

A05117B
174897

25893

11330

-0007±6.9
+000
18 50.0 +14 28-043

6.5 9120 +1076

+138
+80
+800
1872.3

1595 1896.8 +14 28 26.56 1872.3

037
63 2

1.645
648

1.644
652
650
+018

2.64
29.2 0

26.83 1932.9
26.79

39.4

26.92

26.79 1939.57

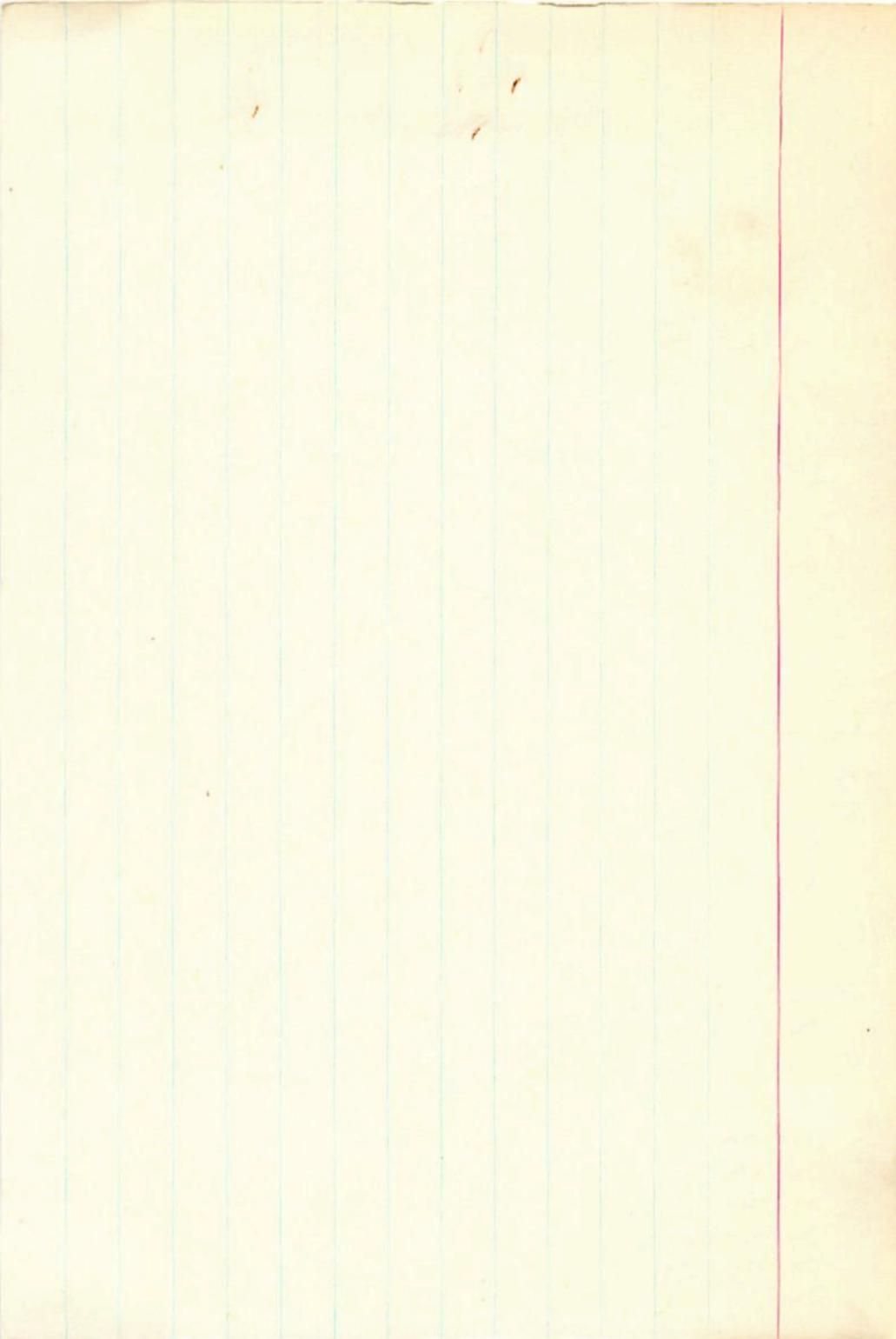
26.86

247

36.2

53.9

-2.34



mm

-79.6 ~~10.1~~ 6.36

112 km 17g

18 50.1 21 2/

7113

-22.5

174933

1.43

5.44 - 0.06 0.48 2E

x14

2.8mm
2347 Ca
2355 Ca

-0.37
-0.42
-0.35

585

126
124
123

2.8mm

588
596
284

124
117

2.752
2922

16
-60095 -004 B204

588
596
284

124
117

2.752
2922

1.21
1.41
1.21

-1
-60090

588
596
284

124
117

2.752
2922

-60090

-0.5

1.55

-0.112

1.55

-0.5

1.55

5008-005
60090

-0.40 125 590 2.747

118 595 2.823

284

634

1.55

5008-005

27

2823
447
76

25
6-10
10
1

7113.000*

18.000*

50.100*

21.000*

21.000*

-0.008*

-0.005*

6.500*

199.526

-22.500

-0.028

5.95
108.5
284
7.25
84
102

7113 18 50.1 +21 21 B9 II -√11

-09-45

(407)

