

41.5
50.5
2.95

+12.5
2.1

130945
142.5
144
19
dFY

HR5533

5.7

G-19954

34800

-24
-00045
44
-0830
GG+

00071
-0786
+2.0

-0073
-004
-025

-4.76

313
316
114
441
2 SPL
2.6603

316

cut

225 + 8

428
86
54

+2.45

371pa. -9.9 -10.6 -0.5
-278 -225 +95 -078
-0005 = -004

5533.000+

14.600*

47.500*

45.000*

19.000*

-0.000+

-0.075*

275 2.800*

35.5 35.300

-4.700

-0.270

-0.087

101 -0.300

-0.212

0.493

106 -10.029

0.094

0.866

0.4

-004 -084

-4.78

5533 14 47.5 +46 19

1883.2

-084 ± 1.7

-082

25.22

1885.1

31.697

026

923

5.61

83

-0005 -078

-005

31.668

21

689

434

034

25.41

1452.72

-30

25.11

5.72

-9.9

-2780 -10.3 +0.4

+0144 -2924

-0157 -2089

+0104 +0873

-092 459

565 867

-605 791 -092

-438 -236

-10.6

-2246 -8.3 -2.3

+0873

+0977

+3.6 -41

-9.9

-10.6

-0.5



130551

14

47.6 -60 44

+324 80.4 C₂(G)

1996²

7.17 +0.42 FFR C₂

Case num
+056 +107

-39 -6 +14 1024

+0069573 +102±6.0
 +0084 +098
 +056 +107 +32.1 - 083 - 25 246
 -668-745 -873 488
 037

36.833 1907.6 -60 43 36.27 1902.5

$$\begin{array}{r} 293 \\ \hline 1540 \end{array}$$

$$\begin{array}{r} 40.368 \\ 56.080 \end{array}$$

$$\begin{array}{r} 36.448 \\ 2723 \\ \hline 728 \end{array}$$

$$\begin{array}{r} 728 \\ \hline 711 \end{array}$$

$$\begin{array}{r} 36.859 \\ \hline 821 \end{array}$$

29.9

$$-481$$

$$\begin{array}{r} 41.08 \end{array}$$

$$23.43 \quad 1928.76$$

$$-15.80$$

$$\begin{array}{r} 34.73 \\ \hline 1411 \end{array}$$

$$\begin{array}{r} 38.322 \end{array}$$

$$\begin{array}{r} 38.153 \end{array}$$

$$\begin{array}{r} 36.2 \\ \hline 43 \end{array}$$

$$\begin{array}{r} 36.83 \end{array}$$

$$\begin{array}{r} 1536 \\ \hline 37.68 \end{array}$$

$$\begin{array}{r} 37.68 \\ \hline +340 \end{array}$$

$$1444.1$$

$$\begin{array}{r} 7486 \\ \hline 37.4 \end{array}$$

$$\begin{array}{r} 34.0 \end{array}$$

SB

HR5532 14 47.8 +28 49 -3d

$$5.60 + 0.05 + 0.08 + 0.37 + 0.21 = 6.31$$

$$\frac{+0.13 + 0.06}{N}$$

$$\frac{+0.24 + 0.06}{F}$$

$$\frac{+0.19 + 0.06}{N}$$

482 574

230871

14 47.9 107 01

+7.2850

906 545 507 231 (1)

909 553

1059405

+0012 ± 3.8
+0022

000 ± 3.1
-005

131040 14 47.9 + 51 35 6.4 dFY - 5.18 5B
19969 16" 9.9 dG7 - 290 50

7017

84.885
- 056

82.7

+51 34 50.57 1898.8

HR 5537

(38.0)

6.18
48.655

54.839

43.6
13.7

49.61

1926.4

50.476
- 50.10

50.30

50.23
- 34

166
35.5

843 34
54.889 27 911
- 848

1084

50.35 1945.26
- 19

50.16

1895
3916

54.889
+ 14

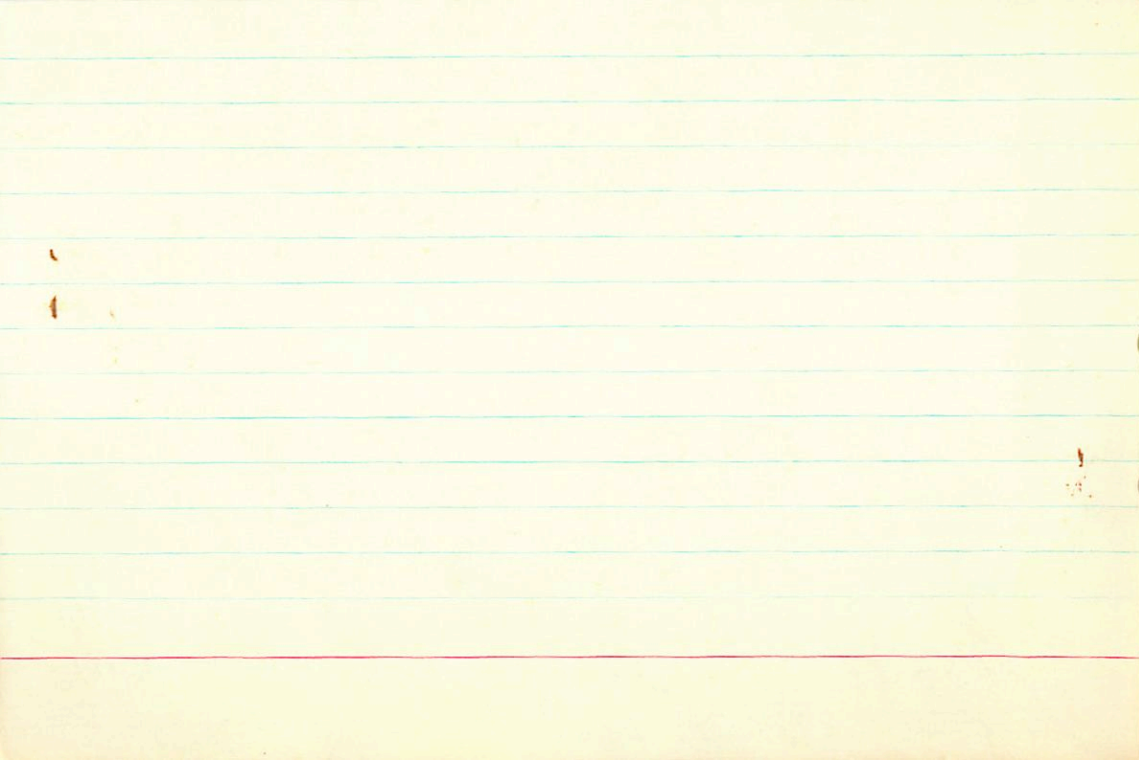
50.3

50.83 1947.29
- 16

50.67

(40.8)

50.38
- 19



5520

14 48.2

- 72 59

5.59 GC

+ 38d

+030 +022 GC

+7

+4

+028

+037

! ! !

! ! !

