

172462 18 38.9 44 17 +41.5 ± 1.4 5(5)

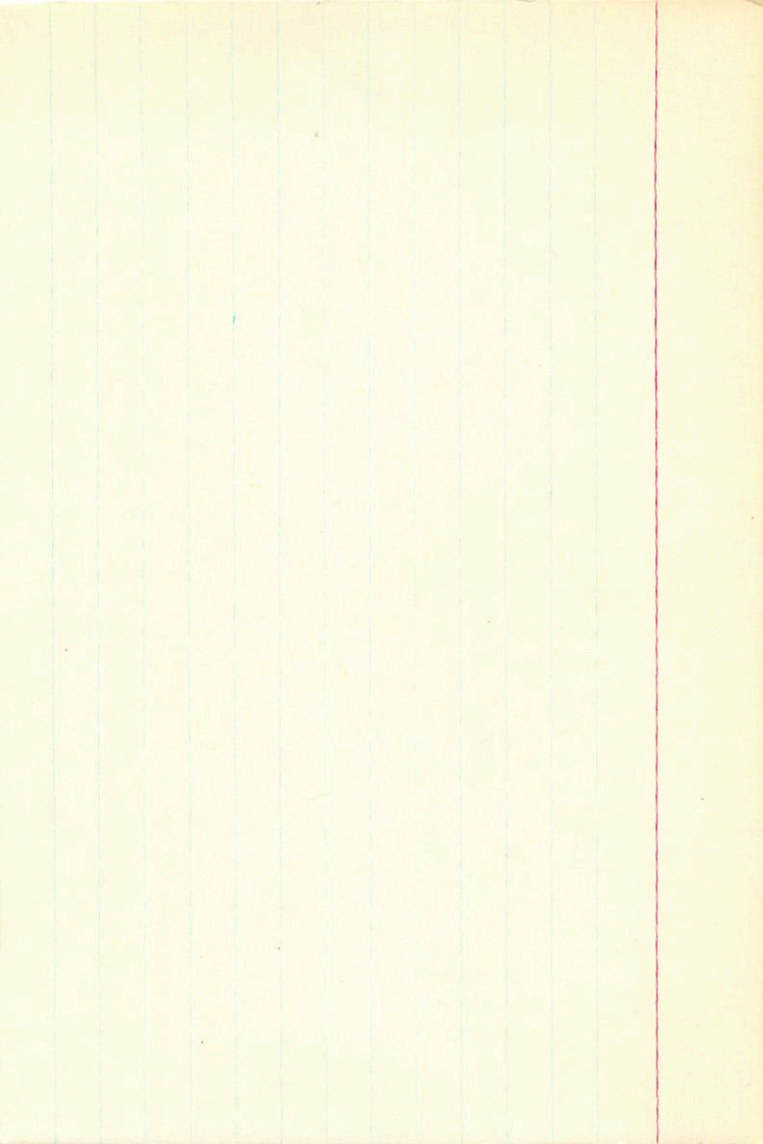
25565 8.75 734 FSIR

52.297 1903.7 -44 17 26.60 1904.2

$\frac{0.51}{1.348}$

$\frac{1.01}{25.59}$

$\frac{-0011 \pm 13.0}{-002} -0.22 \pm 15.0$
 -0.20



706-35

+3103330

18 35.0 +31 30 +33C W(2)

day

Y4314

8.50 70.84 +0.65 R3UR

W11135

S=0.05?

A0511576 $\Delta m = 2.6$

11.7409"

6061

+100 - MCR

+085 AR

57

W(+6.3)

+05 -02 in

+076 -292 R

-99 -6 -36 .039

+072 -840 Ring

8.54 533 461 279 (4)

3/A(12)

3/M(17)

no

31±7

-586165 522 853 +076-782 +33.0 -413 H7 -3203 ✓

075 -407 013 -070 687 -1567 +281 +5 -25

+24-78-71 0365

-100 -6 -41

+3103330

18 39.0 +31 80

103 V

AD811576

15m=2.69°

8.54 + 0.94 + 0.635 (2)

8.04 + 0.36 (2)

20.6

17.5

1.75

1.15

17.54 + 1.585 + 1.15 (4)

+072 -836 Recg → N30

+040 — 11(2)

10.34 + 0.89 (1)

10.01

1.16

8.97

20



2

31.333*

18.000*

39.000*

31.000*

30.000*

0.000*

-0.836*

1.750*

22.387

33.000

-3.310

-0.471

-89.649

-1.269

0.839

-0.730

-1.811

0.273

-31.519

20

woolly cotton
30 lb

ADS 11574 18 35.4 +30 15 +15.5

(3)

+3003271 +0019 -060

100^W

+218	+843	-492	+0258	-2397	-2139	-214	-6.6
+407	+350	+830	+0482	-1081	-0600	-60	+11.2
-887	+351	+260	-1051	-1084	-2135	-214	+3.5

