

HR6784

18 06.3 +14 17 Am - 9.10

166095

6.30 +0.18

-016-018 GC

24734

6.30 +0.17 +0.21

10590

16.958 / 1599.6

+14 16 3114 1893.8

Alt III m on

12th
-0010 -004

055

+1.01

17,013

32.15

16.928

32.10

1933.5

3
981

32.19

16.975

36.8

32.34

1939.4

984

32.25

729

982

32.24

36.4

-031

+09

42.6

166229

18 06.3 +36 24 gN3 669

GC24735

5.47 + 1.17 + 1.21 1121R

-6.90(7)
-6.40(14)

W10591

W(10.7)

Y4161

+3603027

HR6763

-81 -58 +14 .010

-100 -187 64

-53 -42 +9 .015

$10 \pm 6 \text{ at } 125$

-008373.6
-0056
-19772.8
-206

18.077 1902.5 +36 23 42.26 19060

394
471

4823
50.49

509

26.07
52.202
118.202
279
551

259

1926.5

284

~~194~~

4
248
22

338
1188
4509
46.63
41.49

176
4538
41.61

22.4

18.202
22

45.6
-33

130.4

45.27

166097
+903576

803
155
21

18 06.4 +9 26 RY -19c

10.03 +1.53 +1.77
9.21 +0.615 5M

b = +137

0000

2.19

1897.1

2.17

1533.6

2.09

34.66

2.12

41.19

1.69

1934.1

11
11

101142
 166230 18 06.7 +20 02 5.2 A4 -16.3a
 24793
 10597

+0003#2.5 -024±2.0
 +0001 -029

43.406 1899.9 +20 2 9.47 1898.8
 $\frac{-015}{391}$

10.70
 9.51 1934.2
 +9

43.407
 $\frac{-1}{406}$

9.60 1941.38
 9.64

43.385
 $\frac{-4}{381}$

-20 7558
 9.49 37.8

37.9

955 39.0
 -1.15

393 +1002

166033

18

065

-23

35

9.60

"

0.20

→ ③ Var

9.86 + 21 - 66

115 ②

② 1, 0, 12, 6

138 - 036 - .392 2.613

110 - C'17

024 - 420

FOIE: -17 ± 3 46
-21.5 66

18 06.9 -30 44

166023

FOIE
141E

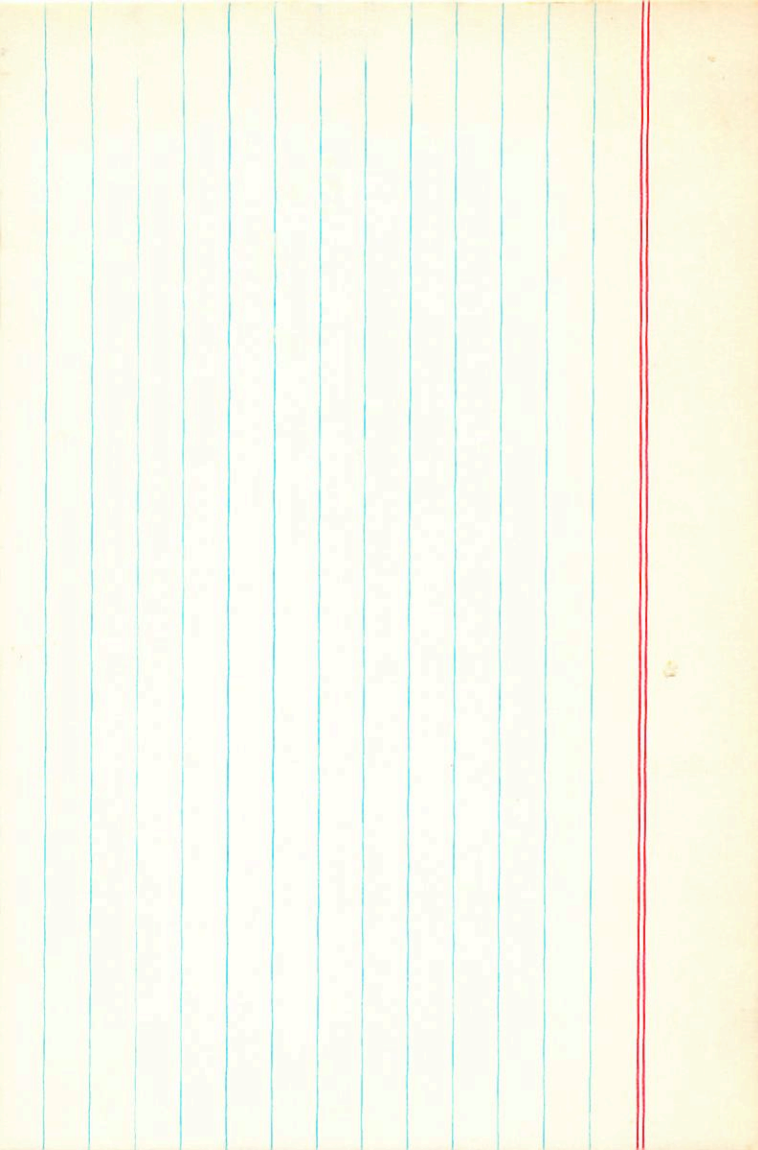
FD1237/8

AB 5.53 + 0.98 (2.01)

141E 5.6 } 40

FOIE 8.6 } 40

+0008 -341 ~~46~~ →



16

T Her 18 072 +31 01

-2 +11 MC
 $\frac{+2}{0}$
 +11

+0009 = 3.4 -0002 = 2.9
 $\frac{+0006}{+0008}$
 +0110

095 862 -496
 477 897 783
 -873 312 374

+0045 +0092 +0127 +116 +72 +60.5
 +0226 +0034 +0224 +24 -72 -55.5
 -0413 +0030 -0383 -25 -81 -45.6

+10

T Her 8.0 +1.30 +0.95 +72 -71 -81 +10 -1220 1654 +22
 6.9 +0.96 9.55 +1 +3 -7 +2

T 1 hr

57.4 + 22.0

E 7 hr

146014

55.2 + 21.6

3.83

-0.02

-0.07

+0.3

375

B5 II

146152

~~73.4 + 18.4~~

~~-24.36~~

-0.14

-0.82

+0.8

6.1

B2 I

~~167220~~

~~65.4 + 2.0~~

-0.5

-2.3

6366
5120
11964

18 07.2

+81 01

R R-H

1.888	7.94	6.90	+101	362.9	0.2	3.96	9.31	7.79	+1.57	710.8
1.978	8.27	6.97	+116	382.8	0.5	4.10	10.54	8.41	+1.88	732.8
2.11	9.64	7.75	+1.52	404.8	.24	4.12	10.83	8.88	+1.93	736.7
2.18	10.39	8.24	+1.78	416.7	.21					

2.235 11.06 8.76 +2.03 425.8

2.41 - 9.14 +2.20 454.7

2.49 12.07 9.83 +1.99 464.1

2.64 9.95 7.96 +1.59 455.7

3.63 12.05 9.59 +2.25 656.9

3.72 11.26 9.07 +1.90 670.9

3.805 9.43 7.97 +1.55 684.8

3.83 9.38 7.97 +1.58 698.8

3.805 9.34 7.92 +1.53 694.7

3.92 9.21 7.83 +1.49 703.8

8.0

6.9 +0.95

+22

163	6.9	3300	241.8525	243.8225
326	1.92	1850		1650
	3.68	398.76		2436.575
	3.49	330		330
	4.63	402.00		690.5
	4.15	403.45		660
	4.15	410.45		7.165
0711	4.15			773
1574	13.45			
1813	1.45			
200	6.9			
100	6.9			