2

5520.000*

14.000*

48.200*

-72.000*

-59.000*

0.037*

0.028*

5.000*

100.000

38.000

-0.168

-0.648

-41.375

0.137

-0.731

-14.041

0.038

-0.215

-4.328

2

o Imp
130807

14977

8625

-0020 + 3.7
-0033
-032

14 48.4 -43

22 4.5

86 +7.0846

+7.421.1

4.32 -12

$\frac{-0026}{+9}$
 $\frac{-032}{+10}$

$\Delta m = 0.2$ " 0.13

+10 684

$S_{(10)}$

21.904 1904.9

-43 22 11.30

1896.9

$\frac{090}{994}$

$\frac{-0017 - 0.22}{9.53}$

$\frac{1.75}{9.53}$

42.7

21.874

10.94 1940.42

95.21

$\frac{-16}{88}$
 $\frac{853}{141}$

$\frac{-14}{110}$

47.6

21.857

16.98

1954.79

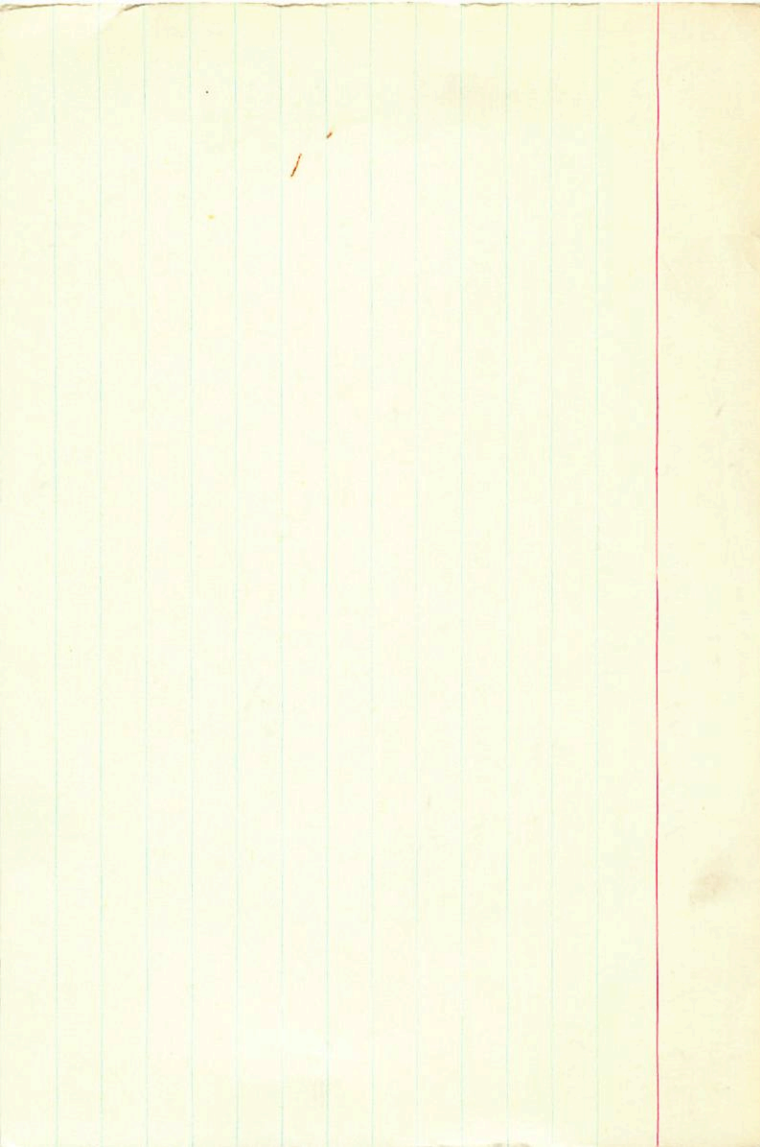
$\frac{-22}{11.20}$
 $\frac{11.11}{1.60}$

-22

11.11

-1.60

50.7



AD99410

-0153 ± 6.3 +041 ± 3.6

131023

14 48.6 +09 56 7.4 dG5 -35.68

19983

9629

37.077 1897.5 +9 55 40.81 1878.9

863
880

150
855
625

-2.92
37.89

853
62

37.329
27

-0147 +046

40.97 1934.4

356
524

-0 +050
-217.1

-24
40.73

6.4
2.8
4.6

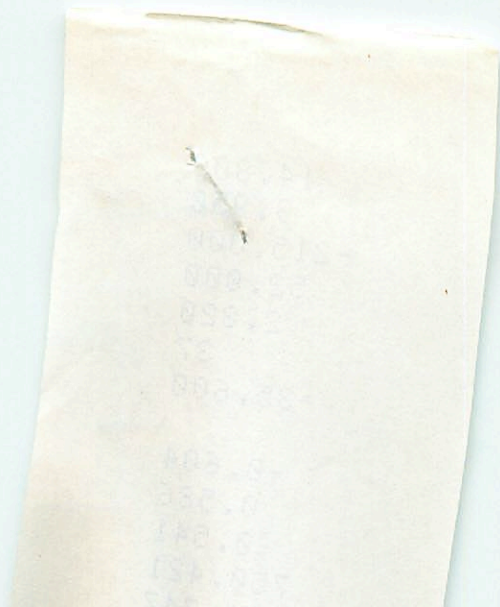
-215 +051

210 +57

AG112

-212 +52

3



14.800
9.950
-215.000
52.000
2.820
37
-35.600

-0.604
0.586
-0.541
750.421
747

130989 14 48.8 -17 35 dFS

GC19585

6.50 +0.46 -0.04 C

.316 .143 .468 2.632 @ 3, 4, 10, 17

[m] 202

[k] 405

380 -26 -33 -5
-1 -4 -4
148
-176
-23
-25
3.8
+25.8

-0.22-125

49888 974 -1019
-1014 32.5
-1016
-127
-137
6074 96.6

$\frac{73}{948}$

$\frac{+213}{5361}$

3

46824

4818

2.61-

$\frac{+11}{835}$

$\frac{-14}{291}$

46805

70.35

3.25

$\frac{+2}{812}$

-1016 -131

$\frac{-30}{3.55}$

-128

-6229



47.64

0.21

+3.11

-24.0

14.800
-17.600
-23.000
-125.000
3.850
59
25.800

-0.604
0.269
-0.750
-96.802
-25.858

130959
19985

616
58

14 48.5

-0014+2.5
-0012
-132+2.5
-126

8630

-17 35

6.7 d.f.s +25.88

10/30

6.52 +0.455 +1.59 2 244

46.825 1897.5 -17 35 0.74 18940
073 +7.13

25

1898 -003 -129

44

59.7

22.947 -0176

34

53.61

-0176

46.10

100000

23.888

+258

13.30

1937.49

-017-123

34

59.90

104

58.96

2699

53/4

850

(411)