-28
+5
-18

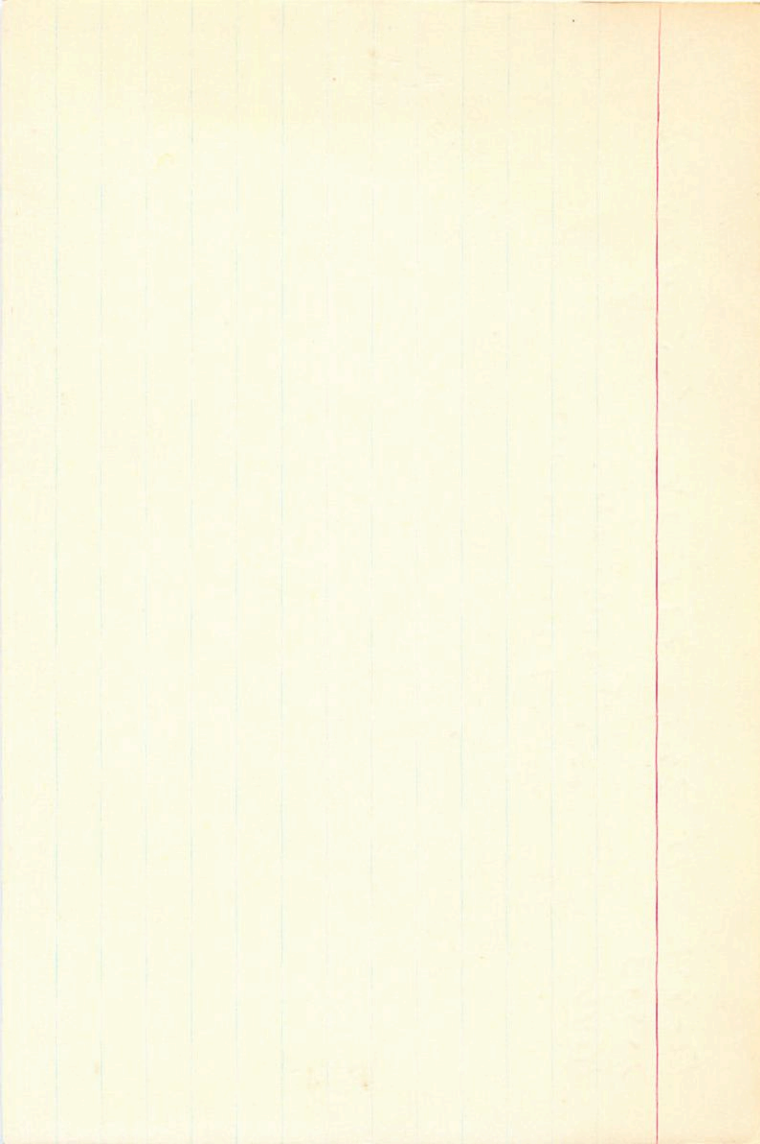
172958 18 39.8 +31 34 6.5 B9m -16.3d

25563

11146

-00018 +019²11130

00005.7 +008²5.366 → 1130



6964

18 40.1 -77 5-3

071950

373 189 392 2.612

640 377 176 406 ⊕

640 370 165 425

173358 18 40.5 42 6.0 +058 -0003±3.5 +060±3.2 -0.800
No III -26.08

25603

11154 30.071 1889.0 462 41 58.47 1885.4

$$\begin{array}{r} 018 \\ \hline 089 \\ -388 \\ \hline 54.59 \end{array}$$

$$\begin{array}{r} 16.98 \\ 13.160 \\ \hline 30.149 \\ \hline 120 \\ \hline 131 \end{array}$$

14253

$$\begin{array}{r} 29.2 \\ 27.62 \\ \hline 56.82 \\ \hline 57.43 \end{array}$$

24

$$\begin{array}{r} 7033 \\ \hline 38.2 \\ \hline 49.8 \end{array}$$

$$\begin{array}{r} 57.99 \\ -10 \\ \hline 57.83 \end{array}$$

$$\begin{array}{r} 57.83 \\ \hline 57.44 \\ +2.87 \end{array}$$

$$\begin{array}{r} 30.075 \\ +18 \\ \hline 1.093 \\ \hline 112 + 023 \end{array}$$

