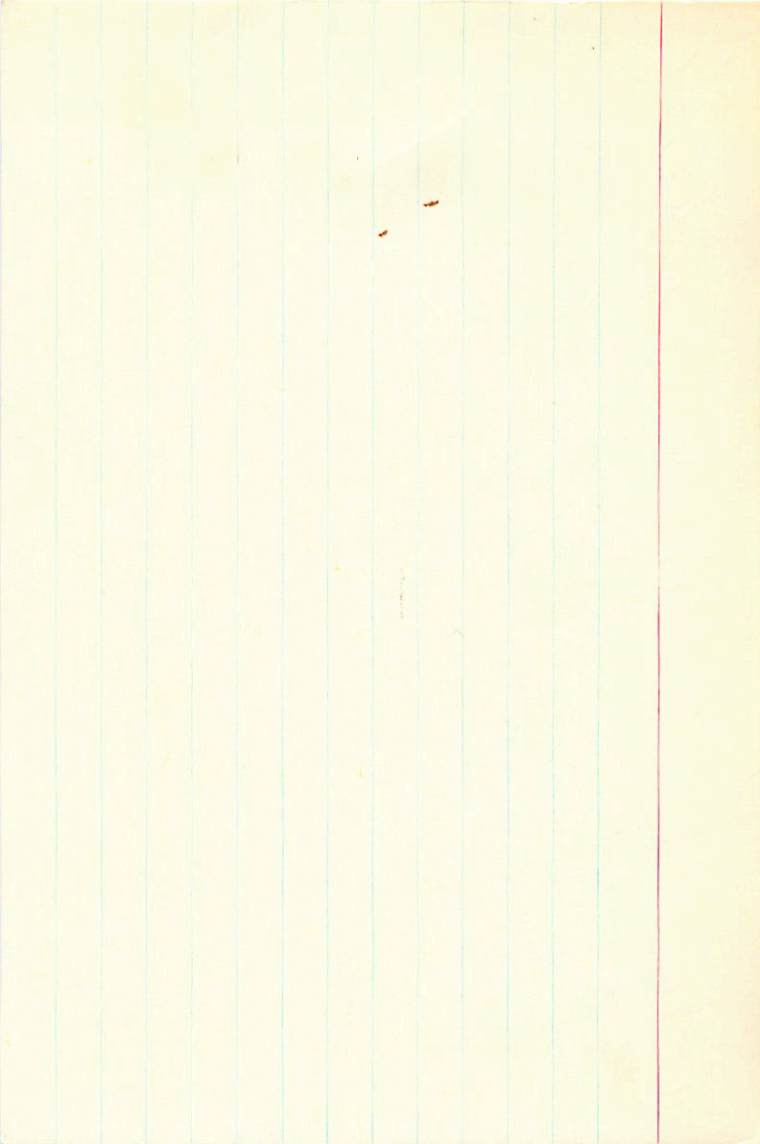


167720 18 14.3 -17 24 6.0 g144 -7.28

24940

10739 0000²⁷ -015²⁸ N30
0000^{24.1} -020^{±4.8} BL → N30



G206-20

18 19.5 429 11

-22-10

28 m⁰

12.56 0.100

$\left[\begin{array}{r} 581 \\ 161 \\ 189 \end{array} \right]$

12.74 0.56

12 = 0.4

18489

-189

-781

ND

546

-72

R.A. : 18.250
DEC. : 29.200
R.A. : -184.000
DEC. : -189.000
STANCE : 7.450
ODULUS : 309
VEL. : -7.200

q1 (U) : 0.124
q2 (U) : 0.845
q3 (U) : -0.520
dU : -851.197
U : -259.297

q1 (V) : 0.462
q2 (V) : 0.415
q3 (V) : 0.784
dV : -723.698
V : -229.286

q1 (W) : -0.878
q2 (W) : 0.338
q3 (W) : 0.339
MP : 365.966
W : 110.653

6

+6005 ± 2.7 600 ± 2.7
+600 (-0.13)