-078

59.25

59.00

-539

46.847

13.700

0

3356858

+617/849

59.44

1940.90

20

0

30.54 32.7

54

+17/59.28

13.1131

1541.44





5



1000 1000

1000 1000

1000 1000

1000 1000

1000
1000

130989.000*

14.000*
48.800*
-17.000*
-35.000*
-0.018*
-0.123*
3.400*
063

0207
248

225

24

-0009 ± 3.0
-0009

-0008 ± 2.9
-010

10 Lit

131027 14 49.0 -18 09 6.8 967 -21.98
19990

8633 2.668 1901.6 -18 9 1.73 1599.7

$\frac{+40}{1.33}$

38.548
24.090
2.638
6.99
6.94

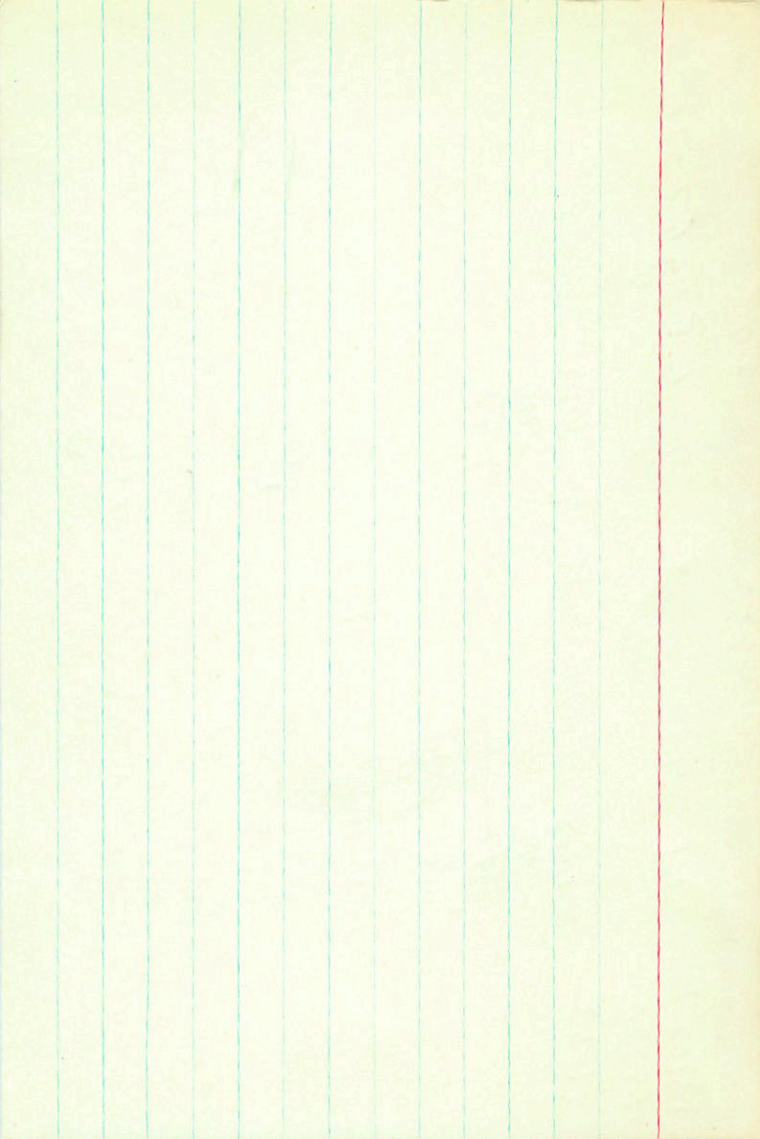
1.77
31.8

49.81 1627.14
12.92

6.88
694
-0.24

66.86
33.4
33.7

1.76 1939.72
1.66
-1.33



130932 14 49.0 -46 33 6.84 +1.64 M311F +13.4

GC19489

+ 0011 -016 Step 1955

-0046 -035

+0004 ±10.6 -030 ±7.5

2.174 1902.4 14.57 / 896.9

019 / 155

-0021 -033

1.59

-0011 -023

17.98

21.796

6.89 1924.23

40.265 / -122.

13.822

202.4 -112

2.024

12.9

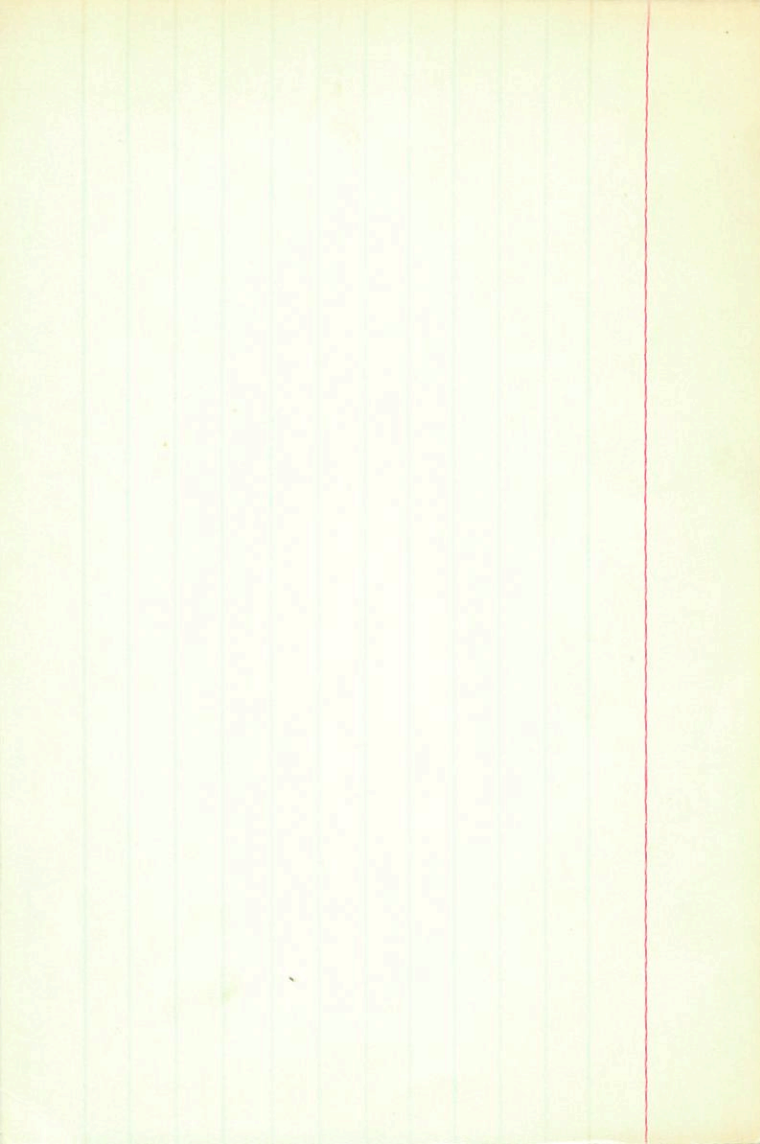
0.35

18.13

0.12

19.10

0.33



733

14 49^m.4

- 45° 23'

#D 130997

+9.13

+1.09

+2.12

KO 10

- 600

- 114

- 792

+ 665

+ 480

- 573

- 445

+ 870

+ 212

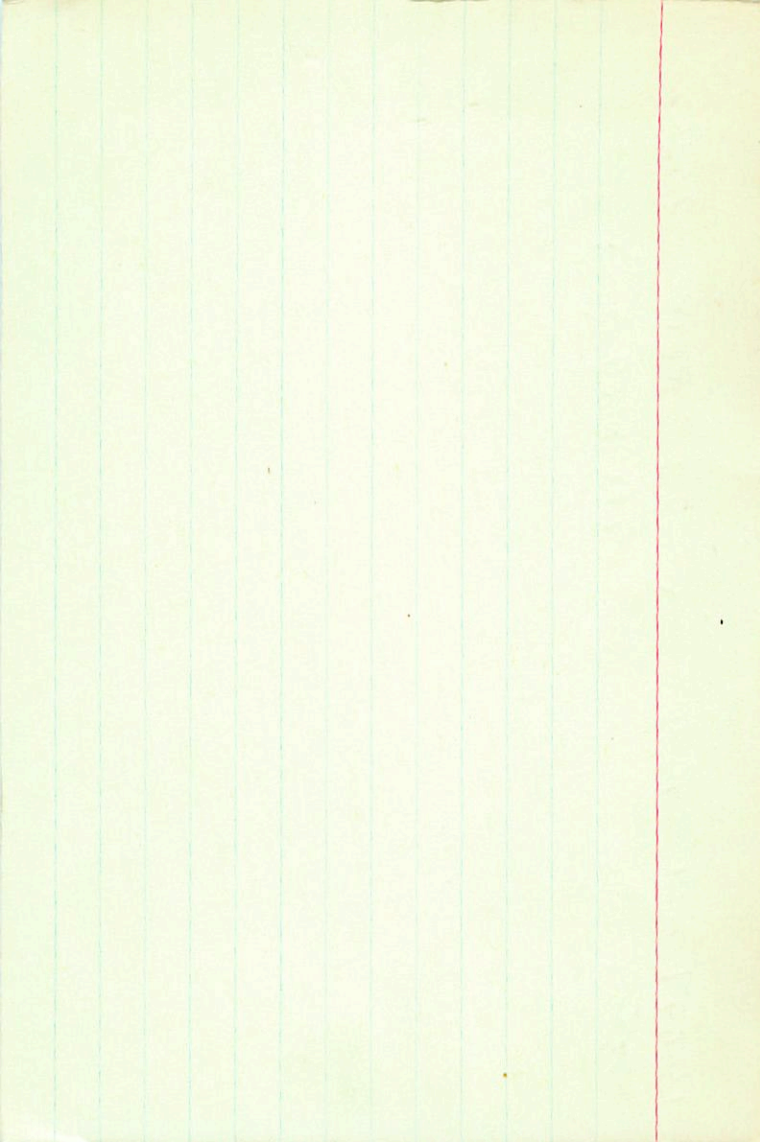
130997 · 14 49.4 -45 23 $\sqrt{1012}$ -2.9 ± 1.2