THU
166382
24757
10606

+0003 = 4.5 = 007 ± 4.7
1654
18 07.2 +31 01 gm3e -122c

12.639 1898.4^{59.1} +31 0 39.69 1898.8
-045
624
-04
39.65 -76

(May) July 13

12.619
19
629

39.6 1930.4

-33

3

39

344 232c

346 2.2

-002 + 011 MC

+1

+000145.7 -032 ± 4.3

(214)

-47 31 R1 III -IV

166006 18 0786

-14.9 ± 0.4

24761

6.06 + 1.20

12 ~ 1.7"

17.717 1905.2 -47 31 26.03 1501.2

1.56

24.47

25.54 1941.38

17.719
-3.83
13.883

-127
25.66
1207

9800

49.0

17.724
-127
15.447

26.38 1956.62

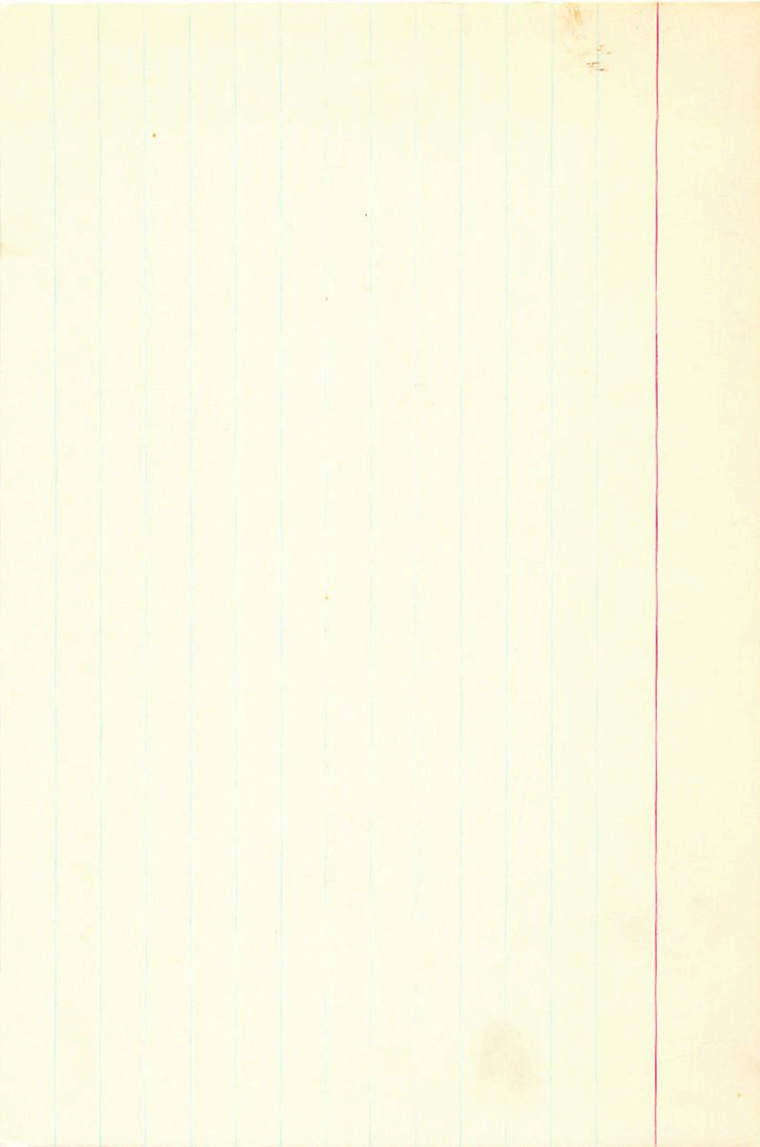
47.5

-3

912

26.41

26.04
-1.57



14R6797

+0011 ± 3.5
+0008

-195 ± 3.8

-19 (2)

ADS11113

166285

18

07.4

+03

07

5.7 dFY -14.48

24764

10612

23.826

1905.5

+3

42.79

1508.6

12.71

-049

777

+8.07

50.86

374

23.805

814

45.85

19333

23.742

791

802

+025

44.73

1940.24

73.54

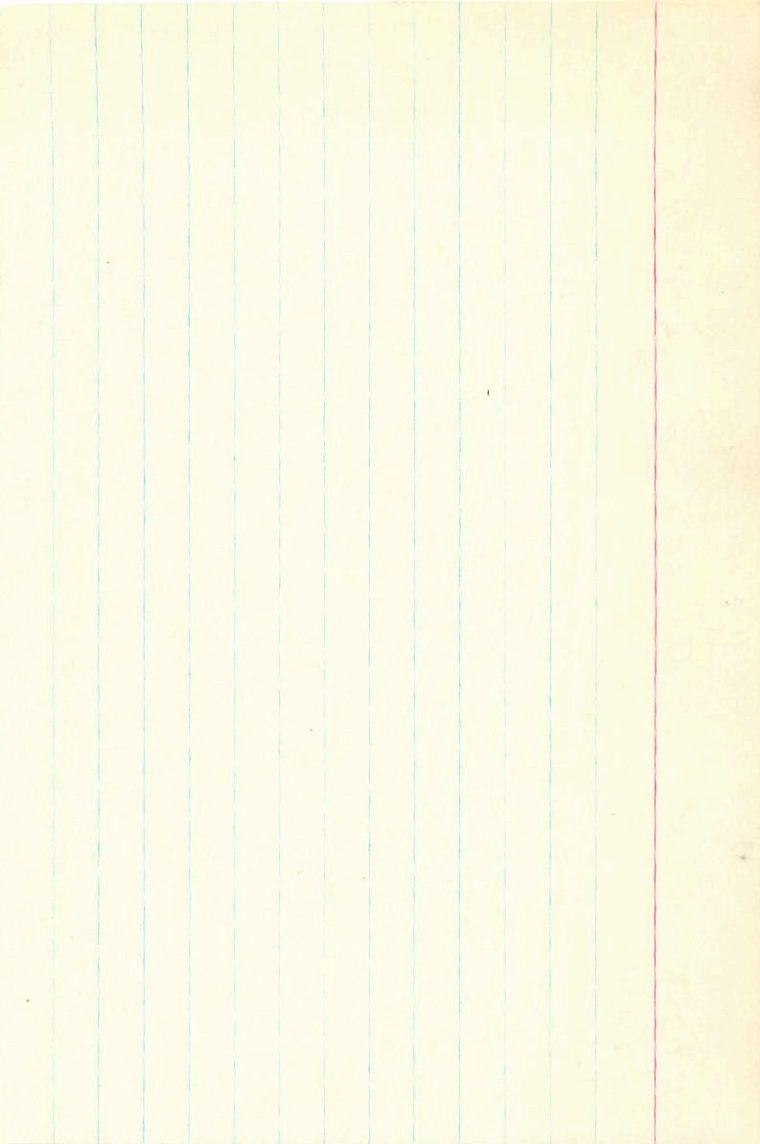
36.8

21.3

28.2

45.30

5.56



ΣT_d
 166063
 24767
 $4.51 + 1.02 = 5.53$
 $5.53 \times 248 = 1371.24$
 $1371.24 + 166063 = 167434.24$