286

143

529

3192

589

196

173009 · 18 40.8 -08 20 5.1 965 -1060-

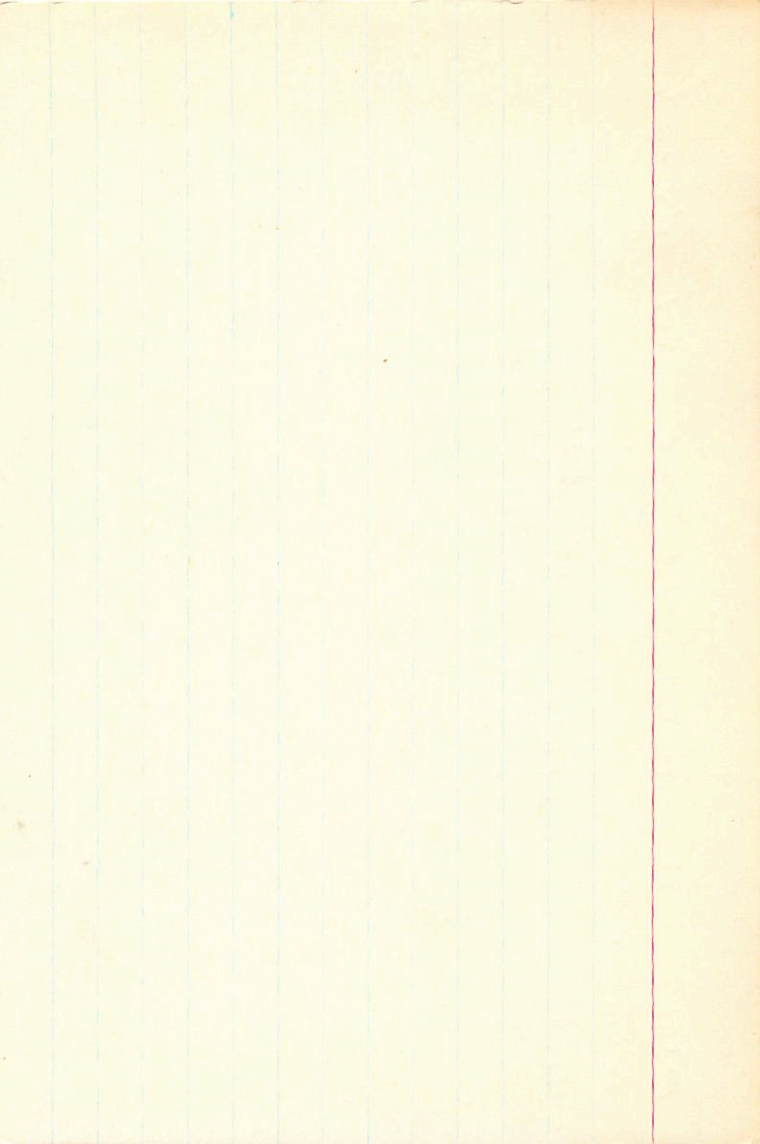
25610

11158

+0013 62 +008 60 N30

+0015 ± 1.4 +010 ± 1.4 CL → N30

-97 ③



110 F8 + A2

+0005 ± 5.2 -012 ± 4.1
+0002 -008

172991 18 41.5 -39 44 5.5 0.5 -17.40

25625

11171 28.805 19103 -39 44 18.34 1906.0

-020
785

+53
17,81

28.808
7
8.5 1586

17.91 1939.36
-2
17.93 027 9625

37.8

28.768
+3
~~771~~
793
+008

18.22 1956.89
-12
78.34
18.14
-33

48.1
41.5

2044

18 46.6

+39

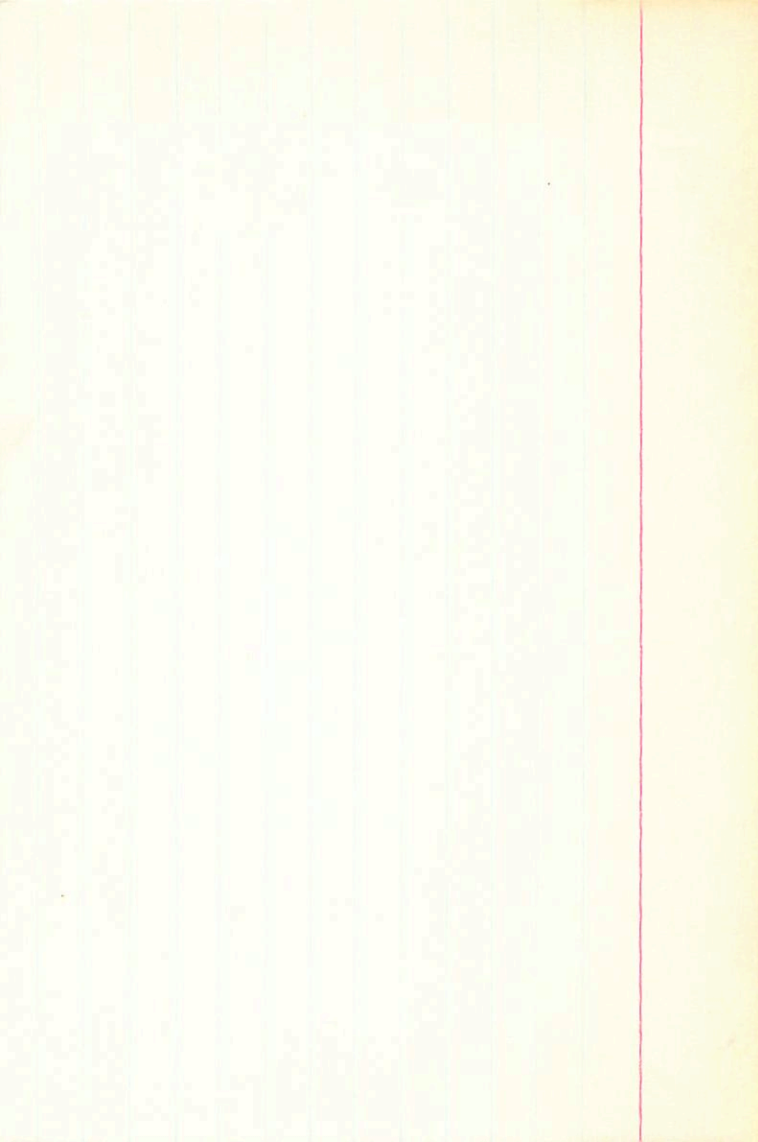
16

6.32 145

-342 5 B (20±)