~~782~~

9.13 + 1.09 (2.12)

S
- 6003 foil CP

3(5)



131078

20001

10.3 0.71

14 44.7

-0032 ± 8.3 -209 ± 7.5
 -0062 -185

-46 26

65

-17.1 ± 0.5

C₂(5)

8.15 + 70

43.634

1900.7

-46

25

51.74

15980

158

43.792

10.87

40.87

43.458

-13

445

47

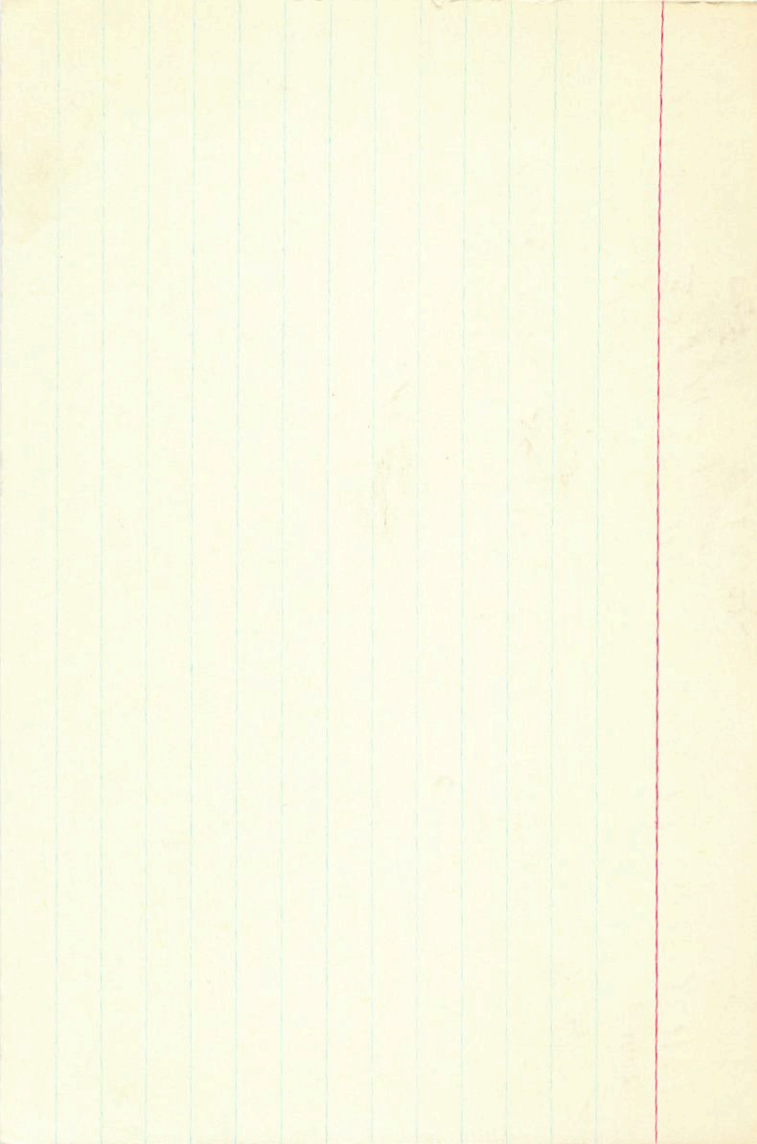
3

51.39

1956.22

-23

51.62



13/10/20

54

46.9

468 10

468.80

-0029 ± 3.8
-0017

-020 ± 3.1

-020

131120 14 49.7 -37 36 5.1 88 +5.47

20000

8640 42.244 1910.5 -37 35 55.25 1907.2

$\frac{115}{1359}$

+0.86

36.7

54.39

42.810

55.03 1939.60

$\frac{-8}{302}$

-14

55.17

94.32

$\frac{290}{-003}$

55.42

47.2

1.03

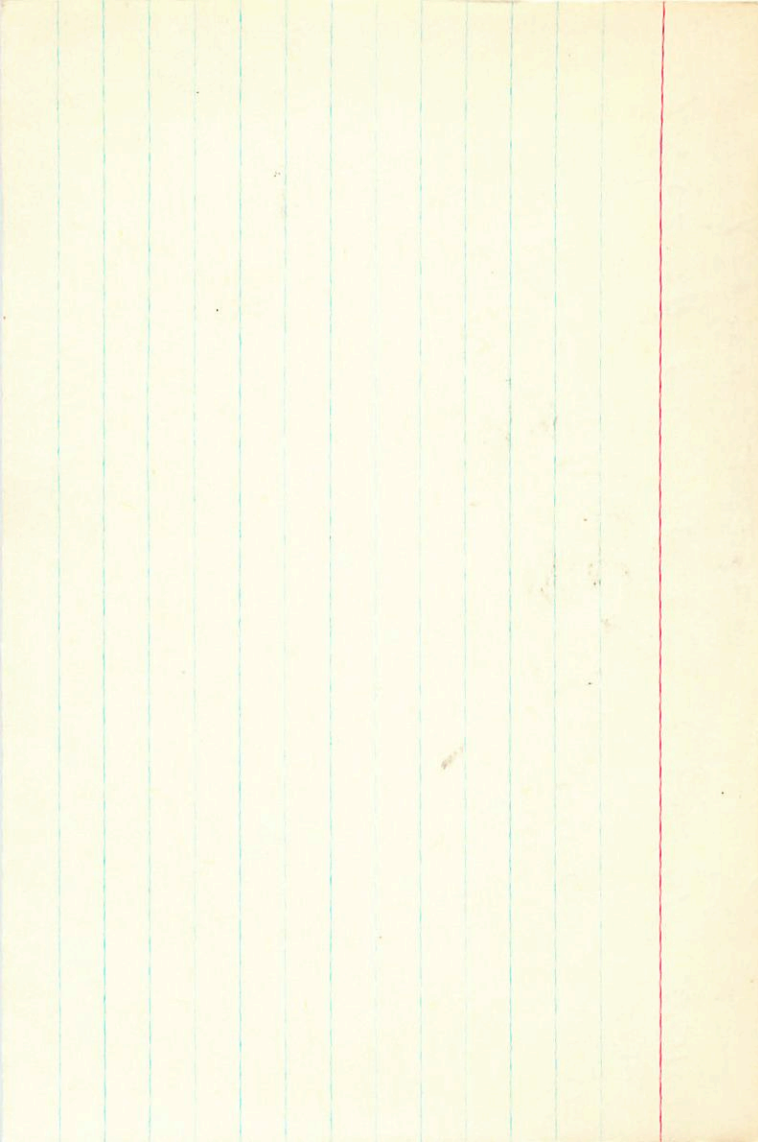
2.58

70.8

42.292
 $\frac{-2}{290}$

55.45
 $\frac{-22}{55.68}$

19854.72



AD594207-902"

