

173667

$\frac{415}{1527}$ 419 242 823 -481 +17 (360)
+15

2. 18 43.5 +20 30 FLU

HR2061

GC28698

110 iter

-00078 -3340 FK4
+177
-0109 -008 -335

4.19 + 46 + 2 J + 232 (18)

1.58
416
2.58

+23.7a

10⁸

[M] 206 +27
72

.314 .150 484 (5) 5PL 2.648 (5)
325

[L] 421 +91 (1.60)
118

1.50 -38.5 +1.6 -8.2

+26
-1195 -826 -627

173649
1995057

7061.000*

13.000*

43.500*

23.000*

33.000*

-9.000*

-9.335*

1.600*

20.893

23.700

-1.198

-9.622

-39.752

-9.825

3.762

3.826

-0.639

9.181

-9.057

21

21

A0511661

-0010 ± 2.4
+016 ± 2.2
-0012
+023

173949 18 43.7 +61 00 6.2 0967 -24.7
25705 -25.3②

11214 42.871 1900.2 +60 59 40.80 1893.1

$\frac{050}{92.1}$

- .91
 $\frac{39.8}{9}$

from 1.5 cm

25.15
17705
955
42. -13
949

6.05 1927.75
34.38

$\frac{40.31}{9}$
40.62
7334
36.7
36.5

42.984
 $\frac{15}{902}$
8.74 - 045

40.71 1948.89
41.25
-14
41.09
 $\frac{40.50}{+1.01}$
43.6

3
9
4
5
2
1
9
7
2
