

98897

15673

11 20.0 -58 07

+002760 -0234.3

0.016 14 4089 944

96015

11 20.2

-77 20

15628

-0214 ± 2.3

-012 ± 7.3

-5.9 ± 2.5 ^{U₂₀} ③

15.577

97.9

-015

1.92

96.4

$\frac{1.115}{692}$

-0237

-007

$\frac{64}{1.2}$

14

24703

3040

48.74

50.420

$\frac{2.328}{1.49}$

$\frac{15623}{132}$

$\frac{01.49}{-14}$

$\frac{755}{780}$

$\frac{1.63}{-246}$

474

435

1.20

15.460

1.04

1.04

1.04

1.04

1.04

-0031±4.5
-0026

98993 11 20.8 -35 53 5.1 NL -4.6e

1564d

6950 47.027 1908.8 -35 53 25.24 1902.1

$\frac{128}{155}$

$\frac{+86}{24.38}$

$\frac{47.085}{101}$

$\frac{24.54}{-10}$
24.64 1939.05

37.7

$\frac{115}{058}$
 $\frac{150}{-097}$

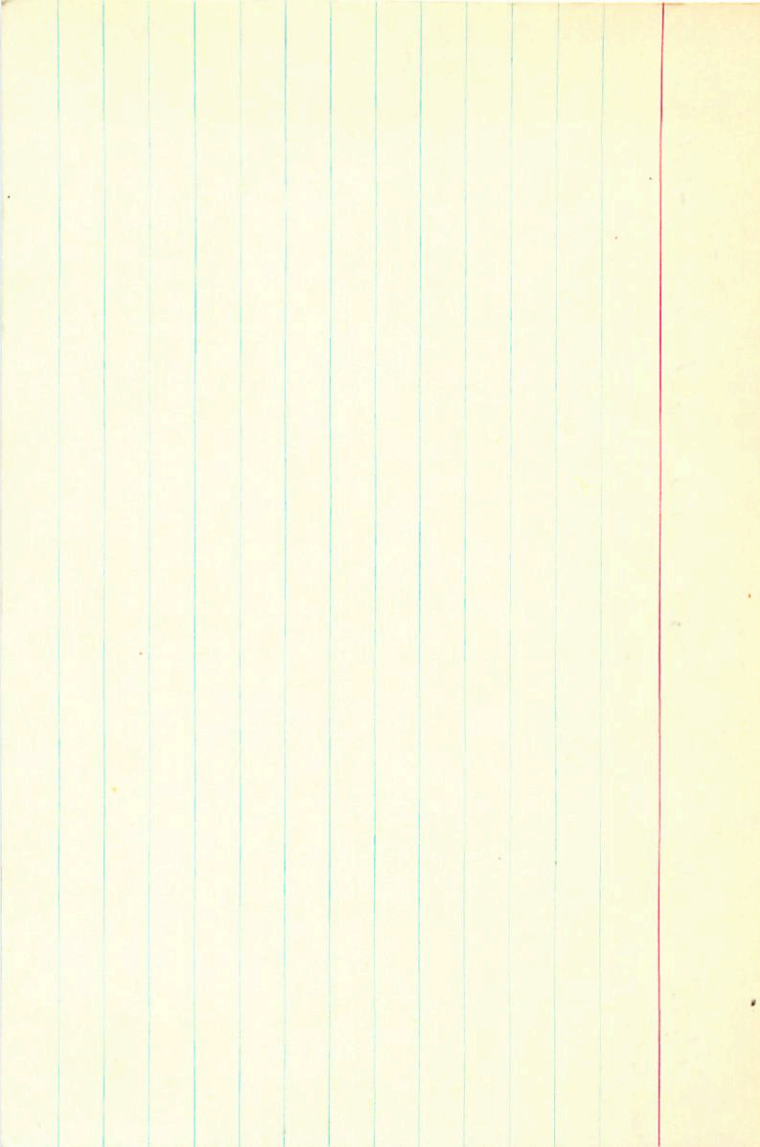
$\frac{94.99}{47.5}$
45.4

$\frac{47.019}{-5}$
 $\frac{610}{014}$

2470

1955.54

$\frac{24.97}{2372}$
 $\frac{44}{-}$



98951

11 20.9 -18 30 dF3 +11.7 a
+12.2 C(4)
+9.7 C(3)
+130 Out
+6 1 Sta F51B

G-C 15644

5.09 +0.42 -0.06 Name (1)

W6451

~~5.08 +0.40~~ Cape $\delta = .07$

42638

5.09 +0.42 +1.59

-1703367

S = 1.5 X 0.2 = 0.3

14R4395

-0.221²⁷ -0.37

-3.03 -0.34 C-C

+59 -41 -22 .020

-0.220 ± 2.1 -0.38 ± 2.2

-0.41 ± 4 -0.38 ± 10 Y

+48 -35 -16 .025

-2.95 ± 7

Cape Ref.

+39 -30 -12 .030

8 Y(10)

27 C(6)

14 ± 8

$$\begin{array}{r} -0034 \pm 5.8 \\ -0032 \\ \hline \end{array}$$

$$\begin{array}{r} 11 \\ 21.0 \\ +17 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.0 \\ +0.12 \\ \hline 7.12 \end{array}$$

$$A3 - 0.78$$

99004

15645

6952

$$1.139 \ 1893.7 \quad +17 \ 24 \ 59.49 \ 1891.7$$

$$\begin{array}{r} 191 \\ \hline 330 \\ \hline \end{array}$$

$$\begin{array}{r} 1.204 \\ \hline 211 \end{array}$$

$$\begin{array}{r} 388 \\ \hline 194 \\ \hline - .136 \\ \hline 1.167 \\ +18 \\ \hline 177 \end{array}$$

