

128642
-4909033

14 41.8 -49 42

$C_2 = -4.8 \pm 0.6 (4)$

43328

8.38 +0.95 1037
838552 470 302 (3)

14 36.5 -4 28.9
-1.040

866
866

-2.56
-2.44

+48 -53 -4 .050

+75 -87.5 -10
+219 -279 -28

+53 -58 -6 .045

6267
45276

+57 -64 -6 -0.42

-665 20.5

-348

-629 ± 5

CR

-374 ± 2

-702 -624 ± 4

-381 ± 4 CP

-376

-672

20 ± 11 C(8)

-68 -38 Cin

-684 -381 Comp

-656 -378
Comp Mean

26.87
 23.47
503.4
 50.9
 6.953
42.068
4.013
1.80
168

55.3
 5.2.1
49.8
 42.772
 29.60
23.73
53.33
12.22
52.13
52.24

1902.30
 1928.22



21V Dia
130082

SR 27.4

14 42.5 +56 19 gMI -35.08

8564

-0048 ±5.1 +013 ±7.3
-0033 -004

4R. 33.547 1920.5
142
33.5689

+56 19 3.19 1919.8
-39
2.80

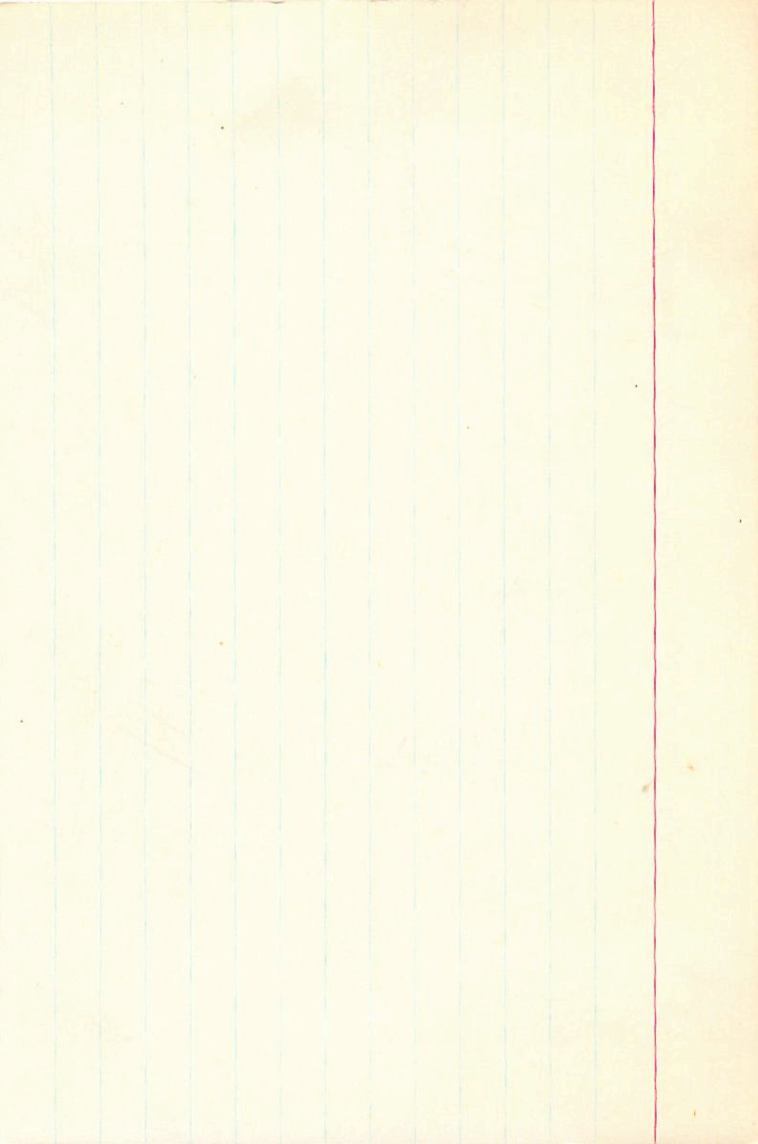
33.585
16
601

2.89 1947.29
-21
2.68

10,6
- 48 +13
- 33 - 4
- 25 +3

- 35 +4

4 de
-0026 +003
+1 0
-25 26



129747 14 22.5 -45 40

-536 ± 1.2 9 (5)

