

109764

12 346

tg 04

17118

89,2016

1035

1035

1034 ± 35 - 102 ± 3.2

351681 941 - 1035 - 103 18.24 880

$\frac{211}{899}$ + 1032 + 102 $\frac{17}{18.36}$

351649 41.80

1838

1035 - 101

1035 + 101

10523

1050 + 105

$\frac{116}{645}$

35.756 342 340 18.25

+ 15

+ 18

964 - 928 050
1001 1000
- 034 1201 0010

13.04
0052
6-41

$+7.4$	$+0.23$	$+4.4$	$+0.22$	$+0.264$	-0.037	$+0.54$	$+0.37$	$+4.54$
$+3.3$	-0	$+3.8$	$+1.91$	$+0.539$	-0.848	$+0.52$	$+0.52$	$+0.52$
-4.23	0	-4.23	-2.15	-1.596	-0.519	$+0.27$	$+0.22$	-0.52

$6.50 = 2.00 \text{ Pa}$

$+103 \pm 0.27$
 -0.21 ± 0.16

$+3.76 \text{ km}$
 $10.51 - 0.30 - 1.08$

$+0.50534$
 12
 0.49
 $+0.5$
 0.0

RUN

12 26.0 +7 16 -25.0

6612212

6.83 1402.4 -0020 ± 3.5

-005 ± 3.1

+202561

57.679 1506.4

4688

1900.9
~~1696.1~~

689
689

-0026 0
+003 +4

47.12

7674
38

1526.4
576.5

-0026 -038

+007

47.72

4771 1936.4
1536.4

+27.5

576.3
+19.1

-038

48.11
47.89

1900.9
1936.4

-049

666

47.56

48.2

1936.4
1936.4

57.66 - 10.1
+0.12

+0.3
48.23

1936.4

9.6

48.23

1936.4

3888

-038 + 007

2000 no.



-853	505	-130	+1536	+0417	+1763	57.4	1324	1503	+3.2
514	793	-320	-0985	+0243	-0670	200 ² .k	-12.1	+8.0	
058	340	939	-0104	+0412	+0009	+33	-23.4	-22.4	

+70

32000

466.2
-16.8
-230

F104 Handwritten

(+2) (+4)

~~087~~ + 1000 Mc

-35' + 8 Mc

-35 + 9 Tonbur

-36 + 9 Meridian

965

-25.0

9993

- 9929

1194

-0893

236.91 058

F-10 20 ✓

Plan

E = +0.2

R Val 6.5 +1.50 +0.8
 +1.50 +1.50
 HR 4808 5.4 +1.00 +0.96
 +0.96

5.40 1.18
 5.36 49.45
 38
 4.98
 12.4
 7.4
 3.4
 7.4
 3.6
 -3.6
 (2.45)