5.41 -035 103 584 2.755 B9↑

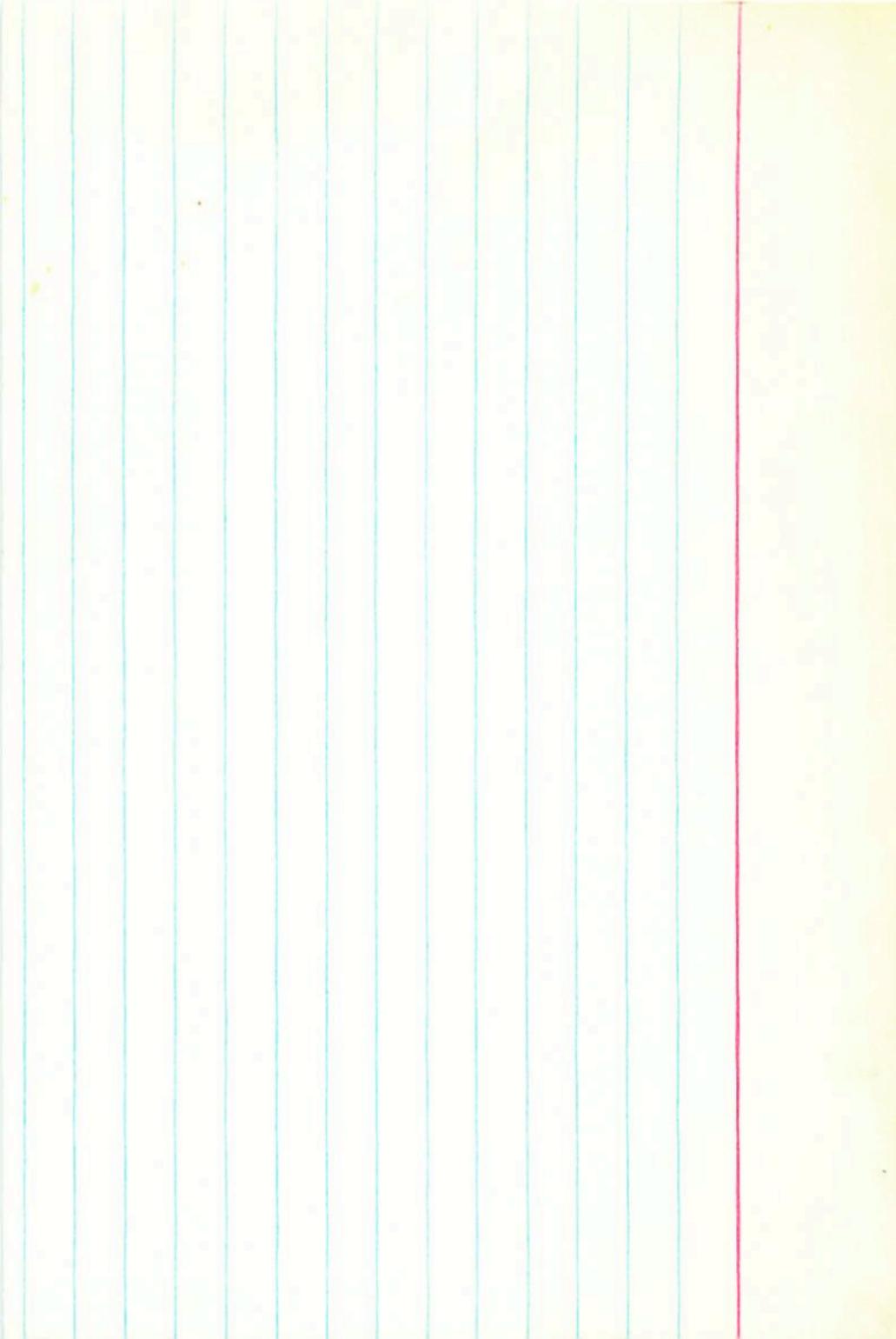
112 591

227

815



$$M_V = -0.25$$
$$\frac{103}{5.2} = 19.6$$
$$\frac{5.41}{5.45}$$



175036

18 50.4 +26 28 7.9 dF8 ~~51.2~~ 26

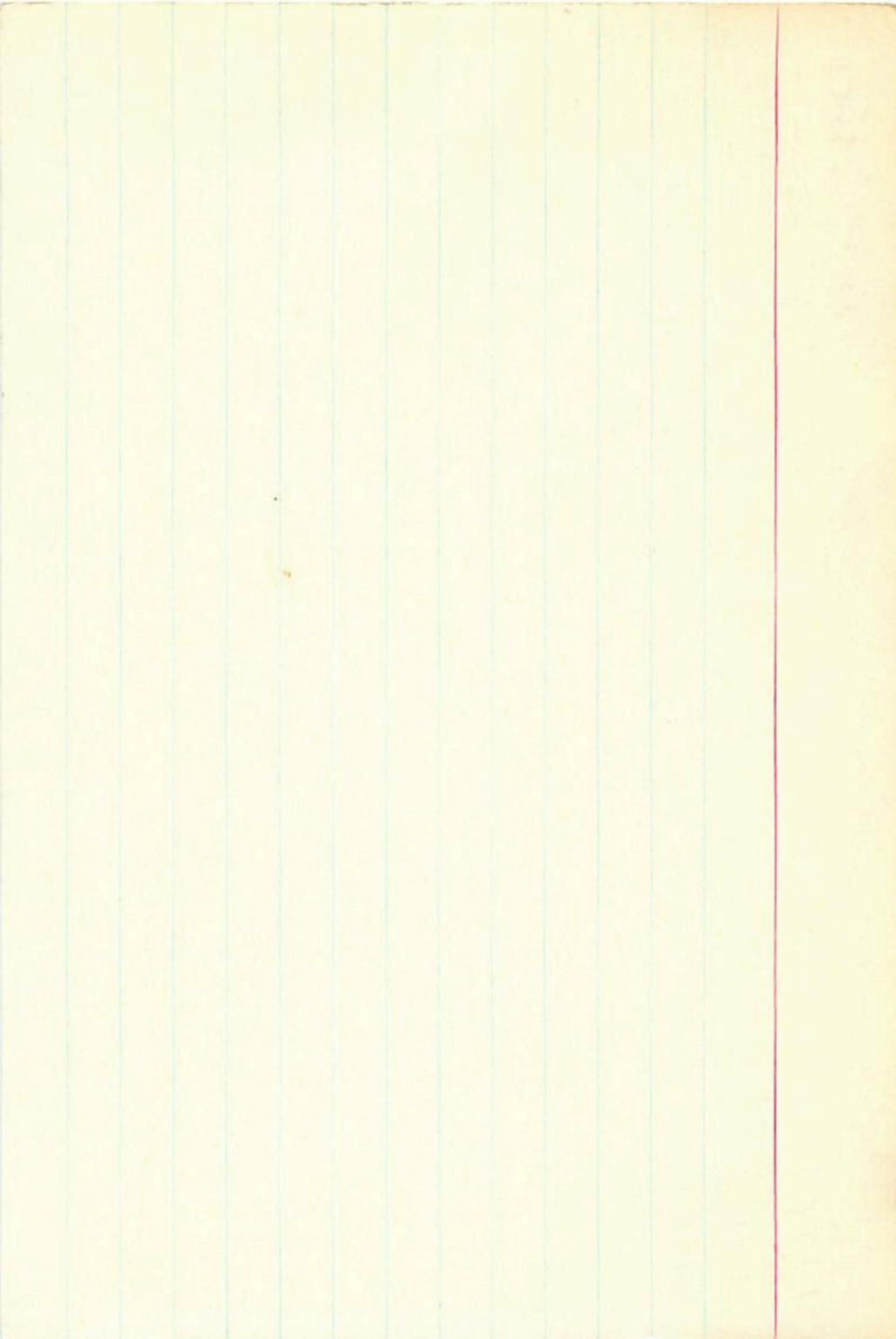
⁶⁰⁰
P02 Wick -5h 5a ^{DP/L}

+26⁰³³⁷⁹

11336

+100 +147 7

$\frac{-7}{096}$ $\frac{-3}{144}$ → CV



-0053 ± 2.7 + 208 ± 2.1
-0046 + 262

175225 18 50.5 + 52 55 5.6 d 68 + 1.86

-0.4 00

25904

11337 27.723 18940 + 52 54 35.03 18940

-15.01
20.02

35 ± 1

297
28,020

40.0 1927.4
48.25
28.25

5-4.12
33.725
27.84

826
-194

59 4209
28.17
28.87

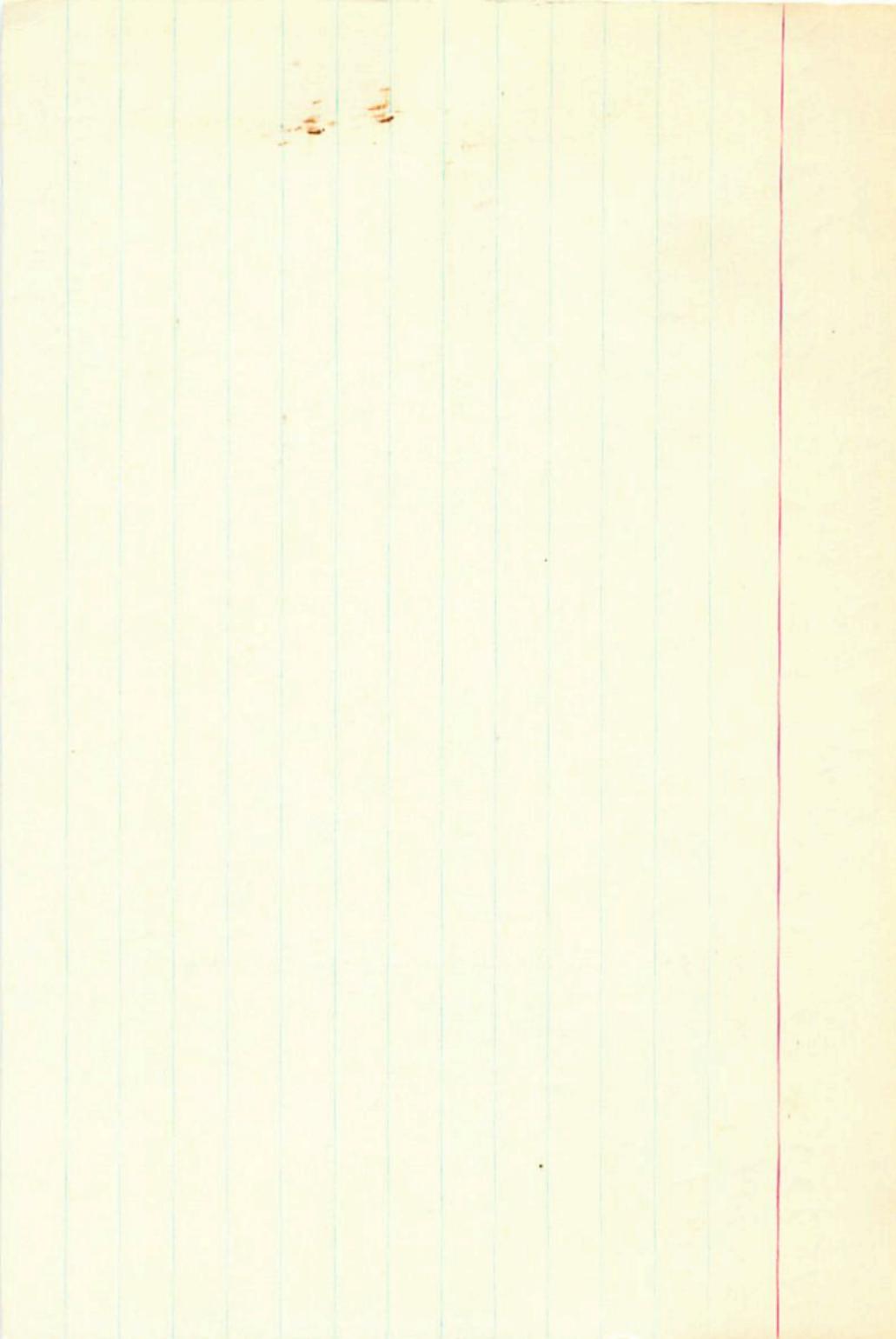
279075
807

33.44 1144.89 7229
-21 36.1

42.1

33.2
31.04
+ 1102

42.1



NG 66705

M2

-0.0011

M3

-0.0060

∫ +13.0

M11

trans -00148
+002

18 50 -6 20

1660 po.

+254 +460 -980

+394 +793 +471

-996 +458 -048

-00132 -00138

-00200 -02255

+00463 -01302

-01270 -2.1 -11.4 -32.5