167818 18 14.9 -27 04 4.7 GNS-16.9a

24961 .308
-0.25

10749 55.333 1900.1 -27 3 45.33 1898.1

21422

33865

55.287

286

292

55.346 224

-342

312

+004

76.44 1430.26

29.20

47.39

96.09

+18

48.9

45.60 1939.25

-13

45.73

45.82

- .49

957

348

36.7

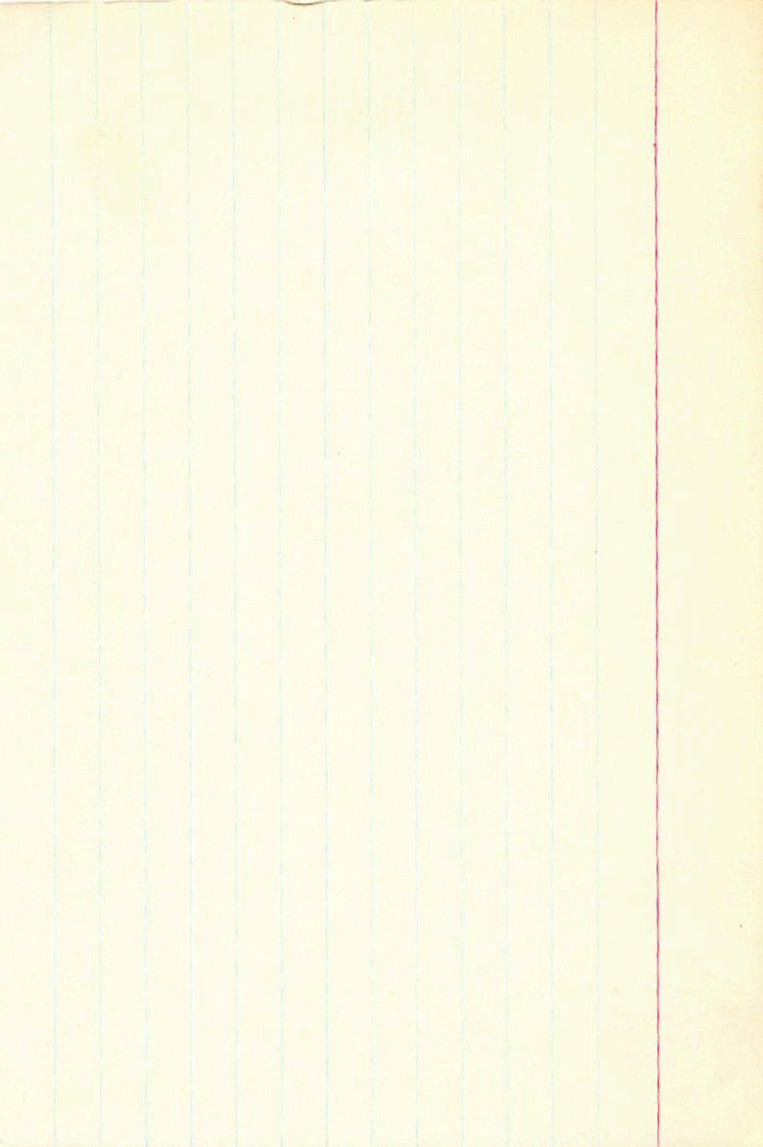
37 Dec

168653 18 15.6 +68 44 6.1 9/12/1 -10.38

24975

10760 +0026³⁵ -057³⁴ N30

+00~~14~~¹² 12.1 -057¹² 1.966 → N30



6846

18 15.5 - 25 39

(2) 4.5M

168147 18 16.8 -44 06 7.18 1.62 MY III #99

B624948

-0009
+0035 = 122 -053 = 13.0

50.305 1903.2

$\frac{167}{.138}$

1.014

$\frac{49.135}{9}$

$\frac{50.179}{9}$

1.140

$\frac{50.274}{114.022}$

0.09 1903.1

$\frac{2.46}{63}$

57.

192736

32.43

$\frac{32.80}{3}$

5.23

$\frac{2.04}{3}$

3.19

$\frac{5.50}{4}$

1.313

6



105 Hm

169932

25603

10795

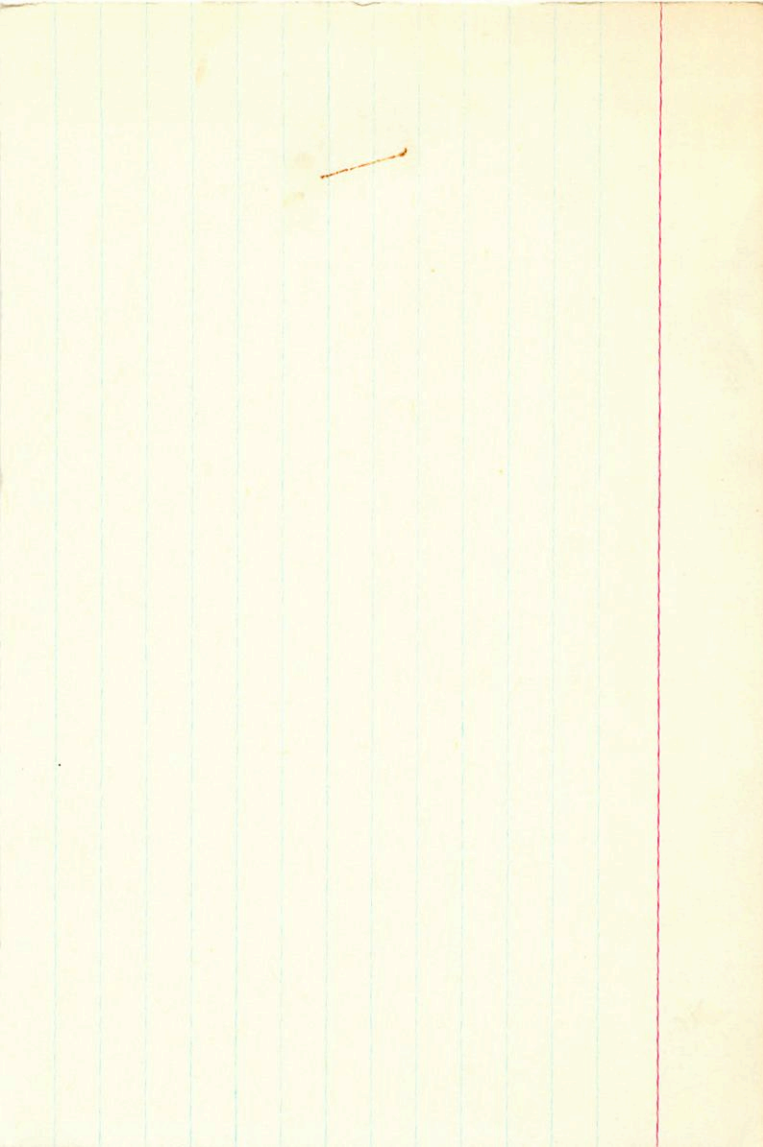
18 17.1 +24 25 5.5 g 24 -13.9g

0000²⁵ +008²⁵ N30

+0006²² +001²¹7

Sp. O. P. =

15.9 Ouband



$$-0058 = 2.6 \quad -091 \pm 2.3$$

$$169027 \quad 18 \quad 17.3 \quad -3.5 \quad 43 \quad 6.7 \quad A0 \quad -25.5 \quad 6$$