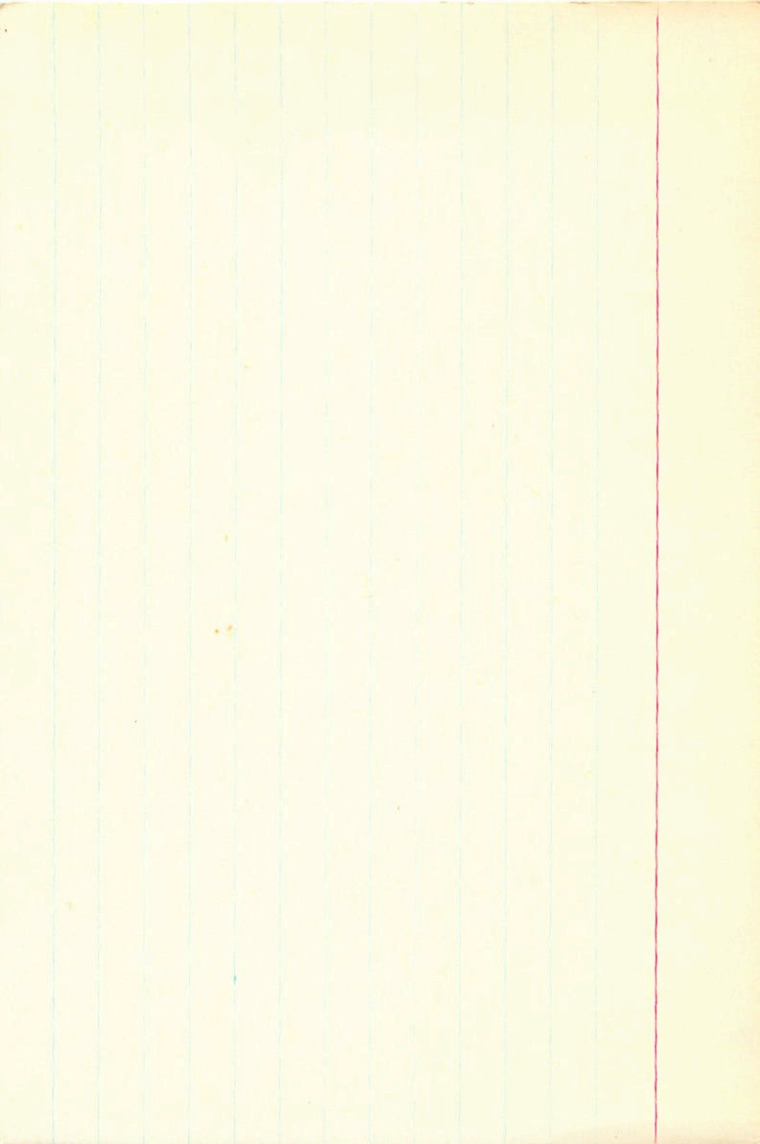
2711 debit

+0.10	-005
<u>-25</u>	+5
1008	00



RZLye 18 41.8 432 45 10.85 A2-240C

1176



173416 18 41.8 30 6.2 68 -60.98

25640

11177 50.836 1900.3 736 30 15.06 1893.5

+0016 ± 4.4
+0033
+36

40

-3.50
17.56

27.5

58.33
52.512
50.845

44.0 1425.5
29.10

55.5
27.8
34.3

846
+090

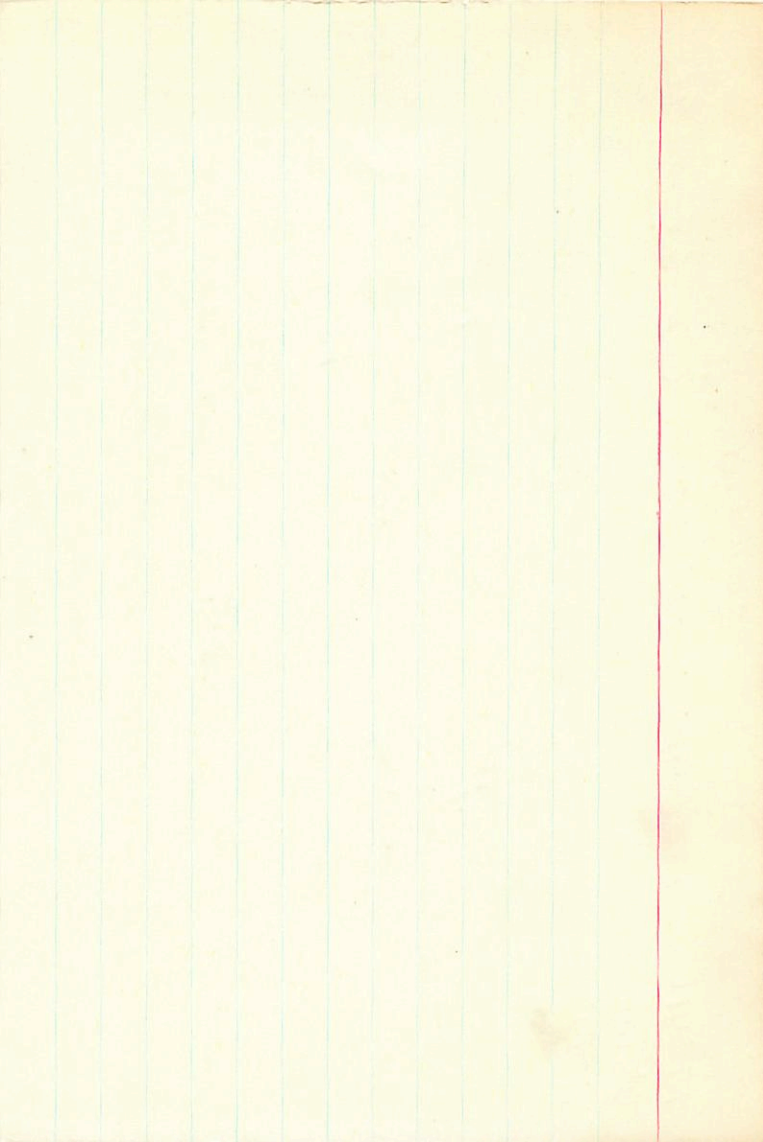
1380
+2.30

13.93
14.00
18.93

50.834
849

14.1 1930.0

-31
13.79



173182 18 42.4 -42 35 68TH -14.150.9 C₂(6)

7.50 +1.05

-8013 +004

-0004 ± 4.9
-0006
-012

173371 18 42.4 -00 26 6.8 BFM -18.28

25654

11187

21.654 1907.1 -0 25 33.39 1907.2

$$\begin{array}{r} 017 \\ \hline .673 \end{array}$$

4.607

17.078

21.682

683

276

656

21.651

43

654

$$\begin{array}{r} 56 \\ \hline 83 \end{array}$$

32

4.06

2935

477

3731

3143

33.717

33.

33.22

-2

33.20

33.18

3.35

1934.66

116

35.6

1936.5

28.4

33.18

3.35