131265

14

49.8

+20

30

6-9

A2

-1.78

20005

8641

50.481

1898.1

+20

29

41.13

1899.7

$\frac{-6}{475}$

+1.11

$\frac{42.24}{}$

50.492

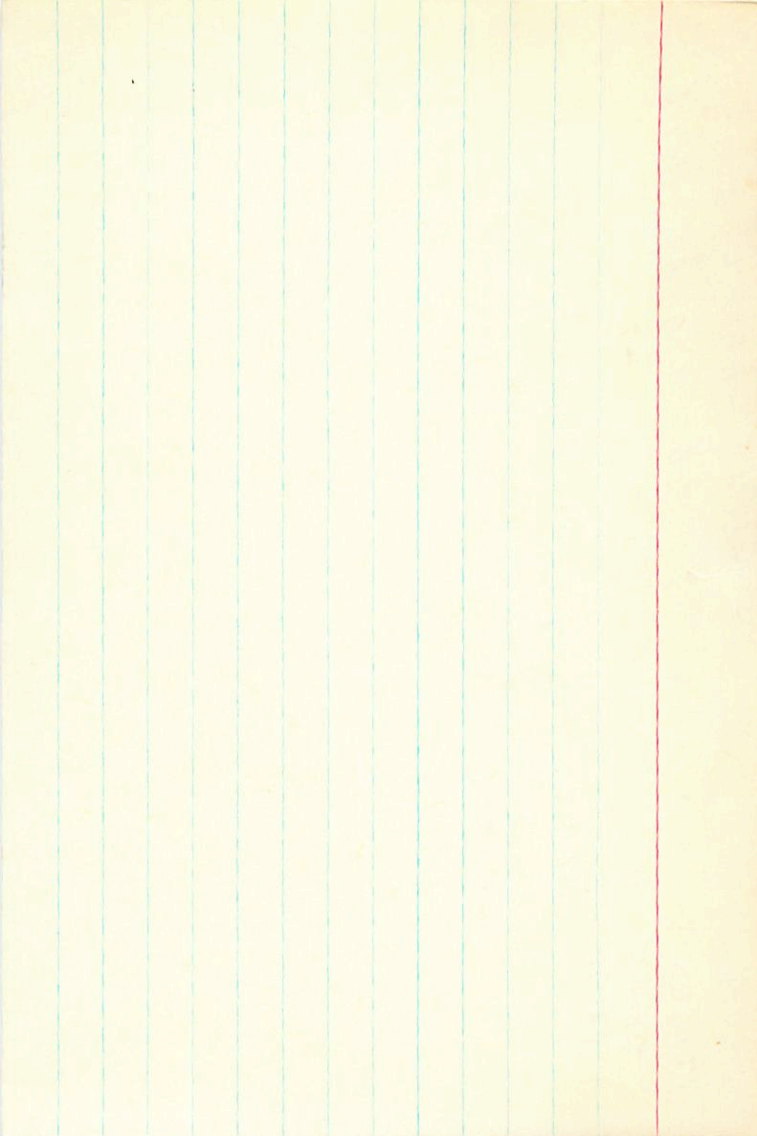
$\frac{-19}{1511}$

41.93

1933.5

0

+0001 54.8 -022±4.9



1002914

14 49.9 -66 12

602
701 #35

130940

2884

~~-253 -186~~

4
3 43

1.376

~~-0455 -204 62 +~~

~~-04525 -198~~

~~-274~~

~~-276 -196~~

(NO)

7.75
44

-0.28 44.1

→ 7.01 +0.595 +0.02

7.00 370 148 406
4.5 3.1

(59) (332)

Value (2.107)

9865 -8570
-3508 -5153

338 3375

+013 +0258

+1.7 +3.2

Σ min 0.65

0376 0375

2.12 2.13

-099357
-207687

55692 33
-1465
-6492
-127
51.71 2.4

2068
37.760
-0755-209
41.56
+985

5565
+01
1240
458
-12-
47.5

1240
5565
458
41.56

55844
-7
1240
variable

55844
-7
1240
487
+7
47.17

130940

14 49.9 -66 13

20007

-0443 ± 8.7 -207 ± 8.7

55642 33 -0489 -185 5741 2.4

2069

-0969 200

985

55761

-0518 -178

4156

250

448.55

42.26

4.877

488.81

2242

56073

388

564620

44

3485

12.121

54.16

1.58

4590

4612

4612

858

472.5

47.5

47.5

10

640

9242

-8477

-5305

-24

4847

44.8

-74

80.50

-185

-0492

-0484

-1742

-246

3460

4880

410354

2.05

127242

32

(2.43)

283

256

1820

327

50.2

32

142

385

32

(2.43)

283

256

1820

327

50.2

32

142

w(2)

14 50.2 + 18 56 460 - 47.68

HD 131334

GL 20013

+ 1902874

41 3363

W 8643

3M(17)

AD 5943 10⁻²
12¹⁵

8.25 + 0.62 + 0.04602

S = .11

- 0.21 + 193 GC

-676 -737 324 546 -001+153 -426 062 -15 868
-014 042-016-046 15² 275⁻ +33 +30 021

4 39 13
19 -20 20
-35 -7 12

4 41 17

20-21 27

-37-8 17

+40 +44 +26
+55 +15 -30

+42 +47 +36

+62 +6 -28

017

131334
CC20013
W8643

ADS9423 $0m=1.72''$

Y3363 $ab=10^{-8.0}$

+1502874

14 50.2 +18 56 d60 -47.68w(13)

8.29 +0.62 +0.04 C-0.2 R

$\delta = .11$

-0.21 +~~93~~ 6c

+44 +12 -32 .030

5[±]12 u(7)

-0015759 +193759

11.882 1594.2

076

958

+18 56 25.59 1594.2

9.80

35.39

3 U mi 131873 14

HR 5563 20029

8640

20029

98 92WB + 0.1

-0086 + 010 N30

-0086 + 06 + 005 + 066C 7K30

5-0.8

774 22

15 VIII

2.00

+1.98 H

(15)

+17.2

(28)

+17.3

+16.9 a

-034 + 009

-032 + 007 6C

-035 + 010 N30

-034 + 0.009

AD99425

13473

20032

8647

AD20.5

119

-0017 ± 6.3
-0016

14 51.0 + 15 54

000 ± 5.5
+ 0.26

6.8 dF9 + 20.88

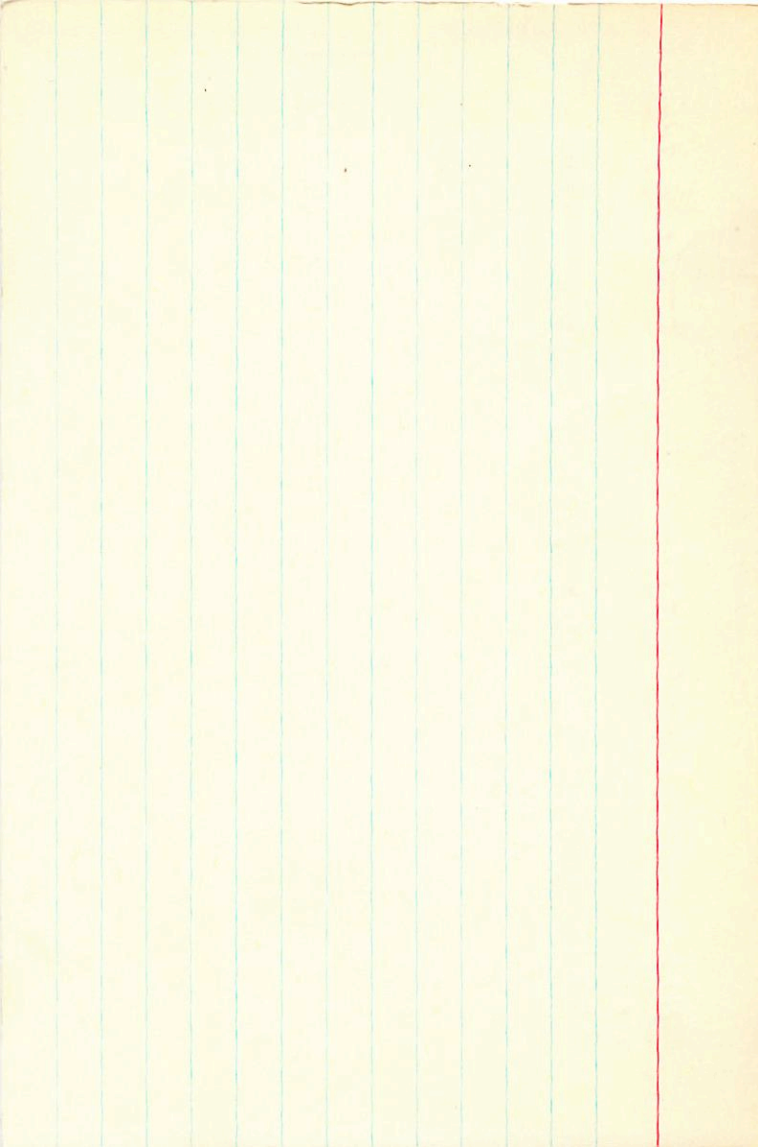
2.578
092
1.670

2.590
19
609

2.578 1895.6 + 15 54 27.40 1892.5

28.55
4
1934.6
28.49

-0017 ± 0.18



-0008 ± 2.3 -036 ± 2.3 +0.4 W
-0009 -036

12/14
131430 14 51.4 26 5.4 122 +8.88

20047 5.22 +1.35 +2.43 1m 24"