1
3

173780 18 44.1 +26 36 4.9 gR1-16.7e

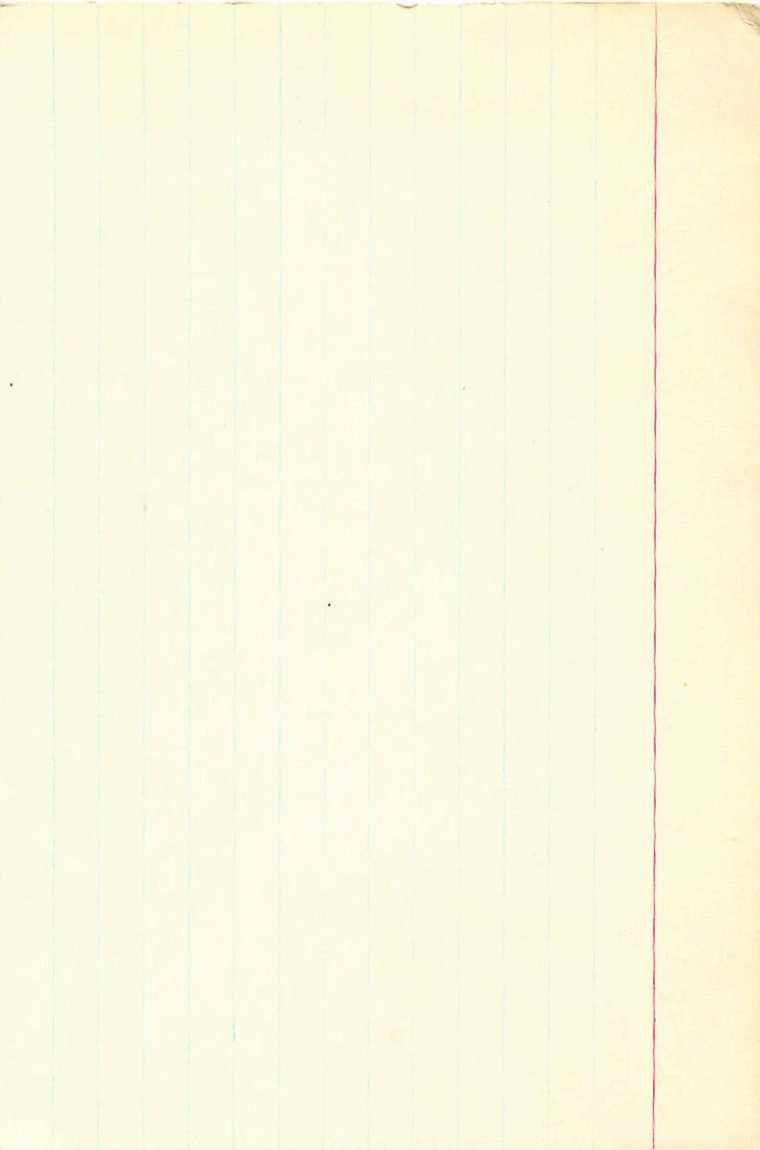
25721

+6013³⁹ +024³⁴ N30

11222

+6011^{33.2} +022^{±3.0} GL → N30

-160



UGA
173540

18

44.2

-40

28

5.362-18.2a

+0005±48

+00074

-016

±44.4

-020

25722

11223

14.842

1906.5

-40

27

41.08

19042

-022

820

+73

40.35

14.909

-027

808

41.41

1941.34

0

14475

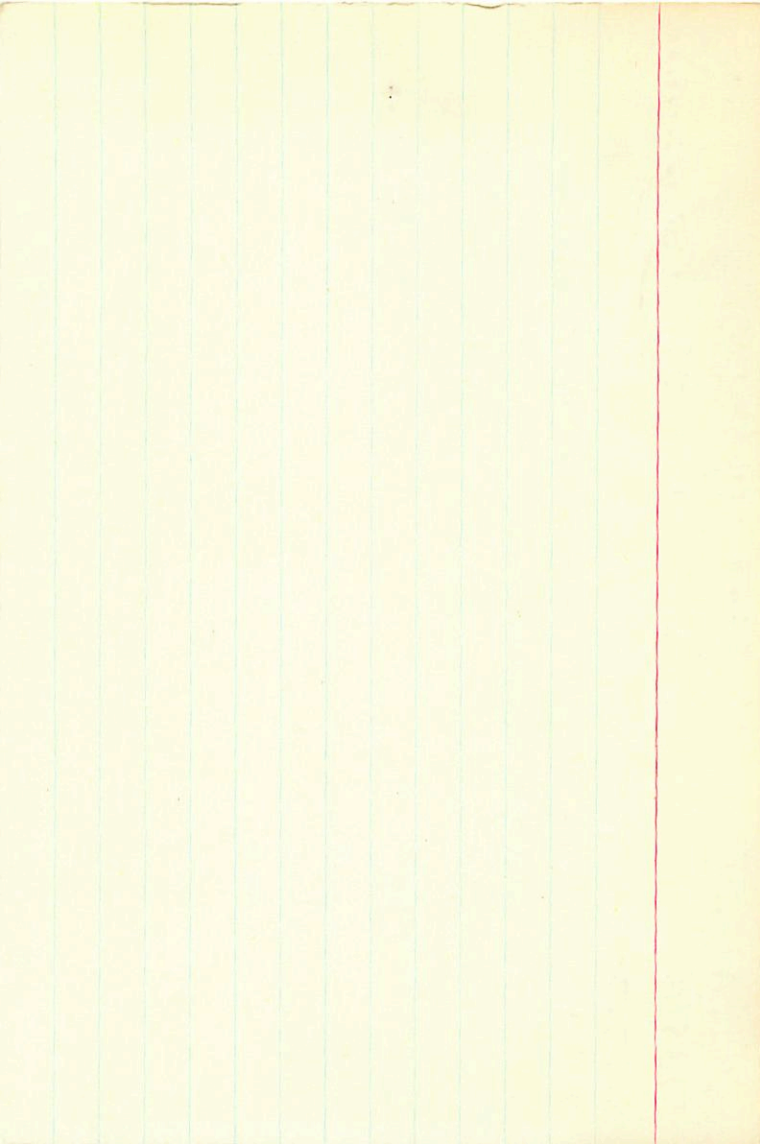
14471

70.64

4160

11

4171



+6401289

-0003 ± 15.0

+105 ± 13.0

+0058

+085

+0083

+066

174156

18

44.3

764

45

7.3

9100

+46.16

25725

11224

20.240

1909.7

764

45

20.10

19084

012
252

20.426

15
444

~~192~~

20.35

35
348

832
416
764

28.5

6^m (m-m)

+64 +46 -3

-4.40

15.70

18.94 1946.13

16
18.83

~~3.13~~

17.9 1930.2

122

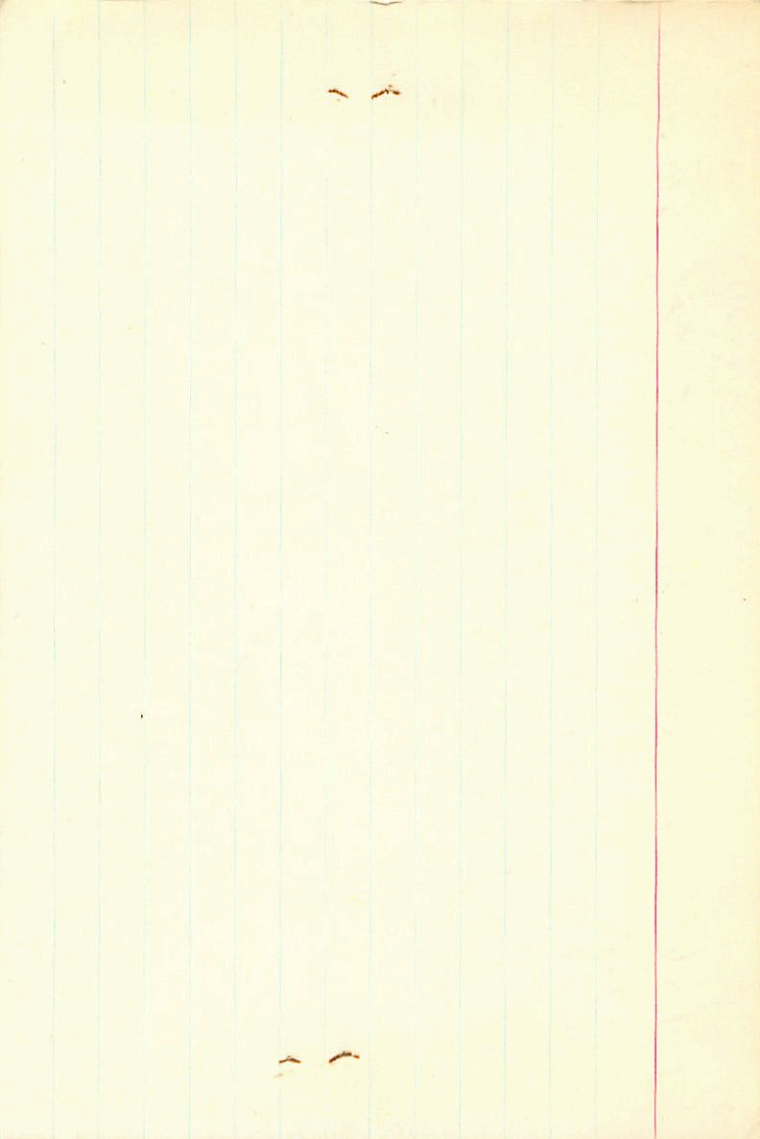
17.08

1651
18.20

~~256~~

7633
38.2

30.1



-12.56

7067 18 445

+18

39 6.12 105

7990-2204
0
44

-224

↑ ;