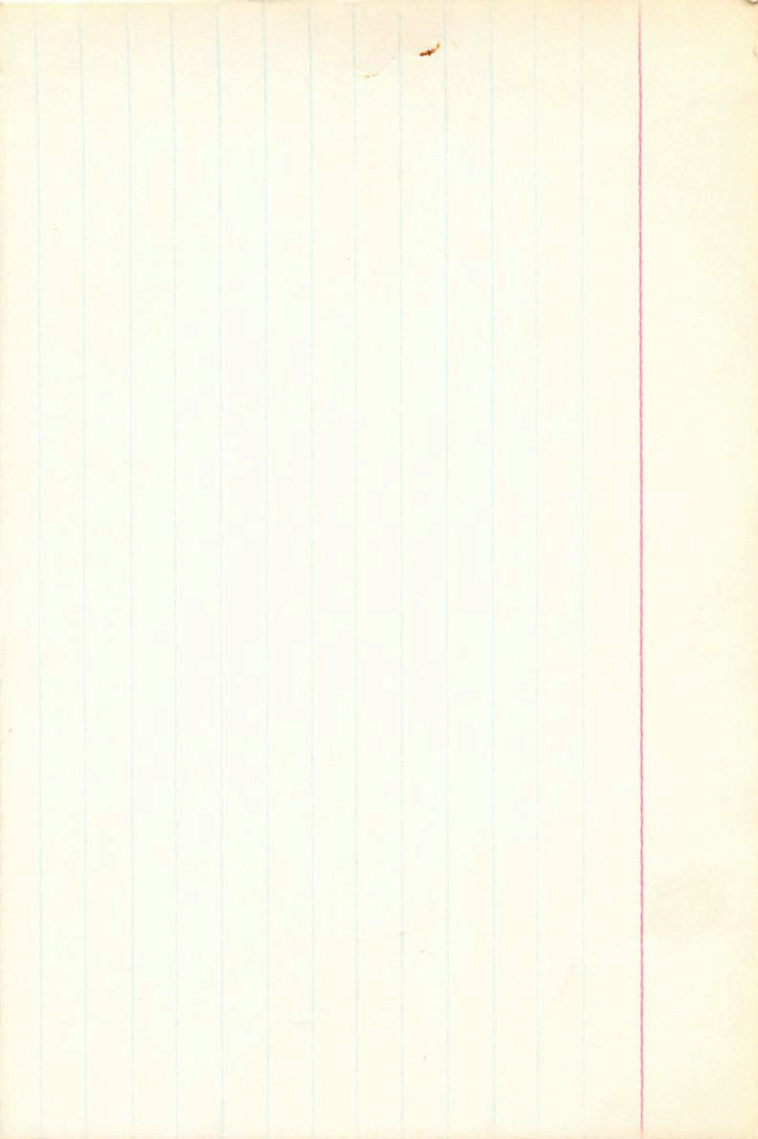
7.4

-36 +005 MC
 -6 +2
 -036 +007

-0025 +003 Tomlinson
 0 +42
 -037 +007

-038 +001
 -037 +005 E

March



109944

12

36.2

-4 05

6.67 + 160 + 197
5.77 + 107.5
+11 Var

~~10264~~ 70

~~10264~~ -0167
1143

-0833 -010 5000

~~10264~~

-0133

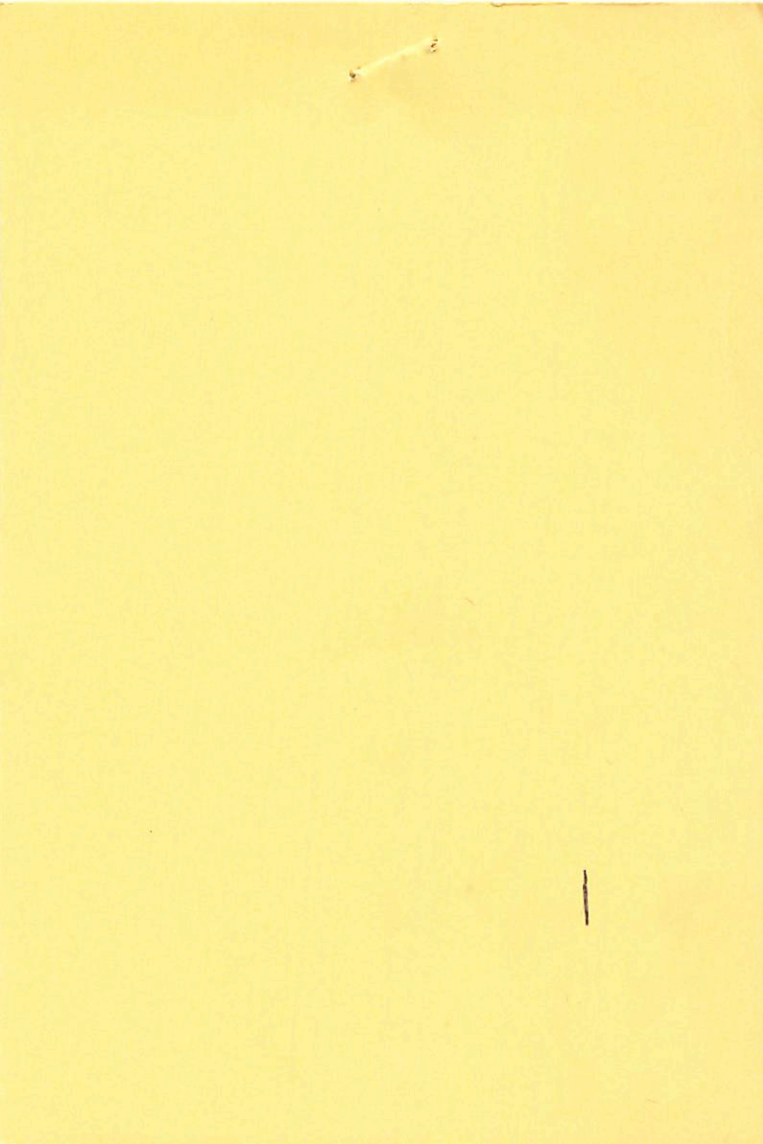
-049

-047 -006

①

9882 - 9980

1301 0090
-0600 1024



12.600
-4.100
-47.000
-6.000
8.000
398
11.000

-0.852
0.468
-0.237
175.915
67.423

0.522
0.713
-0.468
-136.242
-59.391

0.858
0.522
0.851
-26.043
-1.004

7.63 + 0.4 + 1.0

40° 2558

12 36.4 + 39 35

-113

-148 deg

109995

-115 -135

~~2520~~

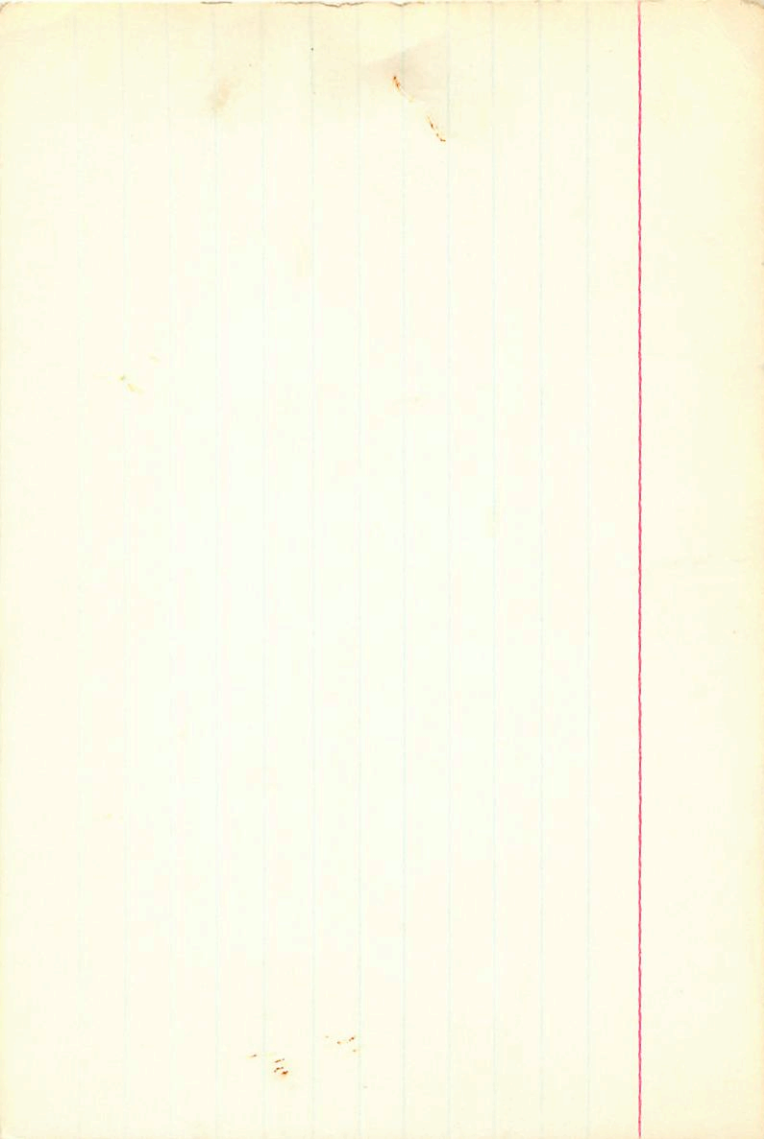
-5

-113 -153 GC

+4

7.62 + 0.42 + 1.39 1.293 -136 ± 1 (D) SWG

7.63 + 0.32 + 1.50 1.270 -132 ± 1 (G) SWG



+40255 12 36.4 +39 35 $p = -133 \pm 2$ *Shelton*

H010995

7.61 +04 +09 A02 -113±6 -148±5 R

-113-153

-111 -151.5

650 0.180 1275

5.60 = 139
244 805
694 -473

~~159~~
~~24~~
156

1216

+846

-144

-151.5