25008

$$10800 \quad 16.222 \quad 1888.4 \quad +68 \quad 43 \quad 19.12 \quad 1879.4$$

$$\frac{375}{1597} \quad +6.42$$

$$-049 \quad -091 \quad +2.0 \quad 25.56$$

$$45 \quad \sqrt{184} \quad -1$$

$$-052 \quad +19 \quad -0542 \quad -0889 \quad 21.0 \quad 1938.4$$

$$-0295 \quad +46 \quad \boxed{2025-090} \quad +1 \quad -25 \quad 20.75$$

$$M_y = \text{Ⓢ}$$

$$20.06 \quad 1935.0$$

$$24 \quad -100 \quad -25$$

$$V \quad -20 \quad -21$$

$$W \quad +12 \quad +3 \quad 498$$

$$16.377 \quad +8 \quad 395$$

$$202$$

6.2

169027.000*

18.000*

17.300*

68.000*

43.000*

-0.025*

-0.090*

6.200*

173.780

-25.500

-0.435

0.137

-78.992

7

168415

18

17.3 + 0.26

- 15

5.1

5.7

9185430.51

25006

10799

15.959

1896.7

- 15

5.1

13.95

1896.6

128
831

1.98
11.97

49.632
26.242
15.924
624

50.30
3408
15.726
14.223
442

40.5

15.943

2
941

935
+ 104

13.9

13.74

+ 4

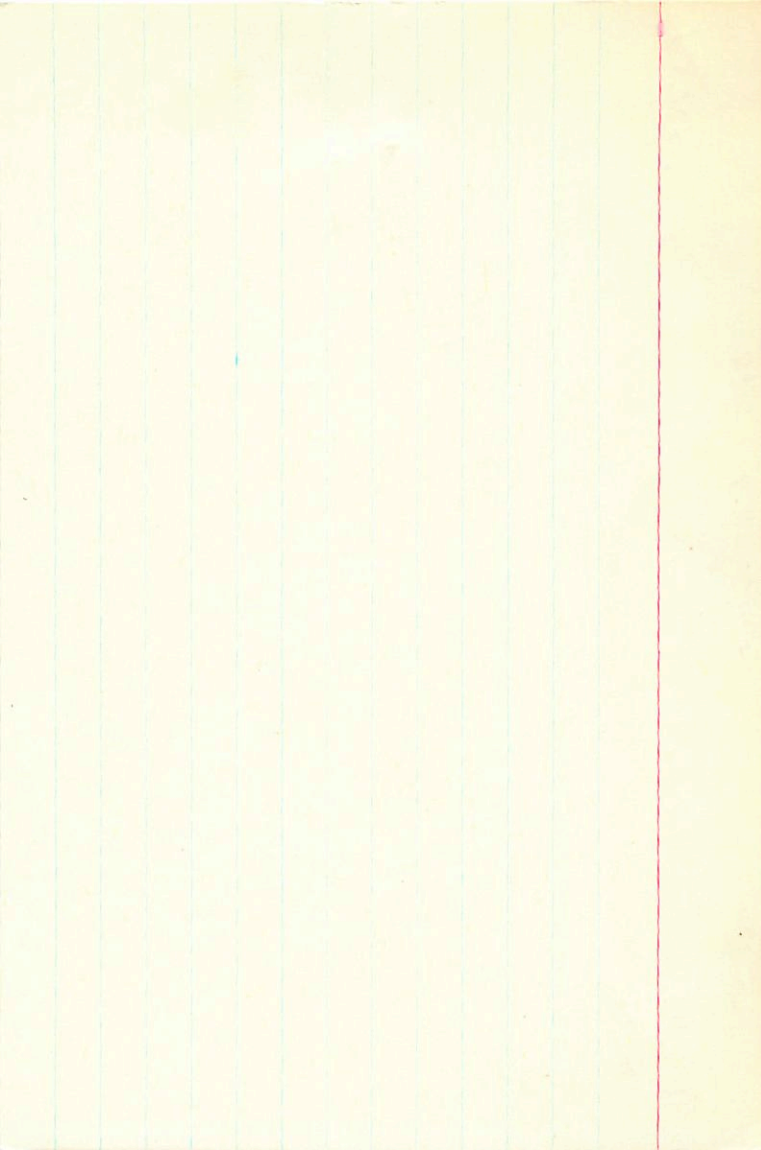
13.72

1939.03

37.2

13.83
- 1.86

40.6



140511262

168459

18

17.4

-08

00

6.6

df2 -49.18

25013

10803

21.911 1891.9 -8

00

13.92

18830

9^{mm} 2.5

-116

795

0.380

21.512

892

21.892

867

21.893

885

876

+081

+54

13.38

51.01 1935.0

34.98

16.03

1.48

14.51

14.3

14.419

+20

1627

14.29

42.5

875

34.4

51.7

1933.58

14.34

96

X Lyr
168775

19 19.1 +36 02 4.3 g M1 -22.3a

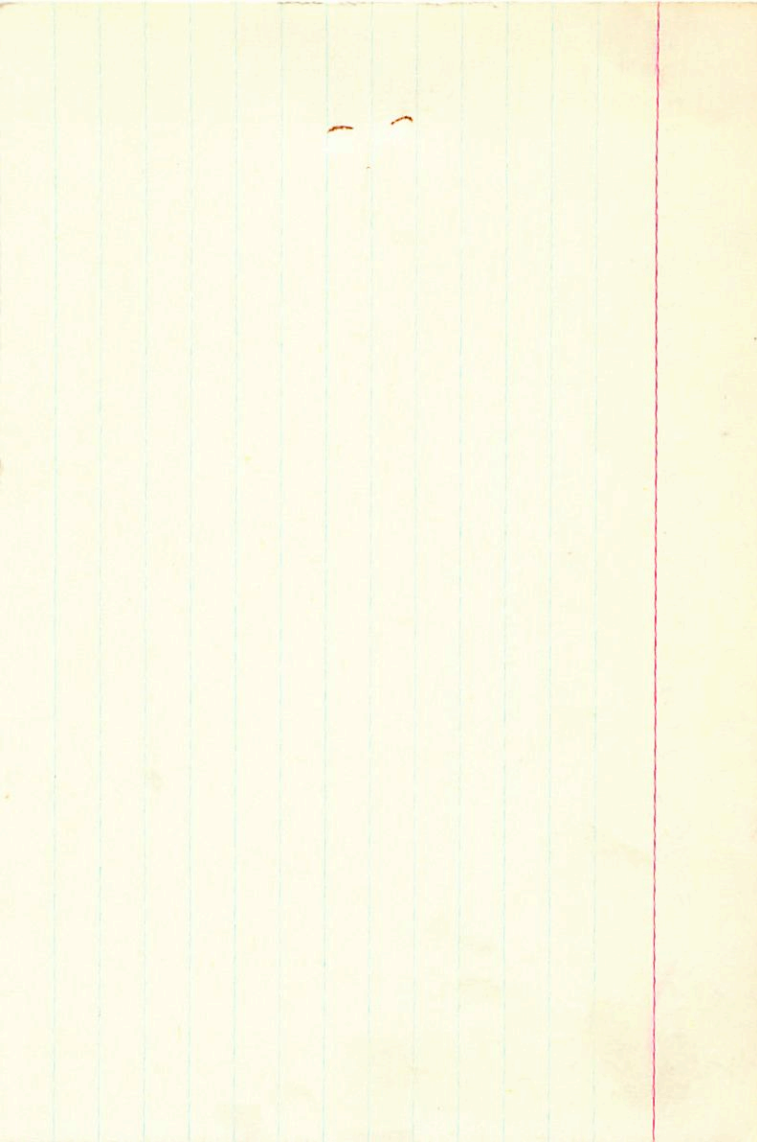
25032

-236 (8)