↑ ;

22



7067.000*

18.000*

44.500*

18.000*

39.000*

0.023*

-0.026*

6.500*

199.526

-12.900

-0.064

-0.645

-4.491

-0.023

0.747

22

-14.134

-0.150

0.164

-32.005

R.D 173787

18 44.9

-0003 -008
-2
-004

+7.0

G-L 25739

+0005 ± 3.3 -005 ± 3.4 354

5

54.347
- 0.005
322

+0001

49.51 1896.9
+ 27
49.24 415

25.342
2844

-0005 -004
+0005 -005
+0001 -013
+0001 -007
+ 3 + 2

86.00 1935.16
34.35

54.330
327
+ 336

+0004 -005

57.62
16.2
50.42
44.84

-5
-12
-11

54.325
8
317

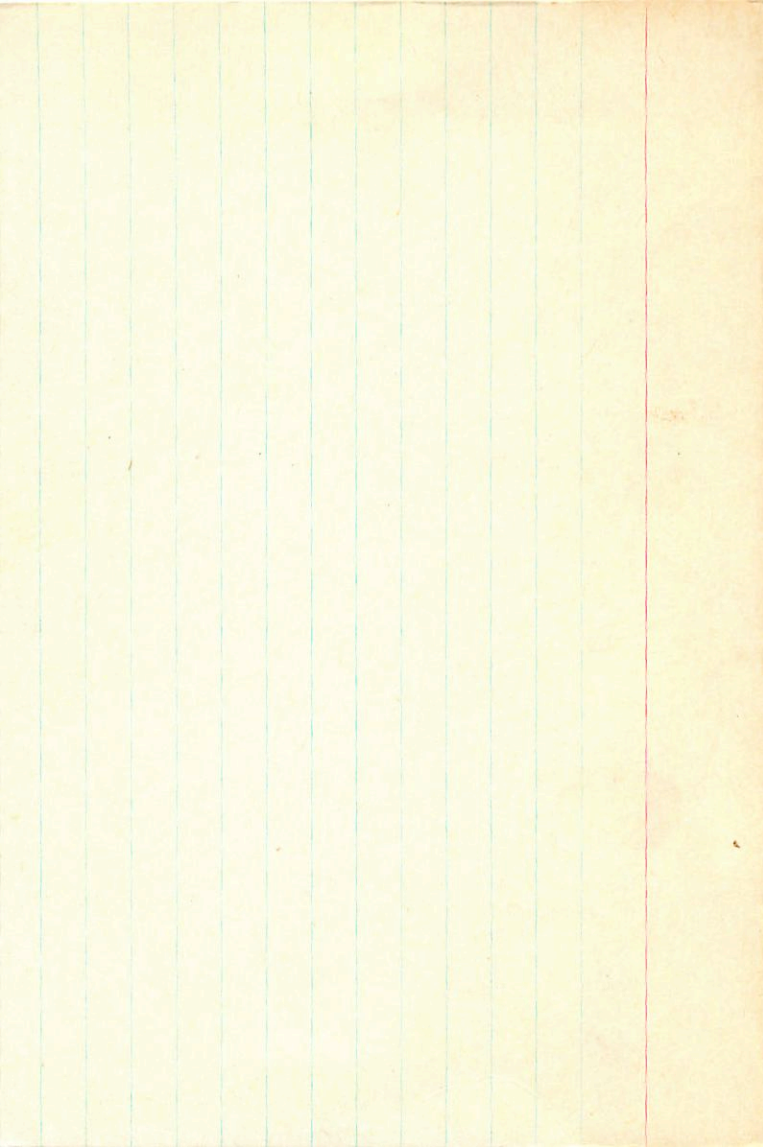
49.75 1941.65
+ 0.2
49.93

11

236 166 -958
395 884 251
-888 438 -143

+0062 +0039 +0023
326 +0103 -0210 -0313
+004 -0232 +0104 -0128

49.80 +1.7 -6.7
-56 -13.5 +1.8
-9.6 -1.0



173697

18

45.2 - 45

19

040

-28.3 ± 0.5 (15)