10616
 31015
 19069
 -45
 57
 55.04
 1903.4

$+1.82$
 $\frac{53.22}{53.22}$

54.65
 1941.04

31.034
 -36
 $\frac{30.998}{35}$

42.4

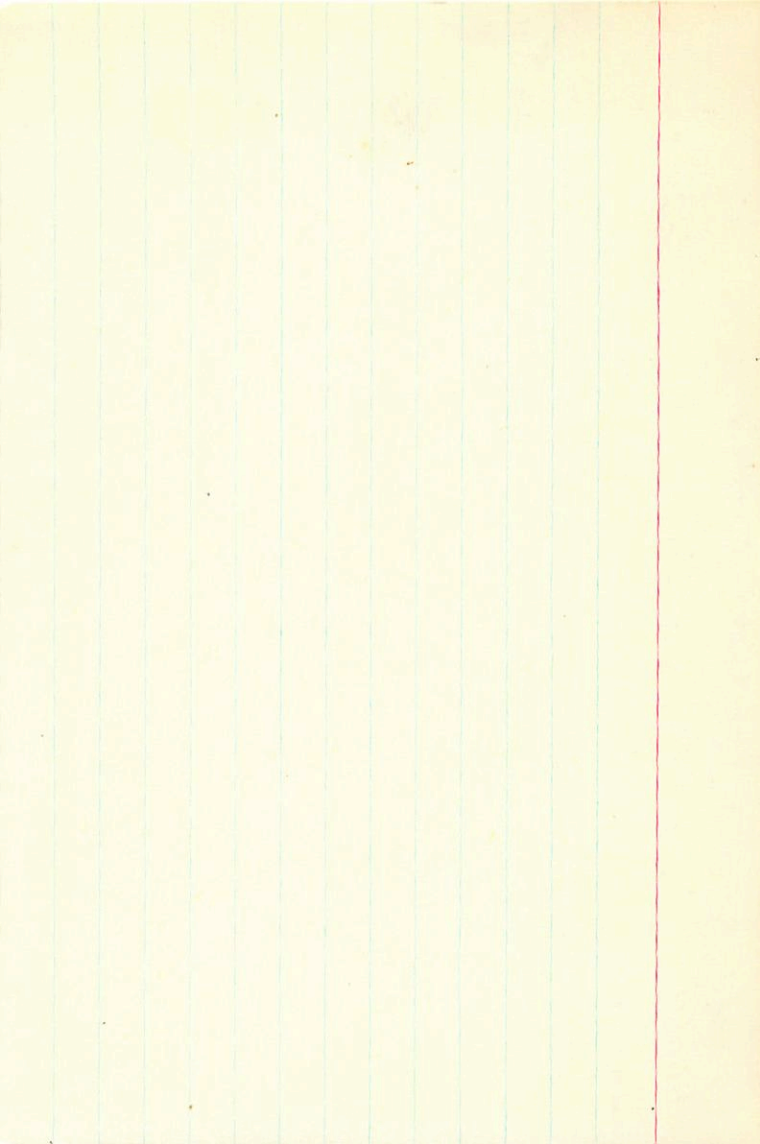
30.970
 -108

54.77
 1079
 55.40
 -2.18

98.64
 49.3
 48.9

30.970
 -7
 963

55.96
 -6
 56.02
 1957.60



0	26	8300-	1614-0604	141 121 510
0	16	1210-	1084-1315	178 867 861
0	220	10458	10176 +0321	1095-212-473

101

1031

1039

1030-1030

1035-032

1023-029 02

1026-031 N30

1027-040

1027

1028

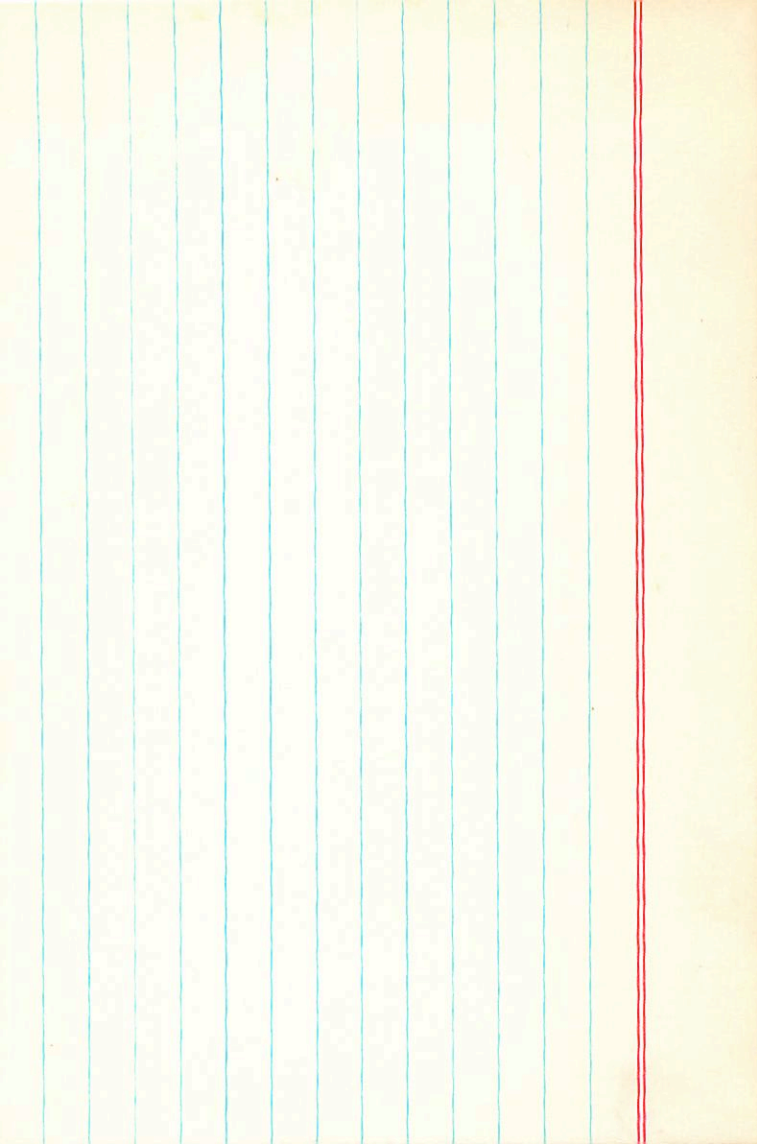
5.85 + 0.30 (1.59)

FD 1239

10 6.4 ym.