42.9

$$\begin{array}{r} 59.98 \\ \hline 1933.0 \end{array}$$

$$59.98$$

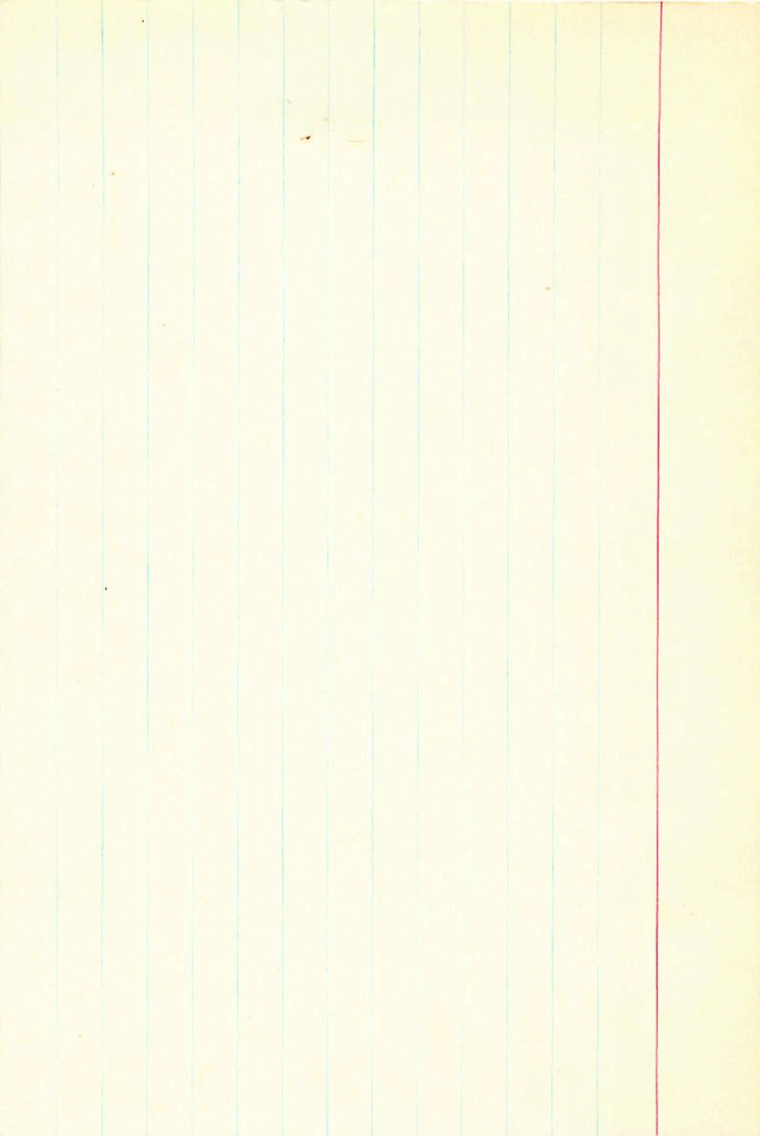
$$59.78 \ 1940.2$$

$$\begin{array}{r} +6 \\ \hline 59.84 \end{array}$$

$$\begin{array}{r} 59.91 \\ \hline \end{array}$$

$$-1.53$$

$$\begin{array}{r} 73.2 \\ \hline 36.6 \\ \hline 44.9 \end{array}$$



- U Ma

H0 99602

11

~~20.5~~
21.2

+37 30

-12.3 b

-00530 -0161 4650

-0631

-062 -012

9564

-9497 0623

2415

-0252 0104

+723

11.350
37.500
-78.000
-12.000
6.000
158
-12.300

-0.871
0.334
0.259

144

Rx Leo 11 21.3 r26 s3

12 red

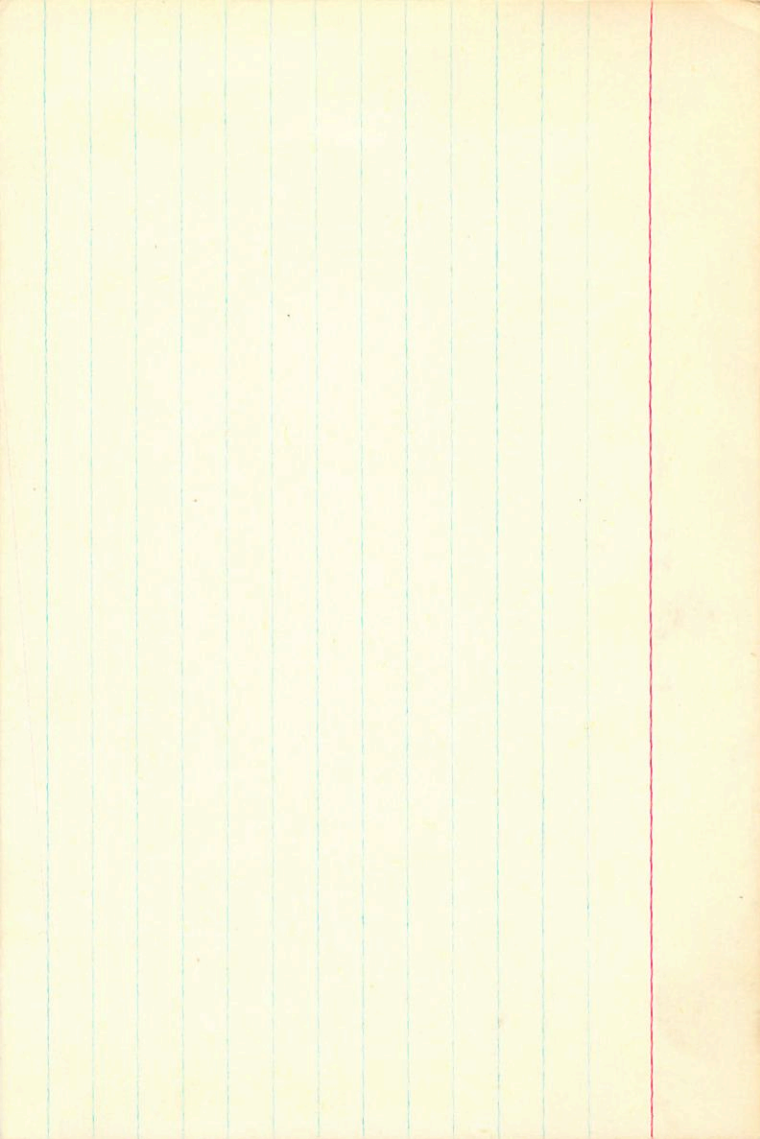
1228

-1

+01056 - 03756

+02250 - 009510 80

+01455 - 02055



42642

11 21.8 + 21 39

1627

157 (2)

1.00 271°

Per & Leo 158

50° 13' N (6)

139-990 368 930 1.000 000 -20 0-7 0

-139 0 -990 0 -659 -4.460 -19.6 +18 -B.

