

-0.58 + 0.43

-0.096 ± 7.1

+0.33 ± 6.4

$C_3(4)$

+0.51

+0.29

6.7 III - IV

+2.0 ± 0.5

84261

9 40.0 - 12.1 - 6.5

5 70.29

6.85 ± 86 1.91

13355

-0.122

6.85 ± 86 1.91

—

59.022 1500.2

-6.5 51 9.35 1897.9

—

$\frac{478}{54}$

$\frac{-0.106}{+0.44}$

$\frac{-1.71}{11.046}$

-0115 +038  
+0419

-437

59.017 42.08

9.65 +2.02

-0724

25.075

8.15

19.22

1528.24

$\frac{-0.64}{+0.46}$

~~34.1885~~  
6.5220

$\frac{0.15}{0.87}$

$\frac{-45.78}{9.02}$

9.04 1537.8

0826  
0071

59.245

59.107

9.02

9.07

+3.9

59.070

59.670

1447.4

19.2

6057

5.30

9.460

9.00

19.2

9.6

+56<sup>0</sup> 1400  
W 2ma 83950

9 38.9 +56  
40.2  
36.7 +56  
max 7.90 +0.63

11 58.7  
24 37.6  
47.3 Orbit  
-432  
-46  
 $\pi = 0.15$

MM 163341  
1973

W 0.15 w03 s

~~033 - 031~~

1.33  
-14  
-29

+0033 -031 ± 1 Y

+020 -026 AGE

~~1~~ M

+025 -028 4 → 1/4

+0032 -030  
+ 2

+0225 -028

+0030 -028

-42  
43

+021 -024

+

573-820 831556 4033-031 -46-026-35-081 ✓  
-019 015-027 021 -180-057 -256 421-15 015 ✓