1985 |

6.49 + 0.66 6.25

+70 -4 -6 .020

-183 -070 6

-0159±4.3 -072±7.5

-651 -759 -716 668 -193 -070 -53.6 050±35 -232

-119 033 139 -038 -384 815 -324 +28 +24

+2 +78 +23 015

27.670 1400.0 -45 40 13.53 1598.1

795
28465

3.74
9.79

~~46~~ +92 +19 012

+50 -25 -3

+7 +69 +25 018

+73 -9 -5

129989 14 42.8 +27 17 2.7 9100 -16.5 a
19856 3" 5.1 43m -16.28 sp. B 11

8567 -0040 ⁶³ +018 ⁶⁵ N30

0059222 -0039 ± 0.7 +018 ± 0.6 66 7a 31 (B) -255 (8) 2Sp
A -157 (8)

Dm = 2.57

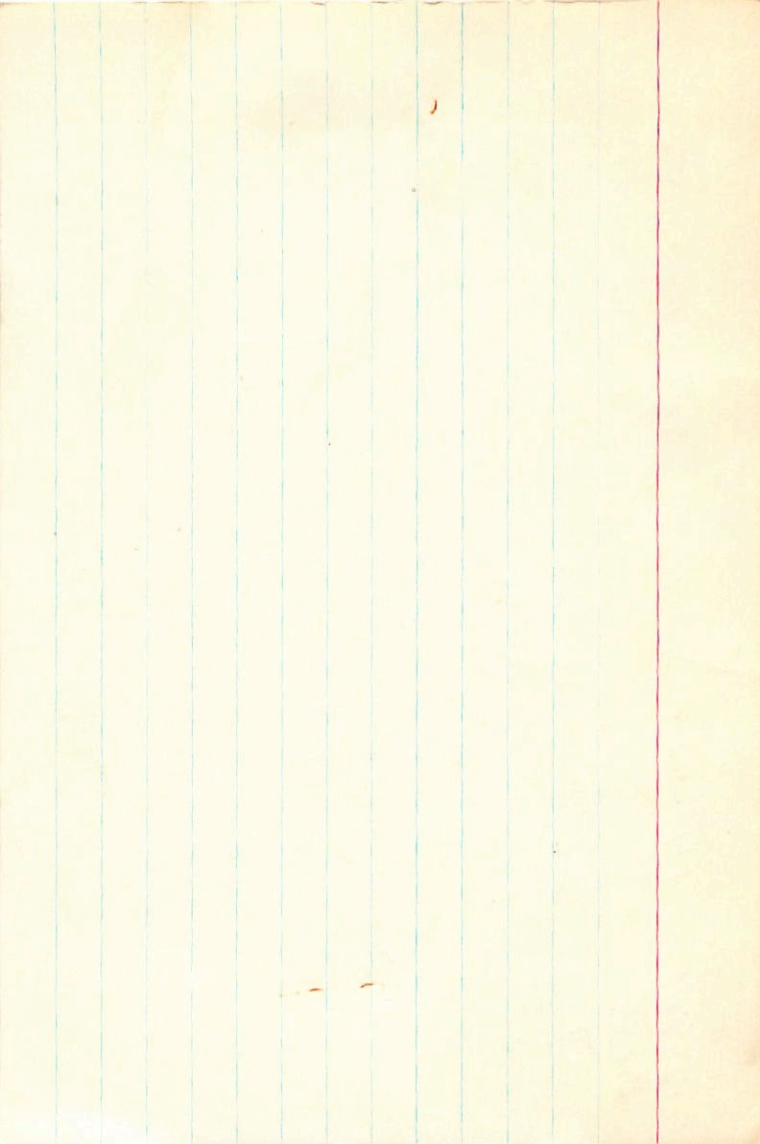
(5505) 00361 +0154 W3 50

00362 +0153

8438 -9161
-4498 4009

0492
F045 +022 0500
-0021

-1.7
0058
6.17 -20.4



52
416

(3.17)

-0.4

Σ 300

14 42.8 + 27 18

NO II - II

5506

5111

129589

AD

2.37 + 0.57 + 0.73 45

512 A2E } 30.6
100 II - II

158 + 0.305 55

2.7

13

112
811
W2

-00361 + 01874 - 456

-16.5 W

-00364 + 01874 ± 2.5

-0.00355 + 0.01889 ± 2.0 +

9688-9480 0-0B

-5034 3144 -0053

-00370

3.15

0443
-0446 + 0.21

8940-9160 0506

-7/6

0054

-4442 4013 -0.6

6.22

0059

0.15

8

0 Boov

-0042 ± 2.2 -058 ± 1.9

29.0 (1)