+0021 ± 10.0 -053 ± 8.7

+0027

25747

7.26 + 0.99 65111-15

+044 -056

10.251 1501.9 -45

19

7.59

1598.4

$\frac{101}{150}$

20.274

50.030

$\frac{101.337}{1.2}$

84.4

$\frac{1.3}{1.2}$

47.4

42.01

3420

$\frac{530}{265}$

$\frac{265}{115}$

$\frac{115}{5.83}$

42.01 1932.04

3420

$\frac{137}{64.6}$

$\frac{64.6}{1.82}$

88.51

44.3

215.9

10.307

$-\frac{1}{2.97}$

7.48 1956.17

7.53

-552

~~244~~ 195 = 207 207 1044-056 -28.3 040 +20 -190

044 040 009008 171 232 20 4 +20 01

+13 443 +1

173715

18 45.2 -43 44

A2 dm

-2.8 ± 1.7

56

FD1247

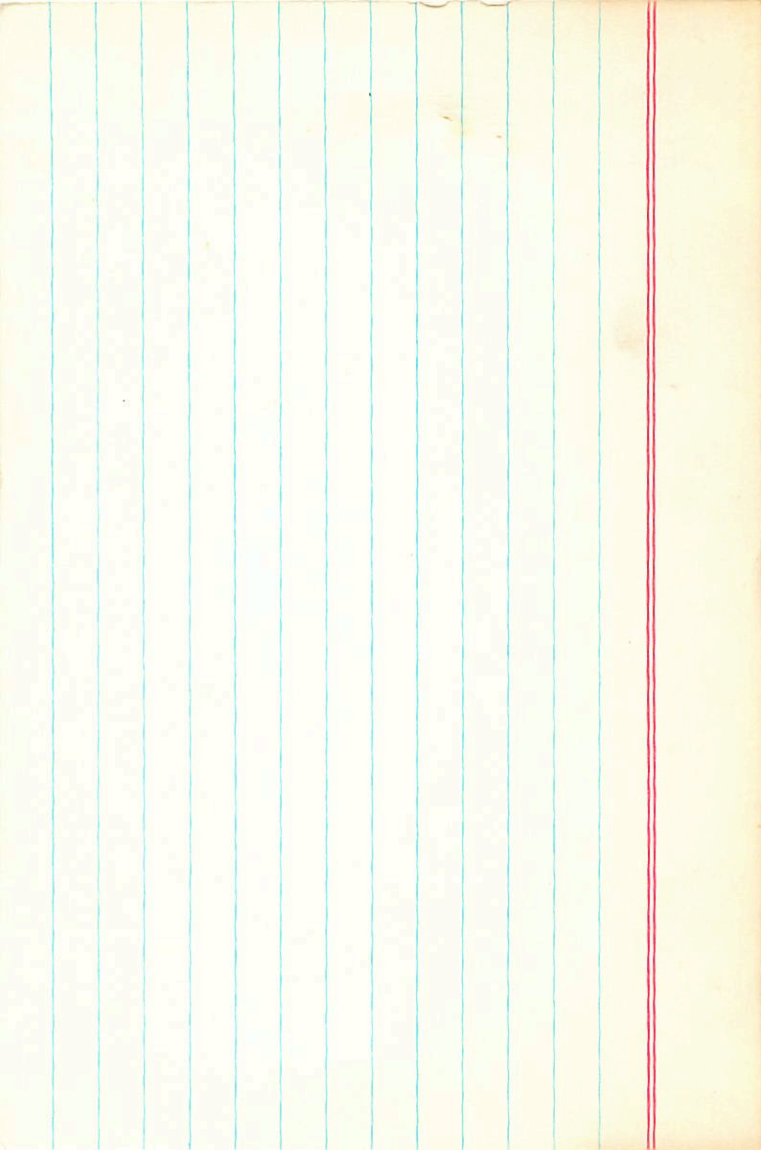
5.48 +0.13 1.56

-6.23
-4.4

+0026 -018 N30

+0029 -009 GV →

+0027 -013



-1905166

25779 02 18 45.3 -19 15 709145 +72

140 17385 41

6.85 +168+149 (1)

594 +0.70 (2)

5.23 45

5.23
485

4.13
1.15

+ 000 710.0 - 043 510.0
 + 000 3 - 013

16.806 1500.9
 01.76 1500.9

$\frac{039}{972}$
 + 2.11
 19.75

18.245
 48.470
 16.960
 16.806
 1634.97

16.806 776
 - 22
 19.99
 20.11
 20.21
 846

10005 - 030
 10006 - 028 Fee
 10008
 10009 - 027
 10009
 19.33.59
 3423

Etc

1787
 17.81
 1009
 18.97
 - 2
 19.99
 20.10
 - 45

23

173854.000*

18.000*

45.300*

-19.000*

-15.000*

0.009*

-0.027*

5.650*

134.896

7.000

-0.013

-0.955

-8.405

-0.096

0.263

23

-11.089

-0.094

-0.138

-13.658

HR7065

173791 18 45.8 - 45 52 HR.7 ± 0.4 C₂(5)

25758 5.90 + 0.89 6612

HR7065

$$\begin{array}{r}
 +071 + 045 \text{ CP} \\
 + 6627 + 0605 \text{ C-C} \\
 \hline
 +066 \quad +053
 \end{array}$$