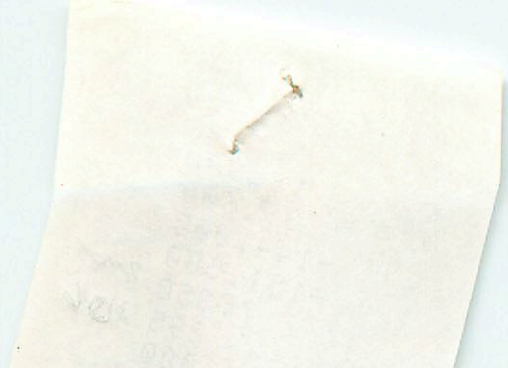
738

-134

13010

850	+500	+154	+4552	-3626	+926	+12.0	-7.4	-5.0
+522	+841	+150	-2796	-6099	-9995	-115.6	-120	-132.6
+050	-208	+976	-0268	+1508	+1240	+16.1	-10.3	-94.2

2



10
- 131.000
- 144.000
- 151.500
1295
000

7/20
3136

9.14 + 20 + 01
23

-7.0

+3502362

12

36.9

+34 29

90

110085

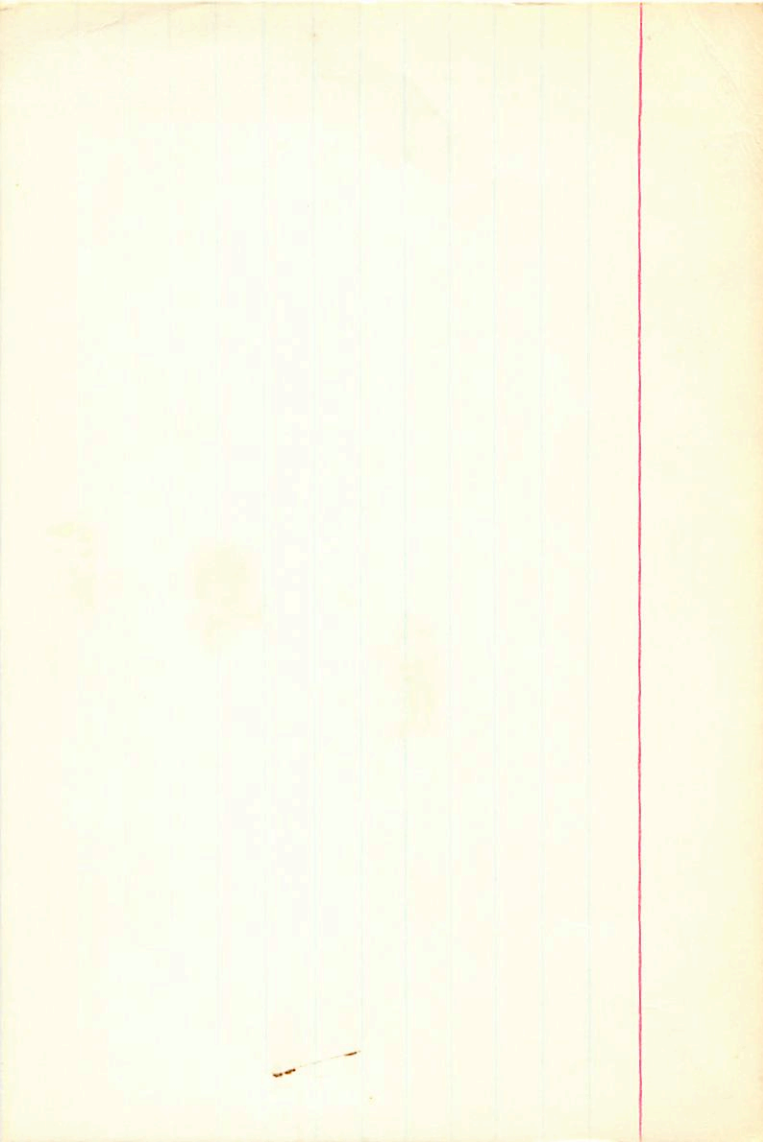
34 ①
24

-0016 -010 FR3

+ 2 0

-0016

-020



RS MMA

12 36.7

+58

45

-26.0

-026 -021 MR

+1 -3

-014

-025

3

18

W

0.000*

12.000*

36.700*

58.000*

45.000*

-0.025*

-0.014*

9.000*

630.957

-26.000

0.073

0.307

37.791

-0.111

0.421

-81.000

0.029

0.853

-4.010

3

old

110035 12 370 -37 50 115 B

Not Yab

8m 20
63.84m

9.11 + 1.02 + 0.91 (2)

~~8.3 + 10.42 (3)~~

5049
5049

$\Delta(B-v) + 0.35$

$\Delta(b-u) + 0.8$

-0.212 - 2.75

-2.54

$\boxed{-2.53 - 2.71}$

110035

135.9 - 0.234 - 0.274

$\boxed{-2.12 - 2.71}$
 $\boxed{-2.11 - 2.71}$

9.125 - 4.505 } 3.714
7.004 - 7.595 } -0.591

M(F) π (at)