18 07.5 - 41 22 Form - 1872 4c

16.114



-0006 ± 43 -012 ± 3.2

166479 18 07.9 +16 28 6-1 dF3 -12.98

24777

10623 54.654 1893.4 +16 27 56.50 1886.2

034
688

+17
57.27

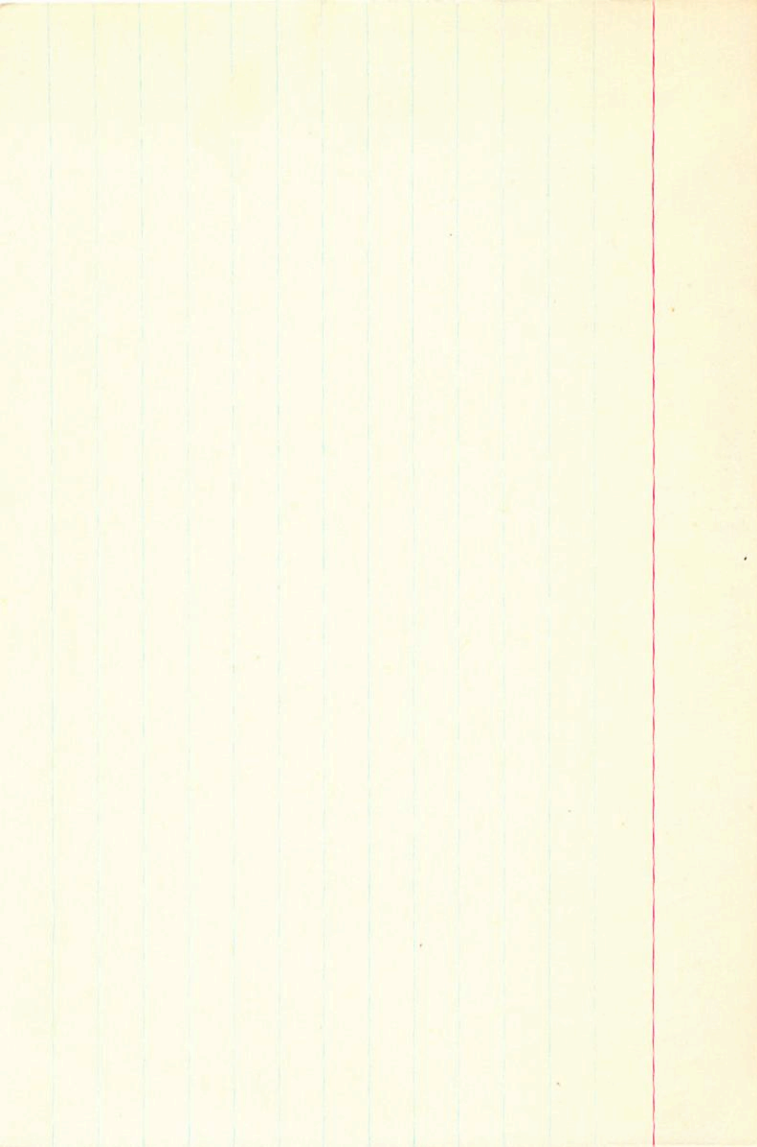
A051123

6.5-7.6 ± 1.2

54676
-3
673

56.43 1433.1
+9
56.52

5



166601
+3003142

18 08.1

730 50

8.0

df5

-67.0

10625

FSK with 2L

+0014 ± 3.6
-007

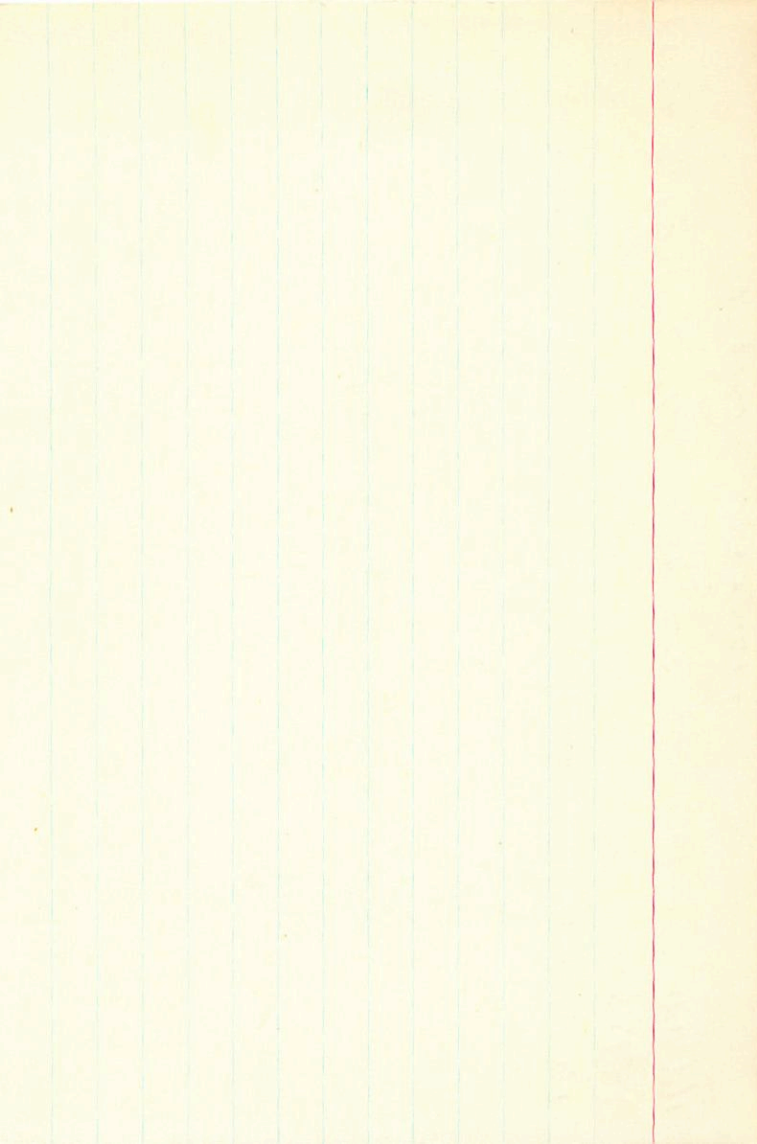
18 08.2 +09 19 5.7 9/12 +9.51

166460
24783

10626 10.337 1914.3 +3 18 46.26 1913.2
 $\frac{-050}{287}$

10.317 46.06 1933.3
 $\frac{9}{326}$
+5
46.11

10.304 46.22 1939.24
 $\frac{-4}{300}$
 $\frac{46.18}{46.14}$
 $\frac{25}{36.2}$
 $\frac{313}{+026}$
21.9
23.0
-16



