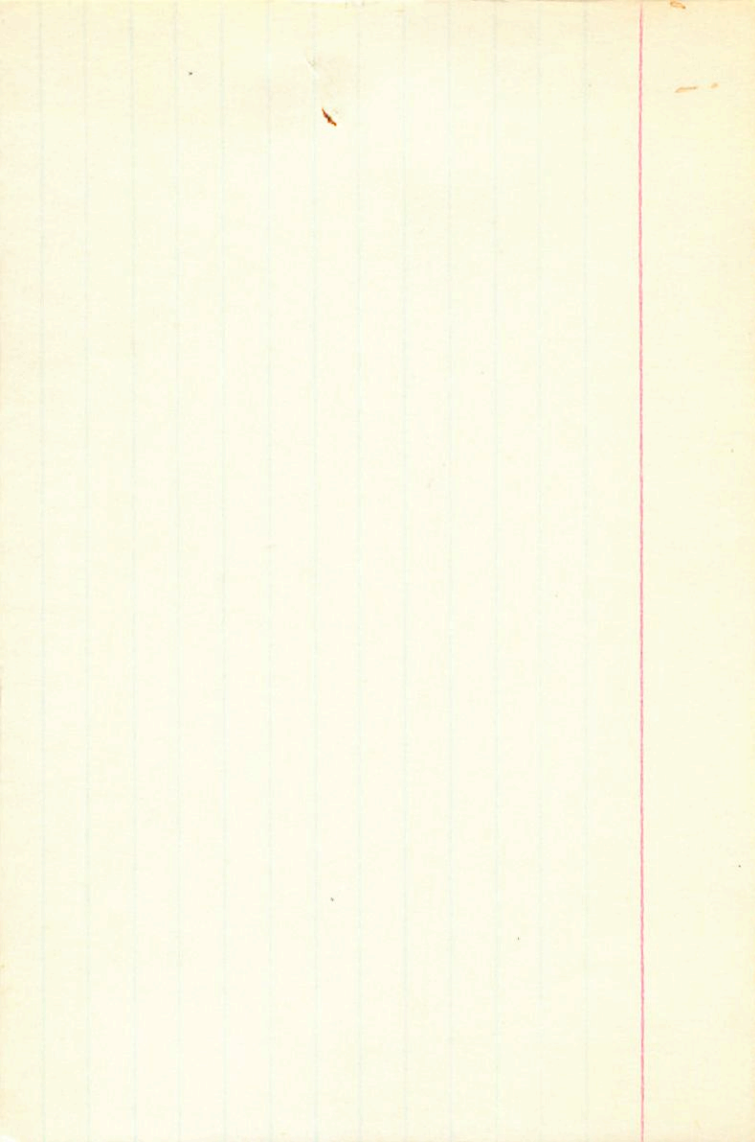
[C] 315

5 805 2025
2075 432.4

4.60 + ~~88.1 - 38.1 - 20.3~~
+ 1036 - 100 - 356

+ 54 4.60 83.2

1872



92(5)