-718 696
+0059±8.7 1060±7.8
+0069 1049

45.775 1899.2 -45 52 56.4 18963

$$\begin{array}{r} -300 \\ \hline 475 \end{array}$$

$$\begin{array}{r} -3.22 \\ \hline 8.86 \end{array}$$

$$\begin{array}{r} 55.126 \\ 50.658 \\ \hline 45.778 \end{array}$$

48.7

$$\begin{array}{r} 44.40 \\ 35.45 \\ \hline 89.85 \end{array}$$

$$\begin{array}{r} 1529.12 \\ 85.82 \\ \hline 47.9 \end{array}$$

$$\begin{array}{r} 45.778 \\ -3 \\ \hline 45.1 \\ \hline 1907 \end{array}$$

$$\begin{array}{r} 14.21 \\ 8.10 \\ \hline 23.35 \end{array}$$

$$\begin{array}{r} 89.85 \\ 6.97 \\ \hline 8.98 \end{array}$$

$$\begin{array}{r} 1268 \\ 637 \\ \hline 2552 \end{array}$$

51.6

$$\begin{array}{r} 45.924 \\ -10 \\ \hline 914 \end{array}$$

$$\begin{array}{r} 5.48 \\ -3 \\ \hline 1956.70 \end{array}$$

$$\begin{array}{r} 914 \end{array}$$

$$\begin{array}{r} 5.73 \end{array}$$

11244

18

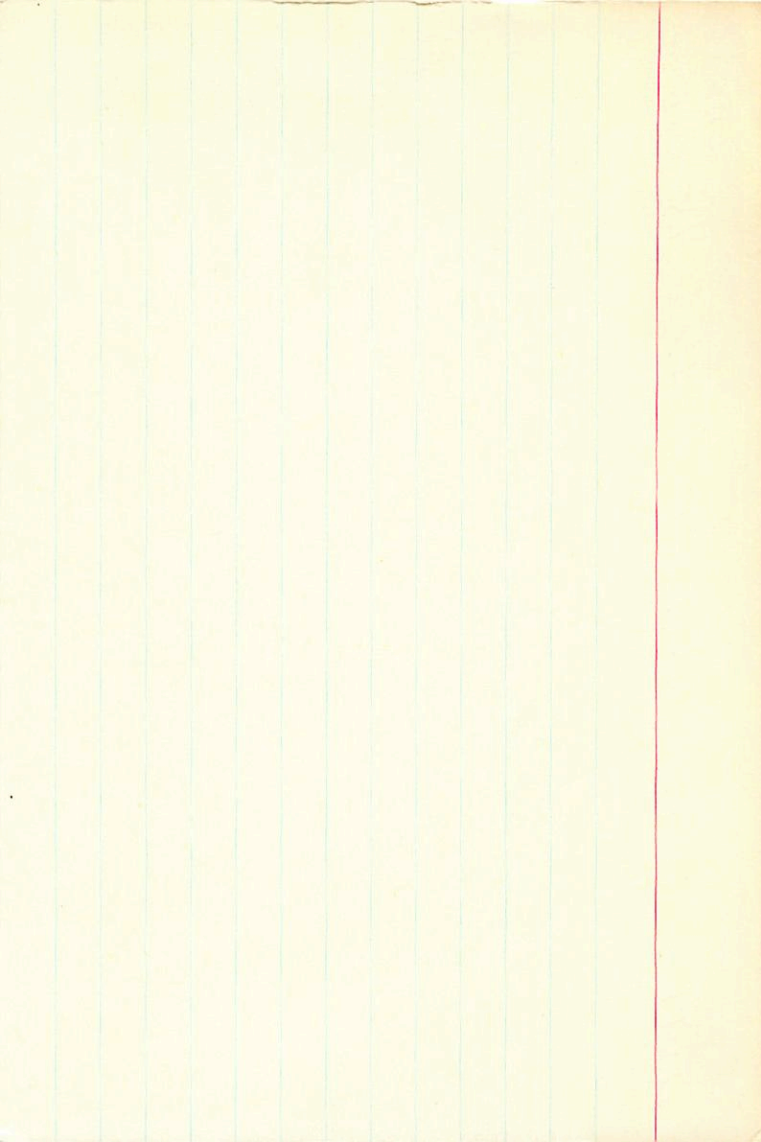
45.9

+35

56

11.5

-129.30
no exp. dno 300



17405
2.4413

18

46.8

-6 03

6.174415

-26.7 (B)

-27.1 (C)

11244 18 46.1 +00 28 dG7 +34.78

+0°40'23

8.55 +1.12 +1.03 3 20"

+015 -037 Y

0 -2

+015 -039

+1 +4

+016 -035 →

2959
174116

25785

11261

4051173

(15000)

+0002 ± 1.6 + 034 ± 2.0
-0006 + 039

18 46.7 -20 23

5.4

914

-18.32

-17.1

P=258d

-17.708

42.082 1902.3 -20 23 0.03 19036

$\frac{-010}{.072}$

$\frac{-1.58}{1.61}$

13.057
29.010

40.70 1927.50

$\frac{42.067}{.055}$
-10
045

38.22

$\frac{2.48}{1.60}$

(31.0)

$\frac{054}{-018}$

$\frac{0.24}{.44}$

$\frac{0.44}{1.17}$

6665

33.3

42.077
 $\frac{-15}{.062}$

0.29 1939.15

(29.7)

+6
0.23

W11268

18

47.0

274.02

968

+2.5a

W11268

47.0

595

399.2

399.2

+3

← 29000 + 108000 →

W11268

399.2

+3

952

93

14
out

28
out

2848

245 540 233

350 510 865

955 124 444

0 +3560 +286

0 -1150 -95

0 +0.00 +38

out +0.7

+2.5

+13

3856

832

2.05.0
047

(1.5.4)