+ 6.03
865

2.62
0.30

-3.17

-2.71

2.30

135.9

+ 3.0 - 61.1 - 23.9

+ 6 - 10 - 12

M, 5.94

M, V + 7.4



9.10
2/1/8/2/5
2/1/2/1

15
22
22

933

12

37.0

-37.0

+35.9(4) < 5

110035

$$\frac{9.2}{9.6} \left\{ \begin{array}{l} p = 63.84\% \end{array} \right.$$

$$A3 \quad 9.04 \quad +105 \quad (2.20) \quad N5Z$$

$$\frac{7.9}{9.0} \frac{5.15}{5.15}$$

$$\begin{array}{r} -238 \\ \underline{\quad} \\ -241 \\ \underline{\quad} \\ +7 \\ \underline{\quad} \\ -234 \end{array}$$

$$\begin{array}{r} -238 \\ \underline{\quad} \\ -275 \\ \underline{\quad} \\ +4 \\ \underline{\quad} \\ -274 \end{array}$$

9.2
is

$$-0212 - 225 \quad +16 \rightarrow$$

Not

number

your

of

-254

$$\boxed{-253 - 271}$$

0.31

680
75

-3707950 \$63 597 453 (C72) Chem II 325 83

HD 110035 12 37.0 -27 02 76.1335682

$\Delta m = 20.25$
342 -36 44

9.09 +1035 +1.00 (2) $-0.234 -0.274 \rho = 135.9$

8.56 +0.235 $\rho \rightarrow m-m=360 \rightarrow 19 -21 -35$
 $n_{mf} = 0.024$

P T E A R F G C L $\mu/\rho^{2.15}$

I. 53.02 166469 0.35 -0.300 -141 +176 -260 0.348 320 150 109
 II 55.47 166426 0.34 -0.306 -109 +142 -240 0.342 26.9 13.0 094

$\pi^3 = 15.8 \times 10^6$
 $\frac{\text{I}}{\text{II}} m_1 = m_2 = 0.54 -27$
 $0.47 -38$
 slightly constant

$3 < 9 \times 10^{-6}$

				I	II	III
1920.64	311.9	0.42	2 Jaw		-3.9 +0.11	-9.2 +0.07
1928.20	349.4	0.45	4 B	-3.9 +0.11	-3.1 +0.03	-2.7 +0.02
1929.84	354.5	0.46	4 B	-3.1 +0.03	-3.8 +0.02	-3.2 +0.02
1931.42	3.3	0.39	4 B	-3.8 +0.02	0.0 -0.06	+0.4 -0.05
1932.27	5.7	0.46	4 B	0.0 -0.06	-0.6 +0.01	0.0 +0.02
1934.34	14.6	0.40	4 B	-0.6 +0.01	+1.7 -0.05	+2.2 -0.04
1935.26	18.5	0.50	3 B	+1.7 -0.05	+2.6 +0.04	+3.1 +0.06
1937.38	25.1	0.47	6 B	+2.6 +0.04	+2.5 +0.02	+2.6 +0.04
1945.39	51.2	0.42	2 B	+2.5 +0.02	0.0 +0.02	-1.2 +0.04
1947.39	60.6	0.38	3 B	0.0 +0.02	+0.4 0.00	-1.0 +0.01
1949.46	70.2	0.34	4 B	+0.4 0.00	-0.3 +0.01	-1.7 -0.01
1951.70	83.7	0.32	3 B	-0.3 +0.01	+0.4 0.00	-0.7 0.00
1956.41	117.6	0.23	4 B	+0.4 0.00	+0.5 -0.05	+0.9 -0.05
1959.20	141.9	0.25	3 B	+0.5 -0.05	0.0 -0.01	+1.1 -0.01
1960.35	152.6	0.25	4 B	0.0 -0.01	-0.7 0.00	+0.4 0.00

1201100035
3609950

I

II

12 343
-36

1564.41 202.6 0.21 43 71.4-0.01 71.0 0.00
1465.34 213.4 0.18 43 -0.6-0.03 -1.1-0.03

Spk
F

51.5

1.3 x 2

294

B P

1972.08 224.4 0.28 2 work 229
1975.16 254.7 0.26 370 305.33

1966.0 224.5 0.207

77.5

15

68.65 264.6 0.216

71.30 246.2 0.258

73.45 317.8 0.312

76.60 333.1 0.362

79.25 345.0 0.440

81.61 355.0 0.423

4

R.A. : 12.600
DEC. : -37.000
M. R.A. : -317.000
M. DEC. : -271.000
DISTANCE : 2.300
MODULUS : 29
D. VEL. : 35.900

q1 (U) : -0.852
q2 (U) : 0.264
q3 (U) : -0.453
dU : 682.495
U : 3.425

q1 (V) : 0.522
q2 (V) : 0.344
q3 (V) : -0.781
dV : %-1068.360
V : -58.832

q1 (W) : 0.050
q2 (W) : 0.901
q3 (W) : 0.431
dW : %-1217.743
W : -19.649

18036

12 370 -37 00

PPM

0216 -272

261 -171

-293

HE-

300

4354

6

— —

12/1

165

R.A. :
 DEC. : 15.000
 PM. R.A. : -37.000
 PM. DEC. : -293.000
 DISTANCE : -274.000
 MODULUS : 3.000
 RAD. VEL. : 40
 : 35.000

p1 (U) :
 p2 (U) : -0.825
 p3 (U) : 0.264
 u : -0.453
 U : 081.374
 : 7.083

p1 (U)
 p2 (U)

0344

231

R.A. : 12.600
DEC. : -37.000
PM. R.A. : -293.000
PM. DEC. : -274.000
DISTANCE : 3.000
MODULUS : 40
RAD. VEL. : 35.900

q1 (U) : -0.852
q2 (U) : 0.264
q3 (U) : -0.453
dU : 601.374
U : 7.683

q1 (U)
q2 (U)

2143
+1.2

334
52.9
431
101

① 5
+ 0135 = 1184

62

+4102318

41-130	12	37.2	+40	56	1925
	12	38.4	+40	48	1450

155

-848	508	153	-6150	-3347	-9497
529	824	181	+3826	5462	-1626
035	-235	971	+0254	+1548	+2002

111

6

18

18

18

41.232*

12.000*

38.400*

48.000*

48.000*

0.153*

-0.153*

0.000*

18.000

0.000

-0.948

0.156

-4.482

-0.167

0.176

-1.666

6

0.182

0.972

37 AB 8.87 277 149 673 2087 618
19 G 5.88 256 141 707 2457 CFI, d=6

116319/8 X 12 38.7

610452/2
6617259/60

AB 5.25

605
685
725
4.