129972 14 42.9 +17 10 4.7 9.66 -9.49

19859

8569 54.383 1895.6 +17 10 29.82 1898.1

$$\begin{array}{r} 228 \\ \hline .611 \end{array}$$

$$\begin{array}{r} 54445 \\ 19 \\ \hline 464 \end{array}$$

$$\begin{array}{r} 464 \end{array}$$

$$\begin{array}{r} 54.442 \\ +17 \\ \hline 456 \end{array}$$

$$\begin{array}{r} 460 \\ \hline -151 \end{array}$$

41.2

$$\begin{array}{r} 3.01 \\ \hline 32.83 \end{array}$$

$$\begin{array}{r} 3043 \\ -06 \\ \hline 3037 \end{array}$$

$$\begin{array}{r} 30.65 \\ -10 \\ \hline 30.55 \end{array}$$

$$\begin{array}{r} 30.44 \\ \hline -2.37 \end{array}$$

$$\begin{array}{r} 30.65 \\ -10 \\ \hline 30.55 \end{array}$$

$$\begin{array}{r} 30.44 \\ \hline -2.37 \end{array}$$

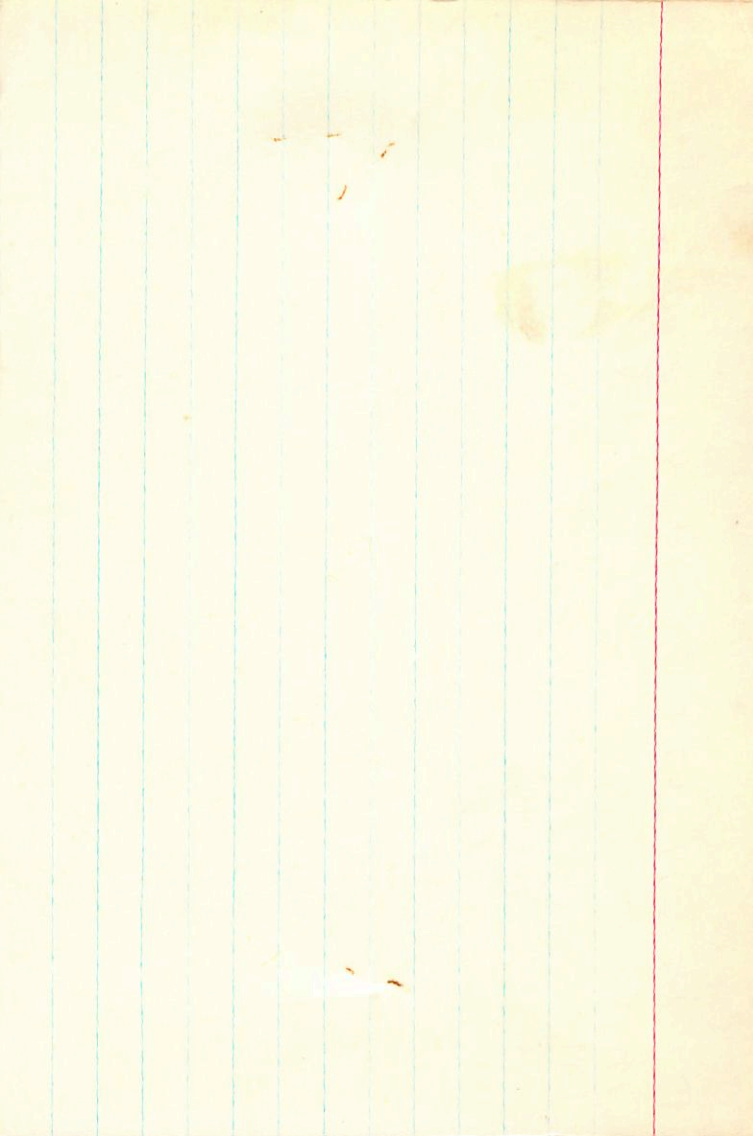
$$\begin{array}{r} 30.44 \\ \hline -2.37 \end{array}$$

$$\begin{array}{r} 30.44 \\ \hline -2.37 \end{array}$$

$$\begin{array}{r} 73.67 \\ \hline 36.8 \end{array}$$

$$\begin{array}{r} 36.8 \\ \hline 38.7 \end{array}$$

38.7



7406-9612
-6720-2759

034 ~ 25 5.55

034

550 43.0 70 56 B9

129956

19860

+100 120 1029 2.935
1264

-25.5 (9) (0.2)