0
1.3.47

+3403326

174433

C2404

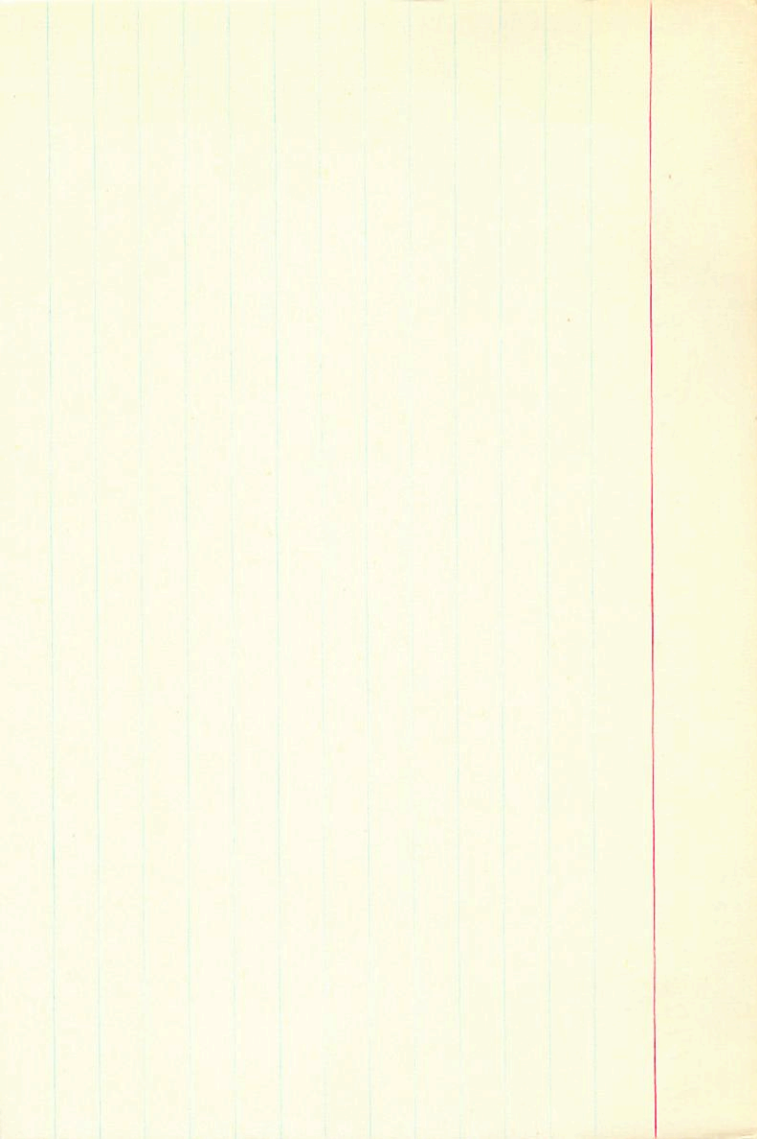
11272

0 A

18 47.2 +34 28 8.4 d/f 6 -12.5

+06 +21

3W



-4108786
174152

.67

18 42.5 -41 07

+006

+0005 -002

-26

+0025 +008

+028

5

85/10 III

-0018 ± 10.0 -111 ± 8.3
-0017 -103

9, (4)
462.4 ± 0.9

174153 18 47.7

25824

7.54 ± 5.2

468.8 156

41.827 1901.2

-44 32

3.17 1897.4

$\frac{85}{915}$

$\frac{584}{5733}$

52.854

57.3

1931.87

49.062

42.35

39.65

41.9379

2.70

2.72

$\frac{83}{845}$

1.76

4.35

41.950

0.74

4.85

-1.0

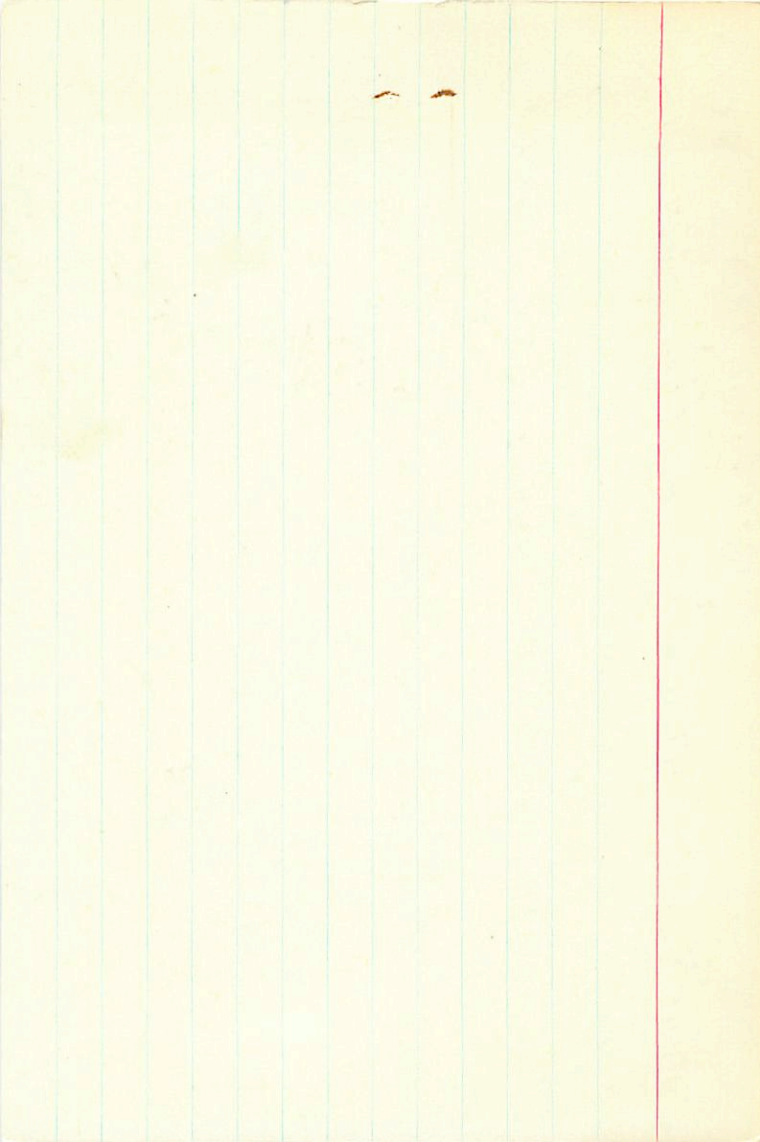
3.56

1956.98

43.2

43.2

88.85
44.4
47.0



6705

18 98 - 6 20

+0013 -0014
+ 74 + 20.0

~~+00~~

+003 -003
+003 +003

11.2

122

24

6703.000*