410-18-42  
-35-19-26





Li. 50-

0'61-

~~820'87-~~

821'86

122'8

842'8-

249'8

00'61-

3'01-

~~844'8~~

168'801-

15 Dec

84107

9 40.6 +30 12 5.7 A2 +15.6 6

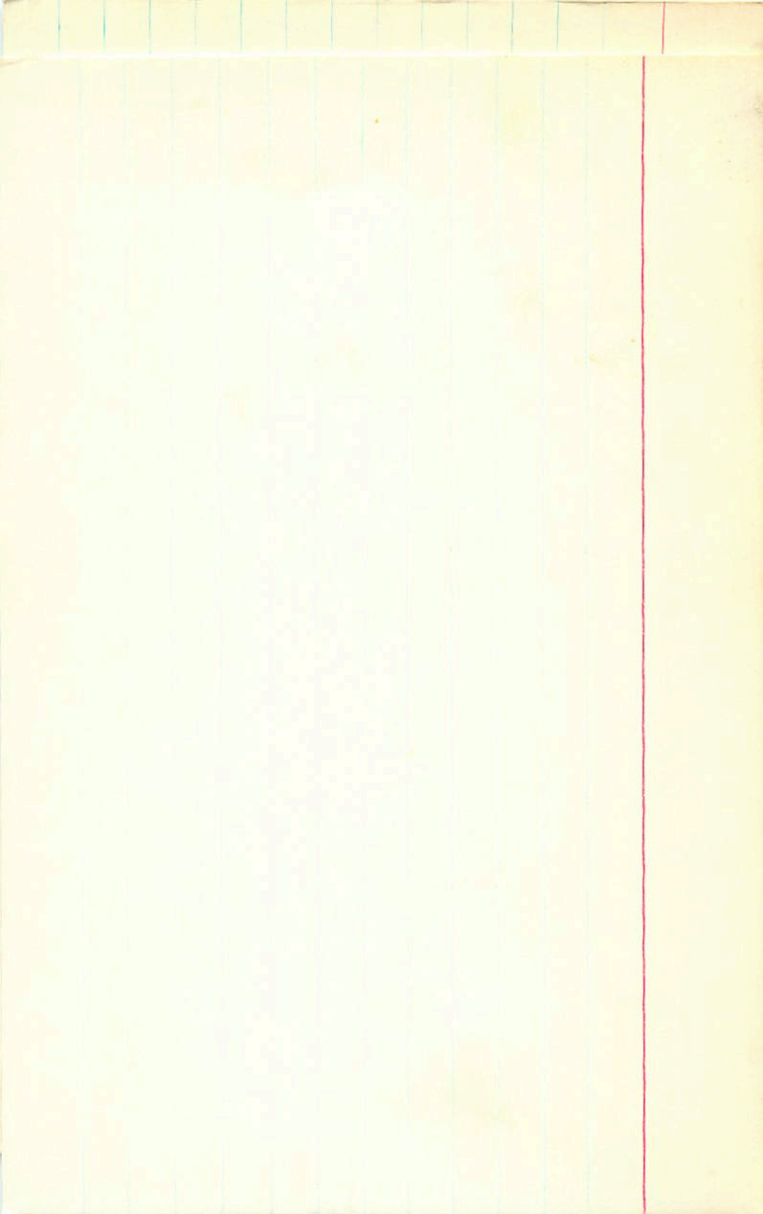
13406

6257

39

-0009 -105 N30

-0016 ± 2.6 -111 ± 2.2 CC → N30



-0017 ± 7.5    -102 ± 6.5  
-0018            -077            wk line

84123            9    41.0            +42    17    6.8    dFop +16.36

13413

6261

59.109    1911.5    +42    16    53.75    1910.6  
    065  
    .174

2789  
34.380  
59.270  
-116  
1754  
159

145  
-029

16.5

47.3    1925.8  
-49.78  
57.52  
-97  
56.55  
56.40

559  
28.0  
17.4

59.10  
32  
132

56.3    1930.1  
-4  
56.27  
56.42  
-1.35



-0004 ± 5.9 -060 ± 5.4  
-059 100 -068

9 41.7 ± 19 06 6.6 100

84252  
13422

6264 43.340 1902.9 +19 5- 34.79 1903.0

$\frac{282}{42.61}$

$\frac{19}{359}$

43.352  
 $\frac{15}{867}$

27.5

40.90 1933.2  
 $\frac{23}{41.13}$

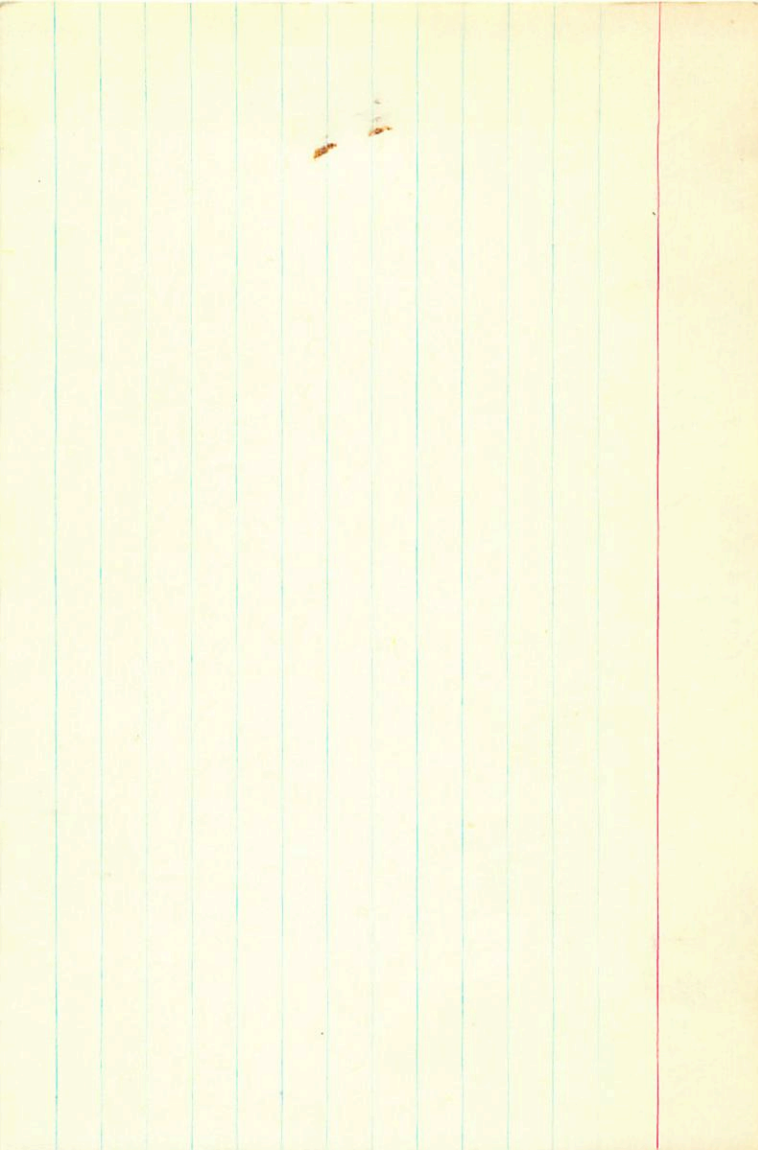
30.4  
27.4

19.873 351  
23.412 - 009  
42.355

82.28 1927.0

~~50.90~~  
~~41.38~~  
40.98  
 $\frac{53}{40.30}$   
 $\frac{40.93}{-1.63}$

31.5  
 $\frac{45}{335}$



3875

9 42.0 -53 40 A05

8446

13426

5.55 -04 (-08) C

121

141

17797

2.86

556-015 145 1037

1758 3252

1960 / 2545- 5500 / 0502

1868

73966

919 049

4785

97654

3

15

R.A. : 9.789  
 DEC. : -45.501  
 R.A. : -556.00  
 DEC. : -508.00

DISTANCE : 0.00

3

DULUS : 10  
 VEL. : 50.000  
 P1 (U) : -0.757  
 P2 (U) : 0.257  
 P3 (U) : -0.037  
 P4 : -304.385  
 U : -4.289

P1 (V) : 0.000  
 P2 (V) : 0.000  
 P3 (V) : 0.000  
 P4 : 0.000  
 U : 0.000

P1 (W) : 0.000  
 P2 (W) : 0.000  
 P3 (W) : -350.000  
 P4 : 0.000

R.A. : 9.700  
 DEC. : -45.500  
 PM. R.A. : -656.00  
 PM. DEC. : -600.00

DISTANCE : 0.00

*E*

DULUS : 10  
 VEL. : 60.000

q1 (U) : -0.757  
 q2 (U) : 0.652  
 q3 (U) : -0.037  
 dU : -204.362  
 U : -4.269

*10r*

q1 (V) : 0.092  
 q2 (V) : 0.050  
 q3 (V) : -0.994  
 dV : -343.749  
 V : -63.106

*10r*

*+24.3*

q1 (W) : 0.647  
 q2 (W) : 0.756  
 q3 (W) : 0.098  
 W : %-3560.668  
 719

VX Nayan 9 43.4 -11 47 -10 -8  
-7 -4

9.8

+1 +9 Clubs -15.8

-7 -4

-3 +2

10.7 0.205 850

10.62 205 170 880 2800

10.77 260 170 740 2775

10.85 270 170 715 2750

Handwritten signature in a circle.

4







~~1000~~ +024

84610

9 434

-37 30

2706041

(36.3)

24.25  
-006

9.9  
-02

344  
24.204

(120.5)

10.59

9.92

-0071

8905-54270557  
4430 5383  
+0054

-00

-0045 +013

-0046 +018

-0547

+6.9

# / #

7052-7022

0065

655

(702)

655

2414E

2007

+284

2 of 10

33.0686

Z = -49

Plan

9 43.9 -62 17

+1.4

-0.00234

+0.0033

FN4

-0.163

-0.0010

-0.0013

N30

-0.13 + 0.07

8.0

N30

400P

-761 +608 -227

+098 -238 -964

+642 +757 -122

+0252 -0086

-0032 +0034

-0212 -0107

+0166 +6.6 +4

+0002 0.0 -1

-0319 -12.8 -13

-0.3

-1.4

-0.2

FN4

400

+0589 +0095

-0076 -0037

-0457 +0118

+0684

+27.3

-4.5

+27

-6

-15

9.7

-623

-28

+7

8.0

+1.4



5

-0174 ± 3.1  
-0170

9 43.7 + 6.3 29 720 + 798 w(3)

74406

6C13457

6.9

w6279

43.954 1985.8 + 6.3 28 52.77 1989.9

8.41  
1.38

1.170  
45.124

-116 ± 3 -143 ± 3 6.0

49.705  
54.475

1099.9 1927.2

50.3

44.324 541  
406  
417 44.270

52.78 999

36.1

854

44.104  
10  
124

57.12  
1.45  
55.67

55.00

46.3

55.1 1945.00  
54.27  
54.27

6.38

54.67

560-826 895 4116 -116 -143 +7.9 -128 +7 -303

065 072 096 189 -588 756 +3.5 -3 +2

-18 +63 -16 013

[+11 -63 +25]

846.07

9 43.8 +2 1

d/FU

HR3879

5.64 + 35 + 09 C

GL13459

5.64 +34 +14 2849

5.64 + 345 + 115 (6)