+8-74 -7 066

-67-34-21

Σ 67
99167

11 22.1 -10 35 5.1 9.10 +3.1 6

15665
6962

~~10049~~ 15
NS
+0.92
+1.8 18

-0021 ± 2.3 +022 ± 2.1
-0019 +019

4.927 1894.5 -10 35 5.45 1888.2

$\frac{128}{5.055}$

-1.36
6.81

$\frac{4.956}{15}$
971

$\frac{968}{-0.87}$ 47.0

5.97 1941.28
+5

$\frac{5.92}{3.06}$
41.5

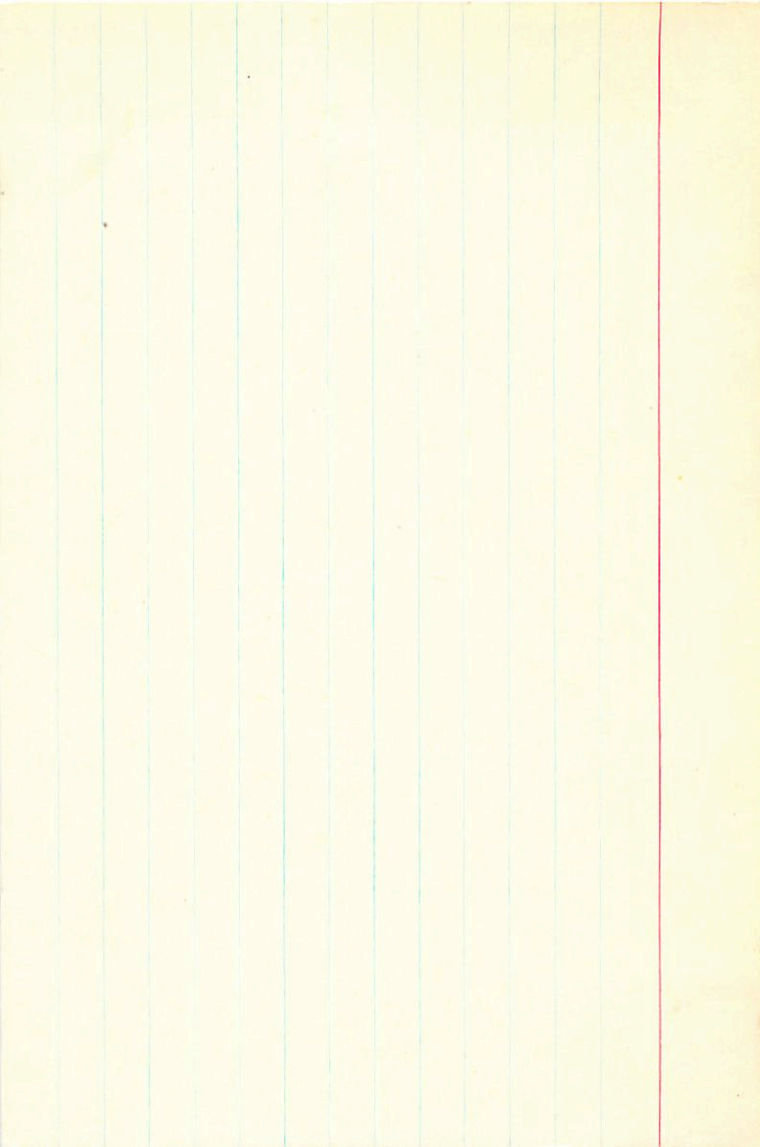
34.640
30.310
4.972
4.976
-1.2
965

48.06 1941.78

$\frac{17.62}{5.48}$
5.79
5.71
-1.02

53.3

+4
5.67



99302

-0024
-0039

Bank
+00
+003

23.1 + 27 01 7.30

6.914 1910.7
094

+001

20.27 1910.4

7.88

-0024 / -0027 -0001
-0027 +002

28
19.99

6.892
+
6.093

19362

20.02 1935.5

-
20.00

44.35

6.877

220

899

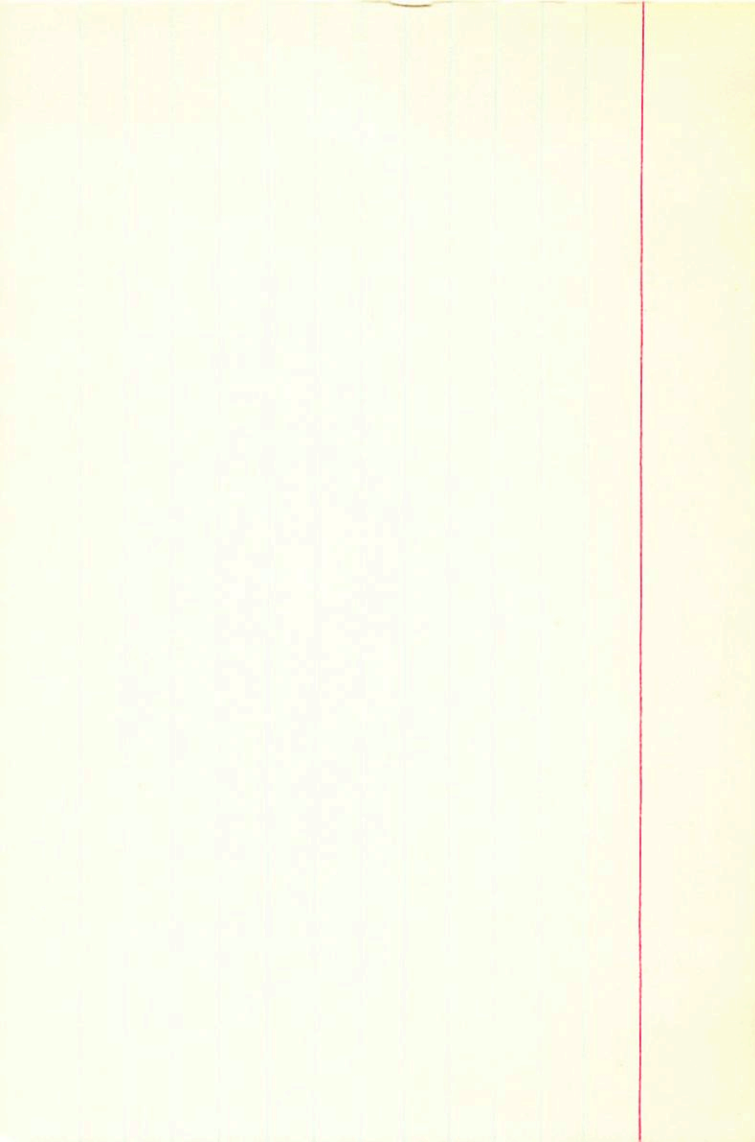
896
-102

19.99

1952.50

-4

19.95



99283
15686

11

23.1

-0087

-0082 ± 2.5

+56

07

+042 ± 1.8

+045

5.8

966

-5.96

6970

8.577

1895.7

+56

7

29.04

1893.7

$$\begin{array}{r} 445 \\ \hline 9.022 \end{array}$$

$$\begin{array}{r} 43.78 \\ 25.132 \\ \hline 8.912 \end{array}$$

$$\begin{array}{r} 170 \\ -170 \\ \hline 747 \\ 749 \end{array}$$

$$\begin{array}{r} 8.600 \\ 1 \\ \hline 599 \end{array}$$

$$\begin{array}{r} 8.579 \\ 0 \end{array}$$

1927

642

-380

43.6

-2.36

$$\begin{array}{r} 26.68 \end{array}$$

42.4

14.15

1826.0

$$\begin{array}{r} 28.25 \\ -23 \\ \hline 28.02 \end{array}$$

-23

28.02

-3

27.99

29.18

-18

29.00

29.24

4

29.18

$$\begin{array}{r} 28.72 \\ \hline + 2.04 \end{array}$$

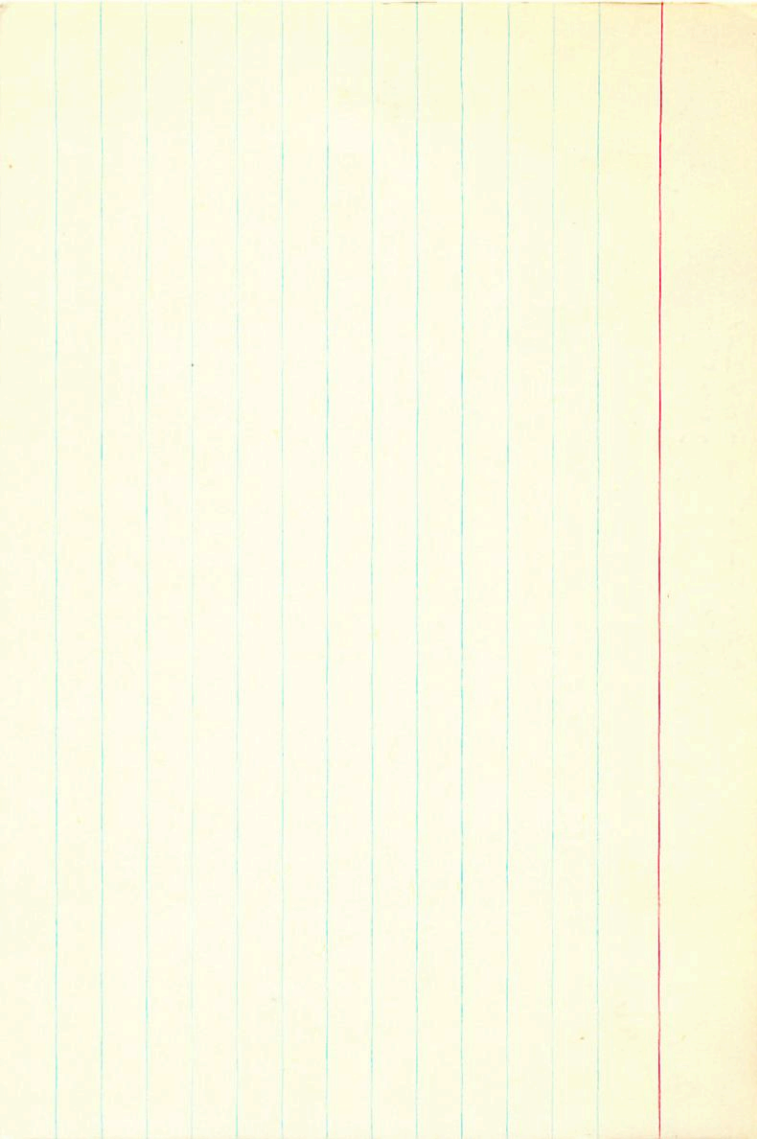
1844.98

1947.14

11802

393

45.6



11 23.5 6342

4413

99453

16 171

812

55776) 321162 2153

8444 222

441

123
229

-315

-314-068

65.5