AD51133

166464 18 08.7 -23 43 5-1 g 120 +4.46

+0011 52.6 -025 ±2.8
+0008 -031

24799

10631 40.196 1901.3 -23 42 47.50 1900.7

1502

-054
142

8.626

31.490

40.162

104

167

40.186

-16

170

+025

+1.23
46.27

44.60 1928.1

15.62

48.98

47.37

47.14

67.04

33.5

32.8

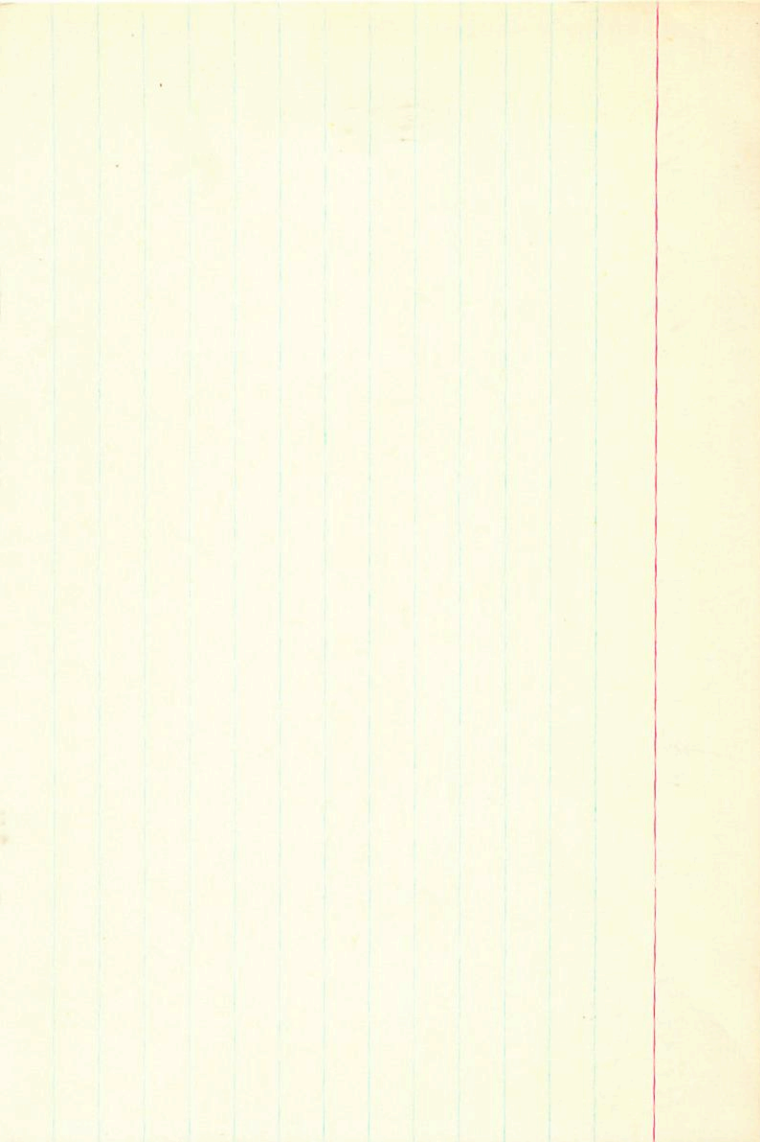
32.2

47.49 1938.93

-4

47.45

47.30 / -1.03



167027

18 09.2 +56 15 7.5 g 123 -52.38

24810

10642 9.432 1400.2 +56 15 17.52 1889.3

$$\begin{array}{r} -108 \\ \hline 324 \end{array}$$

$$\begin{array}{r} -2.06 \\ \hline 15.46 \end{array}$$

42.52

26.860

09.385

~~382~~ 390

9.390

1208

403

~~1089~~

9.400
23
403

~~39.6~~
~~35.6~~

52.1 1427.3

19.02

16.12

49

16.65

1444.62

16.91

-30

16.61

16.64

+1.18

11.9.31

39.8

50.6

7.92

36.4

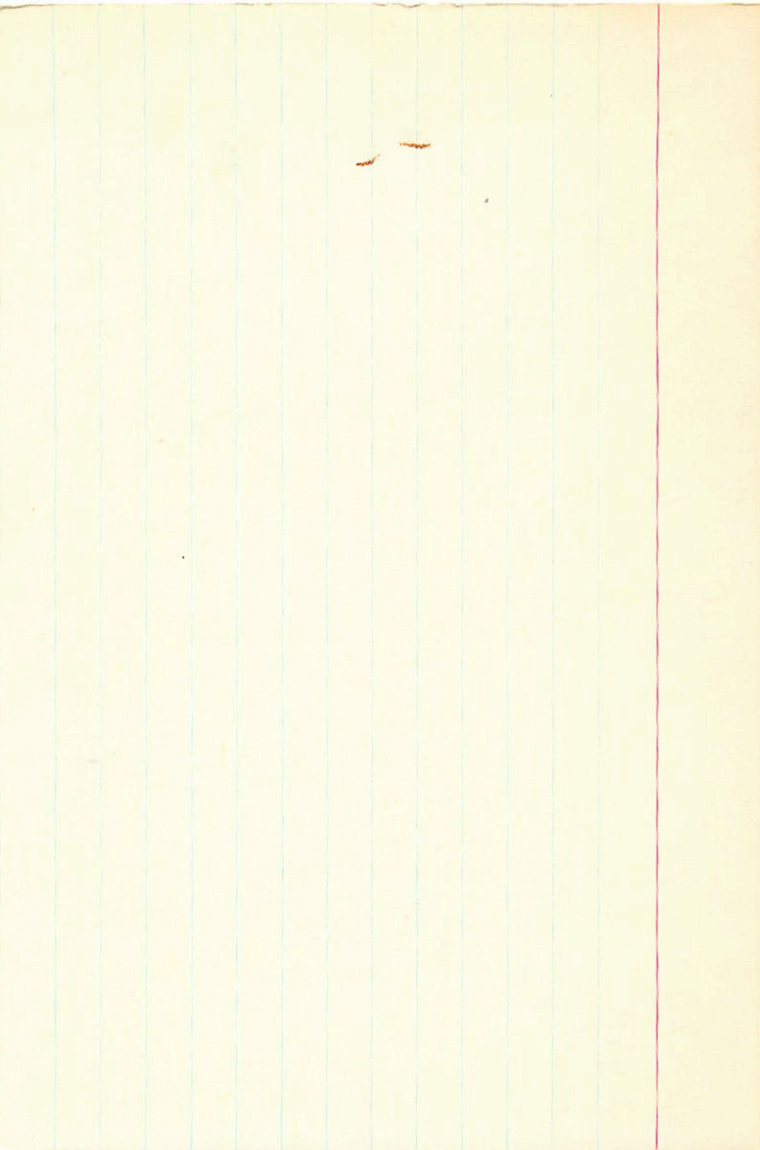
46.7

1447.34

17.13

-83

16.70



25,3640
G-140-46

15 800 405 24

③ 5.1 - 1.5 ③

R, 1001

.803 2210

10.43 0.73

-530 -6600

-532

NO

-600

515

-1.5

R.A. : 18.150
DEC. : 5.400
R.A. : -532.000
DEC. : -600.000
DISTANCE : 4.150
MODULUS : 68
VEL. : -1.500

q1 (U) : 0.101
q2 (U) : 0.563
q3 (U) : -0.820
dU : % -1855.857
U : -124.241

q1 (V) : 0.475
q2 (V) : 0.697
q3 (V) : 0.537
dV : % -3174.254
V : -215.412

q1 (W) : -0.874
q2 (W) : 0.444
q3 (W) : 0.197

104 Ha 18 10.0 431 33 943 -0.28

① 250

HR6815 474 4.74 +1.52

$$\begin{array}{r} 474 \\ 474 \\ \hline 2848 \\ 474 \\ \hline 9116 \\ 474 \\ \hline 2848 \\ 474 \\ \hline 9116 \end{array}$$

$$\begin{array}{r} -013 +019 GC \\ -017 +030 FR3 \\ \hline -015 +025 \end{array}$$