13.000*

43.000*

-6.000*

-20.000*

5.000*

-9.002*

11.200*

1737.801

22.000

-0.000

-0.000

-19.823

-0.002

9.457

6.483

-0.017

-0.047

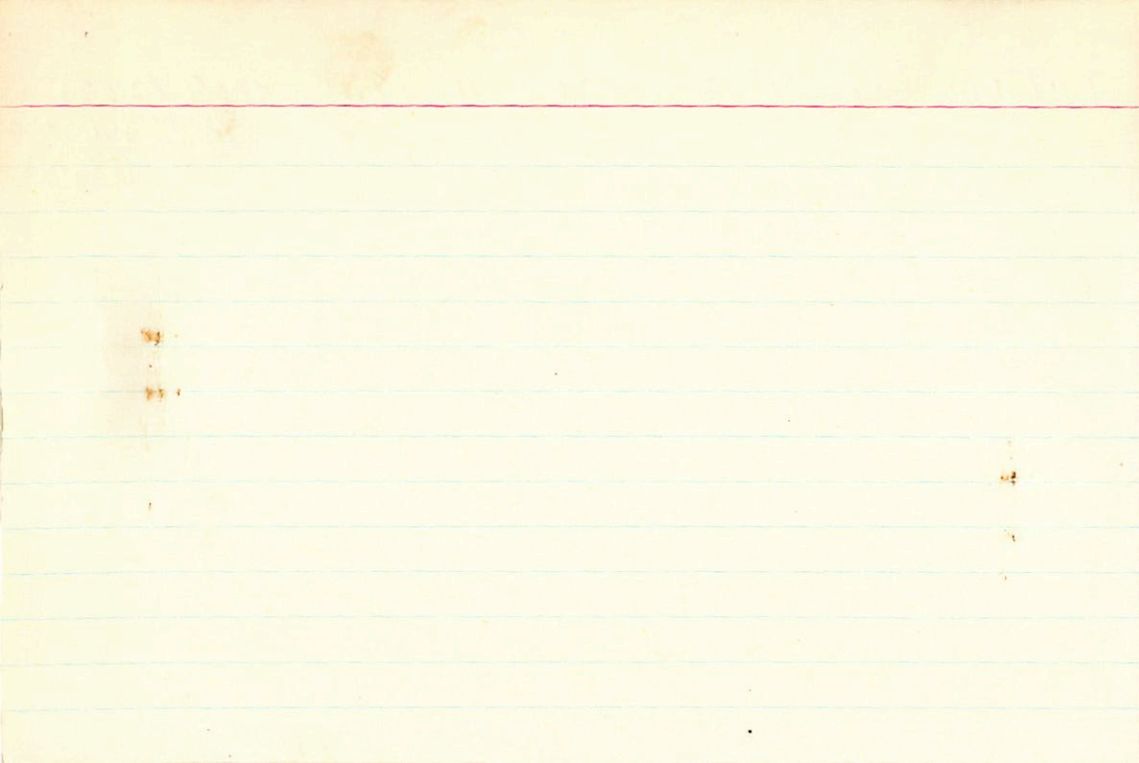
-30.513

24

174360 18 48.2 -30 11 8.10 +109 (2.09)

140 III +46.250.9
Σ(14)

+0015 -001 CP



7099

18 48.4 +10

55

6.15 10512

-23.76

27.50
27.90

+0.18 +00766
0 +4
+0.11

...

...

25



7099.000*

18.000*

48.400*

10.000*

55.000*

0.010*

0.011*

7.000*

251.189

-23.700

0.054

-0.733

30.987

0.066

0.675

0.537

-0.052

0.009

-15.234

25

174553

1000
1000

B1

48.6

-06

25

4074553

✓36.95at

-60452

-1223②
+10.5③

+017 -024 x

-9 +4

+018 -020 8104

183 422

+017 -0155 →

318 / 53842 2725

[510 - 3104
+015 - 015]