5.69 - 0.03 - 0.07 2595

72154

woff

5.70 002 121 5023 25836 (2)
-0.14 733 1.021 2926 2,5,4,6

-25.5

7406-9612
-6720-2759

0428 124 1024
0029 258
1282

l'auvel

015
510

-36

h

14.7
+0.9
-40
-10

002 121 1023 25836
(129) 1023

0024
400

0124
410

0434

0421-009

-25.5
25

4110 25.1 482
-55.85 2525 1278
-56.3 25.25

0028 - 013
 0030 - 016
 15949
 0028 725
 018 222
 011
 012
 017
 019
 3811
 19559

$\frac{140}{253}$
 $\frac{0030}{0028}$
 $\frac{-012}{-017}$
 $\frac{26}{3811}$

-0028 - 014
 -014

35.02 1989.27

$\frac{+16}{504}$
 $\frac{-10}{35.12}$

50

$\frac{52246}{+30}$
 $\frac{271}{271}$

$\frac{51147}{28}$
 (5841)

3814
 3887
 1931.2

$\frac{3786}{-28}$
 $\frac{15.87}{37.93}$

$\frac{52135}{+11}$
 149

$\frac{8514}{-28}$
 3761



43
 150
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 200

91
-187.949
32.13
0.789
0.448
-0.420

13
-14.537
-126.794
-0.070
0.746
0.662

22
22.846
56.581
-0.610
0.493
-0.620

14.700
0.900
-40.000
-10.000
5.800
145
-25.500

-0.620
0.493
-0.610
94.188
29.171
0.662
0.746
-0.070
-160.934
-21.464

-0.420
0.448
0.789
56.435
-11.678

69

288
300
311
320
331
342
353
364
375
386
397
408
419
430
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672
683
694
705
716
727
738
749
760
771
782
793
804
815
826
837
848
859
870
881
892
903
914
925
936
947
958
969
980
991