-02153 -40.8 +6.1 -34.7

-00839 -13.9 -13.9

11-1

28

6705.000*

18.000*

50.000*

-6.000*

-20.000*

0.002*

-0.001*

11.200*

1737.001

13.000

0.001

-0.886

-10.524

-0.000

0.461

5.710

-0.011

-0.055

-19.100

28

o dia

175306

25905

11338

AP511779

511779

18 50.5

+0098⁷²

+0099±1.0

+59

+028⁷¹V80

+029±0.5 G.C. → N30

20

4.8

968

-19.5a

-19.5

968

-19.5a

Sy. B. P = 1389

274379

R Par

18 51.8 -67 18 +36.5

+0048	-0114
+0023	+0065
-0168	+0125
-0366	
+0638	
-0043	

+0006	⁺²¹
-0004	
+0009	
+0004	

+0195
+015
+015

+0009	
+0004	
+015	
+015	

R J +28
R - +66

-00094

+0137 FR4

82
9.6

112

FR4 -0066	-0377	-0443	-7.1
-0099	+0515	+0416	+6.7
+0229	+0114	+0343	+5.5

60

FR4

-35
-10
-10

25

257 -582 -772

384 794 -472

-888 176 -425

100	-0414	-6.6	-28.2
-----	-------	------	-------

-38

-4

-0

N30

+0565

+0428

+9.0

+2.0

-17.2

-15.5

-603

copy 10137

158

(C.O.)

4.34
16
595

copy 1013

(C.O.)