-0180±6.9 +044±7.8
-0172 +065
-28 22 614 +32.4±0.6

89090 10 13.8

13097

7.22±52

47.177 1896.9 -28 21 5537 1895.7

956
48.133

-36
96
5

-2.39
57.76

38.734
8.720
474.54

36.6

27.69 1933.80
-27.12
54.84

502
~~69~~
492

-54.54
-317
55.21

204
33.5
37.9

1933.24

47.497
172
512

55.56
12

5544
55.32
2.44

33



10.200
-28.400
-262.000
55.000
3.000
40
32.400

-0.808
0.585
0.066
1035.342
43.358

0.178
0.349
-0.920
-103.006
-33.915

88815

10 13.9 +73 19

F0 +16

50141

+230489

6.5

-057 -0836

-075+

-061 -074642

-059

-025

447-885 955 287 -059-025 +16-022 +15 -404
026 032-053 064 -186 403 +4.6 -4 +2

-16

015

86192

10 14 05 -55 16 6:30 Ap

86194

87-68

805 -028 +019 0335
near 1020 ✓
212 ✓
0000
rec

0.1
1.25
1.25

22105
55.212

6.105
148
307

1.7

-004778.0
-0030
-0023

+01372.6
+005

024 1275 DB.2

-0035 +010

13 13
75

44768
1740.7

10.427
55.212
6189
43
23
227

2578

-00357 +0146

4454

0273.7
1.25
96

6.010
+11
6021
66.9

12.24

-2248
1227
-43
12.70
-20
12.90

-24
12.50

89053

10 14.3

-0077±4.8
-0084
+41

-029±3.9

43 69 g M2

-32.66

14118

64816

+4502106

18.258

19033

+41

13

3.054

1901.0

$$\frac{360}{.618}$$

$$\frac{48.22}{30}$$

$$\frac{30.22}{30}$$

$$\frac{18.522}{416}$$

$$\frac{.411}{.417}$$

$$\frac{18.37}{20}$$

$$\frac{900}{900}$$

25.1

1.42

$$\frac{4.96}{4.96}$$

32.2 1926.5

27.80

$$\frac{4.92}{4.92}$$

$$\frac{4.18}{4.18}$$

56.7

28.4

27.4

-0076-027

-0083-024

-0050-026

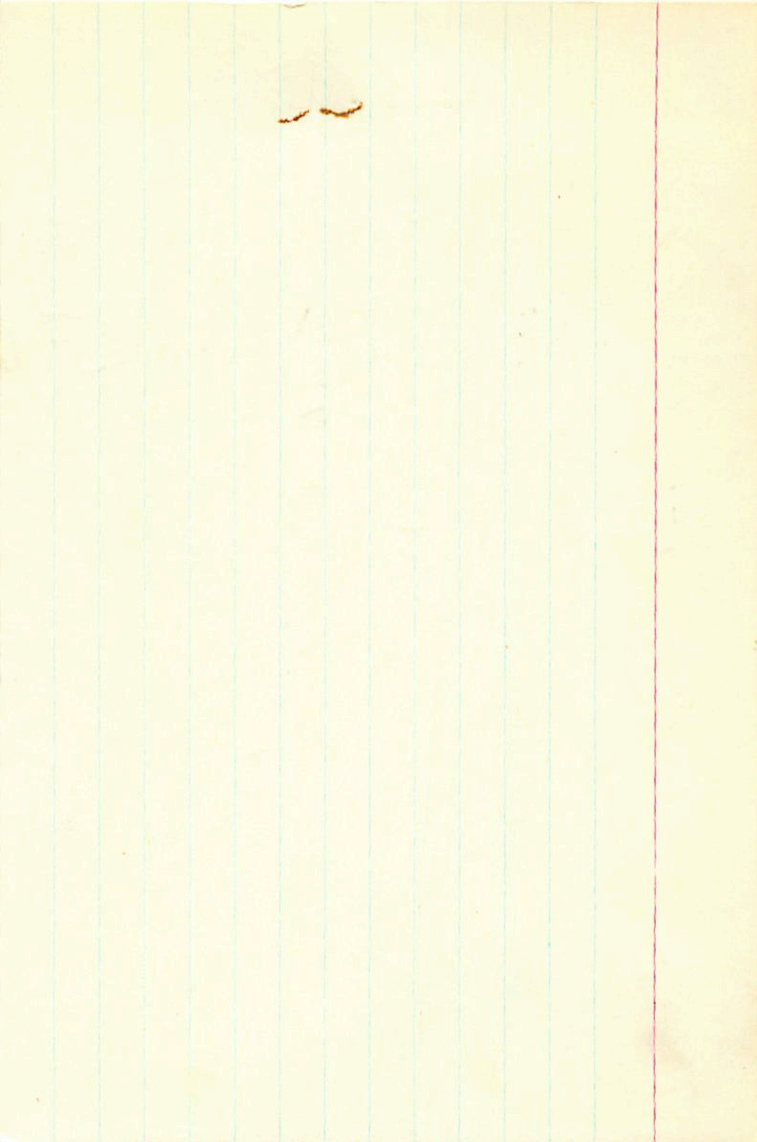
4.1 1930.2

-9

$$\frac{44.01}{44.01}$$

44.10

-0.86



225m(c)
89254

9751
15.1

10 15.1 -7 49 5.4 GF1 H5.28

F. III

14129
6485

5.5

-0108 -001 K30 5.24 +23+10 C

-0107 E1.6 +003 E1.6 Ge → K30

5.18

5123 +30 +1.61 24"

70-17

-01104 -0010 FRY 3.3

-164
[162+003]

!

[Faint, illegible handwriting on a separate piece of paper]

Blank lined paper with a red margin line on the right side.

34

	10.258	
	-7.800	
	-163.000	
736.0	3.000	
-150	3.300	
-116	46.70	
	15.200	50.81
		5.11
	-0.812	
	0.523	
	0.257	
	629.298	
222	32.675	
	0.126	
	8.651	5.0.23
25.0	-8.736	
	-163.101	
-237	-17.274	
	0.553	
	8.558	
	8.626	
	-415.938	34
	-415.240	
	-9.466	

1263 p104

10 15.1 -7 49

4042 HV

ESY

F124

w, 50

81104 - 0010

8048 0030

7093 - 0027

-1641

-1620 +0020

-1632

-1617 +0016

1582

+0350

+8.7

(00)

81029, 08
5099 2740

15.71

0329

8.17

III 13 F 1 III
49254 10 151 7 49
204

MS(3)28
GLH129
LHOMDH
5.24 + 32 + 10 C
5.24 + 34 + (4) C
5.24 + 39 + 1.5 N

49254 10 151 7 49
⑤ 6 + 23 + 42.5
③ 42528
③ 518.70C: 681.
③ 518.70C: 681.
③ 42528
③ 42528

MS(3)28
GLH129
LHOMDH
5.24 + 32 + 10 C
5.24 + 34 + (4) C
5.24 + 39 + 1.5 N

MS(3)28
GLH129
LHOMDH
5.24 + 32 + 10 C
5.24 + 34 + (4) C
5.24 + 39 + 1.5 N

MS(3)28
GLH129
LHOMDH
5.24 + 32 + 10 C
5.24 + 34 + (4) C
5.24 + 39 + 1.5 N

2 List

-2310

B9 -390

back 2
photo

8 SWA

10 75.8
15.8

4044

-28 45

89353

Are Slab

5.07 225 068 1619 2673 5t

5.62 245 64 1689 2658 4 5g

735 137 1640

230

FXY

+0095

-35: +0059 W 50

+0034 +0040

+0085 +0040

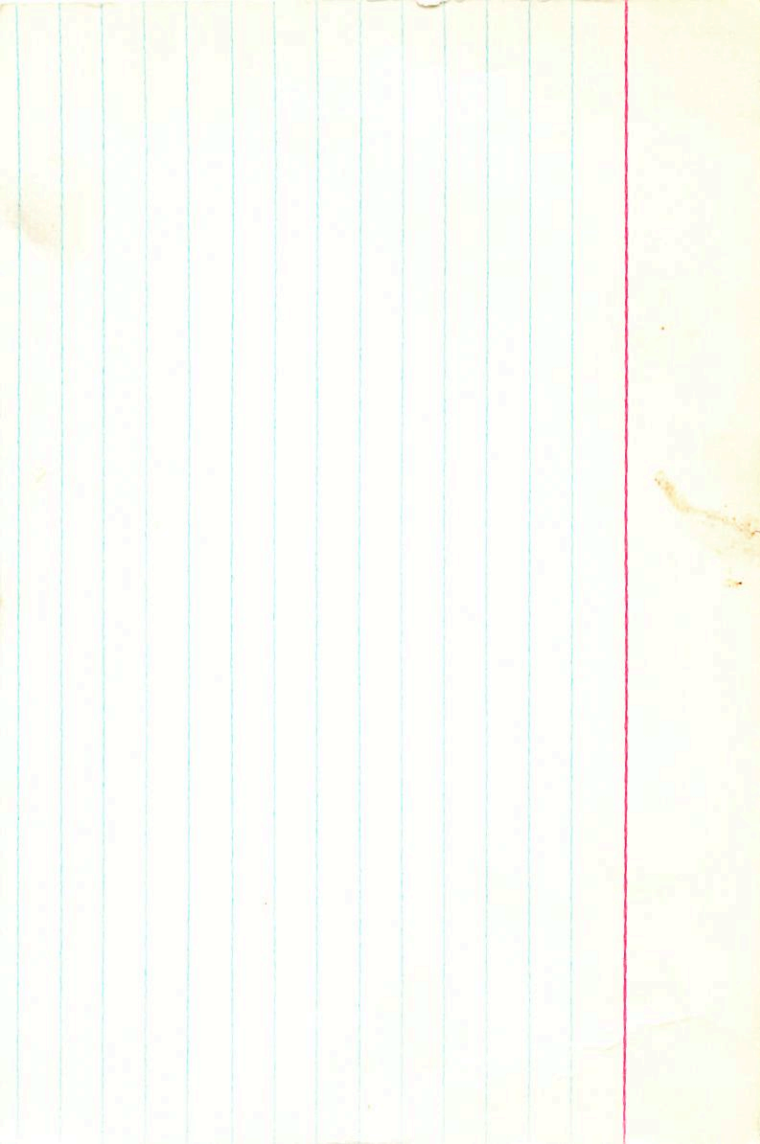
-0152
-013 +012

-0112

-009 +008

0484
9978
-5614

224 54 1.601 2.162



89269 10 15.8 +44 18 6.7 dec -8.38

14143

6490

¹⁰
+0061 -308 N30
+0057 ± 30 -298 E 2.2 G-C → N30

~~W35A~~ ⁻¹⁰

514)