258

-709

-72

175

31436 150
3640.51

-9834 / -3210

8219

-1815 / 00573

5696

32058 10.7

-0962-548
-0703

42.77 6.0 -08934.1

1.8116
45.74
31.747

2014

4867
325
33.95

-078
-074

74

27
979

4898

33114

4112

464

-20

4661

524

-478
-775

-472 -077

-474 -072

HR 4/12

11 23.8 + 33 44

- 24.6

~ 840 + 613 →

6.37 + 0.44 0.00

51.380.

| | | |
|------|------|------|
| -872 | 358 | 323 |
| 364 | 930 | -049 |
| 327 | -080 | 942 |

| | |
|-------|-------|
| 0220 | |
| +1653 | +1545 |
| -0690 | +0573 |
| -0620 | +0069 |

| | |
|-----------------|----------|
| 1673 | +8.5 |
| 3248 | +147.8.2 |
| -0117 | -0.6 |
| +3454 | +12.7 |
| 0669 | -34 |
| 0776 | -5.0 |
| | -23.2 |

| |
|-----------------|
| +0.3 |
| 18.5 |
| +0.6 |
| +18.4 |
| -24.6 |
| -28.2 |



LIT 0510
4230 11 27.4 -25 10 +20

-249749 10.43 +0.70 +0.09

6.40 -0.221 -0.043

4.03

64.100

| | | | | | | | | |
|------|-----|------|-------|-------|-------|------|-----|-------|
| -873 | 464 | -144 | +9145 | -0950 | +8155 | 52.1 | +44 | -2.9 |
| 370 | 440 | -818 | -2876 | -0847 | -4723 | 41.7 | -17 | 16.4 |
| 318 | 767 | 557 | -3301 | -1563 | -4854 | 48.9 | -20 | +11.1 |

+49
-47
-20

+14.33%
AD58166 99525

11 247 -15 22
22.2 -15 06 15.00

$$7.63 + 0.75 + 0.22$$

$$7.34 + 0.28 \text{ (2)}$$

740
3326
784
570
764
31024
777
737
310
42
782
40
622
310
352
757
42

-0023 -197 stuy
0 +2
-033 -192

| | | | | | | |
|------|-----|------|-------|-------|-------|-------|
| -873 | 484 | -064 | +1365 | -4474 | -3110 | 1.2 |
| 370 | 569 | -734 | -0579 | -5259 | -5838 | -13.1 |
| 318 | 645 | 675 | -0497 | -5962 | -6459 | -24.5 |
| | | | | | | -27.0 |