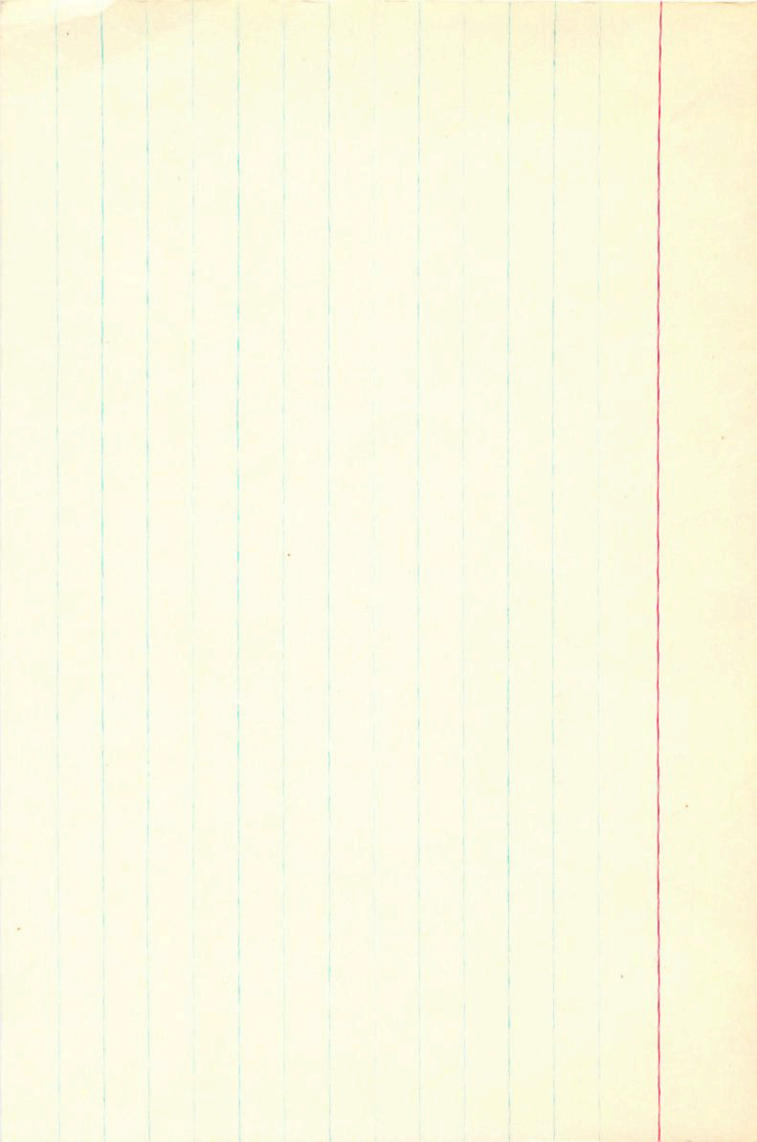
25.510 1901.1 -24 26 20.40 1889.9
 $\frac{039}{549}$
 $\frac{+1.80}{18.60}$

58.423 11.12 1429.15
27.028 9.50
 $\frac{25.455}{516}$

519 201.09
 $\frac{519}{-030}$ 33.0
522 19.53 3961 4824

25.527 19.39 1939.09 34.1
 $\frac{-11}{514}$ 20.00 20.25 34.2

$\frac{19.82}{-1.22}$



RAPS

131109

14 52.1 -76 28 5.4 M0 -31.2-8

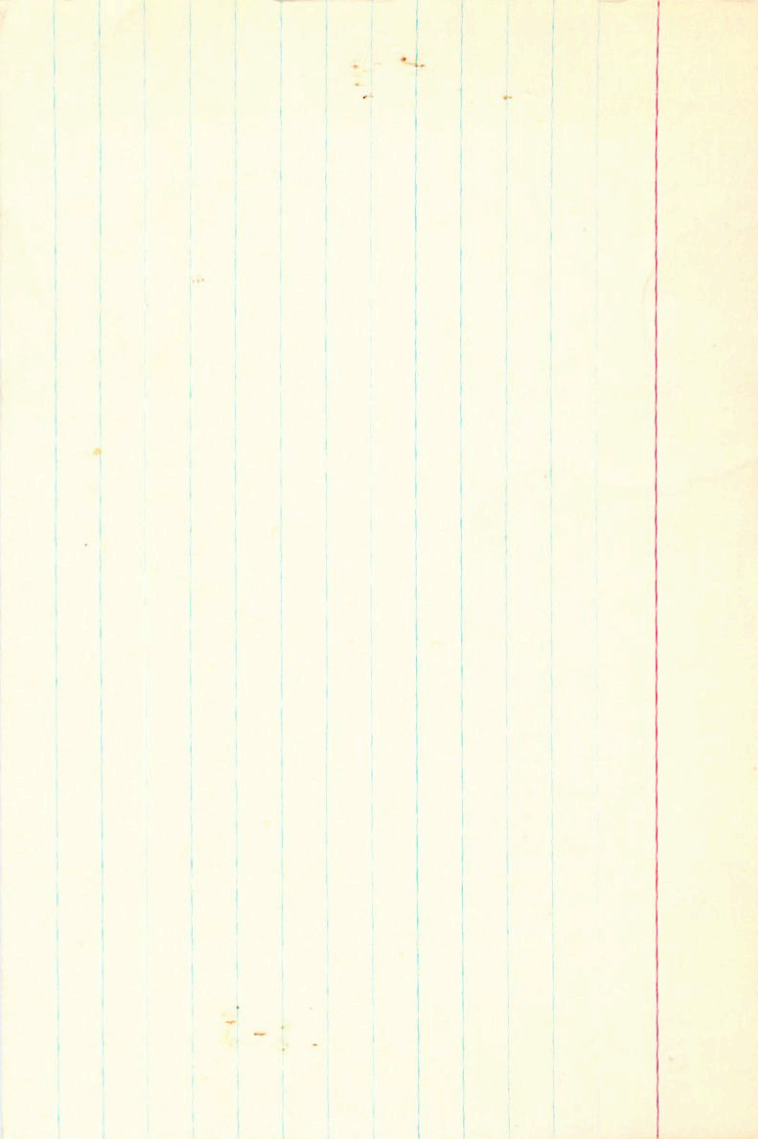
20057

14 14

8654

-0204 -015 N30

-0204±4.9 -018±3.6 LL → N30



8359 47

14 53 -47 41 -2(3)

-6005 -030 step

-0307 -0254

-0310
-032 -0224

133002

14 53.6

+82

4.3

of 60

-43.06

-4400 -438
+444

GC20087

w8660

Y3393

+830431

5.72 +0.60 Sears

+0867 73 -229 79 N30

+0857 ± 1.4 -229 ± 1.5 6c 2070

-85 -12 -4 .018

-78 -14 -5 .020

-67 -21 -12 .025

+164 -230 6c

+165 -229 N30

+165 -230

26A(29)

-9M(17)

26(16)

16 ± 4

-697 -727 992 127 +165 -230 -1308-226-43-137
113 -157 -120 166 -251 -1312 -5.5 +4 +4