10813

-0016³⁵ +045³⁸ N30

-0020^{±23} +046^{±1.6} G6-7 N30



168339
3 Par 250x5 18 18.6 -61 31 gm 112.2g

HR6855 10823

4.35 + 1.48

-003 +004 FN3

8^m 3ⁿ

-003 000 GC

+0010 13 600¹³ N30

+007 000 N30

+0013 # 39 +007 ± 34 GC → N30

000 +001

40013 +0080

FN5

4400 8865 } OVERS
8717 4521 }

67033

R.A. : 18.300
DEC. : -61.500
R.A. : 0.000
DEC. : 0.000
DISTANCE : 0.000
MODULUS : 10
VEL. : 0.000

1 (U) : 0.135
2 (U) : -0.529
3 (U) : -0.838
dU : 0.000
U : 0.000

1 (V) : 0.456
2 (V) : 0.784
3 (V) : -0.422
dV : 0.000
V : 0.000

11 (M) : -0.880
12 (M) : 0.325
13 (M) : -0.347
MP : 0.000
M : 0.000

8

8

-0039±2.3 -057±2.4
-0042 = -049

169028 18 78.8 +51 19 6.2 9 101 -10.38

25047

10826 45.715 1881.8 751 19 29.47 1884.5

266
981

10.56 2242

35.220

45.814

814

814

45.689

694

45.685

700

584

33.20
3.73

51.4 1926.4

34.70