3.7
1.8
1.8
+17.5

-123
-1236
+007
+0084

6c+

-1206
+8.0

13 788

-122 +013

6.0
+1.8
-1.2

.284 .170 .634 2.679 2.423/

[M1] 221 +1

[C1] 577 +176
+ 179

Try to recompute

-1078
-10786 -10054 +100415 +10014

9461 9953
-6884 0965

-1389
-132 +1006
0067

-1146
-113 +010
11346
0009
+0.4
0169 463

1320
+2.3
0130 443

1242
0090
+1445
0130
4140

10

7

1875

1875

1875

47

4821.000*

12.000*

33.700*

-12.000*

-44.000*

-3.122*

3.513*

92K 4.200*

63.183

-12.500

3.517

-2.314

41 +486 33.738

-3.265

-3.564

7 -11 11.255

3.017

3.764

-3 3.471

16w
110073

12 37.2

17236
7608

4.64 - 0.09 + 1.34 $\text{cty } 24''$

9.610 1906.0

-39

42 45.13

1899.4

$\frac{202}{812}$

+ 1.92
 $\frac{43.21}{}$

9.669
 $\frac{-6}{663}$

44.42 1939.10

$\frac{73}{626}$

-10
 $\frac{44.52}{971}$

41.2

-186

94.40

9.594
 $\frac{-4}{590}$

44.87

1955.30

$\frac{-32}{590}$

$\frac{45.19}{}$

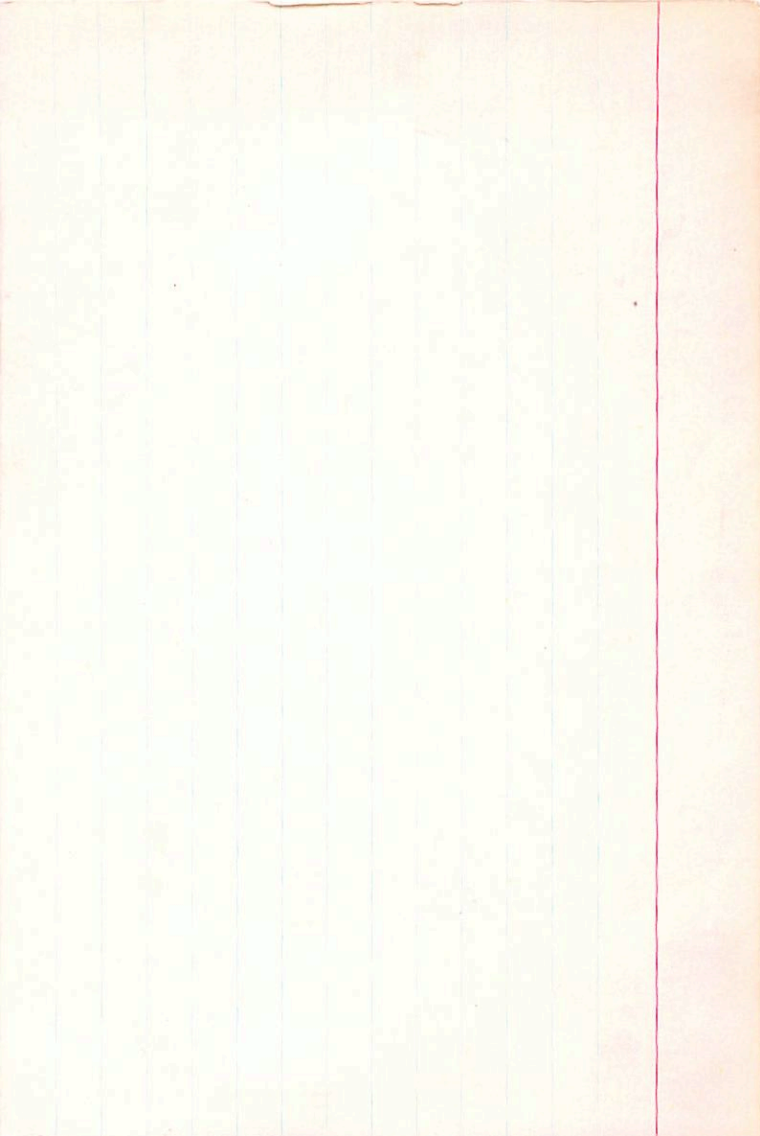
47.2

$\frac{44.86}{-1.65}$

47.8

-0040 ± 4.2 - 0.38 ± 2.8 top

-035
43 4.8 88p + 15.18



13702206
110166

12 37.5 +37 16

-0004 +006

4.469

27.369

31.073

31.765

31.765

31.766

775.42

5391

21.71

21.33

21.38

21.24

21.09

21.

31.742

+9

31.751

0.018

21.48

-20

21.28

+19

1952.07

40.4 (2) 25p

1918.72



HS RY $P=0.29$

Norm 12 37.6 +27 46

2610 mod 13. via

$DS=5$

0 -2
+3

-05956 -01856

-048512 -018512-888

-05755 -01855

0 d w (1)