tbls

14 Par

18

51.8

-6.7

15

+865

18.85
-6.73

-8

+11

7.0

+865

-6.03 + 0.11

$$\begin{array}{r} 48.260 \\ -4.5 \\ \hline 43.76 \end{array}$$

$$\begin{array}{r} 4.7 \\ -1001 \\ \hline -996.3 \end{array}$$

$$\begin{array}{r} +1001 \\ +1001 \\ +1010 \\ \hline 3012 \end{array}$$

CO.C

6.1

$$\begin{array}{r} 48.256 \\ -3.4 \\ \hline 44.856 \end{array}$$

$$\begin{array}{r} 89.17 \\ -8.3 \\ \hline 80.87 \end{array}$$

$$\begin{array}{r} 52.34 \\ -3.3 \\ \hline 49.04 \end{array}$$

$$\begin{array}{r} 49.253 \\ -1.1 \\ \hline 48.153 \end{array}$$

$$\begin{array}{r} 10.916 \\ -1015 \\ \hline -904.084 \end{array}$$

$$\begin{array}{r} 56.5 \\ -2 \\ \hline 54.5 \end{array}$$

10

11

12

18.850
- 67.300
- 8.800
11.800
7.800
251
36.500

ILLEGAL ADDRESS

18.850
- 67.300
- 8.800
11.800
7.800
251
36.500

0.250
- 8.585
- 8.769
- 34.288
- 36.675

8.381
8.793
- 8.475
35.762
- 8.371

- 8.388
8.170
- 8.428
21.879
- 18.110

29

S. S. S.

18

519

736

5-4

700036-002-FAS
Support



30

01/01/2020
02/01/2020
03/01/2020



10.05
10.05

-0008 ± 4.5 -007 ± 4.0

-0009 -0.12

175154 18 51.9 40-18 5.0 BF -2.06

25931

11350

51.114 1408.1 -15 40 1.64 1404.8

$$\frac{034}{148}$$

$$\frac{+0.32}{1.3}$$

20

25.140

25.982

51.120

$$\frac{112}{0}$$

52.91

49.35

3.56

1.52

0.94

2.434

1.7

1.90

1.73

1934.64

28.7

1.07 1.2

32.0

1.72

1.40

51.142

9

133

-0.26

122

1.81

1.71

1.9504

1.71

-10

1.81

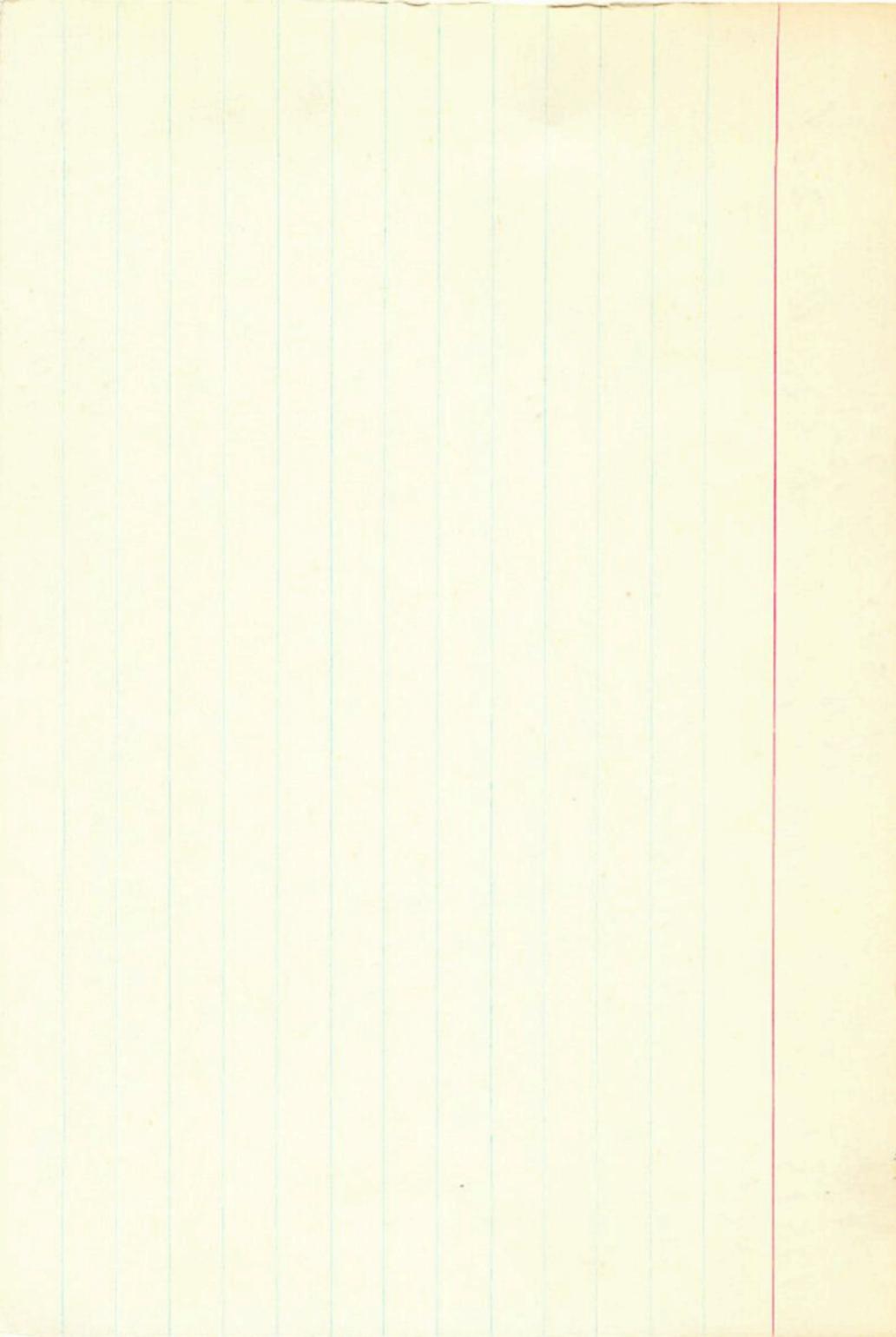
1938.84

13.50

36.8

51.145

1.29



0000 ± 2.9 -029 ± 2.5
-0004 -030

175535 18 52.0 750 39 5.0 964 78.2a
25935 +100

11353 59.203 1893.4 750 38 42.43 1898.4
0 1.50
43.93

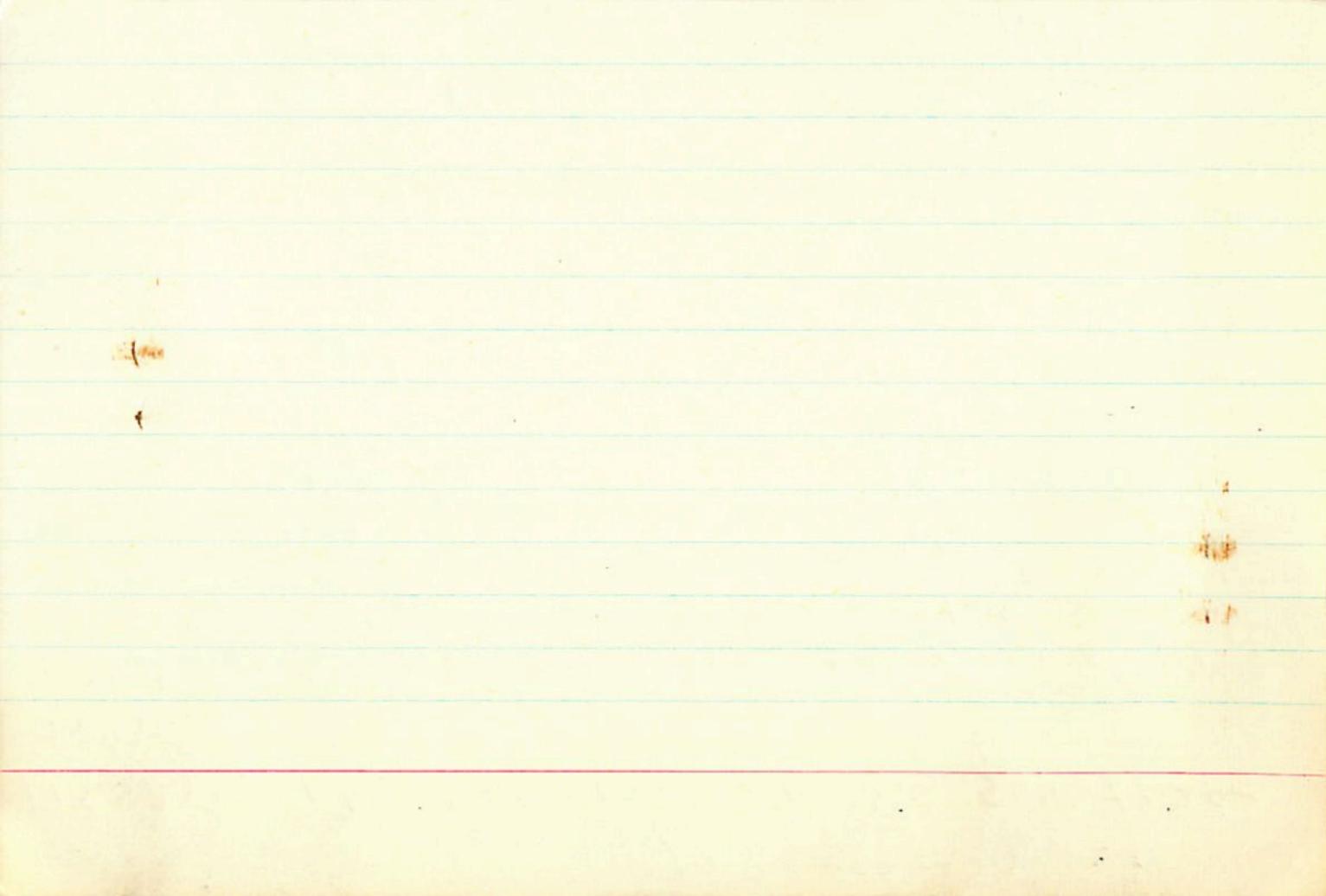
22.03
37.145
59.174
179
59.186
791
185
-018