565 208 192 794

2.780

1215 .178 .800 (2) SPC 2.738

210 185 797 2.734

(3) C

[m] 216 0

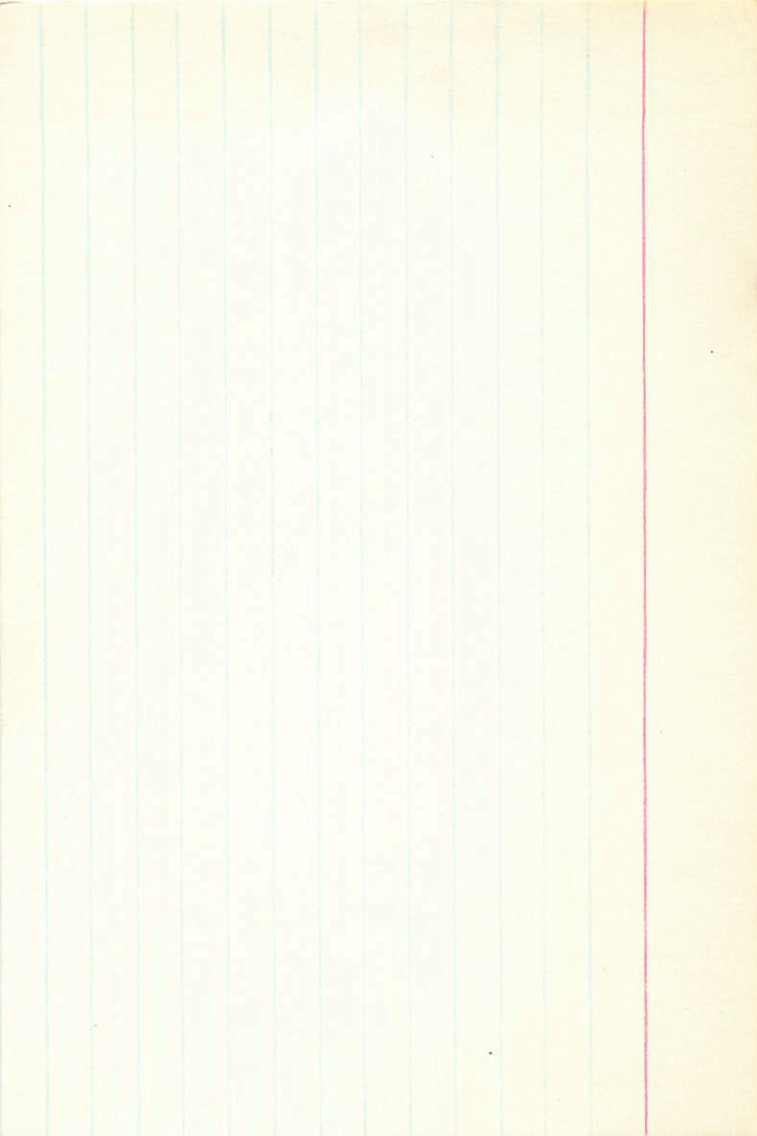
[c] 257

410

74ms +14.5 26.3 -12.4 <sup>s</sup> -0039

+099 -209 -280 -050 +15 c





4R3887

9

44.4 -58 34

C(4)  
+5.550.F

4R4858  
34850

①

FG.12

6.22 +0.44

-124

+0506C

13476

-124 +0506C

-120 +055

124

1928.35	"
1.034	+0.52
copy	

-0.58 ± 7.1 + 0.50 ± 4.5  
-0.140 + 0.61

559-830 -854 521 -120 +055 +5.9 -047 -5.0 137

067 026 100 039 133 597 +3.1 -2.6 +1.7 025

~~0.0~~ 23.505 1400.0 -58 33 48.28 1990.6 +2.7 +25.7 +0.5  
790  
24,295  
-2.97  
**23.0 -9.8 -6.3**