31.64

290

31.73

30.44

-25

30.19

30.19

30.19

46.7

62.2

112.72

2233

39.9

584

1942.39

30.07

30.13-3.07

6862

18 18.9 -38 41 100

148592

5.10 + 149

John N30

730 + 17.88

-0030 -032



-0031±4.6
-0030
-024

168592 15 18.9 -38 41 5.1 MO +17.8 δ

25051 +7 +8

10830 51.728 1908.0 -38 40 53.45 1903.2

474
28
130
858
585
1190
1.40
52.05

-0024 -020

52.99 1940.76

-0030 -032

3748/2
9/4
13
51757
762
096
53.01
96

27.5
11.4
2.7

143 -168 -976
457 985 -092
-879 434 -195

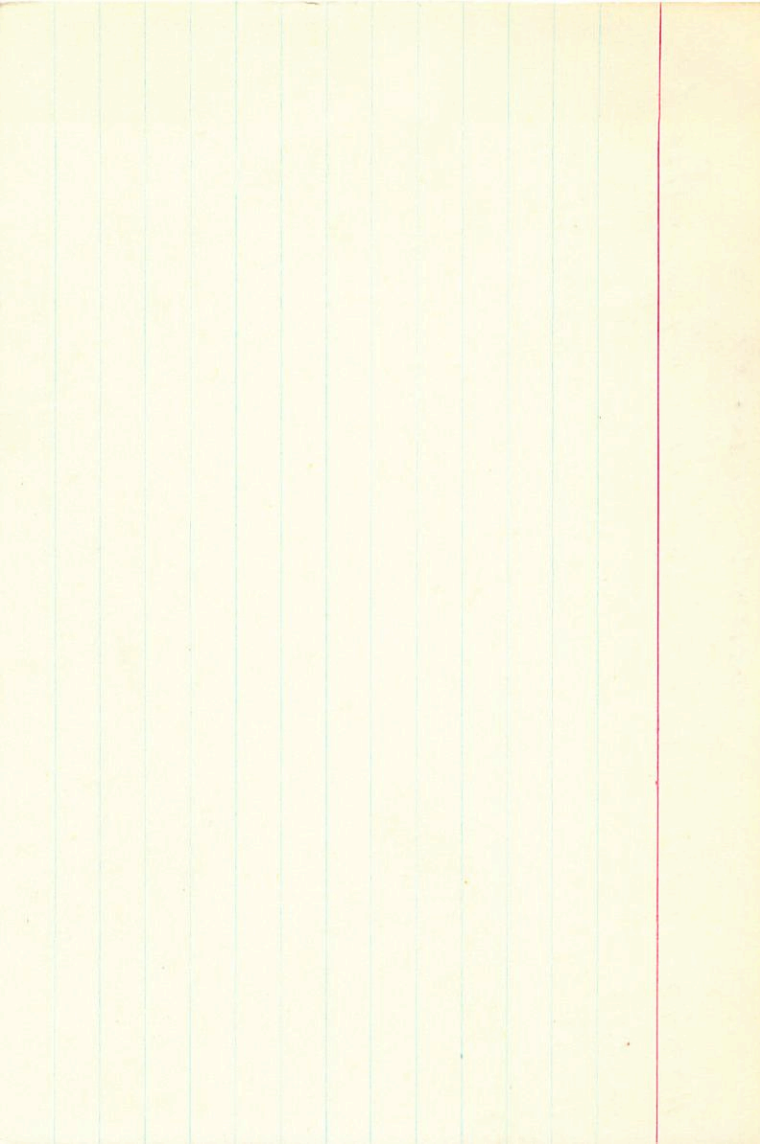
10150 +0159
0607 -0840
+1170 -0412

-0031 -0.4
-14.17 -228
+0758 +11.9

-17.3

-1.6

-3.5



1401R0+A

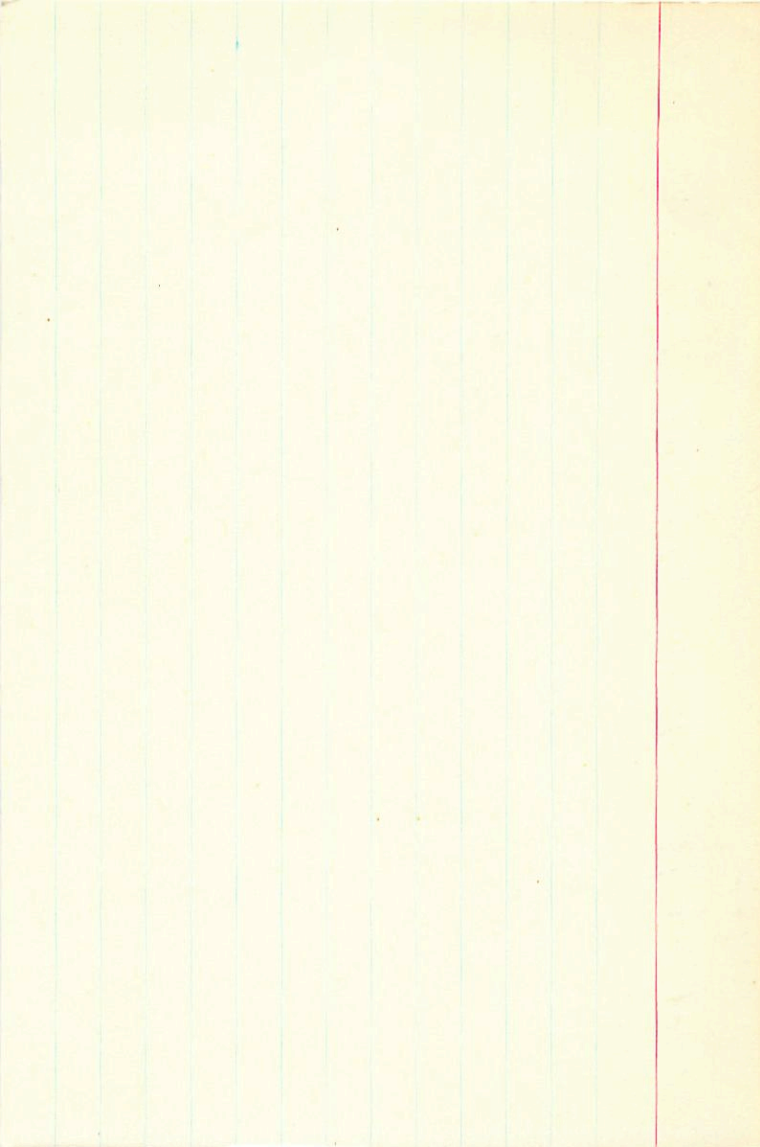
+0009±5.5 -002±4.2

168701	18	18.9	-16	21	7.7	gR0+21.88
25052						

10831	55.611	1901.5	-16	20	57.48	1894.5
-------	--------	--------	-----	----	-------	--------