+00572 -305 ✓

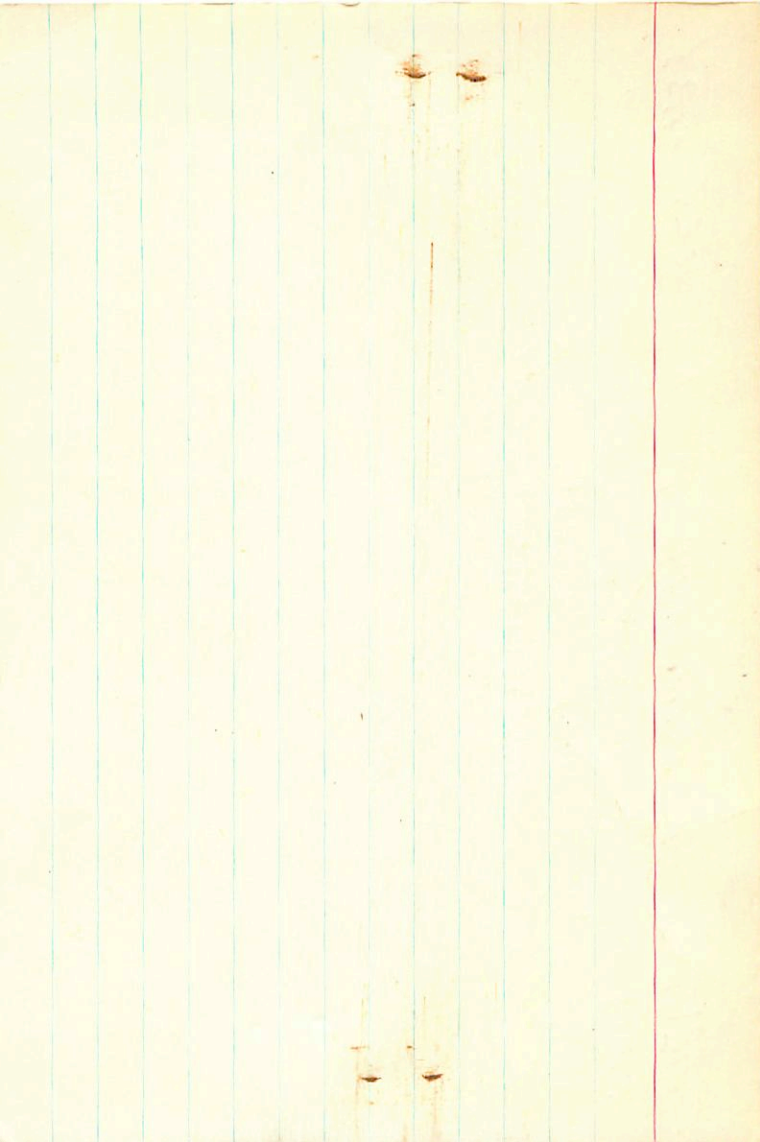
+00564 -306 ✓

9873

1587

6.64 420 208 292 (1)

C0207



4074 10 1500 +47 01 6.35- 21.7 1920

21.6
1920

$$\begin{array}{r} -021 -03560 \\ +2 \quad +3 \\ \hline -019 -035 \end{array}$$

4032 10 B.9 +25 3 }

55

-105 +024 DC



2010-01

2010-01

2010-01

4044

10 16.9

84+

58

39 85.5 20

-92-7-

056-128 62
+ 2
- 1
-094 450

1875

36



4045.000*

10.000*

16.400*

48.000*

39.000*

-0.094*

-0.126*

5.000*

100.000

-6.200

0.316

0.575

28.030

-0.665

0.136

-67.375

36

89569 10 16.8 -55-52 F7E +114 C4

F01174

find near GC1414 2637 1144

2477
-1144
-1144

48278 19006
48278
49765

2852

5.80 + 0.48 (1.22)

0301798 + 11475.4
-0302
1000

3847183.7
-6.70
45.14

0302
+114
-0296

+373

3418
858
858-0426
5004

53614

55302
+ 15.84
216

4843

414
26
416

40754
+
887

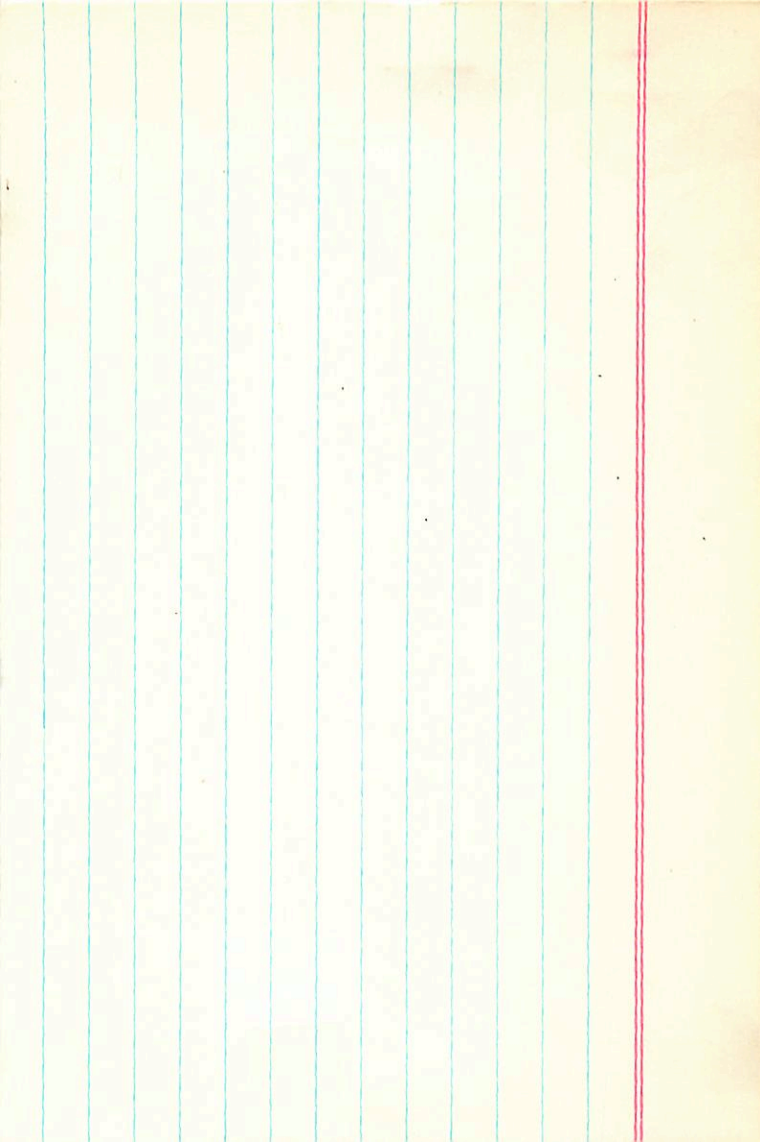
40.11
+
40.11

11.03

41.33
+
41.33

4144

1428.79



-0096 ± 5.0
 +038 ± 4.5
 +048
 -0101
 6.4
 7.8

89389 10 17.0 754 02 78 -20.66

14172

6501 2.340 1897.4 754 1 48.22 1896.0
 505
 2.845
 25.545
 37.195
 2.735
 -1.905
 -1.549
 553