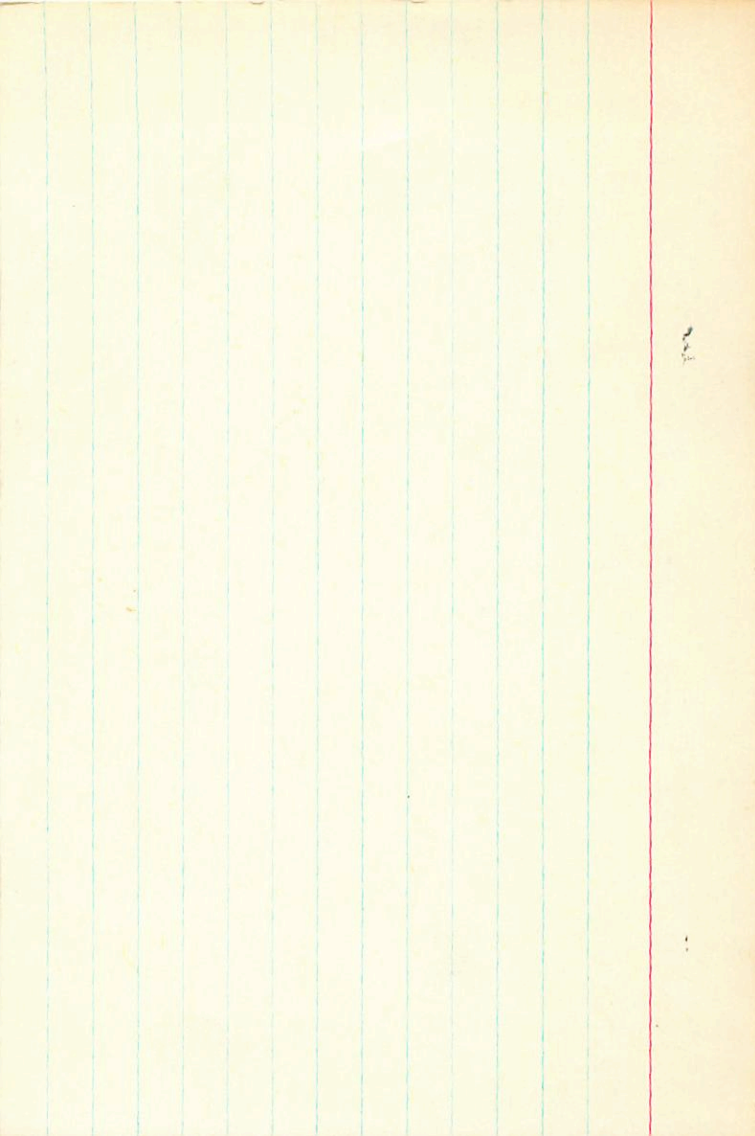
$$\begin{array}{r} -5011 \\ -5011 \\ \hline -10022 \end{array}$$

147

105 866-488
 473 388 791
 -875 314 368

$$\begin{array}{r} -0070 +1055 \\ -0343 +0473 \\ +0580 +0382 \end{array}$$

$$\begin{array}{r} +0985 +15.5 +0.2 \\ +0160 +2.5 -0.3 \\ +0962 +15.3 -0.1 \end{array}$$



6805

120

18 10.9 - 63 04

165599

24861

5.66 + 0.555 + 0.69 2F

0.25 + 0.81

797

747

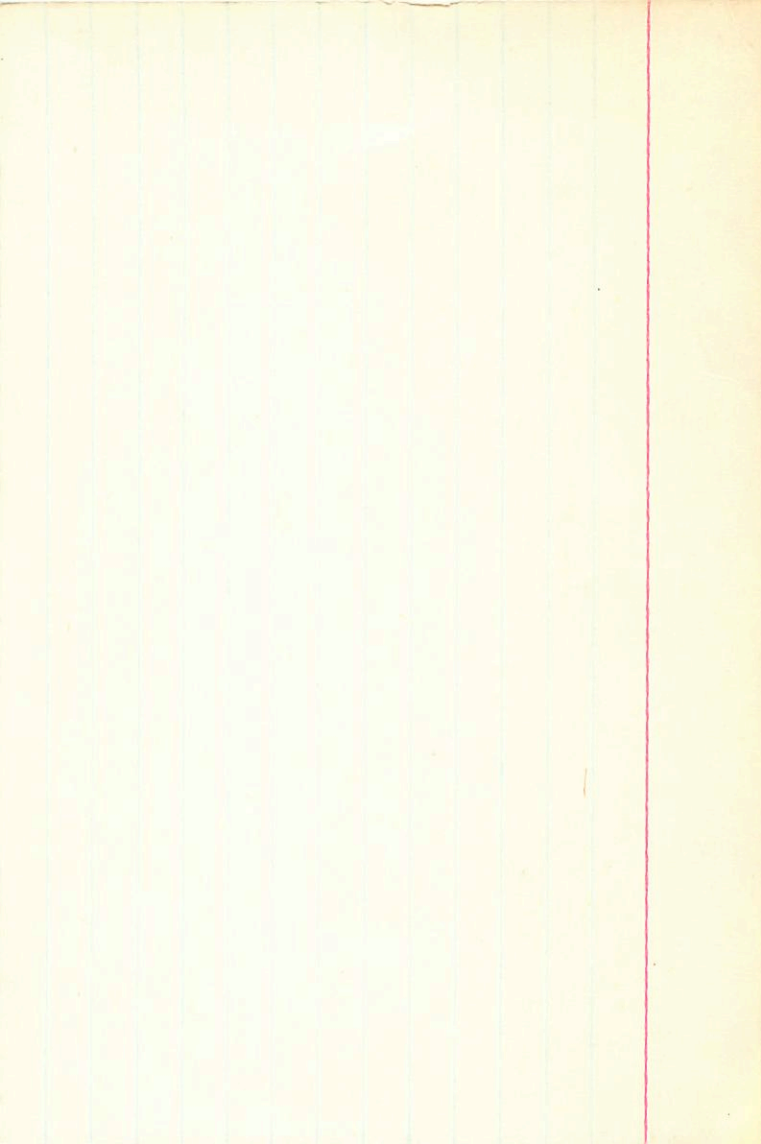
734

584

1156

11.28 + 0.485 + 0.035 2F

$\frac{4.0}{73}$



$$\begin{array}{r} -0033 \pm 3.8 \\ -0049 \\ \hline \end{array}$$

166599 18 10.9 -63 04 5.6 110 -6.56

24861

10677 55.927 1906.5 -63 4 16.52 1502.0

$$\frac{147}{171}$$

$$\begin{array}{r} -0041 \\ -029 \\ \hline \end{array}$$

$$\frac{1.68}{14.84}$$

56.071

$$\boxed{-0027 -024}$$

$$\frac{1.68}{14.84}$$

55.878

-016

15.44 1940.04

$$\frac{44}{829}$$

$$\frac{12}{15.56}$$

36.4

15.7 1945.7

155.83

$$\frac{10}{16.10}$$

5.74

$$\frac{119}{824}$$

$$\frac{42.9}{15.83}$$

42.9

40.9

$$\frac{99}{1.99}$$

-177

288 po.