-163 -987 464 885 -057 -018 0 -008 0 -076
-009 -001 056 008 0 261 0 0 0 0 0 1

0 +261 -76
+192 -184 -78

0 +130 -38

002

+130 -91 -38

RR

8.75 - 13 - 38
-0.5

40.40
25.50
14.90

-89.0
③

+3702306

12 87.5 + 5716 8.4

1930.20
22.20

1918.72

15.60
14.40

27.00

110164

31.73
1.5
1.5

27.00

31.73

110164

15.60
14.40

27.00

110164

1918.72

75.22

1.464

110164

1918.72

53.41

1.369

110164

1918.72

21.31

1.274

110164

1918.72

22.00

1.333

110164

1918.72

22.00

1.333

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

21.00

1.300

110164

1918.72

70.0002 -010 Bad

+00104 -017

+0008 -014

+009 +4

-0009 -010

① -010
+3
-007

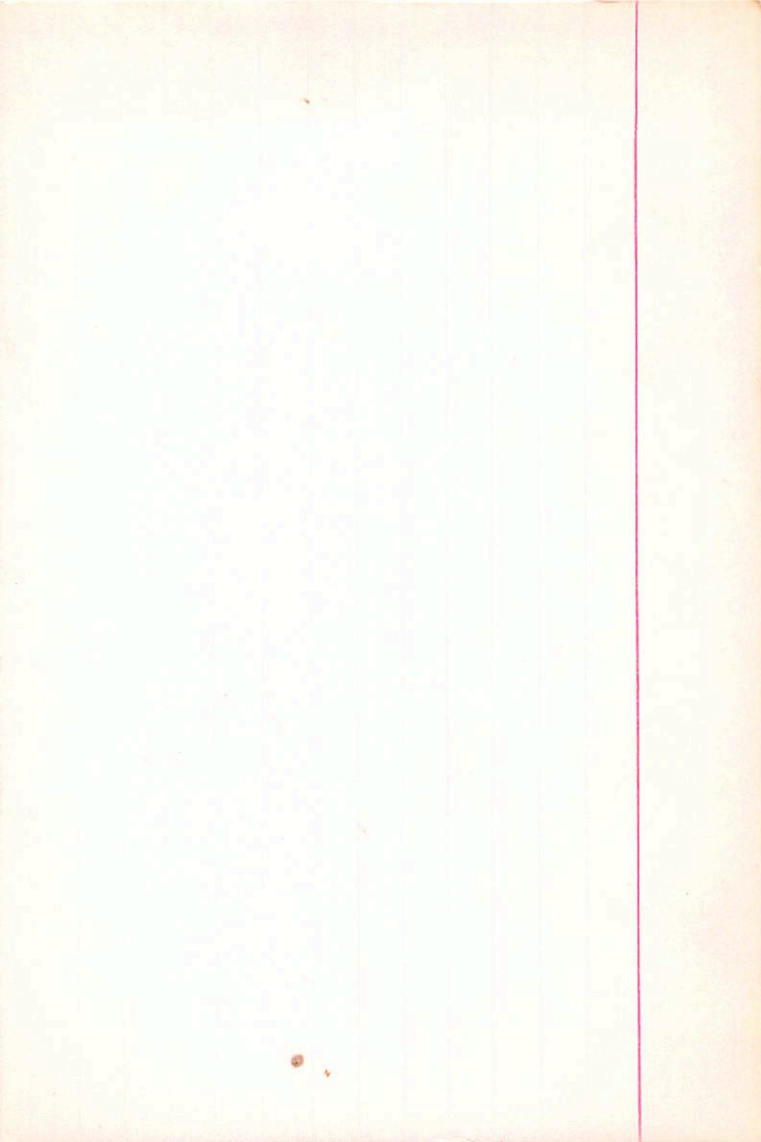
21.48 1953.07

-9

21.39

8.76 -046 +109 +65 506

8.75 -042 +070 742 -84 ± 2 ⑤ PWA



2.47 + 29 + 16
2.5

-14.2

+31⁰2396

12 38.1 + 80 39

7.8

110248

✓ 12.4 (17) Van

AGK22 - 0018 - 070 N20

+ 0002 - 066 Klame

-0004 - 068

7.66 + 178 + 244 + 770 - 24 ± 1 (2) SWC

7.67 170 263 764 - 14.2²¹ (5) Peng

THE UNIVERSITY OF CHICAGO

PHILOSOPHY DEPARTMENT

PHILOSOPHY 101

LECTURE NOTES

PROFESSOR [Name]

DATE [Date]

TOPIC [Topic]

1. Introduction

2. The Problem of Induction

3. The Problem of Causality

4. The Problem of Free Will

5. The Problem of Truth

6. The Problem of Meaning

7. The Problem of Knowledge

8. The Problem of Ethics

9. The Problem of Religion

10. Conclusion

110287

12 38.6 -45 52

+6.950.46, (6)