$$\begin{array}{r} +000144.6 \\ +0004 \\ -0008 \\ \hline \end{array}$$

173664 18 42.4 +53 49 6.1 A2 0.06

25657

11188

$$\begin{array}{r} 25.024 \\ \hline 019 \\ \hline \end{array} \quad \begin{array}{r} 1901.2 \\ +53 \\ +49 \\ \hline \end{array} \quad \begin{array}{r} 12.00 \\ 12.00 \\ \hline \end{array} \quad \begin{array}{r} 1897.6 \end{array}$$

53.11

31.942

25.053

$$\begin{array}{r} 049 \\ \hline 053 \end{array}$$

103

$$\begin{array}{r} 25.006 \\ +5 \\ \hline 011 \end{array}$$

$$\begin{array}{r} 25.024 \\ +13 \\ \hline 039 \end{array}$$

38.3

$$\begin{array}{r} 63 \\ \hline 12.63 \end{array}$$

174 41.0 1926.2

$$\begin{array}{r} 36.08 \\ \hline 08 \end{array}$$

$$\begin{array}{r} 12.57 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 12.62 \\ \hline 2 \end{array}$$

$$\begin{array}{r} 12.63 \\ \hline 12.63 \end{array}$$

$$\begin{array}{r} 12.40 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 12.15 \\ \hline 15 \end{array}$$