37.545  
463237  
23.86  
15  
682  
4  
886

37.4  
1542  
771  
-524

508.35  
53.44 1528.53  
55.00  
48.49  
-45  
48.94  
-10  
49.04 + 2.85

7483  
37.4  
46.8  
1701  
48.50  
-85

23.64  
16  
1656

47.3 19 46.3  
-67  
47.9

-1302948

C1161

9

44.0

-14 18

9.2 dG4

-4.28

36

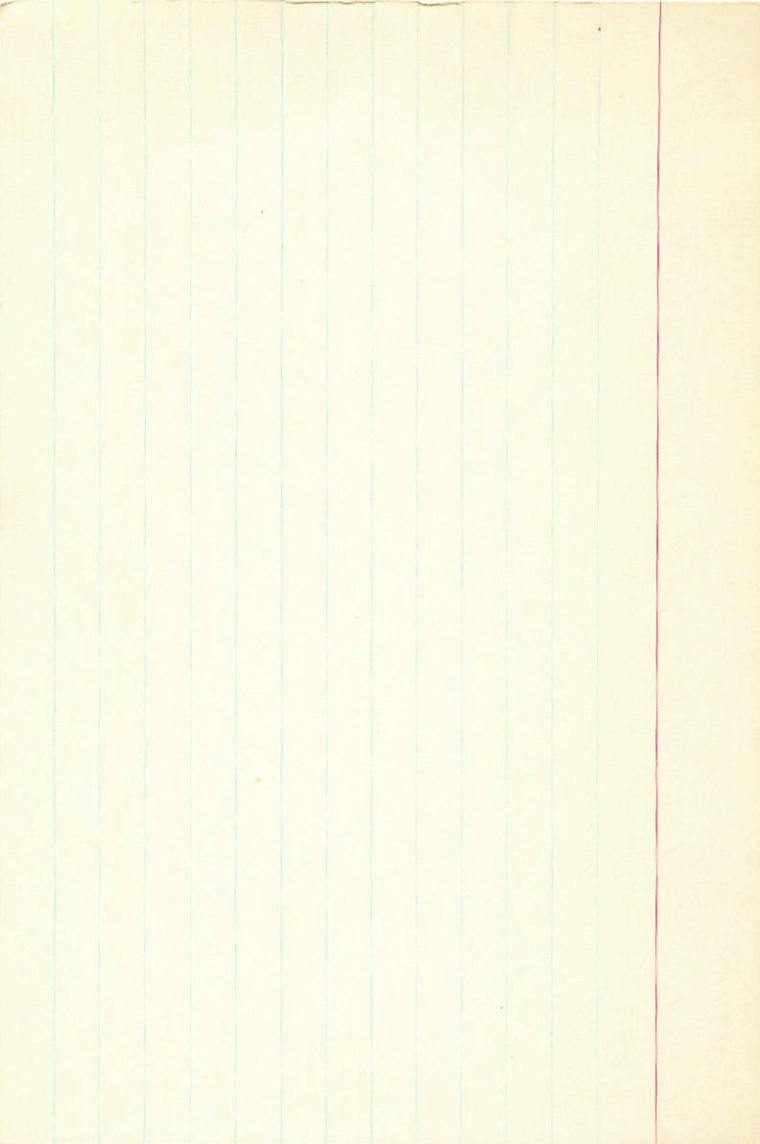
6284

423.4

180

-1.25 + 20 cm

-271.5 + 190.55 GR



1960  
84722 9 44.7 F11 48 6.4 A3m -3.76

13485

6297 74.767 1699.8 +11 48 1.26 1895.6

186  
44.953

87 EK  
-00386 +001K

44.816  
22  
83.8

-00351 +0030  
+0040

24.095  
20.775  
44.831  
64.27  
83.8

0015  
-050 +008

151 4

6997  
0380

44.901  
17  
512

-0037 ± 2.4  
000 ± 2.2  
-008

0.84 1934.1

$\frac{11}{0.95}$   
 $\frac{0.97}{0.29}$

56.18 19.28.57

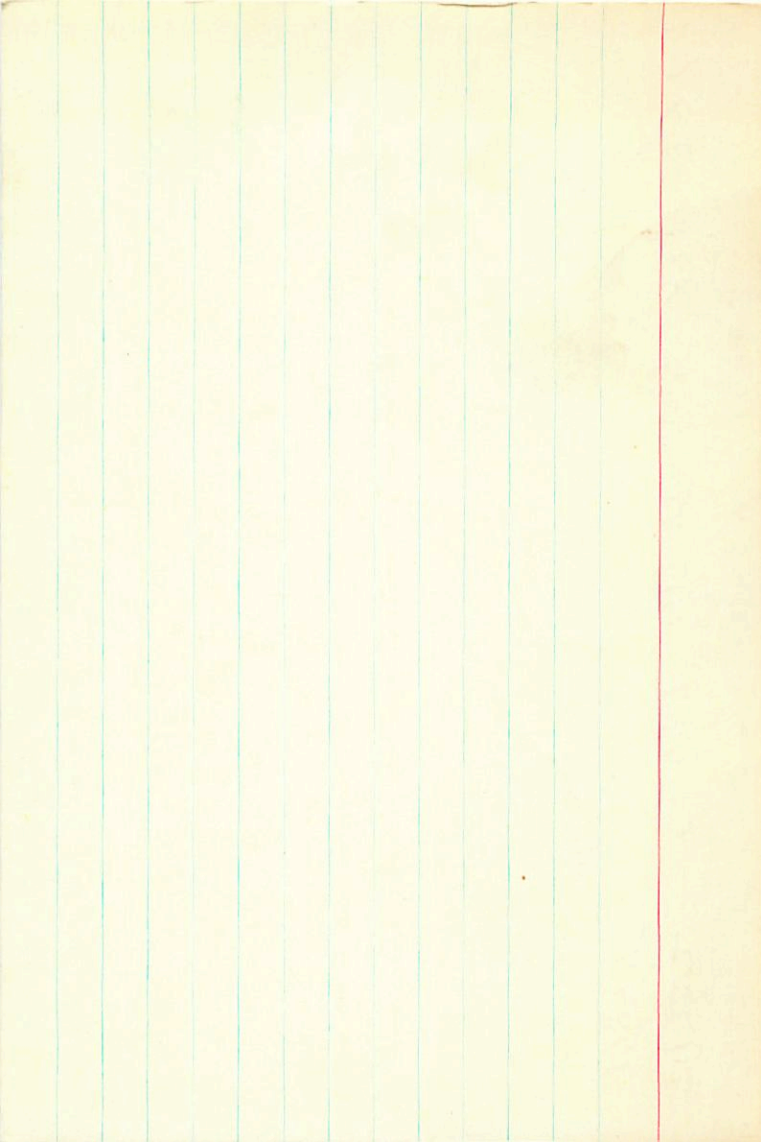
841  
343

10227  
34.1

38.5

0.97 1939.60

$\frac{+2}{0.99}$



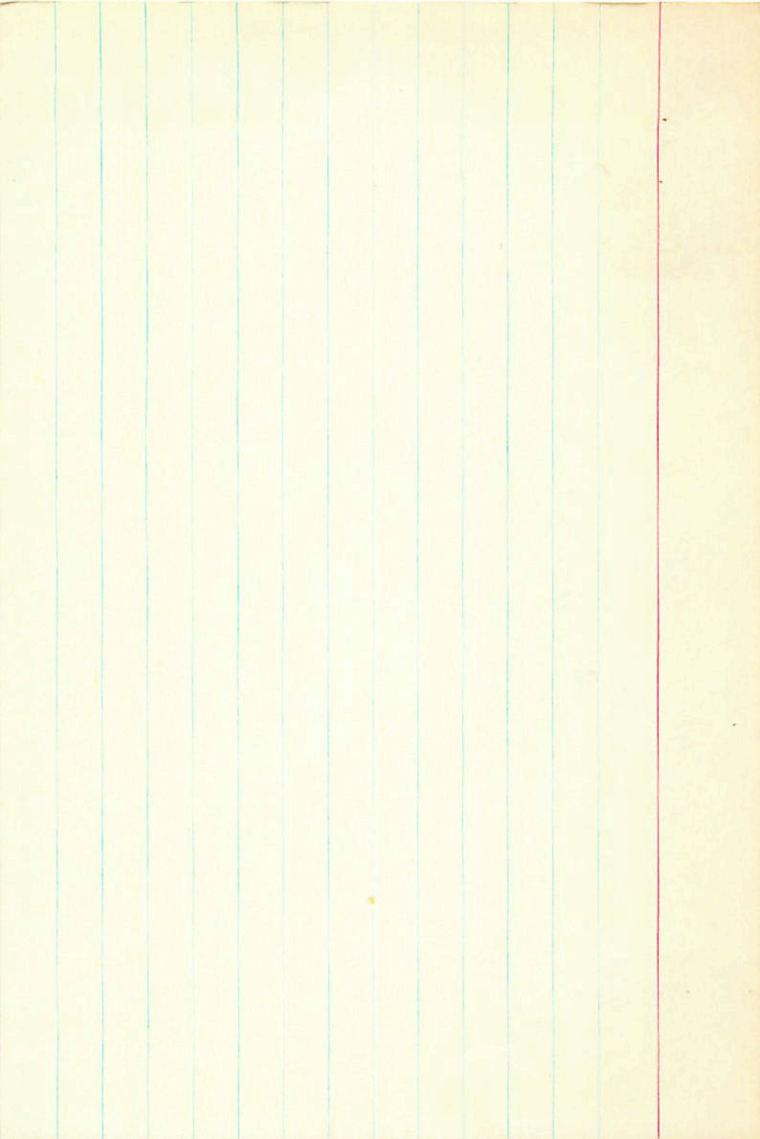
84739 9 44.9 +20 50 7.8 dF2 -15.48

13492

6290 +0053'' -011 N30

+0054 ± 2.7 -008 ± 2.2 66 → 630





3890

9

45.9

ST

-64.8

-64° 50'

3.15 FO

2 Cari

13506

6293

4.26

+13 (5)