F=100

26

18.000
-6.400
18.000
-19.000
7.6 8.500
331.13 501.15
0.000

0.247
0.387
-0.888
-4.6 -13.905
-6.959

0.388
0.800
0.457
-13 -29.164
-19.629

+0017±13.0

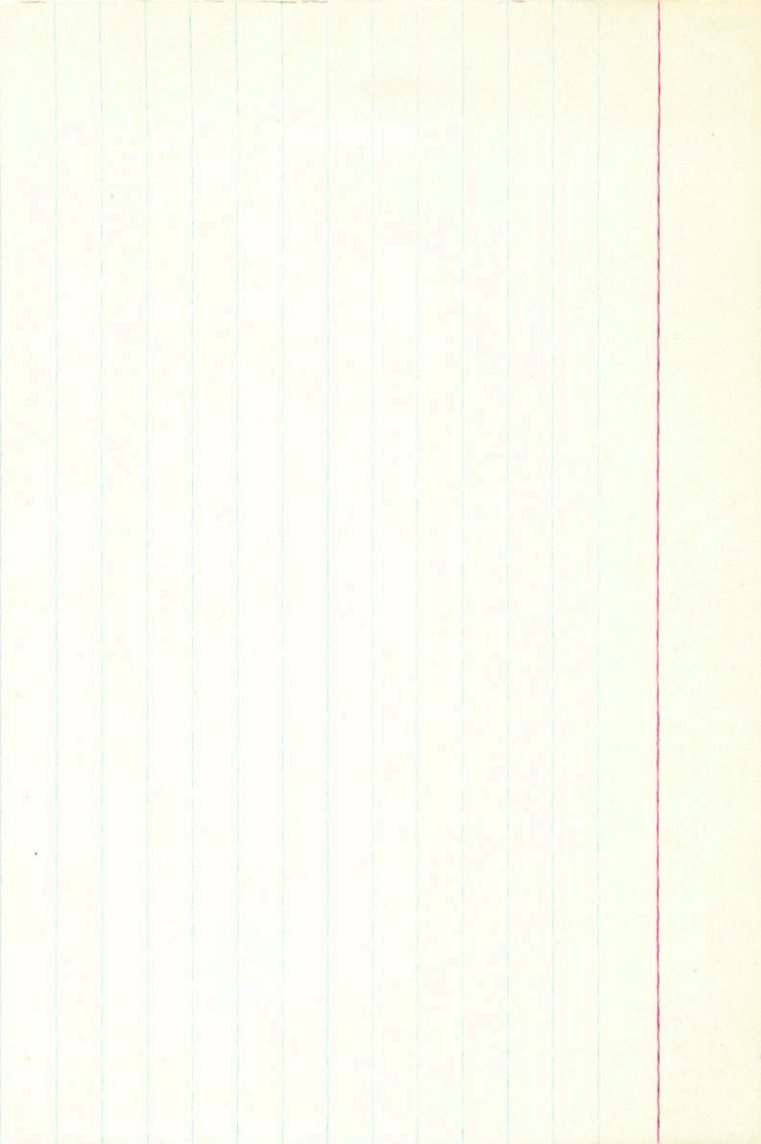
194386 18 48.7 -44 24 F2D

8.17+40

25860

43.099 1402.9 -44 23 48.28

C₂/4
→2.1±1.6



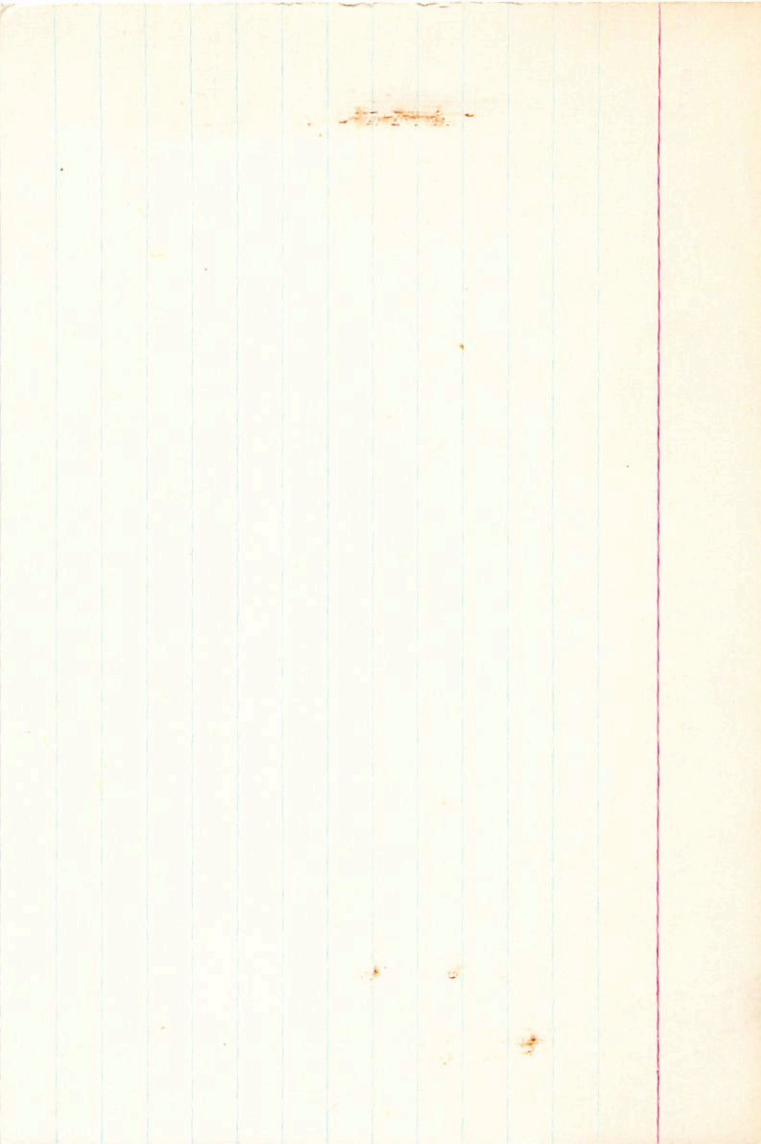
XTM
174295
25859

18 48.7 -52 10 5.3965-44.3a

11312

+0057¹⁰ -097¹⁰ N30

+0049±5.4 -100±4.0 Gc → N30



AS Her 18 48.8 +24 40

-16.06

+2403552

~~-075 -019 1/4
 -11 -14

 -026 +4

 -026 -029~~

No. 0 Output

+0.002 -0.012 -Part
 0 +4
 0 +3

25-4	792	-555
384	444	810
-888	414	191

+002 -005