11852

$$\begin{array}{r} 9.5 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 41.9 \\ \hline 41.9 \end{array}$$

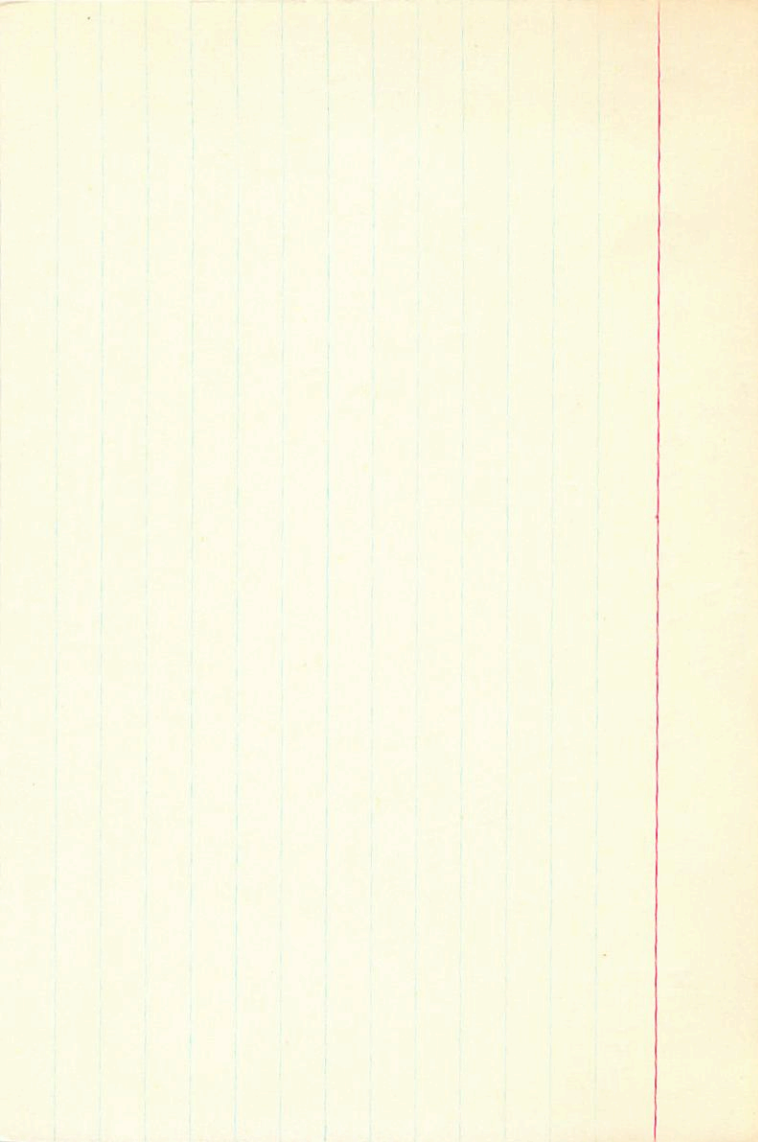
$$\begin{array}{r} 12.31 \\ \hline 12.31 \end{array}$$

$$\begin{array}{r} 12.32 \\ \hline 12.32 \end{array}$$

$$\begin{array}{r} 1944.93 \\ \hline 1944.93 \end{array}$$

$$\begin{array}{r} 12.45 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 1947.39 \\ \hline 12.16 \end{array}$$