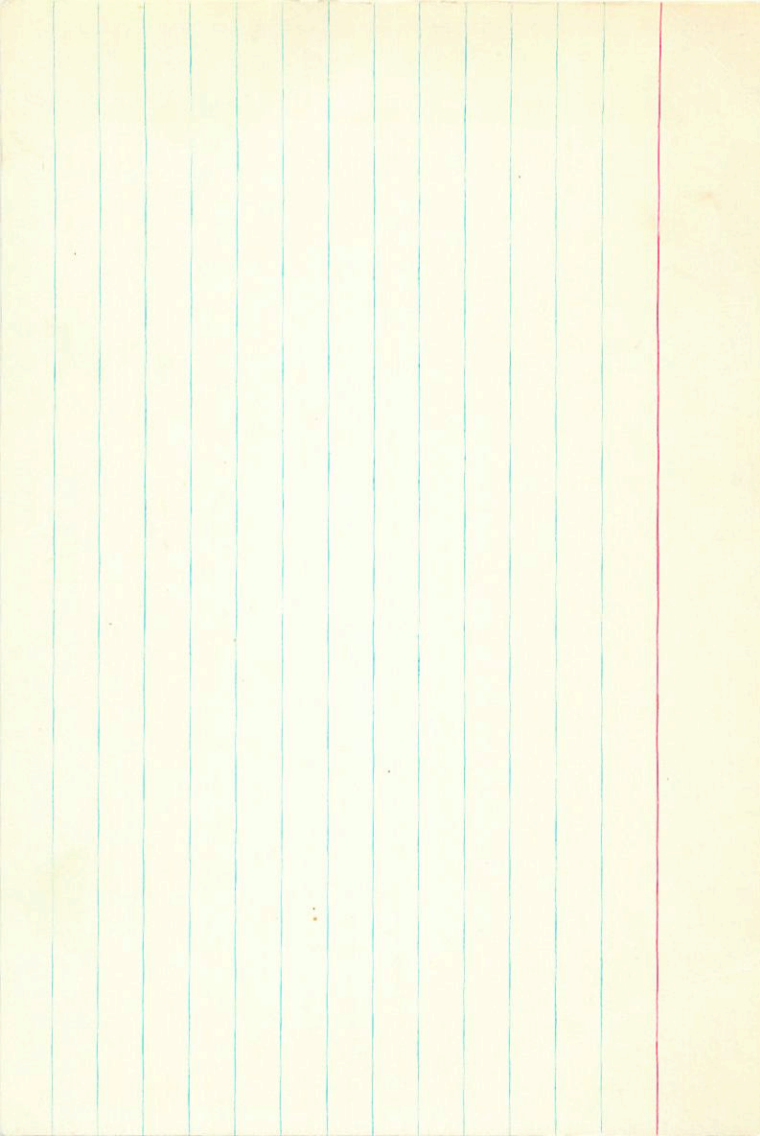
+13.6 a

-11

-0017 +002

One of kidney, 5", cpm

+0400	+0056	+0456	+3.5	-0.765	0.591	-0.256
-0053	-0027	-0080	-13.0	0.104	-0.280	-0.955
-0332	+0071	-0261	-2.0	0.636	0.752	-0.152



8483

9 442

713 59

68618

74835

803 303 056 354 11

534 302 074 354 5

534 308 083 352 6

305 071

305 080 353

059 Pg  
part 1

4425

4134  
1101

7410

Amber  
+02224

9 46.6 + 55 19  
10 ~~59.4~~ 710

+58.0251

-304 (2)

+010 -041 XGHR

+028  
~~+010~~ -037  
028 -027

+034 -033 Y

9.75 9.8  
+562 +55.3

~~632~~ -033

37 32

030 -031

-27 -30

2.75 2.75

-42.5

HR 3898 9 48.0 -45 30 +12 A

5h

-0.0024 +0.001

-0.029 +0.001

" -0.032 ~~0.002~~ GC →  
" -0.030 0.000 GC → MSO ONLY

400 ps.

-767	638	-048	<sup>465</sup> +1093	+23.6	-0.6	+46	+43	+16
108	050	-993	+0154	-6.2	-11.9	-16	-18	-13
632	767	108	-0999	-36.0	+1.3	-37	-35	-12

+1054	+0030	+1084	+433	-0.6	+43	400 ps.
-0148	+0002	-0146	-5.8	-11.9	-17	
-0869	+0036	-0833	-333	+1.3	-32	

GL13547

48 0.468 1909.7

-00302.80      -00243.4  
 -0031      -002

55.68 19016

+ 120  
388

+10  
55.67 -002

-00305  
 +54

55.56  
 -17  
55.73      1939.48

-00288

0.495  
 -001  
0.494  
 092

-0.030 001

55.73  
 06

Sting 1955.67

-0.0031 -0.004

+2 +3

-0.0026

85198

9

48.0

+17

SF

df6

+24 c.

+170226

-066

-049

625150



545-239 309 551 -066-049 +24 -015 +7 -223 ✓  
036 008 055 013 109 298 +22.8 -19 +12

-8 +42 -15 01

① 1688 N  
 157 159.08

W Sep 9 48.7 - 1 48

-16.2 +2.2 LB

1/ 0  
 -1.5 +2

450 Pa.

850 Pa.

-767	458	404	+0845	+0047	+0592	+50.3	+235 =
107	721	-684	-0076	+0068	-0008	-0.7	+10.4
632	481	607	-0149	+0096	-0403	-31.2	+35.8

+74 +26.5  
 -71  
 +2 -10.0





4.50  
94  
1.24

412  
129  
253

432  
136  
294  
424  
7  
+044 -006 +3.0

270

300M

-281 600 125 | -1528 -0170 | -1798 -514 +0.5  
129 420 -854 | +0269 -0122 | +0147 +21 -2.7  
611 675 413 | +1274 -0142 | +1084 +1.2