FD

14.700
0.900
-36.000
-11.000
5.800
145
-25.500

-0.620
0.493
-0.610
80.094
27.134

0.662
0.746
-0.070
-151.911
-20.160

-0.420
0.448
0.789
48.345
-13.137

89

564

129978

14 43.2

-15 15

6.6 9102 -3588

-0023 ± 1.9 -008 ± 1.8
-0026 -004

19870

8576

12.061 18944

-15

15 0.14

1891.4

AD59376

128

+ 47

11th 3rd

.189

39.67

39.68 1922.66

49.360

22.658

21.30

0.028

12.1048

.096

149

39.7

+ 39.98

68.16

102

084

+18

34.1

12.064

-105

53.50

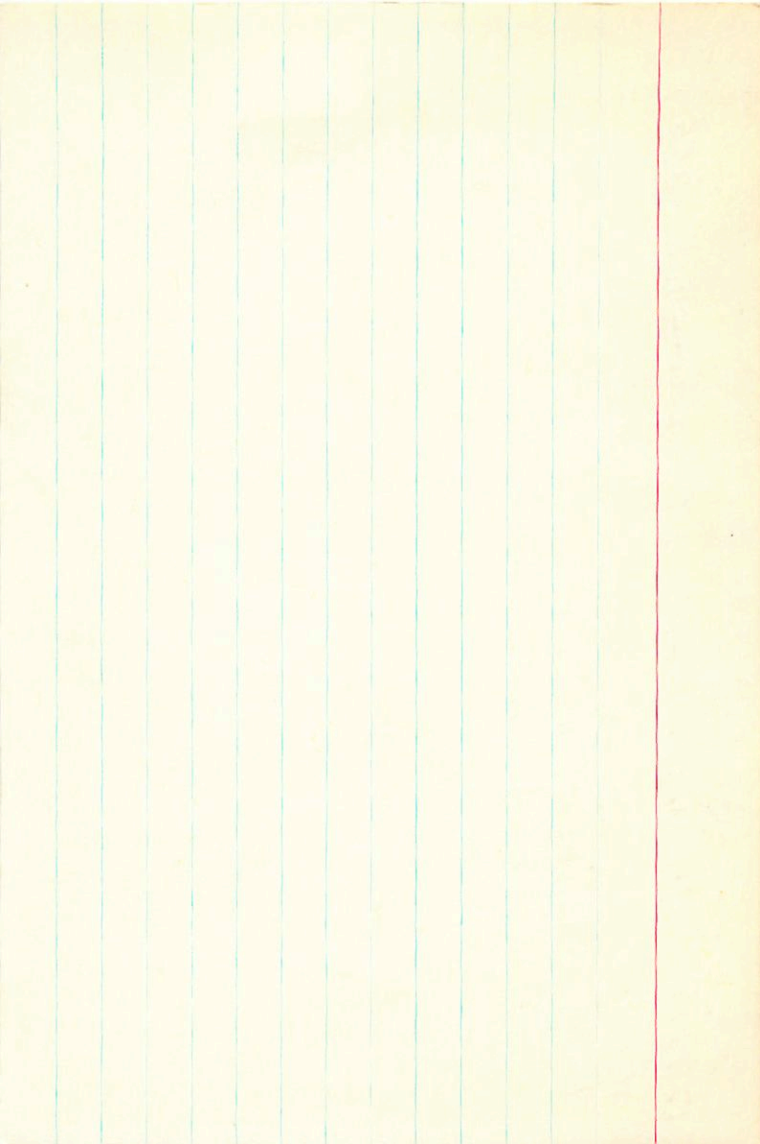
42.7

55.87

067

59.84

-0.17



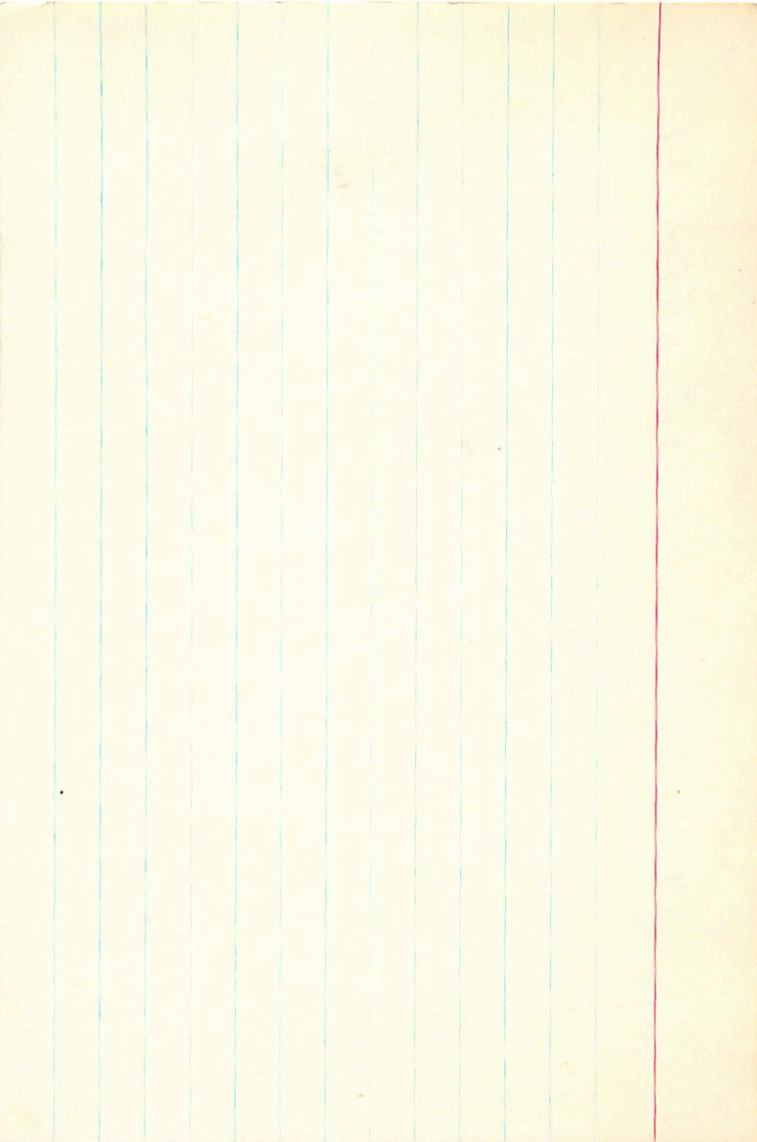
129944 14 43.2 -22 57 5.9 965 +7.38

19871

8678

+0018²⁹ -063²⁷ N30

+0017^{5.6} -060^{5.2} 66 -9430



125893 14 43.5 -52 10 5.2 26 -20.86

19874

8580

30.572 1609.5 -52 10 24.19 1907.1

097

669

+4.12

20.07

30.612

-33

579 38

23.00 1941.03

-38

23.38

9948

48.7

41.0

787

23.94

-3.87

30.569

-28