-8 -60 -49 0205

-75	-13	-6
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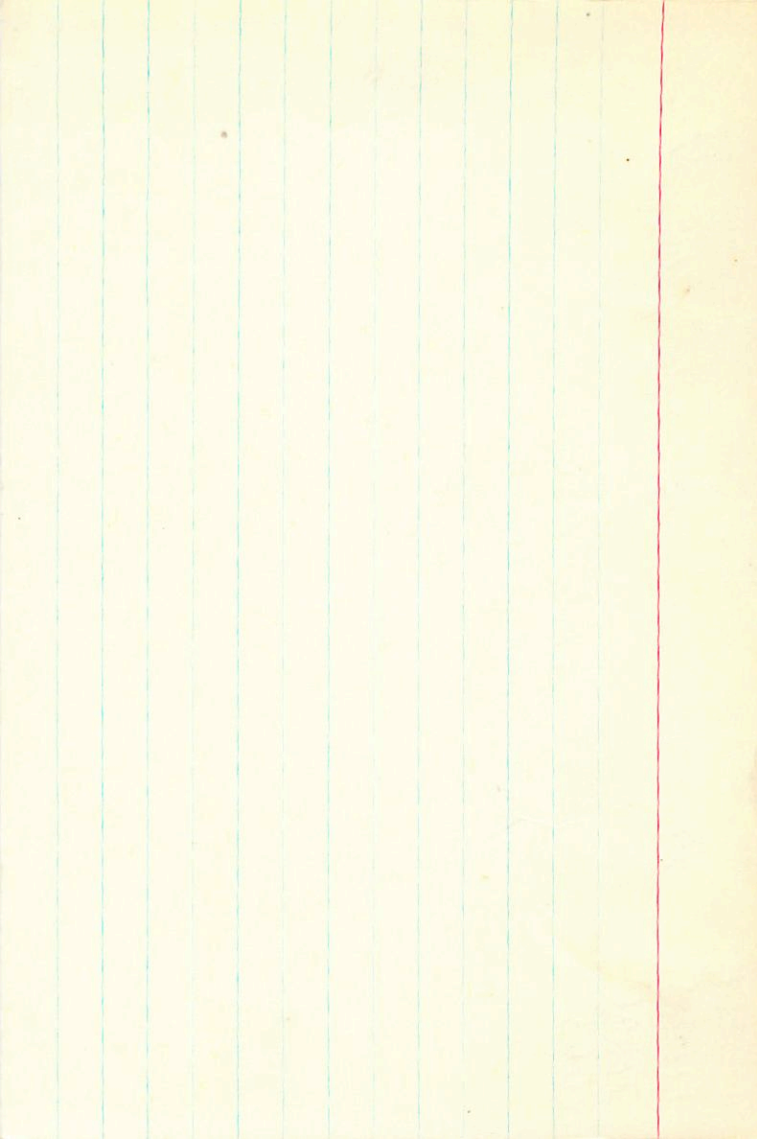
15 Jul
131918

20096
8665

14 54.1 -11 13 5.6 g 124 +1468

+000565 +0066 N30

+000451.0 +004±1.0



132254
14 54.7
495 50
DF7

HR5581
GC2079
563 150 101 3E45W

338 .174 .410 2500 2.646

362+

235 +11
342 +34
747

-584	810	-049	610	018	485	-	666	513	542	977	-464	-284	839	180	180	180
-2980	-8600	-0865	+3409	1010	+3005	-2305	-2980	-5448	1150	1150	1150	1150	1150	1150	1150	1150
-11590	-11290	-11290	-2006	1040	1040	1040	1040	1040	1040	1040	1040	1040	1040	1040	1040	1040
06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511	06511

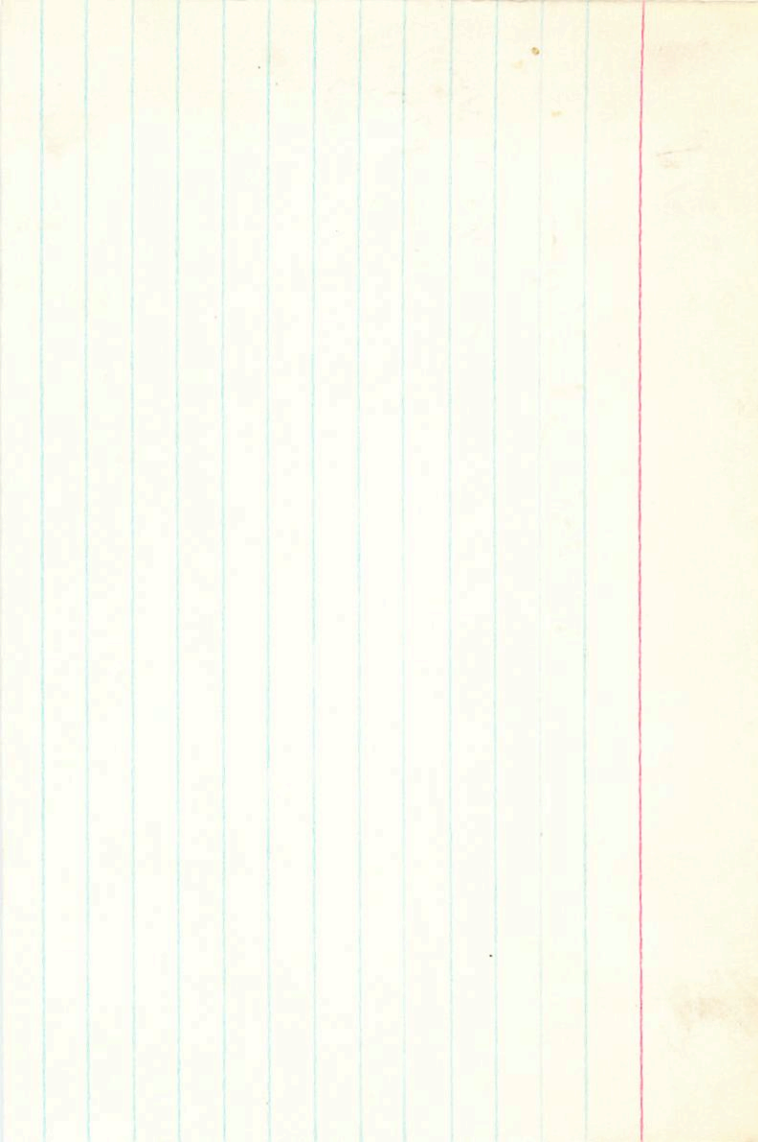
808
+108
+012
-146
-224

200

+0.7

-7.9

-12.2



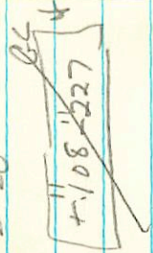
8671 18 54.7 249 50 5.7 d(27) - 1448

20119

132257

5.62 +0.51 +0.015 2 20"