270

-46

+2

+30

A057545

85235  
13559 9  
6312

-000451.5 +01421.4  
-0006 +013  
48.7 +5418

-180000  
-11.9

AR36GM

13.069  
0222

5.1  
+5417 56.46 1891.9  
-004 +014 6.6

0.83  
42.418

55.65  
-81  
59.10  
57.20  
-1.10  
56.20

41.7

43.196  
059  
061

56.20  
56.20  
+  
35.9

71.78  
35.9  
44.0

060  
025

56.20

56.45 1944.76

43.079  
010

31  
56.14

542

542 -840 812 584 -004 +013 -11.9 011 -9.7 035

002 -006 002 -009 052 -019 -6.9 +5.8 -3.7

02

+8.4 -48.7 -7.5

-7.0 +0.3 -10.1

+11.0 -4.6 -7.9

01

-6.7 +1.5 -12.4

85441

9

49.6

+27

13

8.1

dRo -12.16

+0092±5.9 -183±3.1

13579

6321

33.862

1903.3

+27

13

9.88

1856.4

-480  
432

9.81  
19.69

A067551

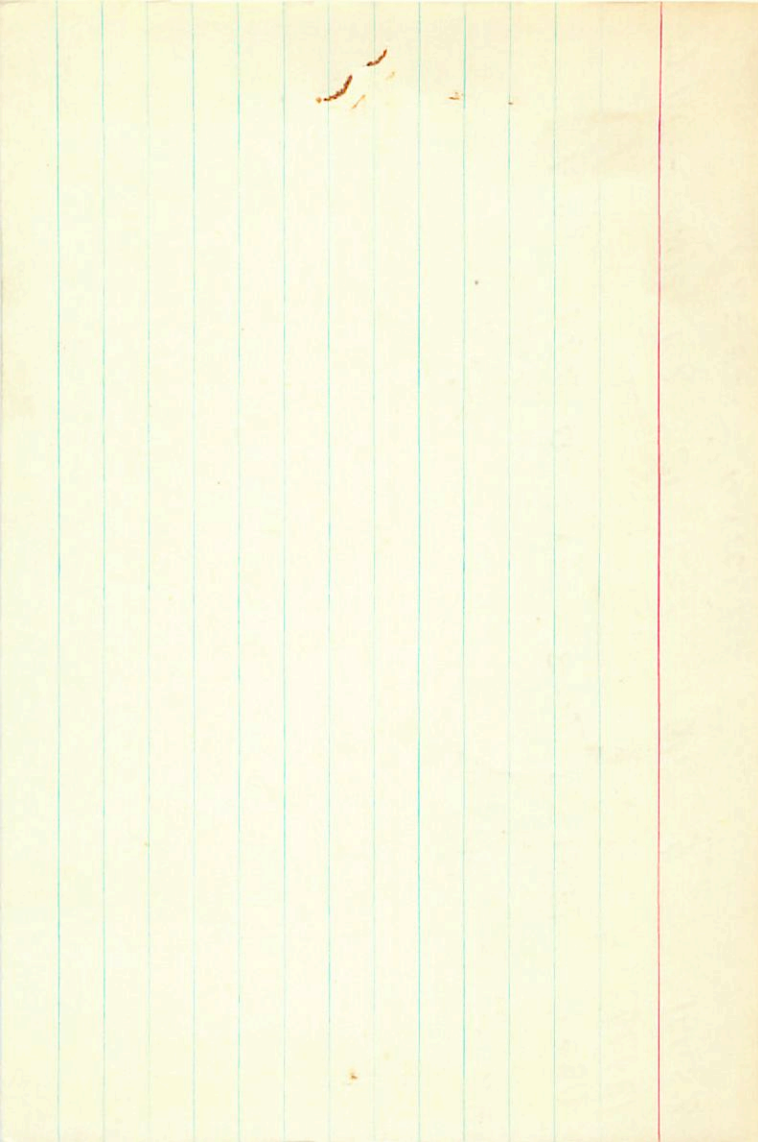
8.5-90

<sup>m</sup>  
Dm = 1.0

11  
2.5

phyp.





3812 9 49.7 -46 19

-00 25-010

-00 226-0068

-0234

020-003

642-1153 2548

646 71.76 2547

644

$V_{amp}$

118.1

(11)

7254

6889

1198

1150

6410

6409

2000

644



6



R.A. : 9.800  
DEC. : -46.300  
1. R.A. : 0.000  
1. DEC. : 0.000  
DISTANCE : 0.000  
MODULUS : 10  
D. VEL. : 0.000

q1 (U) : -0.768  
q2 (U) : 0.637  
q3 (U) : -0.060  
dU : 0.000  
U : 0.000

q1 (V) : 0.109  
q2 (V) : 0.038  
q3 (V) : -0.993  
dV : 0.000  
V : 0.000

q1 (W) : 0.631  
q2 (W) : 0.770  
q3 (W) : 0.099  
dW : 0.000  
W : 0.000

6

3901

55380

NO 373

9

486

50

1382

360	187	411	2624
368	174	415	(357)
354	189	(414)	
643			

3506

9 49.6

+2 41

412

85504

13582

-17 127 | 1040  
1043

2836

6.02 -05 -08 C

014	136	1070	2.817	after
-017	132	1051	2.837	56
-015	134	1045	2.823	

-030

Bank 51

147.1

-0122 +098 4.15

1054	268
1.322	
1.251	

60

132

1643
244
1309

-1828

-181 +092

6.0

37.150

15.41

69.32

7



1890

1891

1892

1893

1894

1895

1896

1897

1898

1899

1900

1901

1902

1903

1904

1905

1906

1907

1908

1909

1891

1902

1913

1914

3906.000\*

9.000\*

49.600\*

2.000\*

41.000\*

-0.181\*

0.092\*

6.000\*

158.489

97.100

*Cost*

0.864

0.436

*196*

179.260

0.240

-0.622

*-19.*

-22.368

-0.350

0.650

*+*

7 Sep	9	49.6	+0.2	41	A1	+97.18
85504		6.02	-0.04	-0.09		+95.8w(4)
G613582		6.024	-0.4	+1.45	(24)	+98.7v(2)
W6322		6.05	-0.05	-0.5	1(19)	
72337		6.02	-0.05	-0.08	Cage	
730280						

-183 +089

+128 -37 +32 .010  
 +138 -34 +27 .009

56 + 2 (5)

613-024 139 1043 2.968

6A(16)  
 7M(8)  
 -10Y(10)