0312
54858

11 243 -60 50

4415

95556
15709

526-07-61 C

2747

④ 888 + 2584
108
538
134
268

150-1000

③ 2.687
110

-012-1009

+40 +546

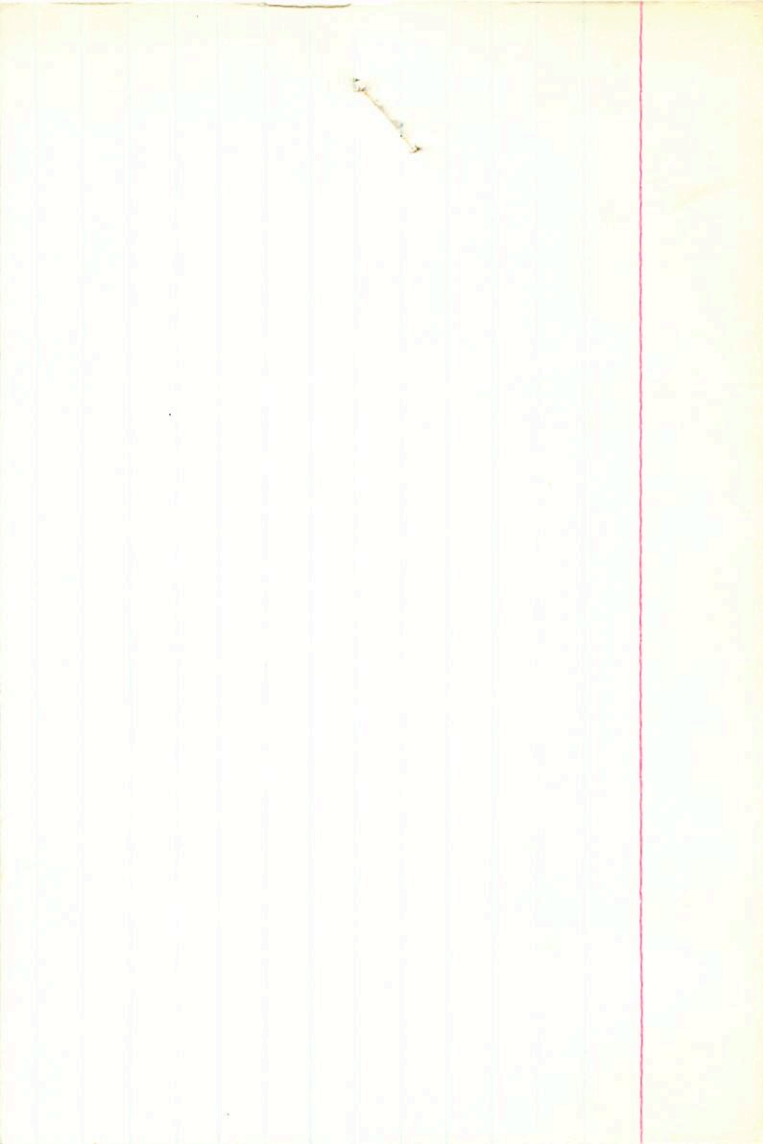
+14
r₀ = 4.84 / 8.15

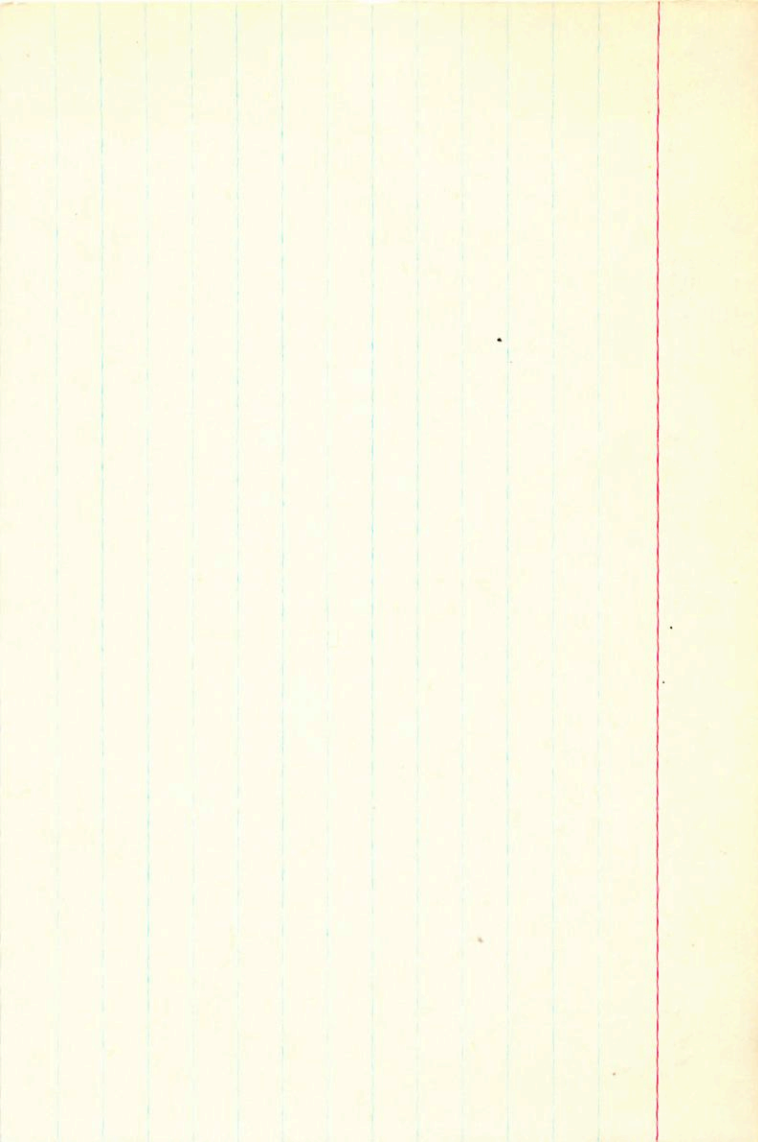
4.8
-31
74

13.83 1.78
2.10 0.25

-74
11V -332
-3.05

8244 4780
5620





4488

11

2602

-47-

24

6618749

~~6618749~~

1035-102-

-0168 ± 3.1
+236 ± 2.6
+238

99747 11 26.2 +62 03 5.9 d/f=1 -8.16

15745

6989

14.015 1887.0 +62 3 62.15 1881.6
1.058
15.073
-16.74
2 48.01

(142)

48.07
26.508
14.571
-2.14
14.304
+10
3.74
12.7 1927.9
15.22
57.48
-118.00
86.50

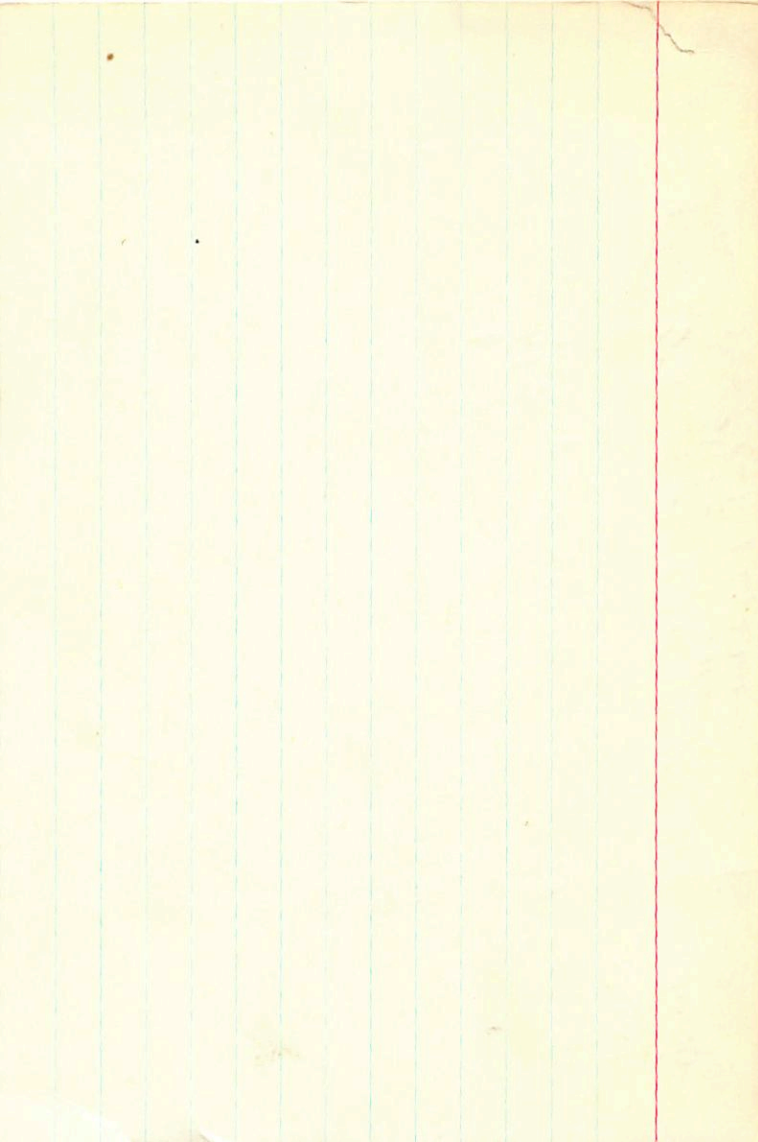
(49.2)

496
248
-825

7246
0.84 1944.56
-10
8.74 1818
36.23
54.6

14.112
10
1220

5900
12.99
+ 12.99



494 230

4934

56302

4933

4932 194214

4931

5003

5022

5148

517

5122

2.19

377

426

431

402

401

4142

540

559

561

562

563

564

565

566

567

568

569

570

571

572

4937

4938

4939

4940

4941

4942

4943

4944

4945

4946

4947

4948

410

363

264

22

0158

0959

463

0113

945

810

876

1409

8510

0910

0010

0020

0030

0040

0050

15486

15487

15488

15489

15490

15491

15492

15493

151-025

041-039

5339

15740

98859

11

26.5 + 57

114424

98859

11

26.5 + 57

12 + 3.2 6

031

26.5 + 57

11

11

98859

04073.0

01173.6

0113

1270687

98859

11

26.5 + 57

148-959 835 545 -080-041 +8.2 -034 +8 -104
+013 005 089 034 -095 445 +5.0 -5 +1 015