43.2

50.9 1927.9
51.38
42.28
42.65
42.93

7311
36.6
38.2

42.90 1945.21
-25
42.65
42.79
-1.14



+15.30

7137 18 52.2 + 27 50

-21-07660
+4
0
0724

31



7132.000*

18.000*

52.200*

27.000*

50.000*

-0.021*

-0.072*

5.000*

100.000

15.300

-0.385

-0.513

-38.356

-0.175

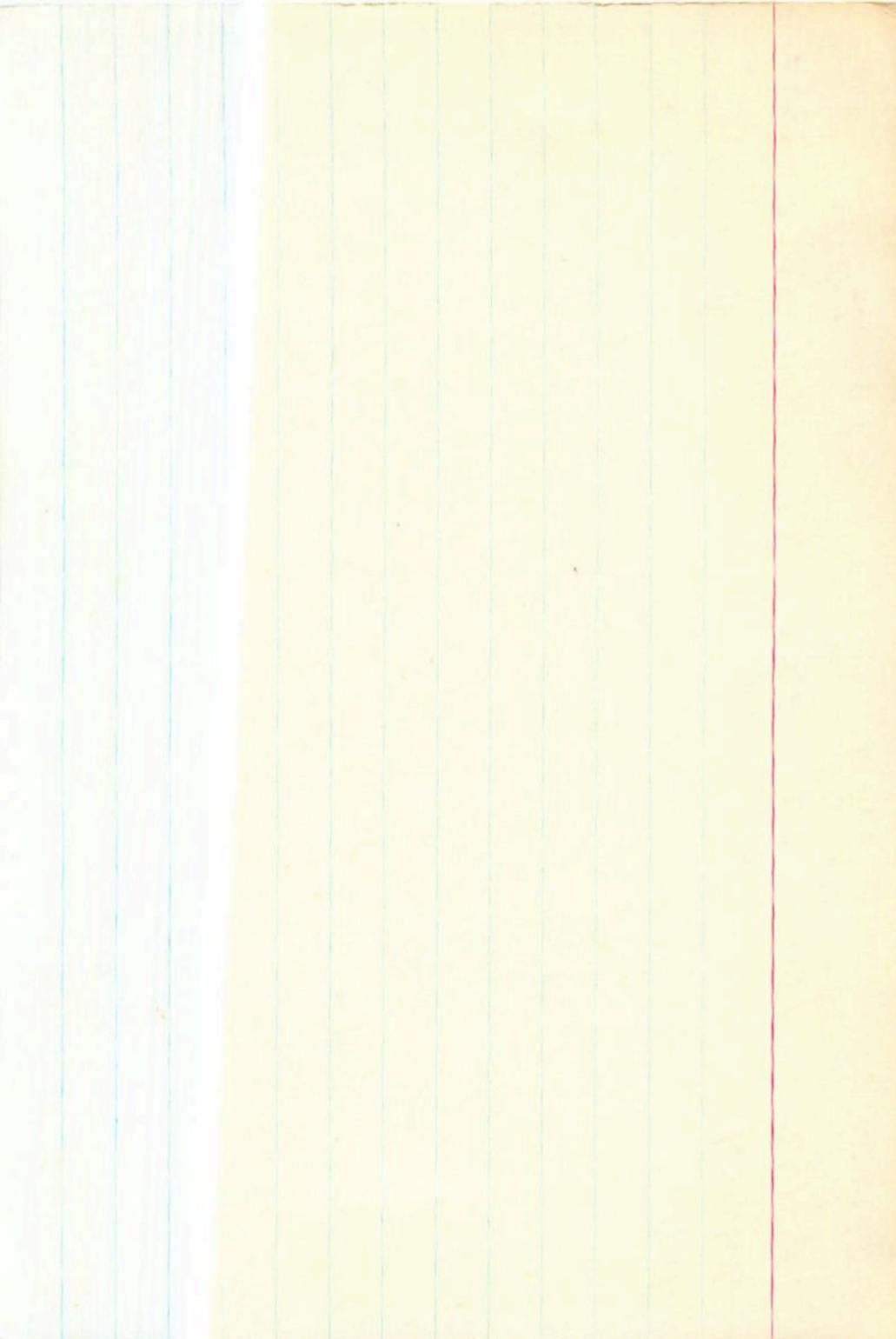
14060 + A3
 113400
 175492
 25954
 11364
 18002 ± 2.4
 52.6
 18
 1001 ± 1.7
 -0.12
 22
 35
 46960 - 235a
 -2390.6a
 Sp. B. P =

38.152
 -0.11
 141
 34
 49.52
 -0.6
 1895.0
 +22
 1892.2

38.130
 -1
 129
 95
 48.96
 1934.2
 49.05

38.175
 -7
 168
 95
 49.12
 1940.05
 -20
 41.28

148
 148
 1007
 48.92
 37.1
 45.0
 -1.54



175 219 18 52.7 -42 47 B5 -21.281.11

GC25956

GL III-IV

-21.00.4 62/8

W11367

5.35 +1.00 +2.05 Ston

-21.19

X4368

~~0017~~ ~~46~~ ~~184~~ +47

-039 -028 GC

+59 Y(12)

-6035 ± 5.1 ~ 028 ± 5.0
-0028 -029

43.210 1907.1 -42 44 33.28 1905.2

$$\begin{array}{r} 154 \\ \hline 1,364 \end{array}$$

$$\begin{array}{r} 41.25 \\ \hline 52.03 \end{array}$$

$$43.311$$

$$\begin{array}{r} -31 \\ \hline 280 \end{array}$$

$$32.99 \quad 1935.86$$

$$\begin{array}{r} 4 \\ \hline 32.95 \end{array}$$

501

$$43.225$$

$$\begin{array}{r} 221 \\ \hline \end{array}$$

41.2

$$33.34 \quad 1956.87$$

$$\begin{array}{r} 9 \\ \hline \end{array}$$

$$9668$$

$$33.48$$

$$48.3$$

$$\begin{array}{r} 250 \\ \hline -114 \end{array}$$

$$\begin{array}{r} 33.20 \\ \hline -1.17 \end{array}$$

43.1

+0019±3.0
+0023

175823 18 52.9 +57 25 6.4 915 -5.16
25960

11370. 54.257 1898.4 +57 25 21.35 1892.2

-095
159

+46
81.