Rep. J. Seydel Vol 1/4 man 1913

9 ± 5

37.444 18940

$\frac{653}{39,132}$

37.527

$\frac{545}{545}$

37.642  
 $\frac{25}{667}$

$\frac{1412}{606}$   
 $-.526$

-0122 ± 2.1  
-0123

+2 41

42.7

+089 ± 1.8

+057

17.24 1986.4

$\frac{-5.62}{11.67}$

16.20 1940.25

$\frac{+20}{1540}$  1202

1545 1433.1

$\frac{19}{15.62}$

$\frac{16.01}{+4.34}$

335

$\frac{36.7}{49.5}$

3406

9 446 + 2 42

+970

75enf

132 1043

85504

-0.7 137 1040 2.886

601

1307

+2.88

+0.01

- 0129 091

-193 91

-193

91

574

+97

R.A. : 9.800  
DEC. : 2.700  
R.A. : -193.000  
DEC. : 91.000  
STANCE : 5.400  
MODULUS : 120  
VEL. : 97.000

q1 (U) : -0.768  
q2 (U) : 0.463  
q3 (U) : 0.441  
dU : 902.029  
U : 151.270

q1 (V) : 0.109  
q2 (V) : 0.775  
q3 (V) : -0.623  
dV : 234.292  
V : -32.234

q1 (W) : 0.631  
q2 (W) : 0.430  
q3 (W) : 0.646  
dW : -390.588  
W : 15.705

8

8



CC13543

-0034+3.0 -0437 2.0  
-0039  
-051

-0037  
-044  
-050

1.847  
235  
2.135

1588.9  
-0037

52 2.35  
2 + 2.44  
4.91

1593.2  
434

2.135

1.811  
04.17

8.65

7.40  
431  
7.29

1438.50

42.2

50 1.939  
445

21  
43

8.64

7.29

216  
36.0

45 47.547  
1 14.355  
50 1.952  
1.942

1.553  
182

45 513.0  
7 1.22  
52 6.94  
71.28  
6.93

1433.26

1.822-67.27

843  
14

8.93

9.11  
2.20

843

843  
14

6



✓ M : 119.15  
PM : 487.883  
d3 (M) : 468.0  
d5 (M) : 342.0  
d1 (M) : 332.0

U : 150.25  
UP : 198.921  
d3 (U) : 227.0  
d5 (U) : 778.0  
d1 (U) : 811.0

U : 142.81  
UP : 527.42  
d3 (U) : 238.0  
d5 (U) : 232.0  
d1 (U) : 477.0

WAVELENGTH : 000.21  
DISTANCE : 001  
DEC : 000.2  
WAVELENGTH : 000.24  
DEC : 000.25

DEC. : -57.500  
PM. R.A. : -45.000  
PM. DEC. : 5.000  
DISTANCE : 100  
MODULUS : 12.000  
RAD. VEL. :

q1 (U) : -0.774  
q2 (U) : 0.535  
q3 (U) : 0.339  
DU : 94.762  
DU : 13.541  
U : 13.0

q1 (V) : 0.118  
q2 (V) : 0.647  
q3 (V) : -0.753  
DU : -169.891  
U : -26.027  
V : 280

q1 (M) : 0.622  
q2 (M) : 0.543  
q3 (M) : 0.564  
DM : -283.787  
M : -21.611

Q

+15.94

85741

9 50.2

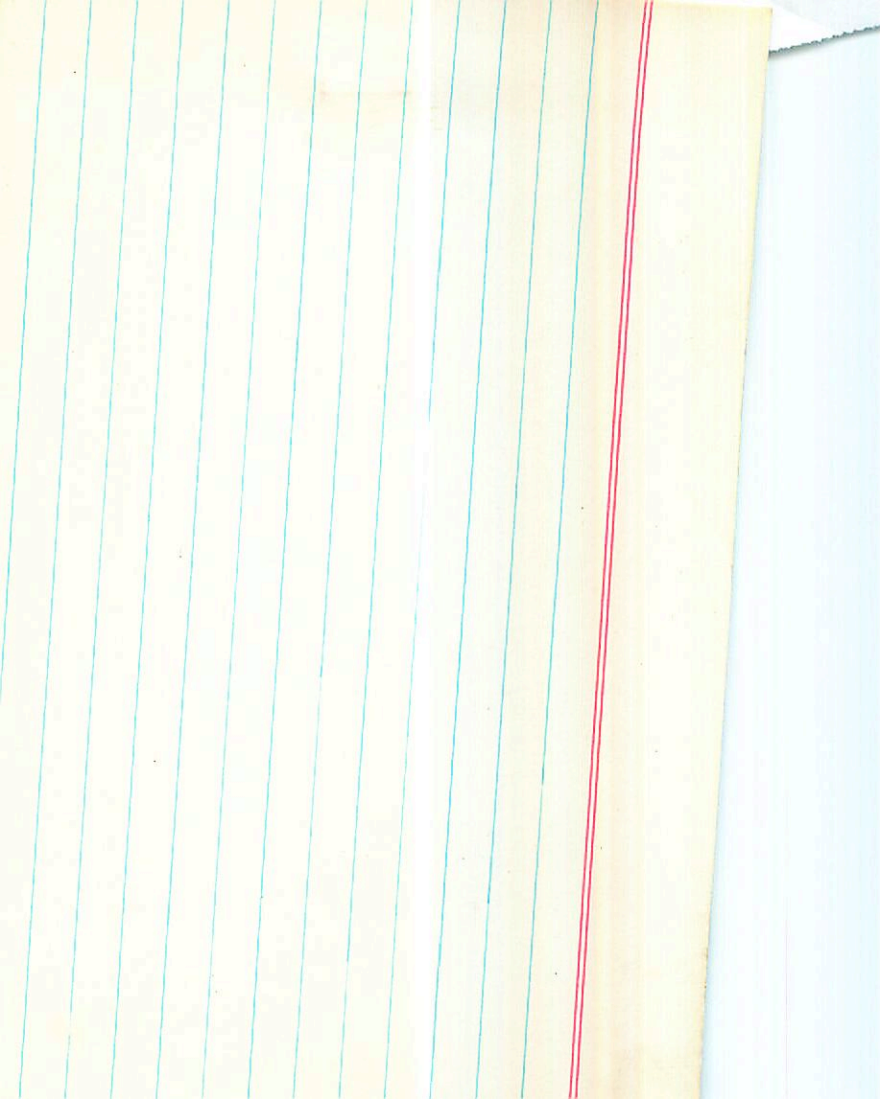
-60 21

10 11-12

FD 1168

7.26 + 0.95 (2.01)

3618595



52658

9 505

-27.06

346

629 391 206 422 ①

+650743

85515 ~~85515~~

-0152±8.0  
-0163

2 51.0 +65 29 9.1 d65 -1728 400

13607

6330

(Cylinder)

59.121 1907.7 +65 29 19.54 1911.1

$\frac{643}{764}$

$\frac{6.34}{25.88}$

NEW YORK

-063-163

59.34  
50  
599

22.8 1930.0  
-10  
22.70

-0152  
-0163

-163 GC  
-168 mm

8161 -2390 } 1781  
-8778 -8710 } 1811  
1878 } 1878

-0114

-071 ±1 -149 ±5 G-R  
-071 -142 G-P

9 Ent  $-0020 \pm 2.2$   $+012 \pm 1.9$   
 $-0019$   $+004$   
 85762 9 51.5 7 5 11 7.0 9 MO 127.2 8

13617

6333 25.931 1896.6 +5 10 54.57 1889.5

$\times 502248$   
 $\frac{107}{30.038}$   
 $-0020$   $+008$   
 $-00205$   $+0045$  FLY 53.84  
 $-73$

54.28 1938.22

$\frac{39.1}{-0224}$   
 $\frac{54.28}{+14}$   
 $\frac{54.28}{-4.42}$

$\frac{25.941}{+20}$   
 $\frac{25.941}{96.1}$

53.78 1933.2

$\frac{965}{-073}$   
 $\frac{53.78}{114}$   
 $\frac{53.78}{53.84}$

$\frac{25.946}{23}$   
 $\frac{25.946}{909}$   
 $\frac{53.9}{4.5}$   
 $\frac{4.5}{2.0}$