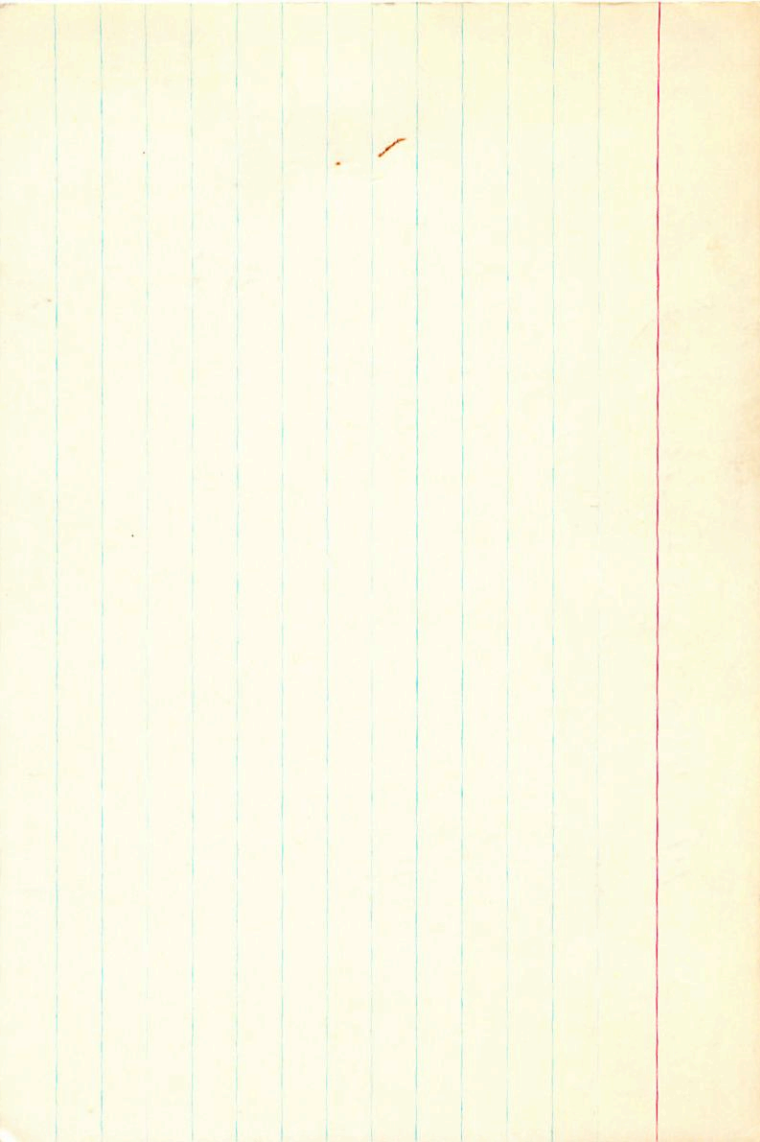
547

2423

-28

2451

1956.35



11.67 + 0.58 = C 50.11 gm

-0072 ± 3.7 + 047 ± 2.8
-0063 + 045
-0062 + 049

-2.1.16

ADS 937T

14 43.6

I = 11.12
m_r = 6.05
W 8581 130188
1968T

~~00488 4928~~
0.117

Sparks

815 7.39 + 0.46 - 0054 + 062# - 079 + 045 H

Δm = 0.14

36.447
379
826

1897.4 + 42 35 25.37 1893.7

1550 ± 0.55

36.024 74.29
122 202.995 - 2.65
121 1849 2965 25.72

⊙

P = 87.71 (P) = 11.67

36.523

2762 1985.4

a = 0.325

39.95
56.732
36.684

220 35.1

650
32.5

L = 5151

36.684

46.9 1925.6

C = 0.54

36.684

38.5

Constant

40
-0065 + 047

2749 27.46

5.0097
5.07
5.07

-0066 + 051

2720 + 1.74

43.16
43.16
3.2

-0728
00695 ± 0.545

9446 - 8655 0878
3282 5010 - 0178 - 5.35

14.9
14.9

677 736
-655 - 756 ~~1079~~ + 045 - 079 + 045 - 24 030 ~~156~~ -14 156

-052 020 060 -023 -137 379 -15.5 +12 +10 0117

-68 +50

0 +43 -1
[+38 -20 -7]