21. 1926.8

28.29
259622
54.257
241
245

27.4
53.72
2140.

38.0

2277
36.4
44.2

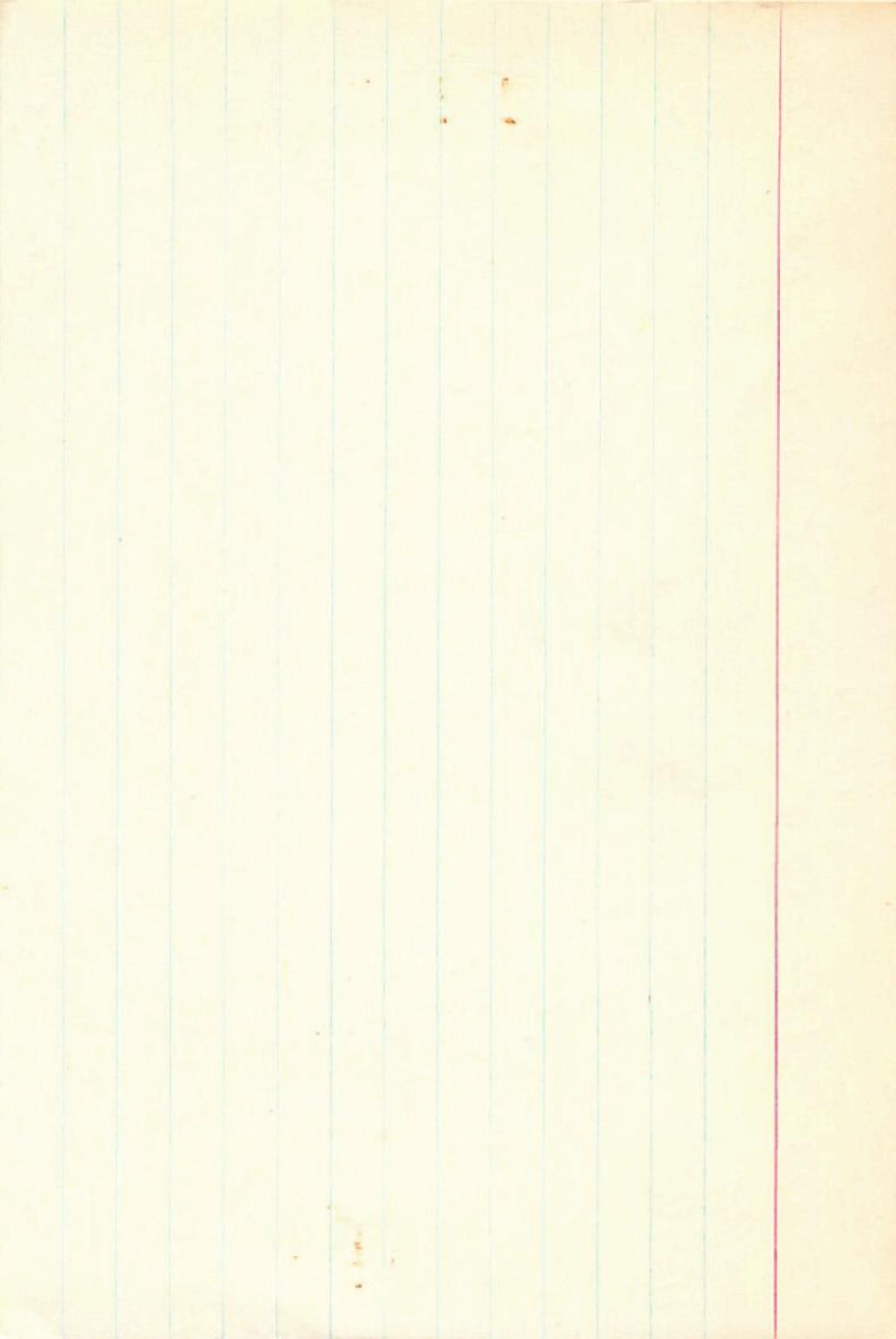
4152
41.55

54.241
247
245

21.29 1945.97
30

245
+089

20.99
21.27 = 54



ADG 1846₁₂ 2.1

-0068 ± 2.7 -122 ± 2.5
-0067 -122

175924 18 53.5 45 45 5.9 1F4 -11.08

25980

11383 27.878 1894.1 748 47 46.19 18909

$\frac{380}{28.258}$

$\frac{7.21}{53.40}$

A(14)