$\frac{35.7}{46.2}$

$\frac{54.62}{+1.78}$

$\frac{1076}{-10174}$   
 $\frac{1076}{-10174}$   
 $\frac{10161}{-10174}$   
 $\frac{10161}{-10174}$

10



85762.000\*

9.000\*

51.500\*

5.000\*

11.000\*

-0.029\*

0.012\*

7.500\*

316.228

27.200

0.132

0.449

53.901

0.029

-0.587

-6.745

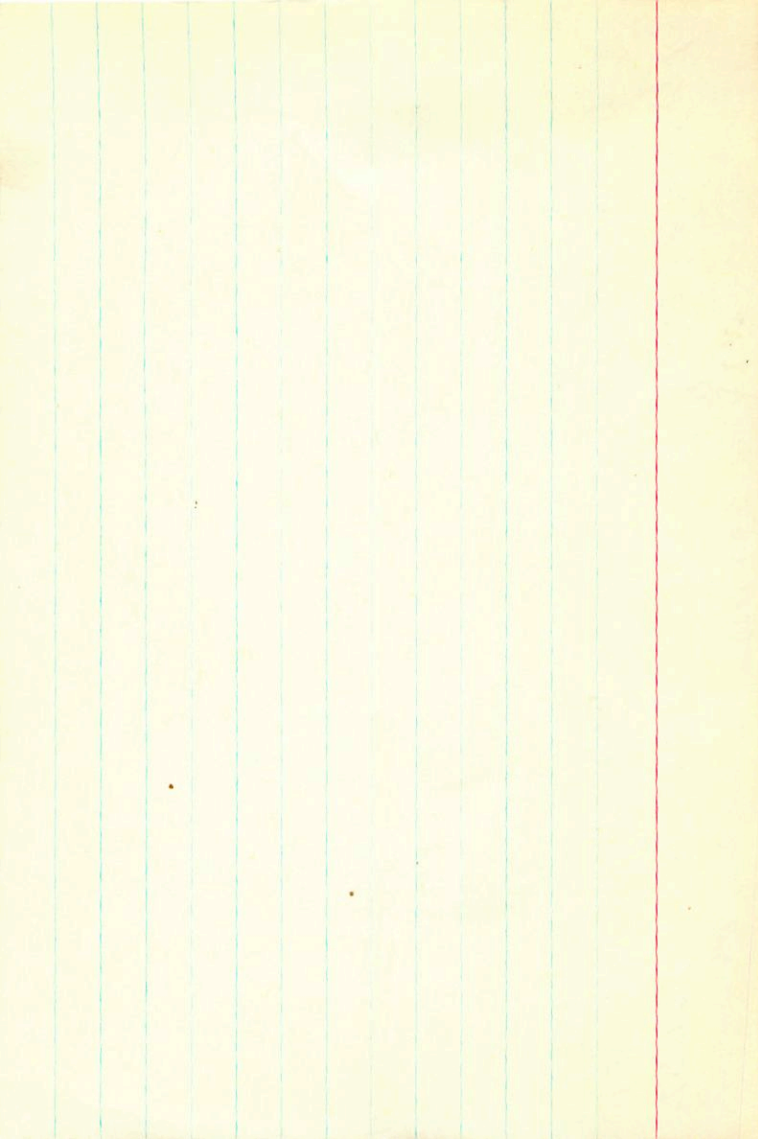
-0.063

0.674

-1.456

10





HR8859

9 40.7 +65 13

-28.2

-0.49 +0.11 →

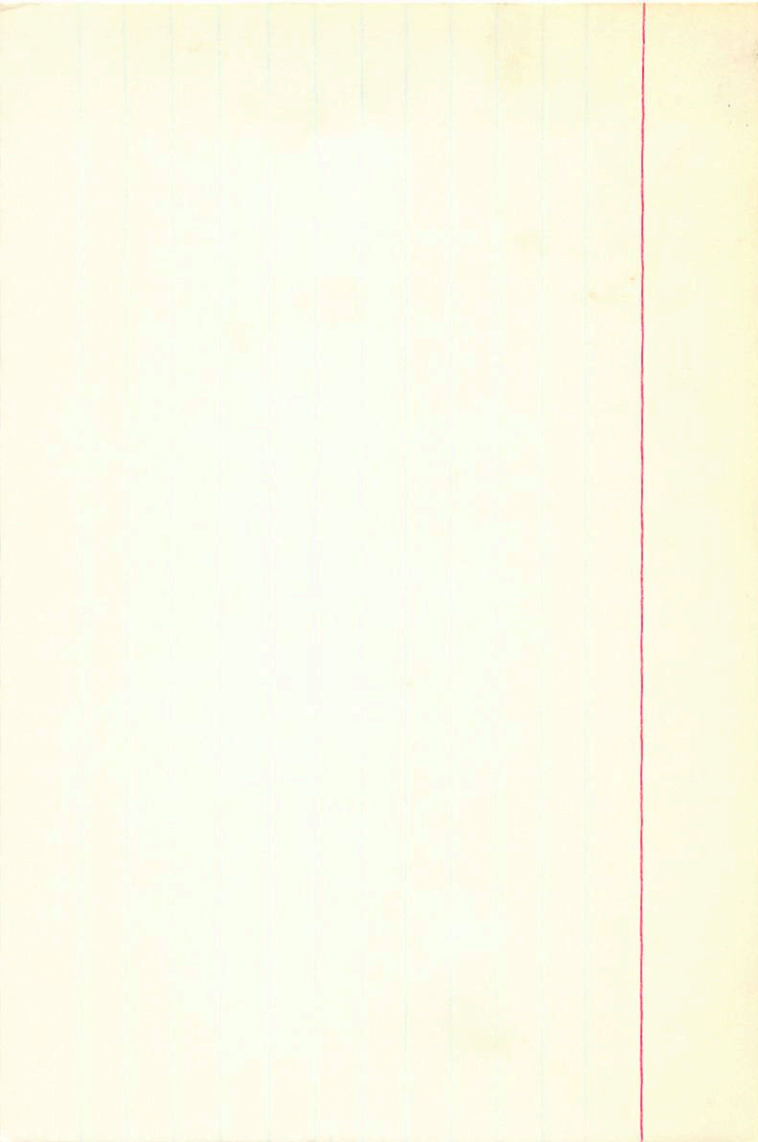
G3A

-753	-200	627	+1749	-0104	+1645	+10.4	-17.6
096	915	355	-0200	+0477	+0277	+1.7	-11.0
652	-352	672	-1514	-0184	-1698	-10.7	-18.8

-7.2

-9.3

-29.5



644-23

9 411 + 27 12

R 93

57 254

-553 -134

-546 -094 h

-644 -090 G