-12 +38 +1

-13 013

-15 +46 -2 01

-13 +40 0 012

W6698

TUUMA

11

27.2

+30 21

+95

W6698

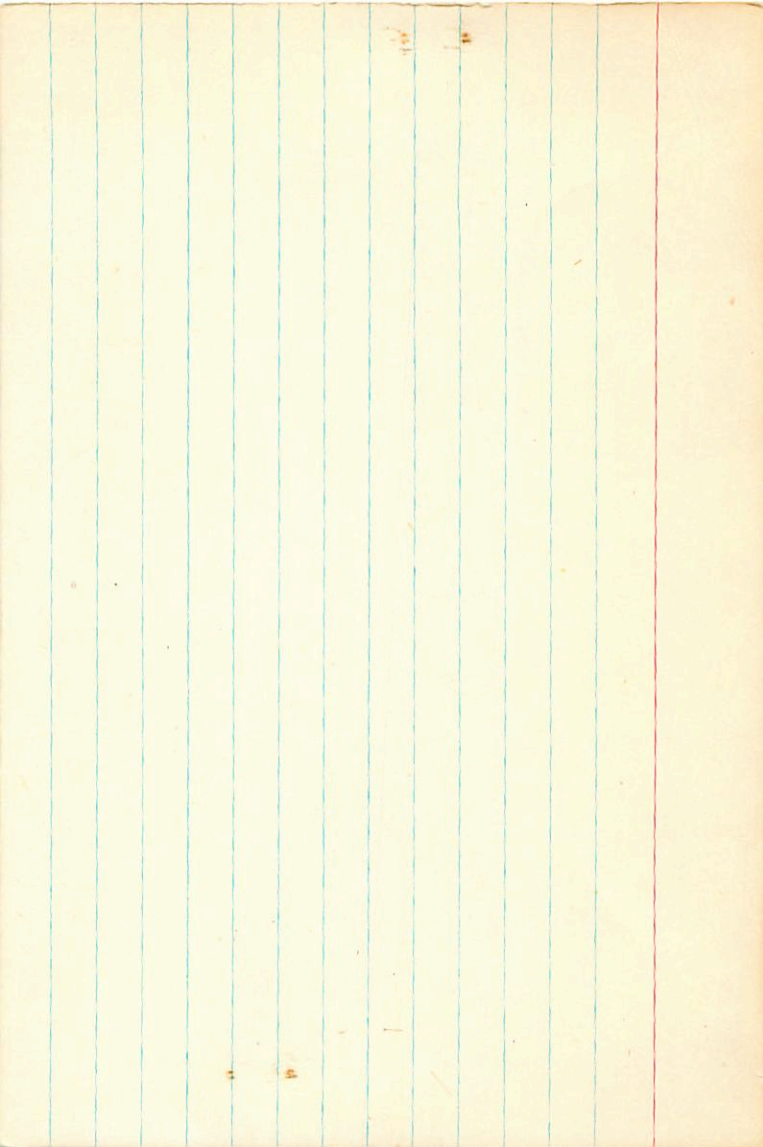
+77 Ⓢ +05 w(3)

$\Delta S = 4$

-07656 -05056

-07656 -04257

+2 -2
0 +2



-222

4427 11 274 454 39 436 65

$$\begin{array}{r}
 1010-064 \\
 \underline{+1} \\
 1011-062
 \end{array}$$

69

65

44

19



-5.115

0.857
0.127

-38.262

0.298
-0.239

-20.807

0.428
-0.114

-22.000

100.000

5.000*

-0.062*

0.011*

39.000*

54.000*

22.400*

11.000*

4427.000*

19

584 ma

99984 11 27.8 +43 27 5.9 dFS -29.6 b

15782

7003

504
-0045 +078 N30

-0045 ± 1.57076 ± 64 Gc → N30

44B |

W350

-00445 +0861

-00455 +0852

1145
+4345

-67

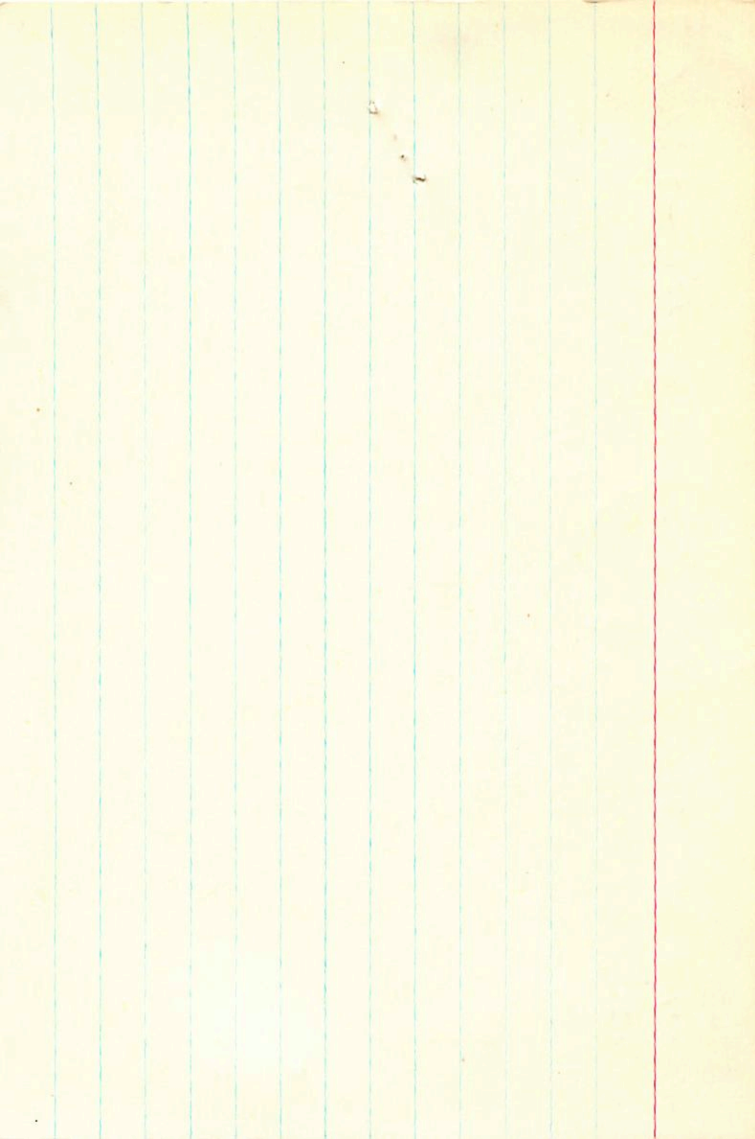
+90

24

-296

-0499

-0604510



59584 11 27.8 +43 27 dFS

HR44H

G-15782

5-9 hmc

5.97 +50 -2 284a

.340 .148 .429 ② SPC-2.628'