17257

5.84 11.52 12.34 copy

6
14
16

21

153

-08923 +041 23 6-6

-070 +054 1130

-062 +058 C P

-073 +051

+78 +27 -60 copy

-0084+5.1 +041+3.3
-0067 +041

986-167 -718 696 -873 +051 46.9 -037-5 168 ✓

072 036 012 006 313 227 +48 -1 +5

37.488 1505.6

-45 52 20.42 19043

+77+42+37

004

339

-1.87

+78+37-60

82.7

22.29

003

37639

20.54 1935.20

37.7

9463

-14
623

-15
2069

47.3

1151
5790

20.01

1555.43

43.0

37.547

-251

-39

20.40

-14
526

20.54

+1.75

20.54

+1.75

Card II
1103178

-0079 ± 40
-0078
-0077

+012 ± 2.6
-003
+002

1729 39939 18976 -12

44 2283 1887.4

$\frac{438}{437}$

40.377

22.038

18.032

40.070

40.034

101

105

066

-311

40.027

028

39.8

133

105 066
-311

40.027
028

410

39.831
+11
842

23.48
-1
46

23.58
-25

9.77 1929.69

14.48

24.25

+26

23.99

+25

23.71

68.88

34.4

47.0

23.77 1939.19

23.68

23.70

-12

-008944.8
-0093
+00143.0

-0042

6m

17260 40.262 1898.8 -12 44 27.03 18406

$$\begin{array}{r} 456 \\ 718 \end{array}$$

$$\begin{array}{r} -06 \\ 27.09 \end{array}$$

13.22 1529.69

$$\begin{array}{r} 22.342 \\ 18.032 \\ \hline 40.374 \end{array}$$

36.1

$$\begin{array}{r} 29.80 \\ 27.26 \\ \hline 57.06 \end{array}$$

$$\begin{array}{r} 49.77 \\ 34.9 \end{array}$$

$$\begin{array}{r} 762 \\ 381 \end{array}$$

$$\begin{array}{r} 27.26 \\ 27.26 \end{array}$$

44.3

$$\begin{array}{r} 40.326 \\ 333 \end{array}$$

$$\begin{array}{r} -337 \end{array}$$

6546

$$\begin{array}{r} 27.50 \\ 27.41 \end{array}$$

1939.08

$$\begin{array}{r} 40.09 \\ 4.11 \end{array}$$

$$\begin{array}{r} 27.04 \\ 27.02 \end{array}$$

$$\begin{array}{r} 27.41 \\ 27.33 \end{array}$$

$$\begin{array}{r} 4.11 \\ 108 \end{array}$$

$$\begin{array}{r} 27.02 \end{array}$$

$$\begin{array}{r} 27.33 \\ -24 \end{array}$$

110317/5

12

38.7

-12

44

df1 -14.12

df2 -11.12

110317/8

ADS 8627

17259/0

7616/7

6¹¹ / 6.5
6 / 6.5

5.27 +0.42 +0.10

Now 70

~~447 +0.56 60~~

-12.62

5¹¹

$\Delta m = 0.03$

11^m
60^d

-116 +0.12 A

-130 +0.01 B } R.C

w 7616/7

$M_0(w)$

-124 +0.07 A Z

df1 A 6.02

+1.67

+1.9

-123 +0.07

df2 B 6.77

+2.42

+2.1

B' 6.77

+2.42

2

-165-954 -220 924 -123 +007 -12.6-002 +3 033

-021 0121002 -109583 -12.3 +12 +2. 015

+5 +41 +5

+35-43 9

+1 +60 +6

01

+55-22-5

+4 +45 +5

0135

+42-16-8

8

4.98 + 27 105 - 8.6
+ 3.0

13102397

12 38.7

20.4 (9) Var
18.5 (39) Var
730 (43) Var
7.1

110326

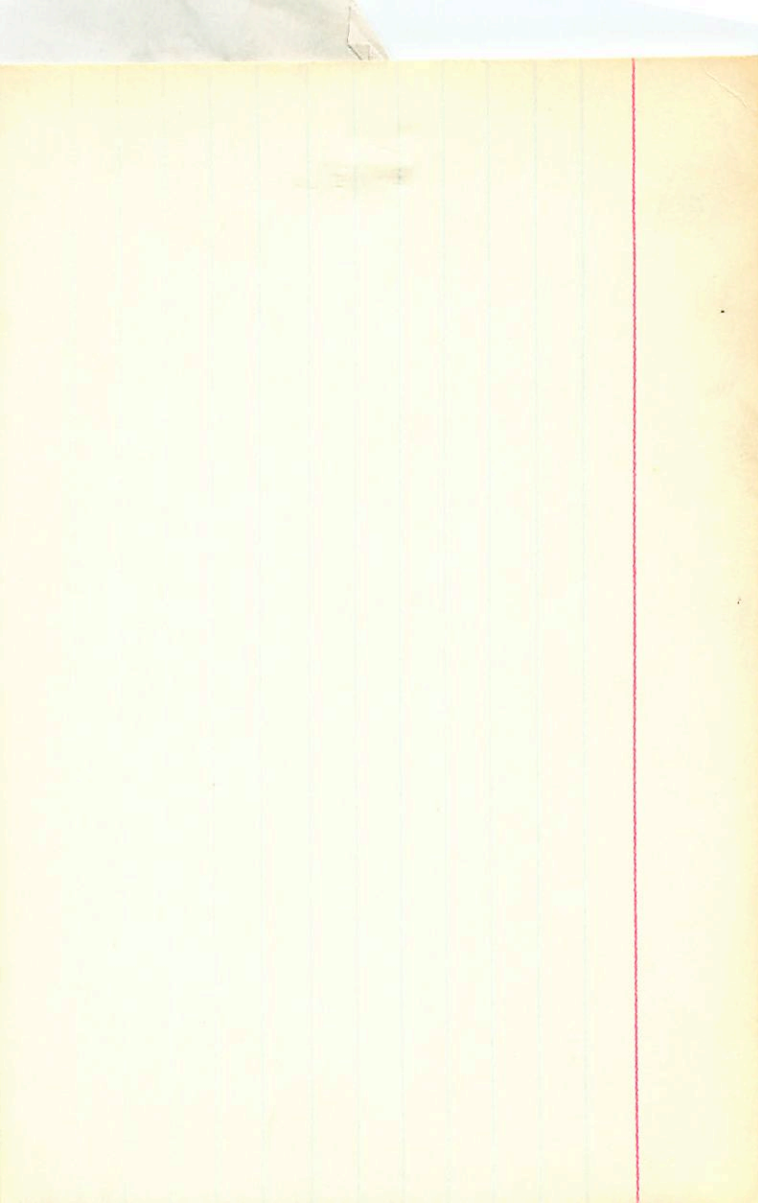
Am $\stackrel{\pm 0.5}{-0.022} + 0.15 \pm 0.4$