-658 +746 -106 +2339 +1768 +41.07 ^{+2.2} -2 +48 +2 10

+656 +636 +406 -2332 +1507 -0825 -8.6

[+43 -20 -5]

-370 ^{-19.2} 2198 +408 +1315 -0469 +0846 +41 -20 -5 105

+43.3

-16.8

-10.6

89

777.0 (U) SP
777.0 (U) SP
777.0 (U) SP
777.0 (U) SP

777.0 (U) SP
777.0 (U) SP
777.0 (U) SP
777.0 (U) SP
777.0 (U) SP

777.0 (M) SP
777.0 (M) SP
777.0 (M) SP
777.0 (M) SP
777.0 (M) SP

			0.000
	U	:	0.000
q1	(V)	:	0.662
q2	(V)	:	0.604
q3	(V)	:	0.443
	ΔV	:	0.000
	V	:	0.000
q1	(W)	:	-0.420
q2	(W)	:	-0.191
q3	(W)	:	0.887
	ΔP	:	0.000
	M	:	0.000

-206-090Y
-204-090S
-208-090Y

130095- 43.9 -27 02 88 +50 van 35A

+435+61

26010505

4000

8.12-70.08 +0.05

62.4 G. L. L. L. L.

50 350A van

-0.211 -0.082 > 60

+3 +6

-0.208 -0.076 →

-207-097

lihat HD Baras
aka Phillips

6-9 (m) (c) β

078 090 1150 2861

u v w 147 B 9 1/2

M₄ = 0.5 + 108 + 286 + 55

5.0 + 62

~~60~~

↓

6 plants
slightly

= 62.4/100

35000 plants

Vanuatu 43500

~~43500~~

10

1875
1876
1877
1878
1879
1880
1881
1882
1883
1884
1885
1886
1887
1888
1889
1890
1891
1892
1893
1894
1895
1896
1897
1898
1899
1900

14.700
-27.000
-229.000
-87.000
5.000
100
62.000

~~7.321~~
2931

0034

-0.620
0.150
-0.770
537.760
6.039

4109.9

0.662
0.626
-0.411
-090.881
-115.387

289

-0.420
0.765
0.488
99.983
39.340

+5744

61

78

9389

14 43.9 + 42 34

48

41.7

 $\gamma_w(1)$

$$\Delta m = 0.14$$

$$= \frac{325(4)}{16}$$

148 7.30 + 0.47 + 0.005 4 60"

35 $\times 10^{-6}$

39

430

665

 $\rho = 87.71$ (average)

c-1 #12

c-2 #12

c 12.46 + 1.34 + 1.18 3

11.67 + 0.555 (5)

13

 $\rho_{int} = (14 \text{ mph}) 0.014$

$$\rho^2 = 76.93 \times 10^2$$

$$c_3 = 24.326 \times 10^{-3}$$

$$a_3/p = 4.462$$

$$\rho_1 = \rho_2$$

$$\rho_1 = \rho_2$$

mv (c)

 $m_1 = m_2$

1.00 6209

+ 35 - 16 - 7

60

2.00 11.11

1.62

4.3

 $\rho = 44 \times 10^2$ 77.1 $\times 10^{-3}$

39.1

M U W

Applies

640

755

740

430

S 19
13
AS
07
AS

+0050 ± 4.3 -268 ± 4.0
+0051 -270

+25.4-6

AD59380

14 43.8 +9 52

0.0185

+0.075 -267H

49.184 1898.3 +9 51 34471887.5

-258
48.926

48.926
48.926

49.093
120

48.926 1834.8

38.43
2.4

35.3

37.9

37.76 1987.6

49.118

16.15 12.4

49.119

38.08

36.2

+193

- 10.46

38.7

-656 -755 171 995 +075 -2267 +25.4 -046 +4 -1226

049 030 057 035 066 412 +25.0 -19 -16 0185

~~-15 +6 -6.2~~

~~-25 -57 -17~~

130145

14 43.8 109 52 dg-1 +25.47w(3)

GC19886

7.62 +0.62 +0.10 $\sqrt{2}$ R

W8584

$\delta = 0.5$

$\Delta M = 0.62$

A059390 $\Delta M = 1.0$

1"