173183

18 42.5

+002658.3
+ 31
-42 37
F27D

-2.240.7
C214

25656

6.42 + 40

29.260 1898.0

-42 37

11.46

1997.1

$\frac{135}{125}$

$\frac{1.22}{10.24}$

42.178

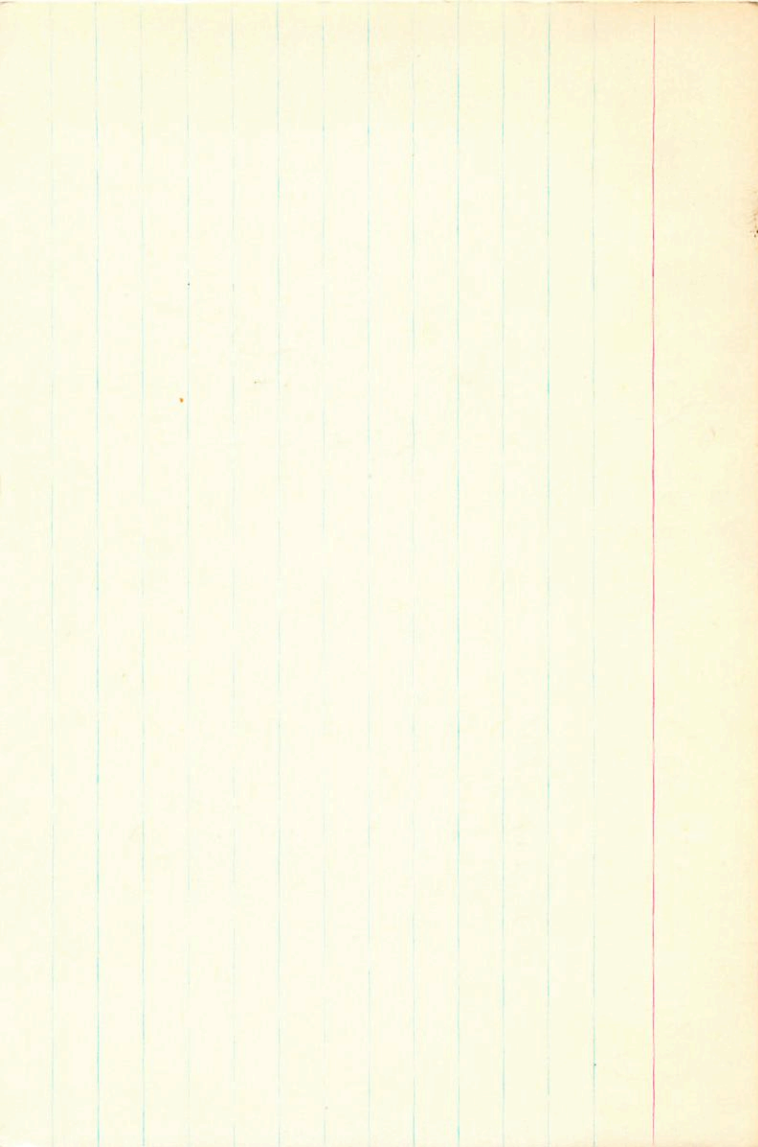
40.89 1931.90

47.105

$\frac{28.577}{12.379}$

29.268
1253
1224
22

12.137
11925
10.146
10.39



9 Sep

HR 7039

W 11690

18 42.5 -27 03 +21.56

3.18 -0.11 88.11

+052 -002 0-0

+056 +002 N

+053 +001 P

+054 000

-1 0 -455 53d +854 00d +21.5 0 -9.8 0
054 0 0 0 256 0 +19.1 0 -19.1 0 2

+12.3 -19.1 -9.8

-20.3 +7.2 -12.1

4 Sept

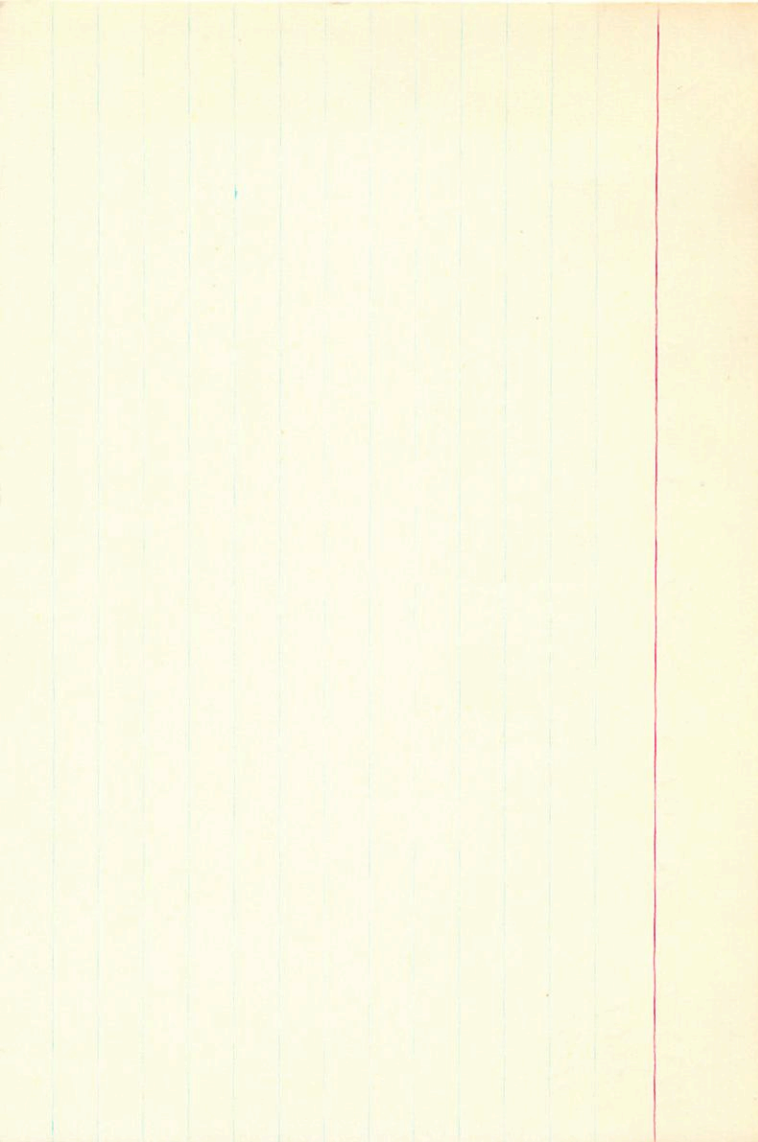
173300 18 42.5 -27 03 3.3 BF +21.58

25661

11190

+0042 55 +002 56 N30

+0043 ±13 +003 ±14 0-c → N30



173494 15 42.6 +23 32 6.2 dF5 -12.06

25663

11191 35.044 1891.5 +23 32 17.90 18903

$$\begin{array}{r}
 35.044 \\
 -193 \\
 \hline
 34.851 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 5.37 \\
 \hline
 23.27 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 35.058 \\