1269

78.4 1926.2
 29.85
 48.55
 -75
 47.80
 47.43 136
 47.93
 39.5
 43.5
 35.6
 39.6

42.1
 38.2

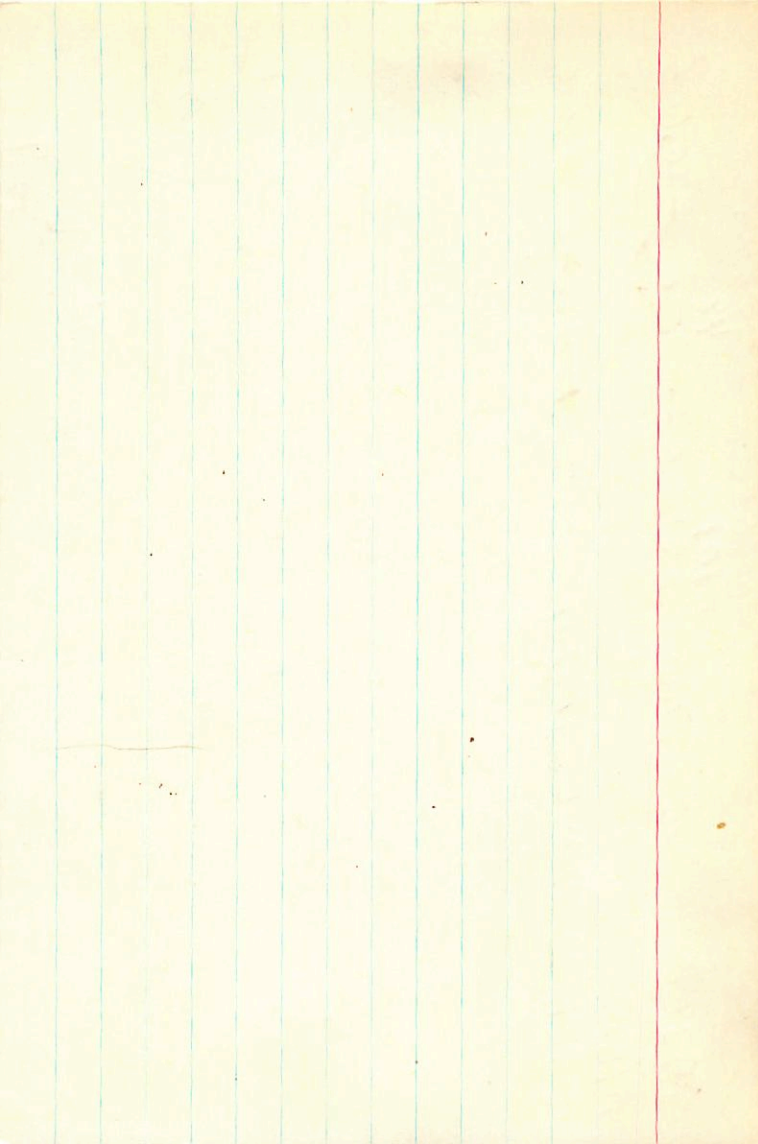
933
 466
 379

417
 2.387
 340
 -42.6

1945.06
 49.84
 -31
 48.53

4826
 42.09

2.328
 1.23



6614177/8

8 Dec

89484/5

10 17.2

+20 06

4057 -361
-362

1.95 +1.04

W 6502/3

5.3 1.84 +1.05

11.04

R man

4058

+20° 2467

Adj 224

Δm = 1.25

11° 07 II → KK A

-36.82 10(60)

† 2423

G7 III + KK B

-36.46 4(26)

+307 -153

+307 -154 N30

OCW +0.6

6C +307 -152 A

+1.7

+312 -174 B

+0218 -154 N30

+0218 ± 0.8 -154 ± 0.8 GC → N30

310 -163

-90 -10 0 .020

-65 -2 -9 -0.30

-80 -6 -4 0.24

12A(14)

244B1

1956

J. L. Stember & P. C. Hanson

H.P. 8. 127, 122-1955

901 434 344 539 / -307 -153 -36.6 -953 -13 -682
277 046 -133 -023 / 1.421 -103 -34.4 -15 -31

-9 ~~47~~ 0245

227

434 -901 344 939 / 307 -153 -36.6 -053 -13 -682
-133 023 -277 046 / ~~403~~ ~~1421~~ -344 +31 -15² -55 -36
₂₆₆ -958 -1203 ₁₀₁ 03
-646 -14 -9.5