17 ± 8

48.35
39.710
28.060

33.7

53.9 1925.6

54.45

$\frac{48.35}{48.70}$

$\frac{556}{27.5}$

88.9

$\frac{664}{299A}$

$\frac{8044}{214}$

49.05

1734

$\frac{48.67}{4.73}$

49.05

$\frac{4904}{4904}$

4.73

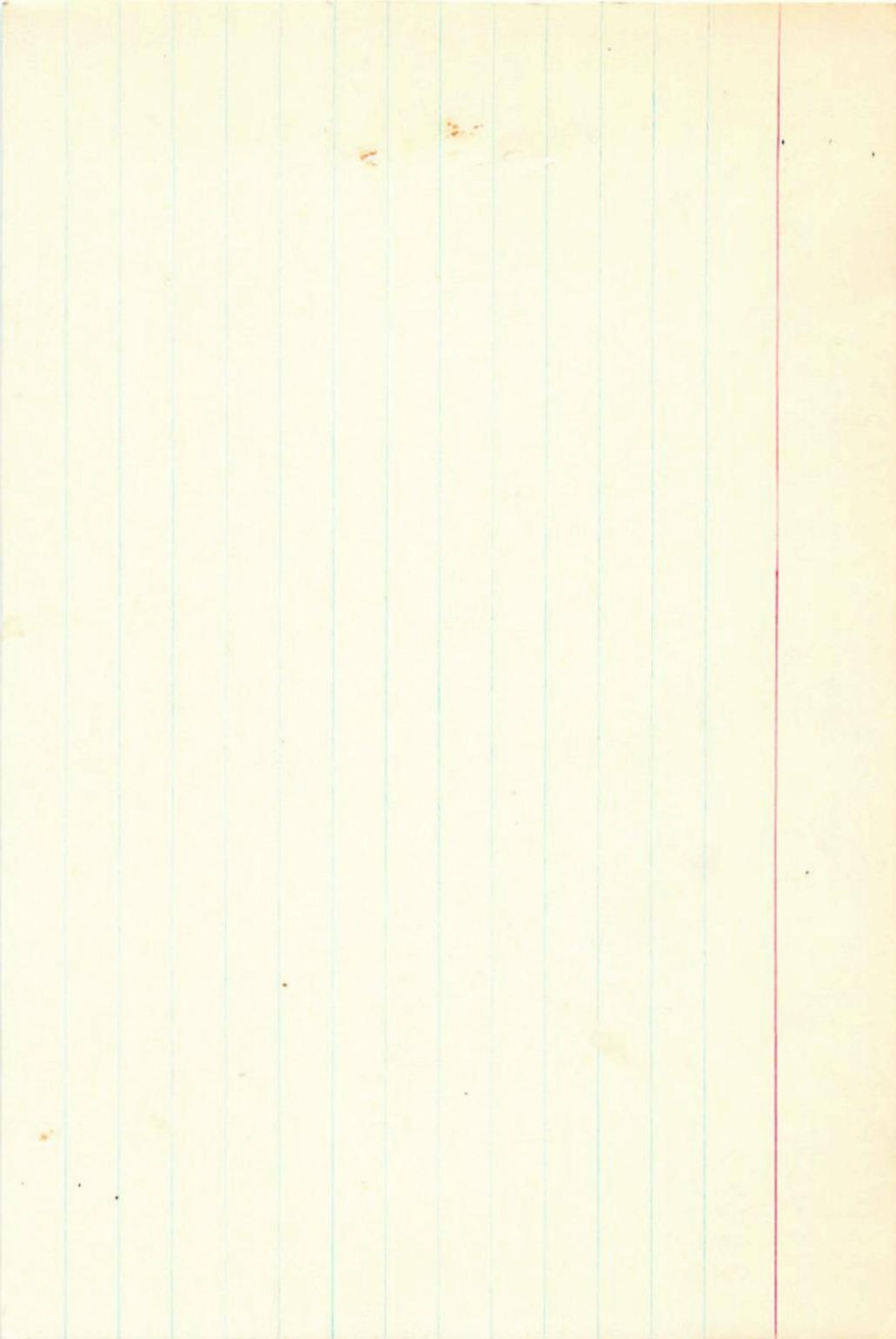
28.013
 $\frac{13}{023}$

$\frac{4936}{4936}$

1530.0

48.64

$\frac{48.30}{48.30}$



K₁ II +1.1

175743

18 53.9 ±15 02

g r 2 2440 0(5)
2p 8 (24)

6025999

5.7 ±1.0:

w(±0.7)

5.45 ±1.1 2.17

W11389

4.68 (4)

74340

±1703779

77146

^{±4} -047 ^{±3} -166 GC
-048 ±5 -168 ±6 Y

-71 0 -7 .015

-73 -2 -8 .014

-75 -4 -9 .013

3 ±5 A (4)