$$\begin{array}{r} -044 \\ \hline 1567 \end{array}$$

$$\begin{array}{r} -11 \\ \hline 57.37 \end{array}$$



17 Syn

18 19.0-25 16

~~19.1 Order~~

A0511282
168815
25062
10841

-001245.2
-0005

-018±4.6
+005

18 19.4 -15 07 24 2125 -28.68

8.0 915 = 250

22.109 130.11 -15 6 49.78 10979

059
168

48.84

56.335 149
25822
22.150
5
162

340

29.49 1334.12 166
3918
50.31
156

35.7
37.2

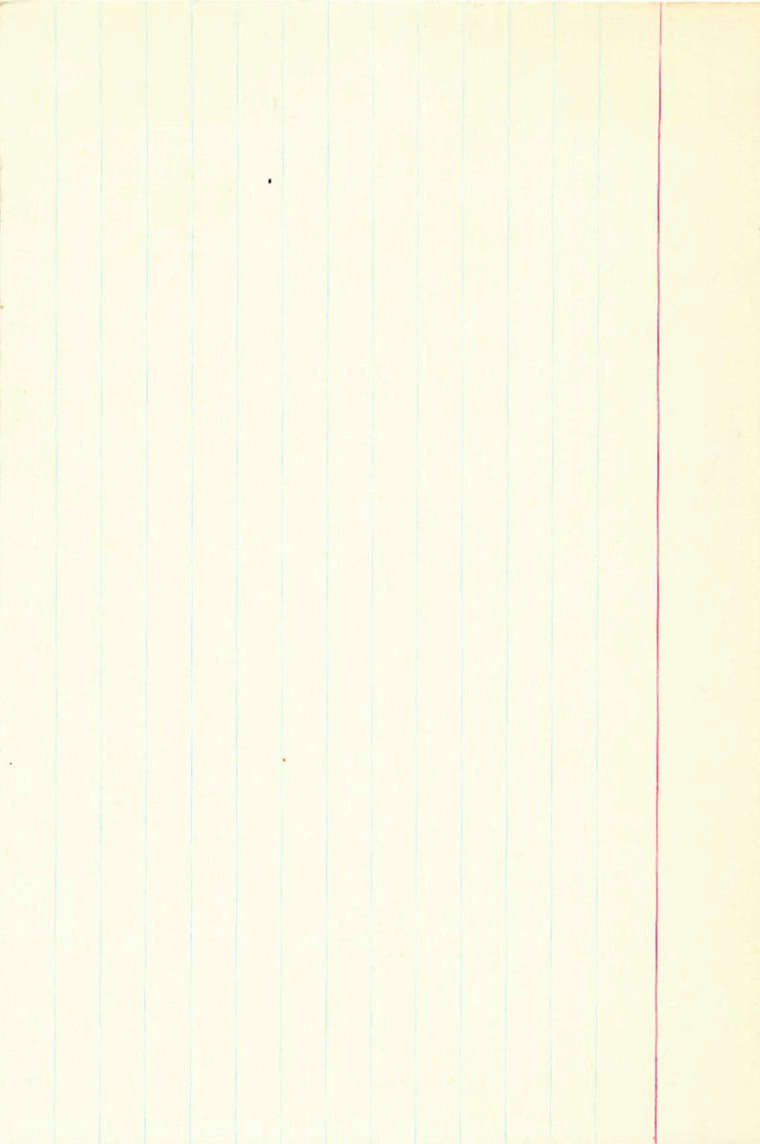
48.66
+18

47.834
31329
22.169
133

48.123
48.52

1433.54 5.49 1937.84
16.427
48.59 49.07
48.67

22.169 154



-0003 ± 4.3 -021 ± 3.6
-0006 -036

168733 18 19.5 -36 425.4 88. -11.88

25067
10845

29.747 1906.1 -36 41 41.33 1902.0

013
760

1.01
40.32

29.729 -0045 -029

41.77 1941.02

7
736

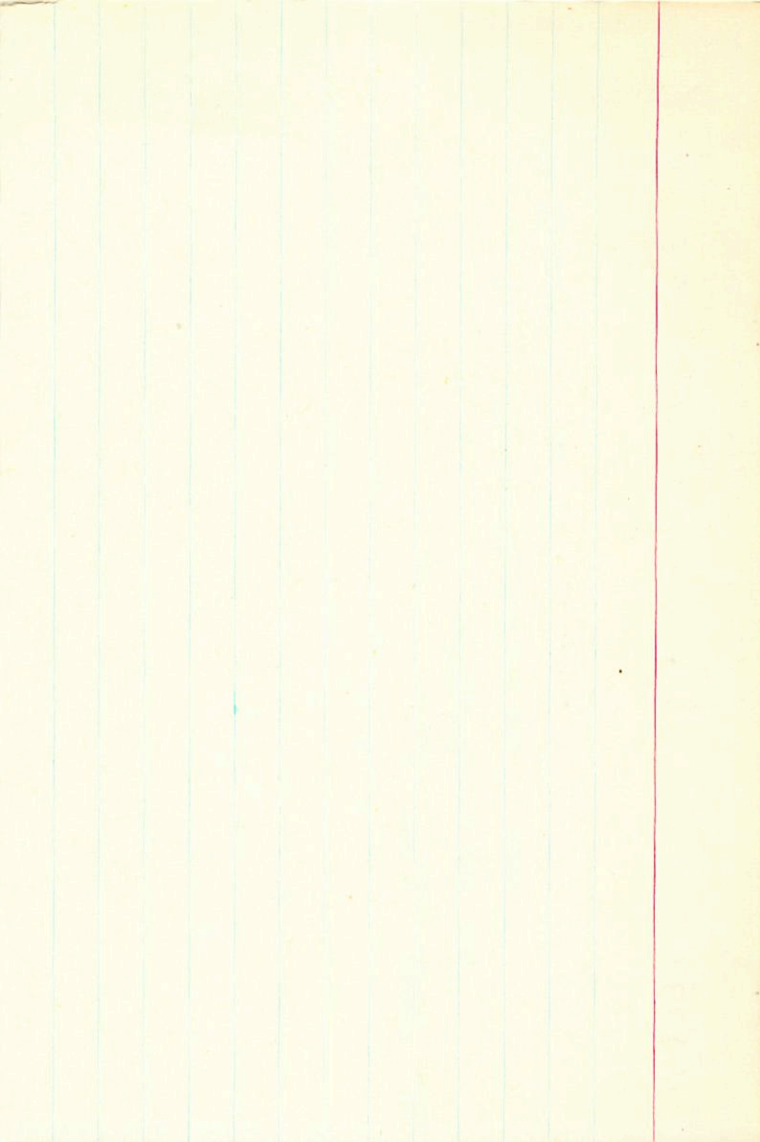
2
41.79

29.71
+36
746
741
-019

32.3

41.5 1935.7
-19
41.49
41.64
-1.32

7672
38.4
36.4



169666 18 19.9 +71 30 7.8 dF2 -40.48

25077

10850 -0131¹⁹ +040¹⁷N30

-0142±2.6 +035±2.6 Q1 → N30

+0005 = 7.3
+0002 -0.12 = 6.4

MR 6883 16911 15 20.3 +12 0.0 40 -55.3 6

25084
10853