-4 -64 -41 0245

-75 -4 -6

0.2 -48.0 -11.8

-23 -90 -55 016

1.0 24.6 -27.0

-107 -12 +9

-1.7 9.0 -11.8

89414

10

17.3 754

28

6.2

9 N3

79.4

14181

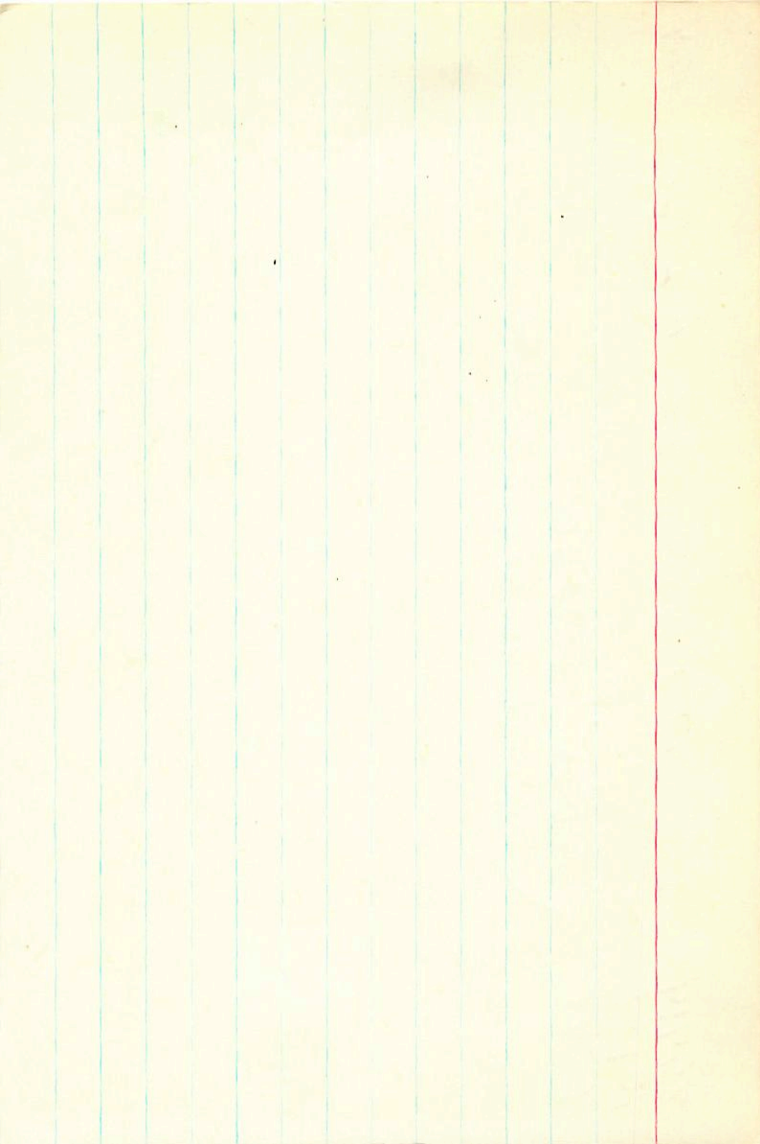
6505

-0035⁻¹⁸

-009 N30

-0040 ± 2.6 -008 ± 1.9 GC → N30

710.1 B

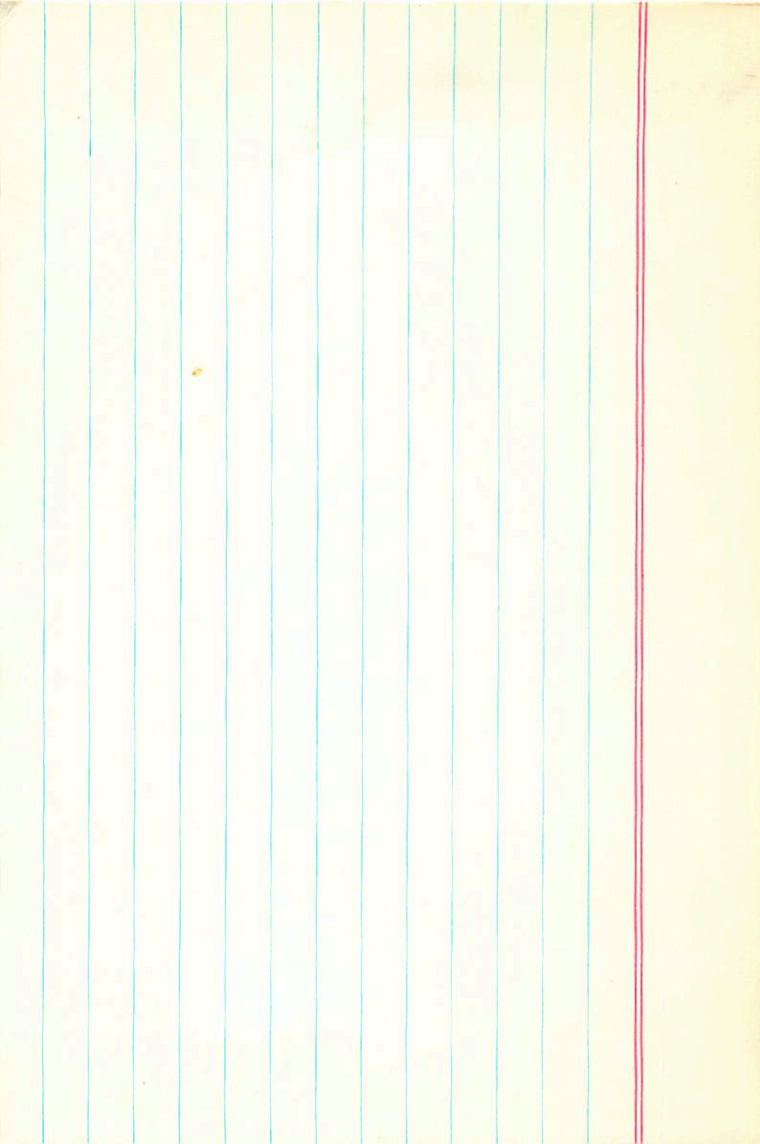


89585 10 17.4 -30 45 65 72 +4.8 < 4

FD910

7.44 + 0.89 (1.94)

-0.22 + 0.06



+7.2252

+0008 ± 4.7
-0006

+2.36

89619

10

17.9

+6

41

8.4

9F7

14191

732-303

103

515

190

6507

55.407

1893.9

76

40

55.77

1885.0

AOS 9730

-045
362

55.286

63.27

55.99

3.70

5947

0.8 Dm = 0.5 ±

55.324

113

42.5

56.98

1932.7

36.4

51.4

9m 8"

344

Both aligned

55.315

338

024

56.59

1938.69

56.90

2.57

23.924

21.414

334

331

57.91

1937.53

-68

-2.57

55.324

334

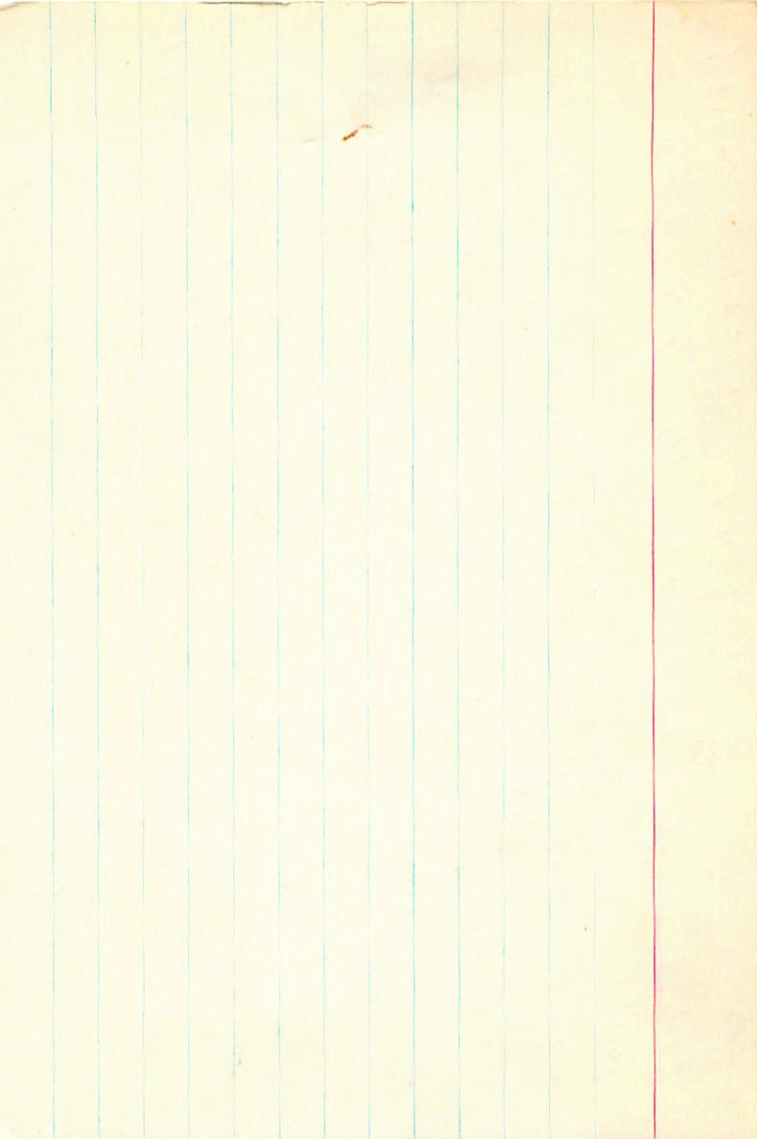
331

57.91

1937.53

-68

-2.57



89777 10 18.9 ~~100~~ $\frac{-16}{48}$ dx1 + 452 w(3)