105 -555 -825
473 758 449
-875 343 -342

-0090 +0632
-0403 +0862
+0746 -0390

+0542 +15.6 +5.3
-1265 -36.4 +2.9
+0356 +103 +22

+21
-34
+12

V725 Sp

105, 489

13 Aug

H6 166

115 510

n ep. 12 vi + 1.3 (18 Aug)
18 10 35 - 36 07 (22)

CBS

-32010943

14

5-5

53

-33

00

9.10

-14

Card #
167193

+0042±5.6
+0041

+046±4.6
+039

9.315 1900.0 +21 51 52.64 1895.2

$\begin{array}{r} -210 \\ \hline 9.105 \end{array}$

$\begin{array}{r} -2.52 \\ \hline 50.17 \end{array}$

$\begin{array}{r} 9.237 \\ \hline 9.027 \end{array}$

51.44 1933.9
 $\begin{array}{r} 9 \\ \hline 51.53 \end{array}$

$\begin{array}{r} 9.229 \\ \hline 9.029 \end{array}$
 $\begin{array}{r} 231 \\ \hline 234 \\ \hline +129 \end{array}$

31.2

51.83 1928.44
 $\begin{array}{r} 24 \\ \hline 51.59 \end{array}$
 $\begin{array}{r} 42.34 \\ \hline 81.2 \\ \hline 34.0 \end{array}$
 $\begin{array}{r} 51.54 \\ \hline 11.39 \end{array}$

10682
24868

18

11.1 44 08

150 - 48.2

167304
167304

AB
167304
167304

6.35 + 104 + 0.98

~~014 - 052 Gc~~
~~- 2 +~~
~~027 - 045~~

8m 2"