8617261

40.914 1902.1

39.99 1898.8

-0.28 + 0.15



0.66

12 38.7 +2043 4.9 A2 -8.64 P2

397

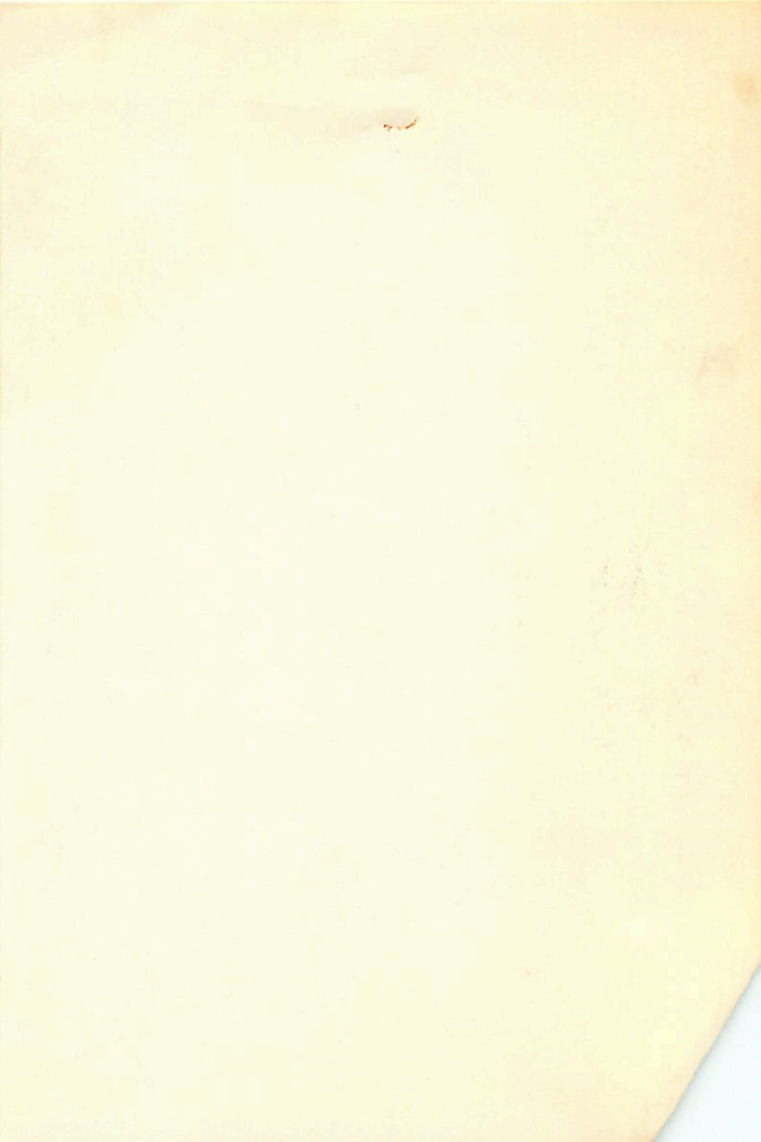
6.617261 6.99 +0.28 +0.04 Am Shalshub

7018 4.30 = 72.4
-6022 ± 5.7 +015 ± 4.3
-0014 +007

40.914 1902.1 +30 42 39.99 1898.8
100
41.02

40.96 21 981
-23 +18
-14 +10
-19 +15 +120
39.2
89.7 1930.1
-22
39.44

-039
-848 +526 +063
+529 +848 +035
+035 -062 +997
+0804 +0374 +1178 +8.5 -0.5 = +8.0
-0501 +0603 +0102 +0.7 -0.3 +0.4
-0033 -0044 -0077 -0.6 -8.6 -9.2
+1.22



6.98 + 27.07 = 33.0

13102397

12 38.7

20.4 (9) Var
8.5 (39) Var
730 (73) Var
7.1

^{±0.5}
-0022 + 015 ± 0.4

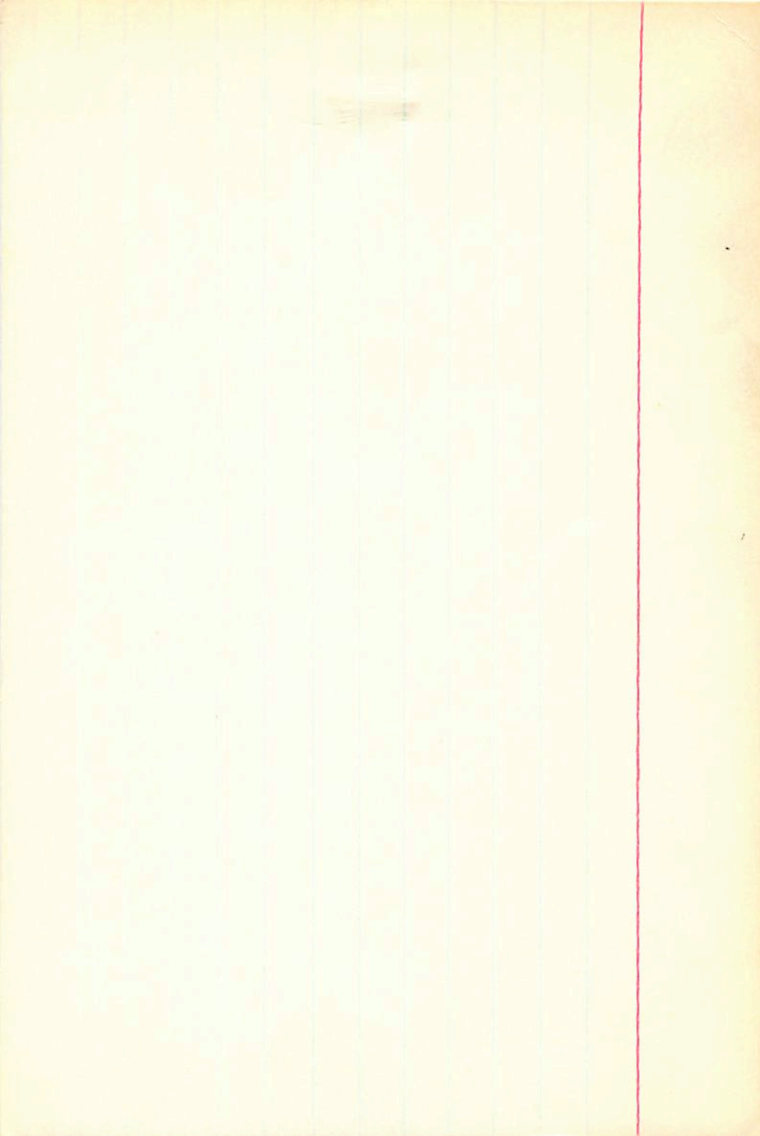
110324

40.914 1902.1

3999 1898.8

8617241

-028 + 015



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~~12.630~~
- 12.750
- 184.000
12.000
3.630
53
- 12.600

8

- 0.849
0.424
- 0.315
746.185
43.677

0.527
0.636
- 0.564
- 412.363
- 14.841

0.039
0.645
0.764
3.718
- 9.423