CC576
WG513

9.39 + 0.73 + 0.34 68E R

42431 9.35 459 302.318 7.1616 $S = -04$

-1603030 936 466 291.315 ①
③17 $\frac{-486 + 1299}{-488 + 1299} \rightarrow 0.6$

+169 -41 +10 .016
+188 -45 -14 .020

$\frac{-486 + 1142}{0 - 13} = \frac{+1299}{+1299}$

$\frac{-48 + 112}{-486 + 14 + 112} = \frac{+102}{+122}$

$\frac{-469 + 116}{4.0} = 4.5$

-003 (102) 6

9510 C(6)

37

89777.000*

10.900*

18.900*

-16.000*

-48.000*

-0.469*

0.116*

4.000*

63.096

45.000

2.122

0.159

141.053

-0.147

-0.826

-46.440

-0.848

0.541

-29.161

37

6.49 103 167
HT 4071 647 207 4376 - 498

19.1 -2325

+12.9 1.4

55816 020

1107
1104
1020
1024

(NO)

2409 93
117
55
1800
1300
1300

3059 107
-79
31.24
38.91
+10228

12 = 2026
V0 635

2448
117
412

31.24
+20
30.99

9222 -9389
4312 - 3741

0509
-0066
3.6

7325
20
745

(644)

30.74
18.87
30.87

-0509
-049 +023

1603

7320
+17
7337

(61.76)
46.11
46.11

30.59
-12
30.71

-10352
-0489
-046 +025

0519
1100
-1076
1.05

40213 P4H Supply

89744

10 19.2 +47⁴²⁷ 29

DFL

HR4067

-01675 -1417^{W350}

+13.5
-12.4

GL14225'

-01084 -1424 546

1336 186 450 (2) SPL

[m] 246 -2

-1218¹⁵⁴

2.64 (4)

[G] 383 68
+66

-1222-134

CF

1.50 -14.2 -11.7 +2.5

-15
-01080 -1450 ±20
-01095 -1412⁺⁴⁰

-100 -282 +153

547
642
-6.56

+33

2.5 -

163
139

-1230

-123 -138

61

2471

646

8.63

8.63
8.63
8.63

8.63
8.63
8.63

~~8.63~~

RAD. VEL. : -6.200
 MODULUS : 18
 DISTANCE : 1.250
 PM. DEC. : -139.000
 PM. R.A. : -153.000
 DEC. : 41.200
 R.A. : 18.300

p1 (U) : -0.817
 p2 (U) : 0.123
 p3 (U) : 0.227
 pU : 371.223
 U : 2.990

p1 (V) : 0.194
 p2 (V) : 0.981
 p3 (V) : 0.012
 pV : -228.881
 V : -13.290

p1 (M) : 0.244
 p2 (M) : -0.120
 p3 (M) : 0.331
 pM : -232.149
 M : -8.281

R.A. : 10.300
DEC. : 41.500
PM. R.A. : -163.000
PM. DEC. : -139.000
DISTANCE : 1.250
MODULUS : 18
RAD. VEL. : -6.500

q1 (U) : -0.817
q2 (U) : 0.153
q3 (U) : 0.557
dU : 371.553
U : 2.990

q1 (V) : 0.194
q2 (V) : 0.981
q3 (V) : 0.015
dV : -758.681
V : -13.590

38 q1 (W) : 0.544
q2 (W) : -0.120
q3 (W) : 0.831
dW : -235.146
W : -9.581

4260
89774

14224
6515

-0024 = 1.9
-0020
19.2 + 15 = 14

6.1 B9 + 8.7

9.084 1900.5 + 15 13 42.03 1899.7

$\frac{119}{9.203}$

$\frac{11}{9.108}$

$\frac{135}{48.390}$
 $\frac{135}{20.975}$
 $\frac{135}{9.108}$
 $\frac{135}{1.17}$
 $\frac{135}{1.17}$