-0033 ± 3.6 -166 ± 3.2
-0031 -165

-972 233 309 951 -047 -166 +11.0 -051 +14 -749

-046 -050 -011 -012 -161 -259 +11.8 +10 -41

53.705 - 1403.1 +18 2 28.73 ^{1405.6} -2 -63 -44 013
155
800

-76 -6 -9

53.773 - 752 31.4 36.10 7505
770

53.735 - 108 31.25 1924.4 37.5
770

30.41 1920.65 31.9
9

50.32
166

30.83
5.27

+1000 2 ± 3.5 -0.13 ± 3.2 -1.000
+1000 2
-004

-15.48

+16008

175674 18 53.9 +02 24 6.3 68 III

26000

11391 54.532 1886.3 +2 24 16.89 1882.5

-0.13
1579

+75
17.64

54514
523

17.53
15

1433.9

489

54522
+120
534

17.58

17.32 193647

525
525
+009

0
17.40
-19

037

35.2

587

R. Lynn
P5865

1

365gn
175687

-0002 + 2.0
0000 -013
15 54.4 -20 43 S.1 A0 +1.9

26012

0000 -010

11394

22.195 1899.4 -20

43 24.67 1896.2

7145

$\frac{010}{208}$

0000 -014

53.082
29 145
22.225
 $\frac{210}{202}$

+6009 -012

21.04 1928.81

+0013

+001.5 -013

54.60
2644

202

22.210

25.14

49.71
34.9

22.230

203

25.51

$\frac{15}{215}$
208

203

25.51

24.84 1940.90

$\frac{208}{215}$
000

203

25.51

24.84 1940.90

$\frac{24.70}{24.70}$
15

24.84 2

24.84 1940.90

34.9
38.7

SL- 29/1

LA- 29/1

v dia

176524

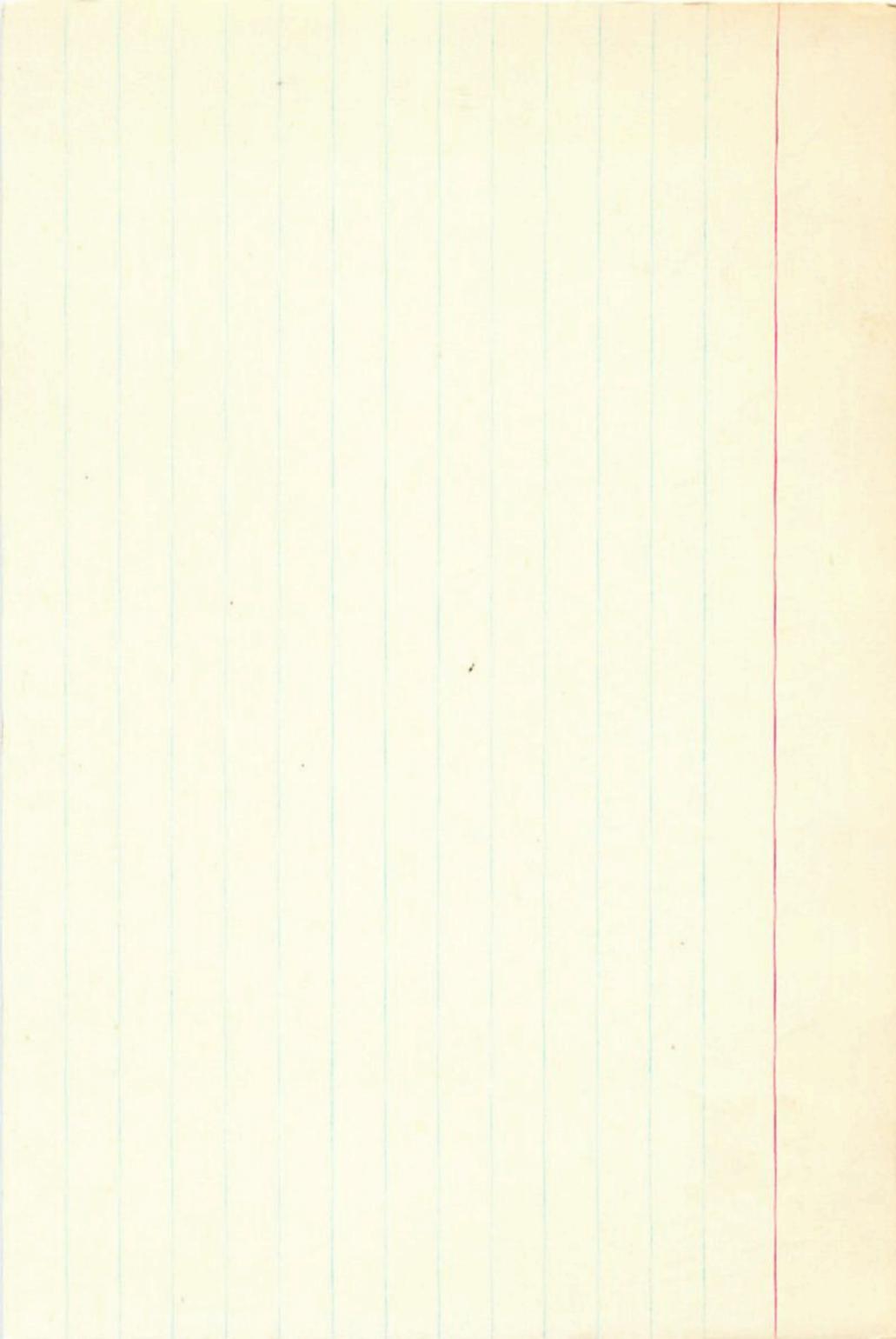
26024

11402

18 55.0 +71 14 4.9 910 -2.18

+009682 +04574N30

+0092±1.1 +045±1.2 66 7430



176051

18 55.2 +32 50

dl60 -472a

G-26030

5.21 +0.59 - 60

-47.8 L(3)
=48.7 V(4)

0011406

47.9 (22)

-43.3 W(3)
-46.7 S(2)

48388

+3203267

+175 ±2 -140 ±3 ✓

AD51187 | 2.56

6248
DM=2.04

+165 -161 G-C

+187162

+16 -40 -26 068
+13 -40 -29 .052

35 ±4V
54M(20)
U3M(T)
5(5116)
56.25

AD511871

18

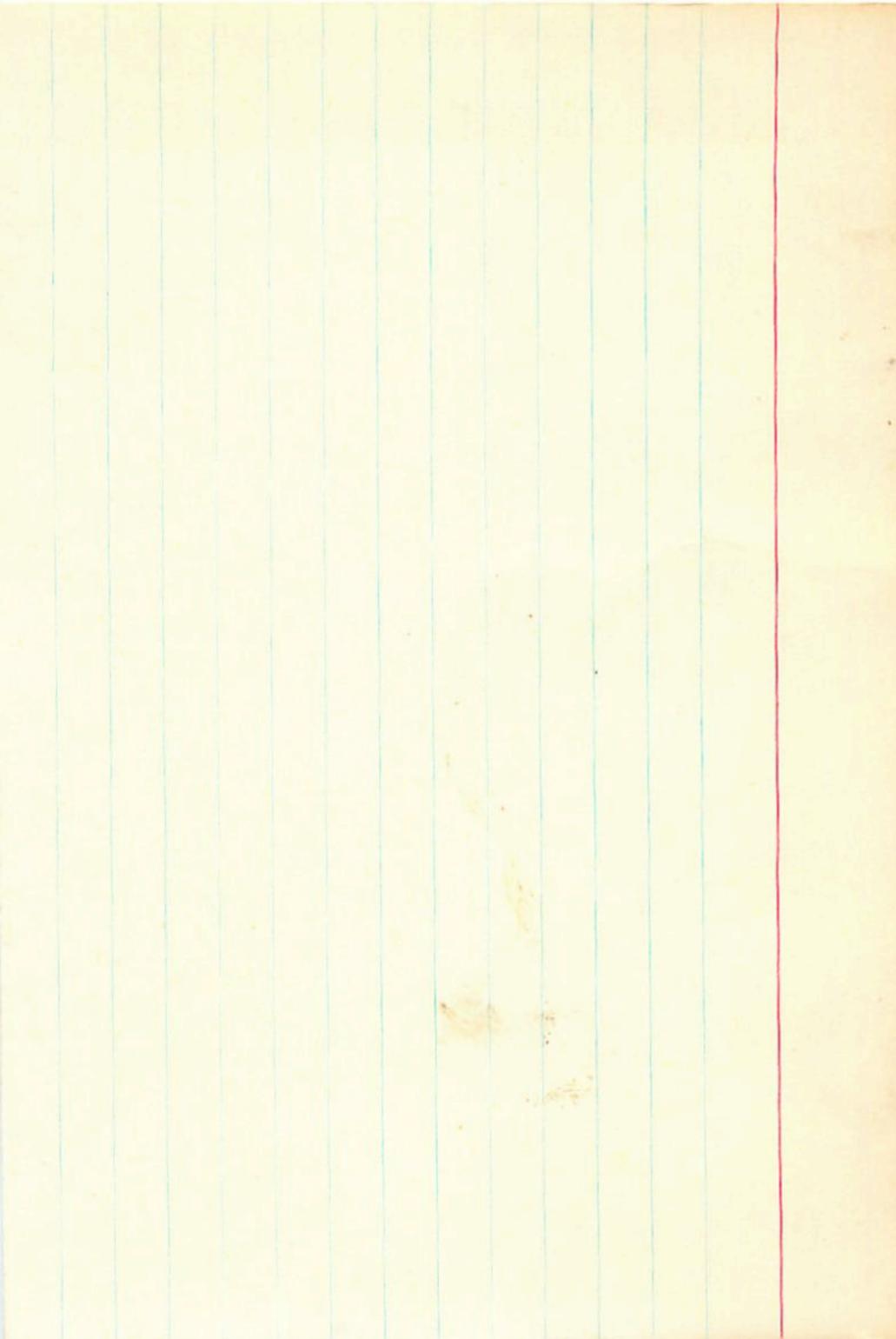
55.1 +32 50

-47.2a

-47.7 (D)

0.0691

+165 -161 6c



-48012816

513

38 X

175674

18 55.2

-48 35

6.5 +9.4

βc 26026

5.722 1901.5

-003 ± 11.3 -002 ± 7.5

28.01 1845.8

10.5 3''

+008 -008 CP

$$\begin{array}{r}
 12.269 \\
 53.708 \\
 \hline
 5.972 \\
 975 \\
 \hline
 024 \\
 \hline
 95
 \end{array}$$

$$\begin{array}{r}
 8 \\
 25.52 \\
 + 55.30 \\
 \hline
 30.28 \\
 \hline
 30.36 \\
 + 0 \\
 \hline
 30.24
 \end{array}$$

1930.23