 \hline
 057 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 19.23 \\
 \hline
 1932.8 \\
 \hline
 \end{array}$$

39.4

$$\begin{array}{r}
 35.047 \\
 +2 \\
 \hline
 049 \\
 \hline
 053 \\
 \hline
 +2.02 \\
 \hline
 \end{array}$$

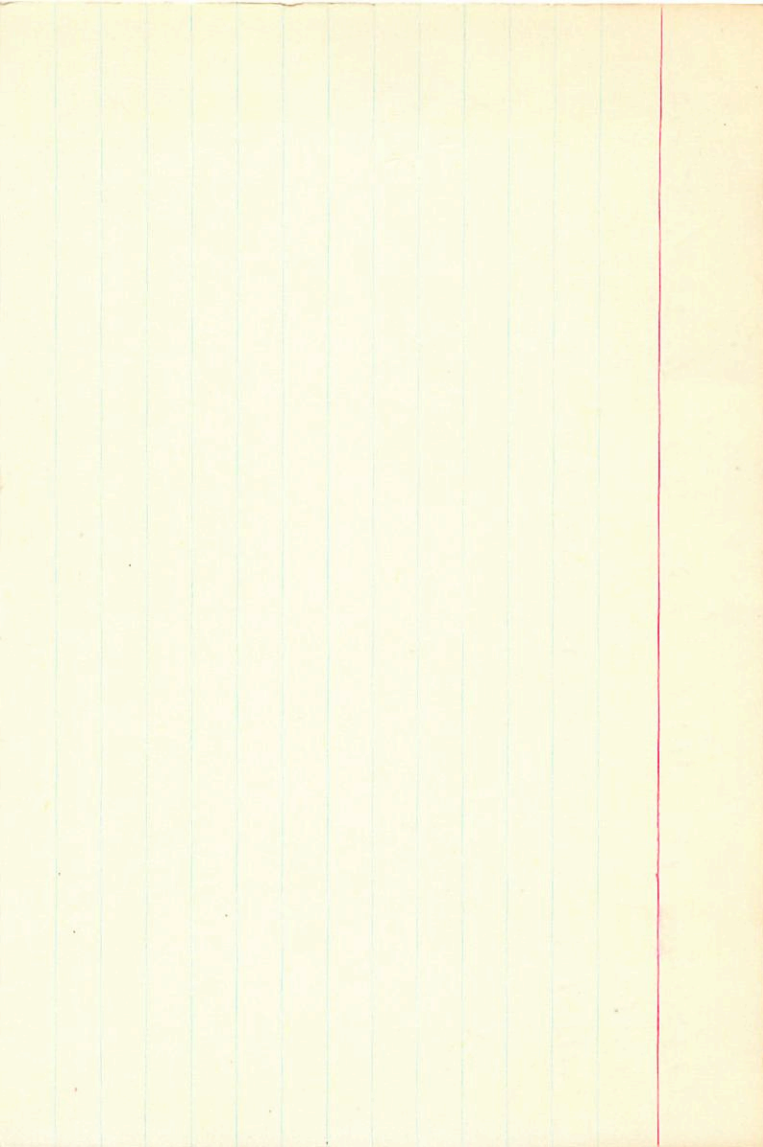
$$\begin{array}{r}
 19.32 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 19.92 \\
 -25 \\
 \hline
 1929.08 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 61.88 \\
 \hline
 30.9 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 19.67 \\
 \hline
 19.49 \\
 \hline
 -3.78 \\
 \hline
 \end{array}$$

40.2



HO173339

(F 43.2 - 43.51

-17556, (4)

7.39 +0.27 A7E

+051 -0556P

01

-982 187 -693 721 +051-085 -17.0 85-9 +12 -289
050 058 010 011 185 322 -12.2 -2 +12 01

+16 +44-17

+32 -25 -29

28 Sep

173460

18

43.3

-22

27

5.8

914 -2.76

25687

11208

38

+0028

000

37

N30

A0511652

+0024 ± 2.1

+001 ± 1.9

004 → N30