9.124 / 140

$\frac{1.11}{43.14}$

$\frac{18}{42.32}$
 $\frac{18}{42.50}$

33.9

$\frac{104}{135}$
 $\frac{104}{135}$
 $\frac{104}{135}$

1933.8
34.4

75.52
32.12

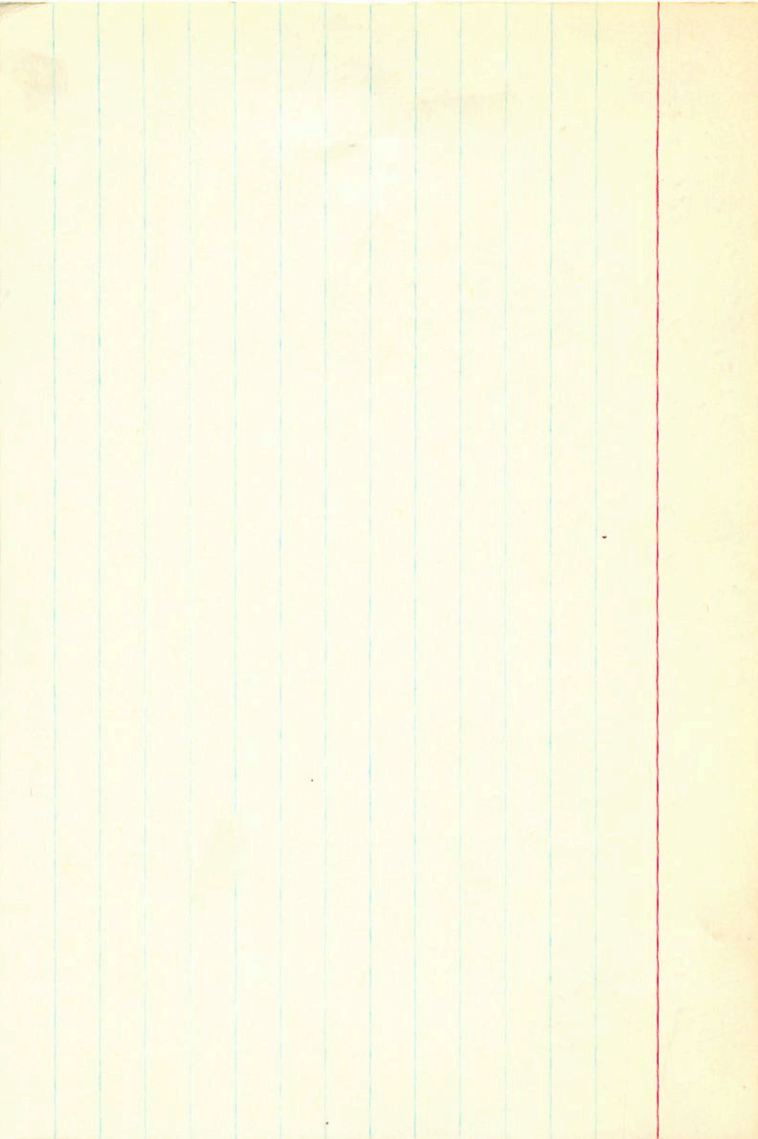
43.40
- 6.1
42.79

42.79
+ 3.6
46.39

193882

42489 / 42.42

9.124 / 140



-20.4 debit

11/11/20 10 18.4 +41 45

1484069 3.00^{var} +1.55 MO III -083 +029

89758 59 Eggs -082 +028 6c

142327 -0071 +029 N30 -079 +029 N30

6517 -0071 ± 0.9 +027 ± 0.8 6c 7000 -079 +029 N30

+1 +2 -27 .025 6 W₂ 50 -081 +029

+10 13 -21 .016 10 155 OF 952.94

4180
 4588 4635
 4588 4635
 4588 4635

[-886.032]

Y26-506 666 776 -080 7025 -20.5 019-14 055
034-008 072-017 242 303 -153 714-7 025

+24 +5 -10

+1 +2 -27

+29 +12 -5

+10 +3 -31

016

+10200

89753

10

75.5

+16

43

8.52 + 55.65

+345

-084-0344

-03551

-084-033

-086-022

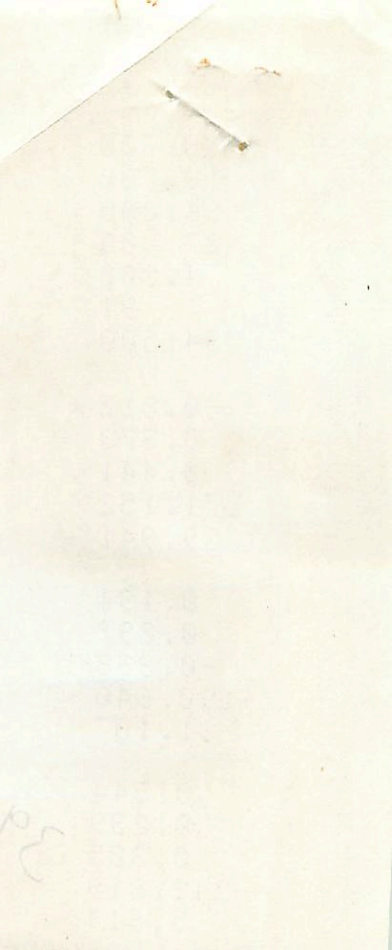
-088-027

45

96

+345 (2)

30



10.300

16.700

-86.000

-27.000

4.800

91

34.500

-0.817

0.373

0.441

271.152

39.941

0.194

0.897

-0.398

-190.640

-31.107

0.544

0.239

0.805

-242.819

5.614

39

070
125

10 17.7 -25 07

84448

10 20.0 -25 19

+ 23,0 Bond

D.3

-020 +074 Y

S.O

-017 +067 Y → 06

-017 +064 F → 04

-015 +073

40



Faint, illegible text, possibly bleed-through from the reverse side of the page.