5.89 +0.04 +0.08 42.2 60
-010 64
+007 -012 66

15.674 1899.4
-025

649

+12 0 10.87 1895.0
66

11.53

15.663
666

11.64 19340
+9

11.75 34
422 36.7

37.1

+017
15.636

12.09 1939.42
-3
12.06 41.4

643
655
+007

11.90
+3

-554 B87 205 975 +007 -009 -55.3 -002 -12 -043
007 002 001 0 033 014 -54.1 -5 +54 B2

-3 +55 -14

+41 -36 -14

169305

18

20.3 +49 06 5.1 g m² +13.6a

25085

-0032'8

+054'18 N30

10854

-0033±2.7 +055±9.0c → N30

+0046=2.9 +018±2.6
+0053 +014

169191 18 20.6 +17 48 5.5 912 -18.7a

25093

10862 36.371 1904.1 +17 48 0.09 1905.6

-211
160

36,

36.324

321

36.349

33.1

-0.80

59.29

59.69 1934.0

+9

59.78 1940.36

0
335
+175

59.71

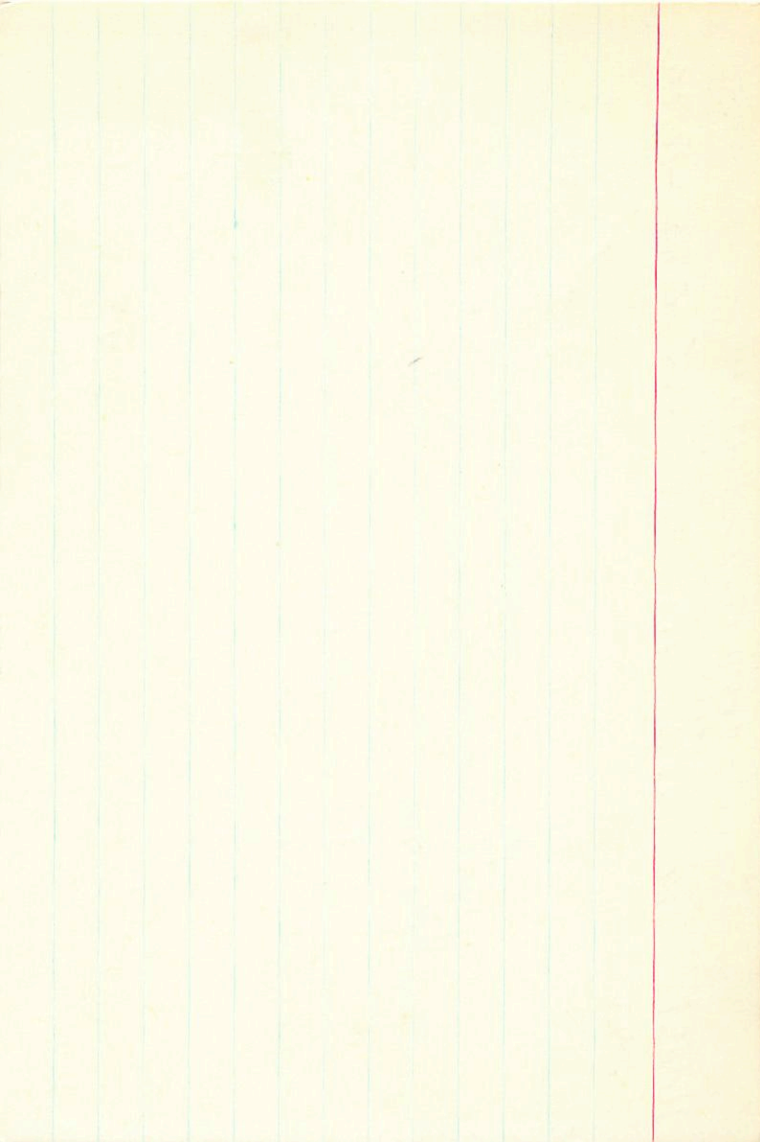
7136

59.74

37.2

+ .45

31.6



8849	8.67	+0.55	0.00	F8D	-13.4		
169245						-0.031	-0.052
						-0.005	-0.002
						-0.086	-0.054
						0	+0.004
726°3230						-0.036	-0.050

18 ^h 20 ^m 41.121	+26° 11' 55.69	1928.44
<u>-0.004</u>	<u>-0.17</u>	
41.117	55.52	
18 ^h 20 41.120	+26° 11' 55.50	1930.4
<u>0</u>	<u>-0.30</u>	
.120	.20	