③ C4

[m] 209

[c] 361

.2.60 -0.6 +5.5 -326

1313 +264 -159

742

124

20

10883 + 5.1 - 0.92 = 3.8
+ 10885 - 10.8 = -2.20

2100 Debt
118 Debt

10889 - 0.93 H

10883 + 5.1 - 0.92 = 3.8
+ 10885 - 10.8 = -2.20

Pr. 85 years
11 28.1 + 41 34
7.0 0.027

7.931 1903.9 + 41 33 50.82
- 383 4.78 1898.4
7.548 55.57

7.837 38.8
7.837 31.0

41.25
16.25
9.12
4.00 + 2.00
2.1.140
1.1.140
1.1.140 + 2.00
1.1.140
1.1.140

51.14 1935.3
4.78 1898.4
55.57

66.8
33.4
35.0

152.55
- 11.48
52.55
- 3.78

162.75
15.85
52.20
152.55
- 11.48
52.55
- 3.78

51.79

129-990 663 748 +059-093 -2.2 -062 -1-332

-012 009 -058 061 -346 -374 -2 -2 0 0127

-30-29-27

-41 -22 +18

-27-29-20 014

$+0020 \pm 4.9$
 $+0030$
 -0000
 -0000 ± 4.2

A058190
 100070

11 28.3
 -06 27

7.6 dF3 + 4.1 b

15793

7009 18.182 1895.0

-6 26 35.3 1894.2

$\frac{143}{18.039}$

$\frac{+133}{3480}$

$\frac{1.847}{16.260}$
 $\frac{18.1310}{147}$

38.8

113433

$\frac{19.07}{15.95}$
 $\frac{35.02}{35.18}$

10¹¹ 10¹¹ 10¹¹

$\frac{154}{18805}$
 $\frac{154}{115}$

$\frac{35.07}{4.27}$

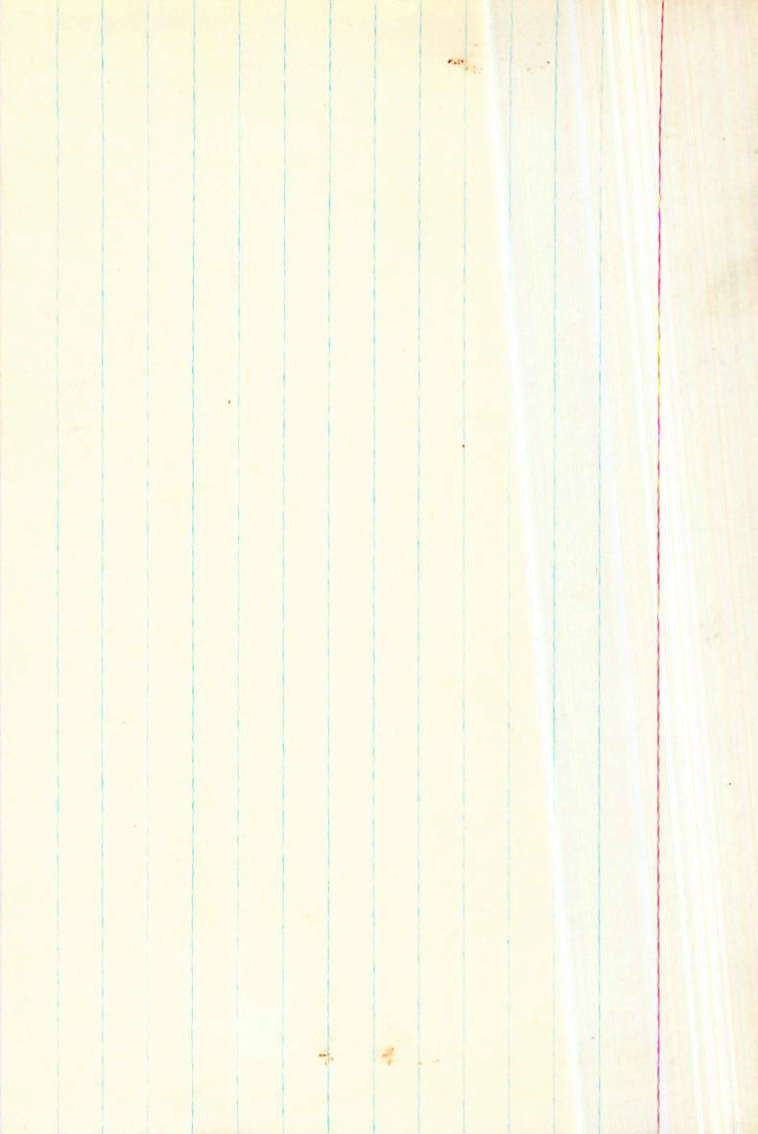
$\frac{151}{18.149}$
 $\frac{16}{157}$

$\frac{35.20}{35.15}$
 $\frac{35.05}{35.05}$

35.21 1933.26

$\frac{769}{33.8}$
 39.6

35.09



32.24

5.77 030 162-1033 2.405

95522 17.2 11 27.2 -24 11

THU

15765 10037733 +036 ± 6.7

041

9.157 60.8 -0032 +010 17.15 55.5
152 10033 +005 7.8
339 10031 +014 19.97

2003

516 -413 45 934

2003

9.112 66.74 18.8 -0032 +012
717 -12 -00314 +0042
126 18.00

3425

9.229 18.16
124
14.17

2487

63.14
-4.10
14.610
9.7 40
224

3487

1140
0000
407
4.78

6843 - 9787 0417
2008
1767
19.11
15.1
17.1

224 5 227

99906

11

271
246

7 5-3
~~8~~ 22

—0007

—025

5-013 9816

8-5-18



4436

11

28.4 + 49

13 6.31 0.5

+ 6.36

-031-0466

+1 +2

-030-0466

25



1.000*
28.400*
49.000*
13.000*
-0.030*
-0.046*
5.000*
100.000

6.300

0.064
0.401

0.949

-0.251
0.205

-23.776

0.029
0.893

0.482

0.8 (1)

2 dia 11 28.5 +69 36 gmo F22a

HR 4434

3.76 +1.65

-041 -020 F103

100029
15799
7012

MONT

WB -0.1

-040 -022 GC

-038 -020 N30

88
-0072 -020 N30

-039 -021

-0072 ± 0.7 -024 ± 0.5 GC

-040

+12 | -6 +10 -018

+18 | -13 +11 -011

11 10
-00778 -0259 W3 50

-00767 -0244

-0401

-040 -021

137-551 937 349 -039 -021 +2.2 -020 +7 -033 ✓
005 003 039 020 -071 199 +7 -7 +1 018 ✓