ON

89948.000*

10.000*

20.000*

-29.000*

-19.000*

-0.015*

0.073*

5.000*

100.000

23.000

0.256

0.032

26.368

0.103

-0.920

-10.905

0.220

0.391

31.027

40

AD57744

0 20.1 +15 36

+18.48

.0295

- 26.4 ~~314~~ GC

422-907 269 963 - 0.265 40.116 + 15.4031 + 5.5.31

112 + 0.13 240 + 0.28 463 1.076 + 18.7 - 17 + 8 0.255

358 1.199 + 157 + 21 + 23

+ 58 21 0

$$\frac{-4 + 45 - 13}{736 - 34 - 117}$$

89906

10

20.1

-0193 ± 4.9 -118 ± 4.4
-0179 -121

+15

36

7.4

dg2

+19.48

14245

6521

3.215

1898.6

+15

35

54.66

1896.1

941

4,156

36

6.36

1.02

AD57744

b2=3.5
orbit

31.131
32.320

3.451
-018

433
-4
427

3.491
1
502

929

464
-692

38.6

57.63
1.48
56.15
-10

1938.22

56.05
-24
55.81

235

232

56.36
18
56.54

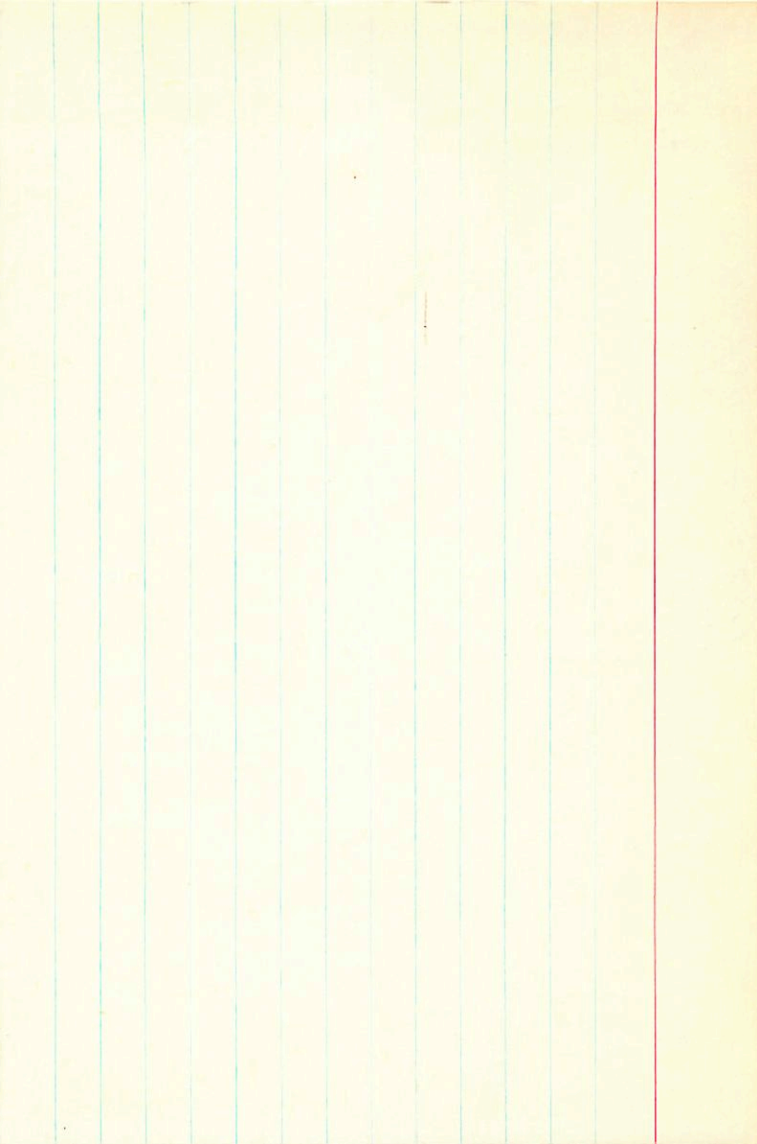
1934.2

36.2

56.17

4.85

40.1



-0008 ± 5.0 + 011 ± 4.0

89945

10

20.2

-9

9

7.2

gms -0.46

14251

6524

12.624

1897.1

-9

8

30.90

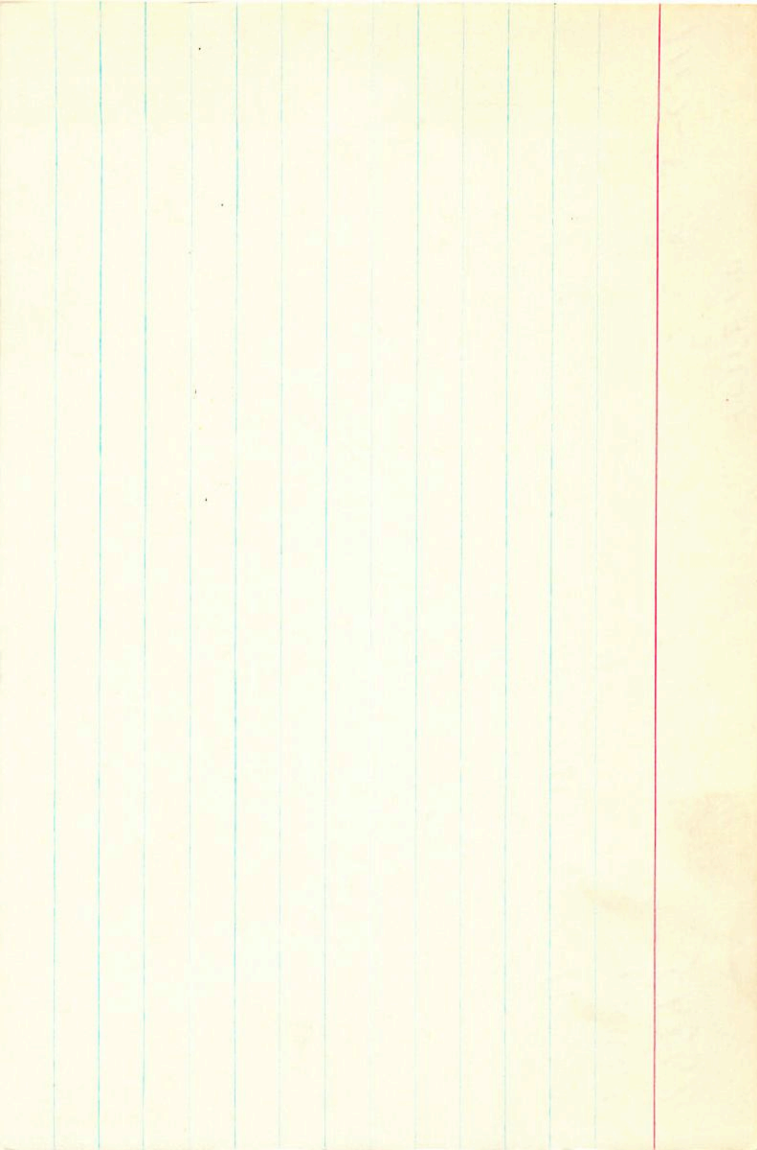
1892.2

$\frac{042}{.666}$

$\frac{-64}{31.54}$

$\frac{58.037}{14.558}$
 $\frac{12.595}{599}$
 $\frac{604}{604}$

$\frac{58.30}{33.20}$
 $\frac{31.50}{-56}$
 $\frac{32.121}{31.85}$



89995

10

-0161 ±3.8
-0163
20.6

-076 ±2.7
-080
57

6.5 F2

14263

6.52 +44 +1.58 = 8"

6529

38,854

1900.0 +5 56 5436 1894.2

HRM074

805

87.587

48.91 12.34

4.24

39.659

4.24

59.60

60386

39.106

4.24

55.29

1933.8

126

128

32.5

55.32

20.831

18.332

39.167

130

29.96

33.62

456.37

55.75

1931.11

491

32.5

38.3

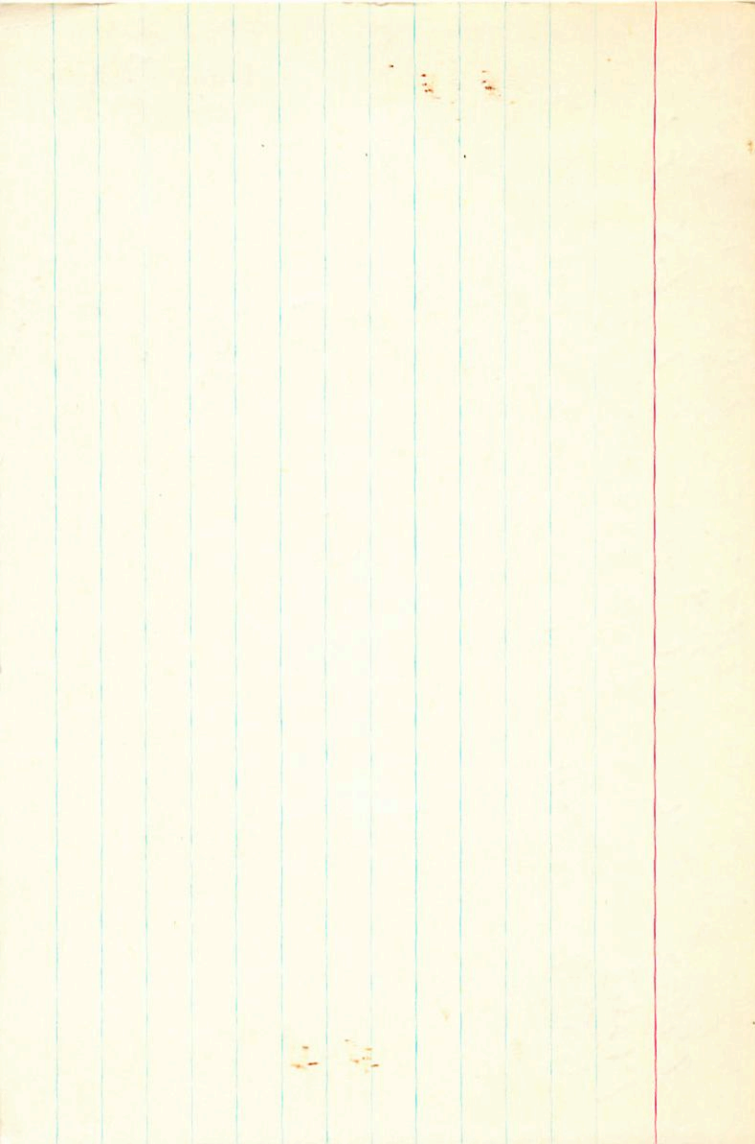
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