3 Set

+0027 ± 4.5
+0037

+042 ± 3.5
+037

18 20.9 - 8 58 4.8 9120 - 5.62

25101

-51027

10866

55.130 1907.4 - 8 57 43.25 1905.9

1905.9

-115

-1.85

015

45.10

33.072

28.39 1934.12

22.078

42.70

55.150

45.69

29.6

-273

41.19

408

112

+14

37.0

55.126

41.03

31.1

124

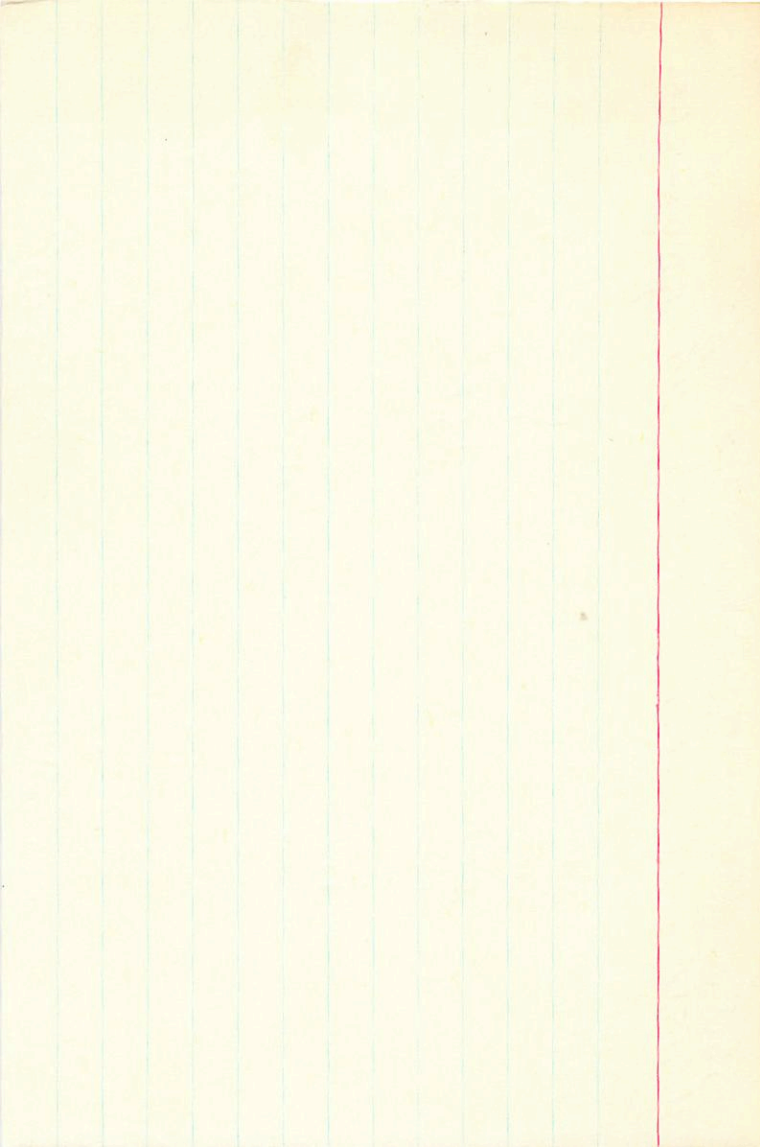
43.84

1939.96

-891 + 109

43.95

+1.15



169118 18 21.1 -26 27 7.57 +1.50/1.51E

$18 \text{ 21:8} - 30 \text{ 47} \text{ No III - IV} - 18.7 \pm 0.4$
 169233
 25120
 $5.58 + 1.16$
 $5,16$

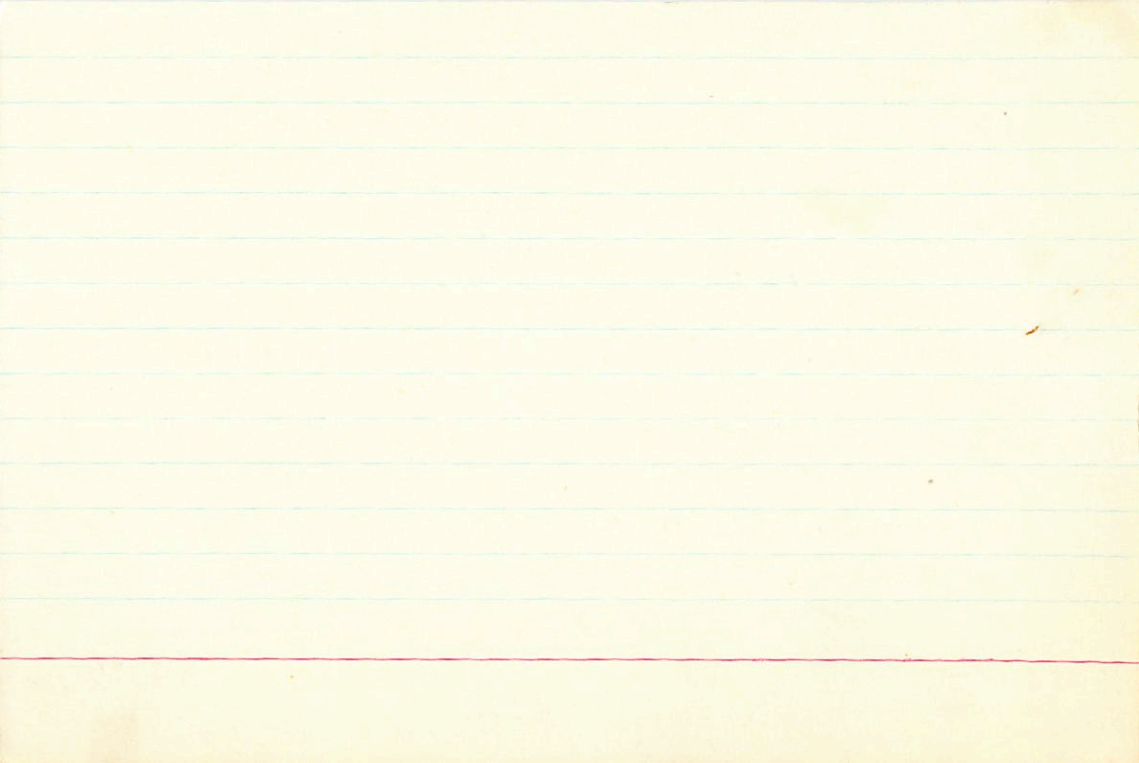
48.566
 437
 49.003
 48.566
 1905.4
 -30
 47
 2.56
 1902.1

954
 47.8
 45.7
 3.59
 58.97

11.7
 586
 417
 42.4
 1.55
 -1.5
 1.70
 1939.66
 -3
 42
 478
 2.39

48.428
 13
 511

2.96
 -1.2
 3.0
 1955.98



6842

15

22.0

-7

6

100

⑤

-25.2 *Heffer*

-704598

6.30 + 1.16 + 1.09 *Case*

+129 -008 *ll*
72 + 2

9

P

6892.000*

18.000*

22.000*

-7.000*

-6.000*

0.131*

-0.006*

5.500*

125.893

-25.200

0.083

-0.915

33.485

0.255

0.400

22.030

-0.561

0.047

-71.778

9