$\frac{1122}{140}$



246

+0112 ±2.6 -231 ±2.0
~~+0108 -225~~

43.382 1888.9 +45 45 55.63 18900

$\frac{-454}{42698}$

$\frac{1384}{6949}$

43.408

+0110 -224

58551 18555

133

~~+0110~~

~~02 -~~

~~43.408~~

1108

~~10118~~

~~241~~
45

~~1408~~

$$\begin{array}{r} +0002.2.6 \\ -0005 \\ \hline \end{array}$$

$$\begin{array}{r} -008.2.2 \\ -010 \\ \hline \end{array}$$

132146 14 54.9 +16 35 5.8 965 -1598

20121

8673 51.705 1902.6 +16 35 18.22 1900.4

$$\begin{array}{r} -009 \\ \hline 696 \end{array}$$

$$\begin{array}{r} 40 \\ \hline 18.62 \end{array}$$

51.657

18.06 1934.4

34.6

$$\begin{array}{r} 19 \\ \hline 676 \end{array}$$

$$\begin{array}{r} \hline 18.00 \end{array}$$

51.673

$$\begin{array}{r} \hline 680 \\ -016 \end{array}$$

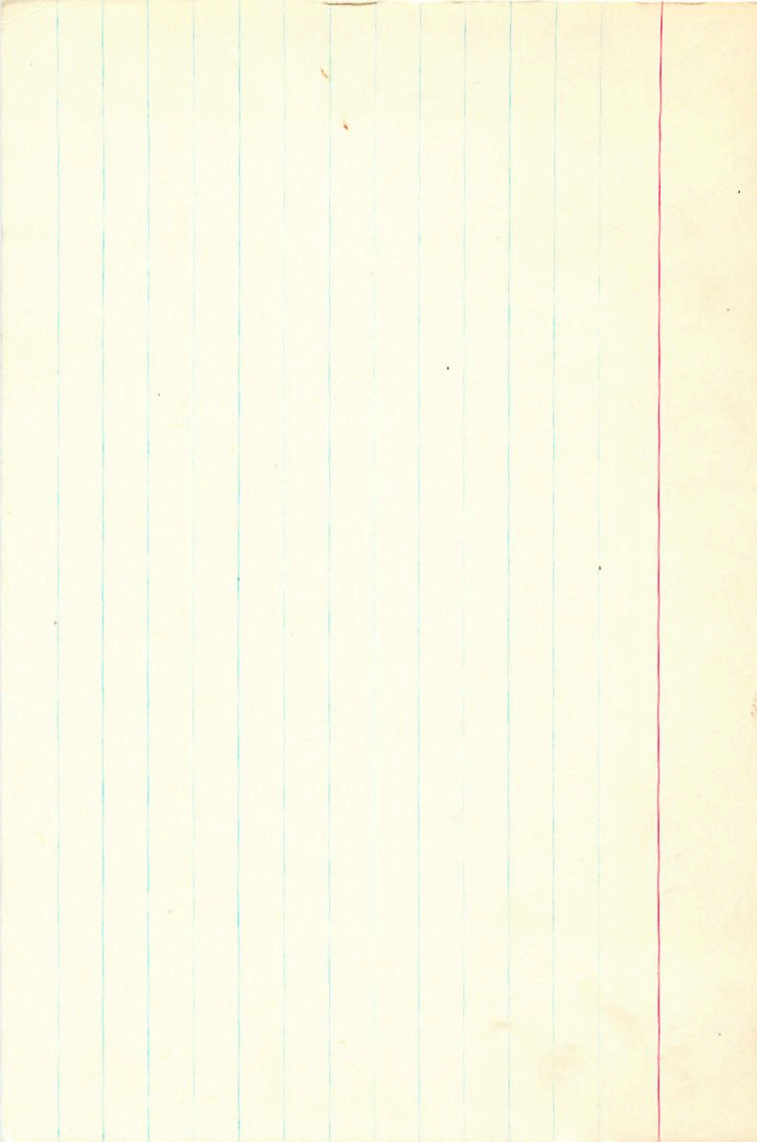
18.18 1940.09

$$\begin{array}{r} 7149 \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} \hline 18.00 \end{array}$$

36.5

$$\begin{array}{r} \hline 18.00 \\ -162 \end{array}$$



132304 ✓

RI

14 55.5 +24 52 123 III

14 56 22 +24 75

6.44 + 1.39 + 1.51 (2)

6.28 + 0.575 (1)

-38.3 000

6.28 + 0.535 2) Mon 76

-054 + 010 take
+ 12 - 18

6.28 + 0.555

-042 -008 6.49

-041 -004

589

-039 -001 + low.

5.10

24

7

6



0.000

14.000*

50.500*

24.000*

52.000*

-0.000*

-0.001*

7.600*

331.131

-38.300

0.102

-0.389

48.545

-0.123

0.274

-51.315

6

4207094

14

561

-24 94

$\mu_x = -0.190$

$\mu_y = -0.60$

$9.45 + 0.35 - 0.05 = 9.75$

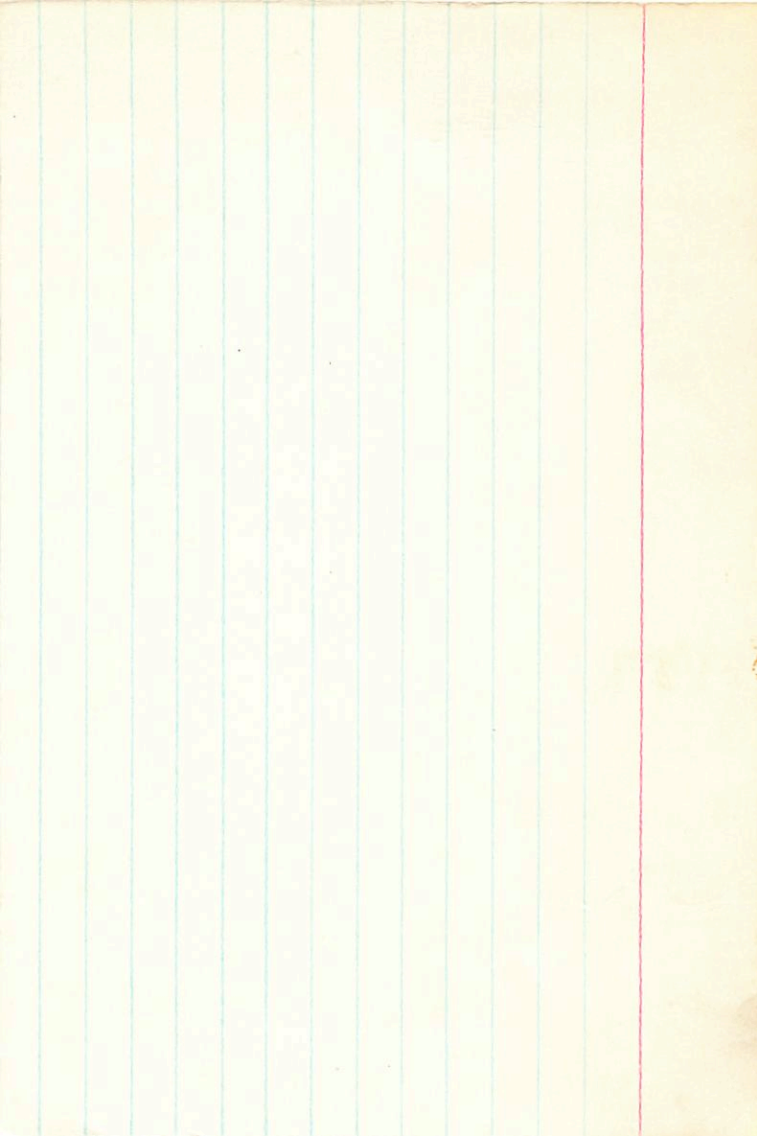
-62 h/w

584	-114	-803
606	495	-858
464	861	210

+	5260	+0338
-	5998	-1408
+	4179	-2449

+	8548
-	7406
+	1730

+	49.8
+	346
-	13.0



47104
0.24

14.800
-17.600
-23.000
-125.000
3.850
59
25.800

+3.11

-0.604
0.269
-0.750
-96.882
-25.858

-24.0

0.664
0.690
-0.287
-477.943
-65.546

302

4

1M

-0.441
0.672
~~0.506~~
-352.218
-5.374

130959
19985

616
58
14

48.9

-0014 ± 2.5 -132 ± 2.5
-0012 -126
-17 35 6.7

df 5 +25.86

8630

6.52 +0.455 +1.59 2 24"

25

Woff 30

46.825 1897.5 -17 35 60.74 1896.0
073 +7.13

44

59

.898 -0013 -129
-126

34

53.61

13.15

22.947
23.838

-0186 +25.8
-015 -123

34

46.10
13.30

1937.49

46.785
52

.939
14
853

850
-078

41.1

59.40
104

58.36
11

59.25
59.44
0

2699

59.00

-5.39

1940.90

116.80
38.9

13.296
335.60
46858 +8
-17 / 849

30.70
28.62
19.52

+17 +1 / 59.28

1941.41

42.9



5