-0110 -037

-011 -037

~~0017 - 011 Gc~~
~~- 0017 - 050 Gc~~

~~0017 - 30~~
~~0019 - 0025~~

+0006 ± 5.7

-0019

3.8 (9 190107

14.45 - 1886.2

4974 - 12848 } 035

-0010 - 037

-012 - 027

-6702 - 7807

3755 480

2

14592
16.7036
24871
10684

18

-0007 ± 2.8 -027 ± 2.9
-0013 -039
11.3 -21 44

5.7 g 123 -58.98

15.613 1901.5 -21 43 42.02 1900.4

034
647

+1.33
40.99

45481
30125
15.606
607
-3
603

35.6

4.95 1930.32

21.32

~~43.63~~
164

41.99
+18

42.04
-1.05

11.19

37.1

36.2

41.81

42.00

1939.65

-4
42.04

42.27

1941.22

51.81
932
49
42.224

39.576
36051
15629
21/605

15.608
-16
592
-047

14 03413

167277

18

11.7

+14

24

7.86 102

-22.2 ③

-035 -041 ⁶Y

-034 -039

-043 -026 AG103

-037 -034 Y →

-041 -029

-22.2

-038 -029

96
10/10

-0026-018 Cambridge

38
-18

7.1

22.2

-030 -018




3

R.A. : 18.200
DEC. : 16.400
R.A. : -38.000
DEC. : -18.000
DISTANCE : 7.100
MODULUS : 263
VEL. : -22.200

q1 (U) : 0.113
q2 (U) : 0.709
q3 (U) : -0.696
dU : -79.940
U : -5.570

q1 (V) : 0.468
q2 (V) : 0.580
q3 (V) : 0.666
dV : -130.439
V : -49.103

q1 (W) : -0.876
q2 (W) : 0.401
q3 (W) : 0.267
dW : 117.183
W : 24.898



36.5

168151 18 13.6 +64 23 5.0 dF3 -35.3a

24916

10727

-33.79

⁴⁹+0530 +035 50 N30

+0527 ± 1.1 +036 ± 1.0 GC → N30

47 ± 6

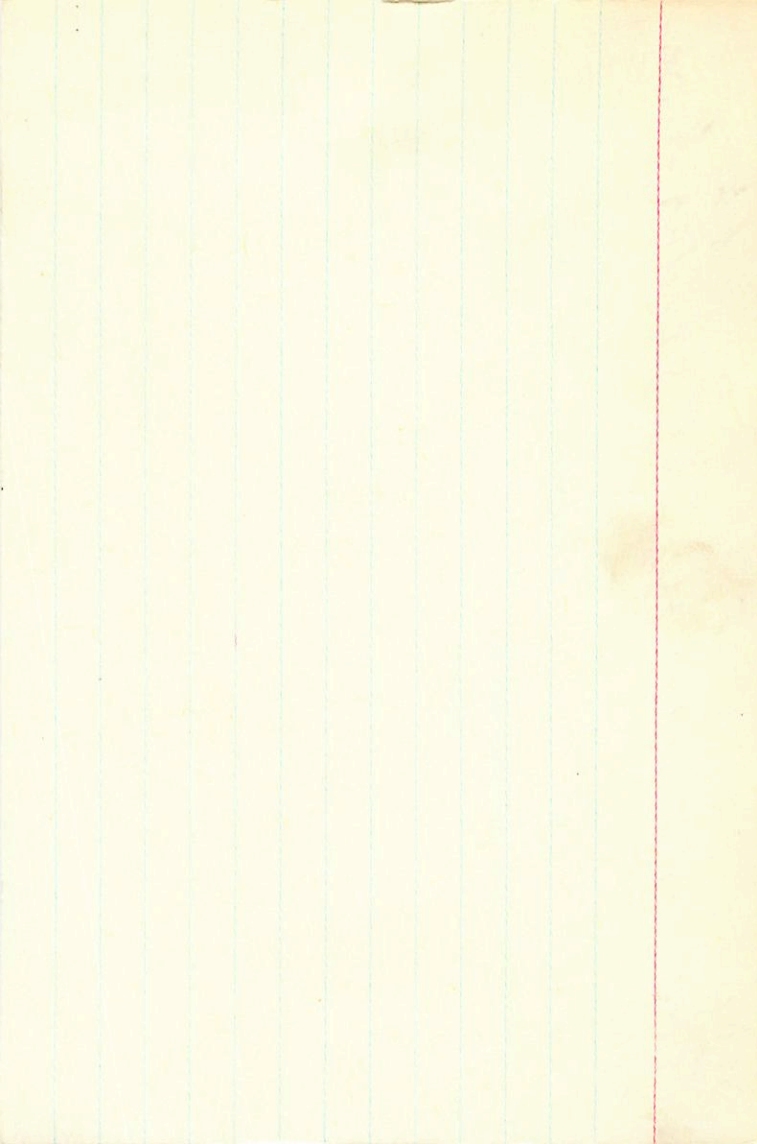
1589

4

287 143 49 → 2633

471 449

—



1065 + A5

17 Sep
167570
24918

18 13.6

+0009 ± 2.8
-0001
-20

34 3.17
962 - 16.176

-9603

10728

36.584 1400.9 -20 83 46.22 1401.7

-044
540

+87
4535

7.162
29.340

13.98 1434.16
24.50

36.520
+8
630

47.78
162

35.0

3.08
36.5

36.559
-16
543
534
-004

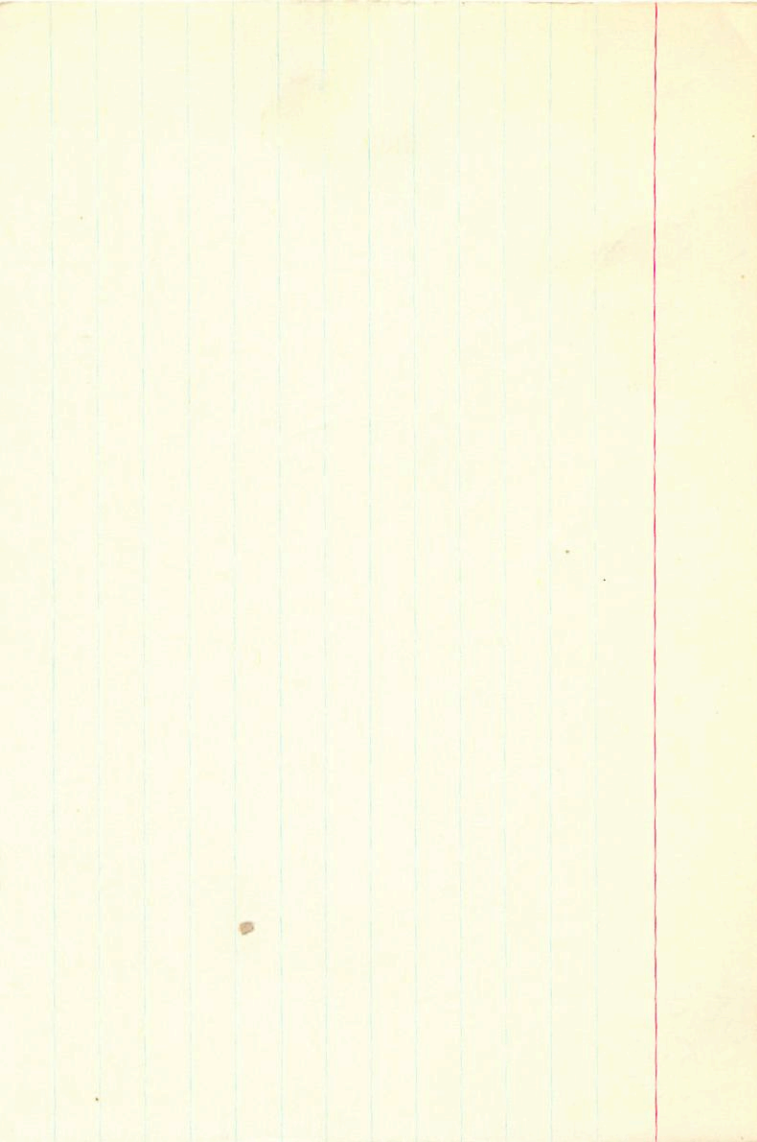
45.88
45.88

33.4

45.79
45.79

45.79
45.84
-49

1429.92



167965

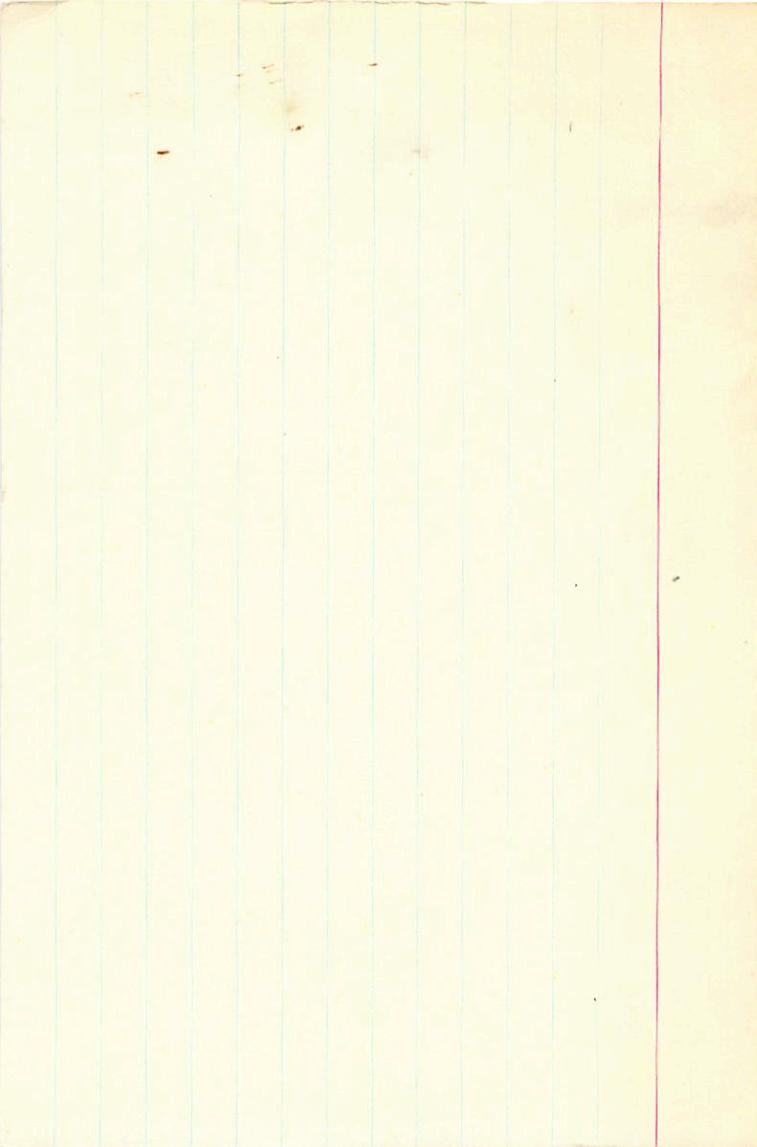
18 14.1 +42 08 5.4 B8M-20.5a

24936

-0006⁵⁴ +002⁶⁰ N30

10734

-0010±1.5 -001±1.4 66-#30



6848

1.5

1.21

442 09

104

5.58-12-46

5.46

(5.45)

-20.5

1000's
1000's
1000's

1000's
1000's
1000's

15

4274
1006

4



5845.000*

18.000*

14.100*

42.000*

9.000*

-0.000*

-0.004*

6.450*

194.984

-20.500

-0.011

-0.318 -62

4.341

AD 39" Jm Hemb 5036. AL
AL 94" AL

AS 39" Jm Hemb 5036. AL
AL 94" AL

167607
1676690

RS Eng 18 14.3 -34 08 V = + 8.0

-0014 ± 8.7 -013 ± 8.7

75.5 Debit
710.4 Debit

17.23 1899.5

~~570~~
17.23

-6008 -006

37.945

4.92

39.435

2760

17.380

37.32

389

33.90

377

33.413

33.1

33.1

1521.26

Al. d

260

4013-008

123	-084	-989	-6035	+6024	-00.11	-0.3	-2.9	-8
462	887	-017	-0131	-0252	-0383	-11.5	0	-12
-878	455	-148	+0249	-0129	+0120	+3.6	-1.2	+2

$$0.154 = \frac{32.7}{(x+3.2)^2}$$

390

$$(x+3.2)^2 = 214.255$$

$$x+3.2 = \sqrt{214.255} \approx 14.6$$

$$x = 14.6 - 3.2 = 11.4$$

30000
+ 1004
- 6000 = 1004
+ 1004 = 2008
- 1004 = 1004

5

	18.	250
-	34.	100
	16.	000
-	8.	000
	7.	550
		324
	8.	000
	0.	124
-	0.	005
-	0.	989
	11.	021
-	4.	343
	0.	462
	0.	007
-	0.	019
-	4.	591
-	1.	005
	0.	870
	0.	455
-	0.	149
-	72.	383
-	24.	617

K