$\frac{11}{+12 -6 +10}$

$\frac{-14 +19 +4}{+15 -13 +11}$

011

4437

08/10/17

AD5896

11 25.2 114 39

① 380

0225 → 190 Amput

326 190

-337

791

0.85

-4

2.5 26.5
2.5 26.5

0.85

3256
-6359

9961-8121
-0465 5836

22

-0001 ± 4.4
-0016

-20.948

100261 11 29.4 -59 10 2.64 79.58

15818 5.12 +1.07 +0.90 1.184

7019 26.835 1911.1 -59 9 57.91 1905.5

+71
57.20

57.46 1939.67

31.9

26.779
-18
76.1577
26.80
14
816.051

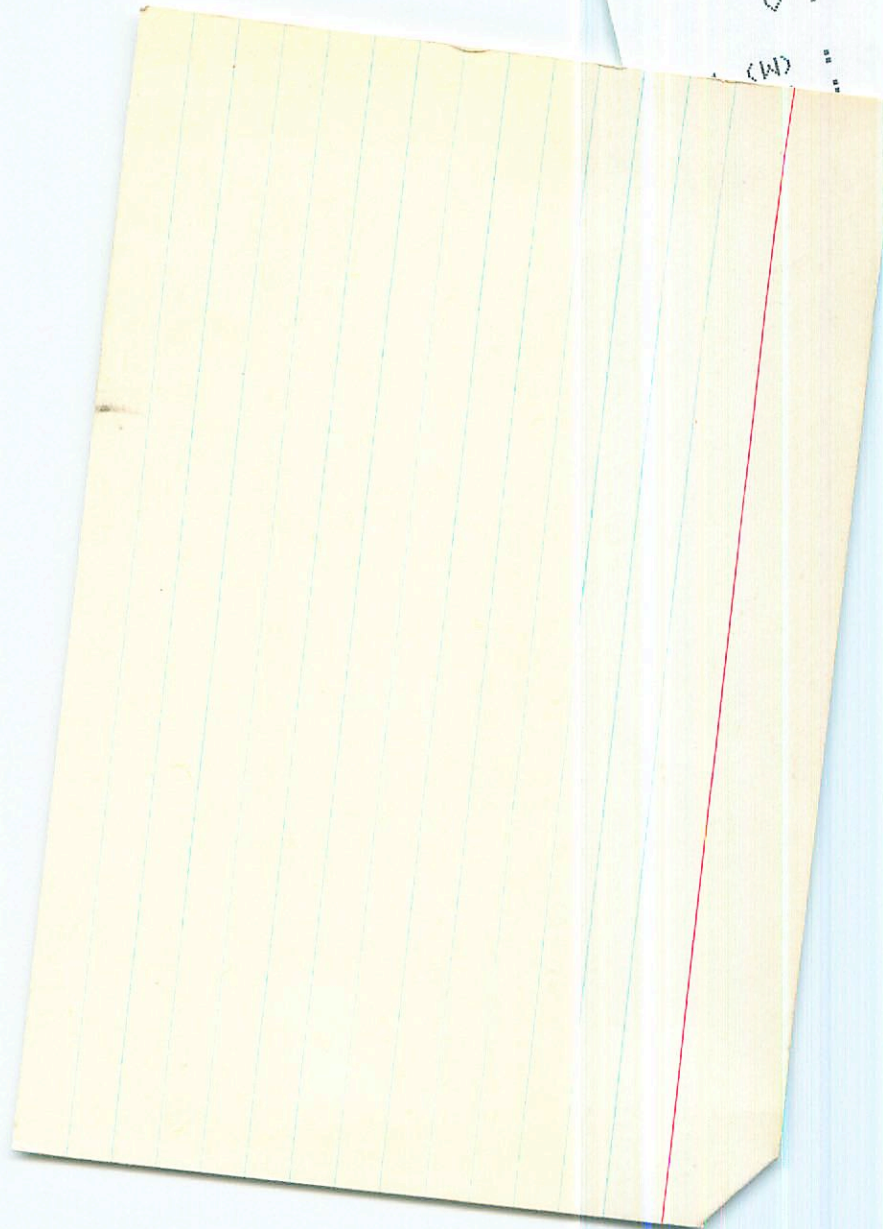
57.79
56.5 1946.4

-79
57.29

86.07
43.0

57.54
-34

37.5



U :
(W) :
0.300
0.234
0.925
674.311
-13.673

-0021±5.0
-0008
-009
-009

~

160262 11 29.5 -59 14 5.3 A2p -16.8 8

15820
7020
+6 12
+0005
+003 M30

5.13 +0.41 -4.48 5.24
5.14 +0.47 -0.14 1.184

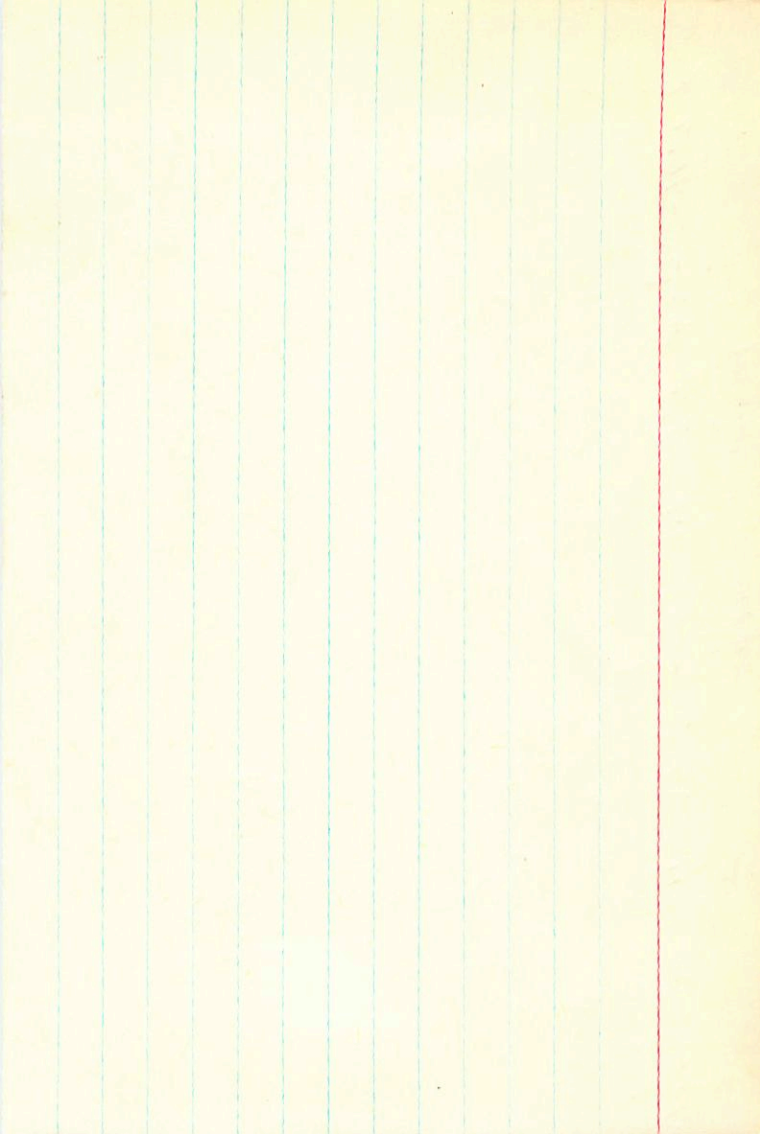
29.493 1912.4 -59 14 22.59 1900.0
79
1572

22.23
22.14 1940.27

30.9

29.538
-18
520
548
-024
29.546
576

22.47
21.8
-79
22.59
22.53
-1.30
1946.4
86.67
43.3
33.3



1002.03
A058197 15822
7021

+0001 ± 3.3
-0015
-0.73 ± 2.3
-0.23

438 (21)
448 (2)
45.9 a

$\Delta M = 1.43$.0366

31.718
 6
712

1883.7

+6121

3476 1892.8
418

 38.94
38.94

6.50
25.352
 8.32
31.220

52.9 1927.1
16.25

 36.62
36.62
 19
36.43

649

+001 -073 CC

133 -991 878 479 +101 -073 -45.9 -064-40 -166

0 009 0 064 -303 043 -22.0 +22 -2 0366

+14-1-45

+21 -27 -3Y

A058199

100214

15826

7022

10th 11.5

-0308±5.7
-0294

+56 22

→ 50

+070±3.4
+075

8.0 dF7 +13.3 b

35.355 1903.7 +56 22 1282 18906

1.426

36.781

12.44

23.800

36.240

-115

1126

131772

35.550

549

35.462

0

+56 22 1282 18906

-4.16

8.66

27.6

16.30

11.390

11.144

809

6.69

12.33

+3.67

12.95

14453

36.0

5724

-1057

35.462

0

119.19

39.73

49.1

194714

13.00

-6

12.94