± 4 ± 4

+074 -268 GC

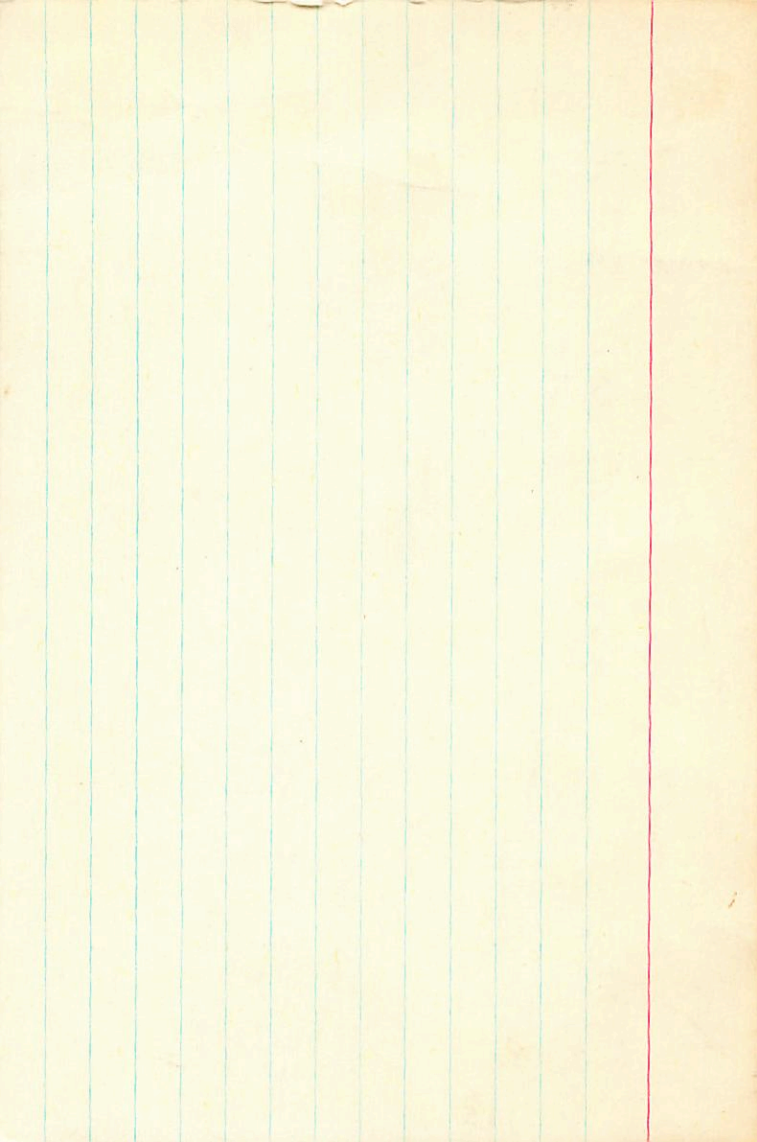
+075³⁴ -267⁵³ height

-41 -18 +5 035

-50 -29 -2 .025

-60 -36 -7 .020

+075 -267



HR 5513

14 941 -21 07

-240

GC 19895
W 8587

$-0015 -0025 \quad 20$
 $-00165 +0006 \quad ac$
 $-0016 +005 \rightarrow$

200

-022

-612	227	-758	+0638	+0054	+0692	+13.8	+18.1	+32
664	669	-336	-0629	+0158	-0471	-9.4	+8.1	-1
-430	708	560	+0448	+0168	+0016	+12.3	-13.4	-1



+1702785

14 44.1 +16 43 DIP6 +47.8 (u(14))

GC19890

9.24 +1.28 +1.06 R5BR

73343

+121 (V) Var

+1702785

W8586

-126 -925 GC

-61 -50 +30 .064

-69 -42 +27 .053

92M(6)

850(3)

420(6)

167 ± 5

-0088±7.1
-0089
-928±7.3
-927

3.032

1503.0

716 43

6.61

1904.0

414

3.446

42.64

4930

3.150

17
167

16.14 1839.42

0

4512

32.6

346
183
263

29.6

484

1425.7

53.05
10228

3.279
287
566
199

28.60
65

2943

4556

2278

2942

26.52

28.6

-26.52

130073 14 44.3 -43 2/1 P1 III -22.5 ± 0.6 YC

FD 1210 $+0.89$
6.24 + 1.08 (2.12)

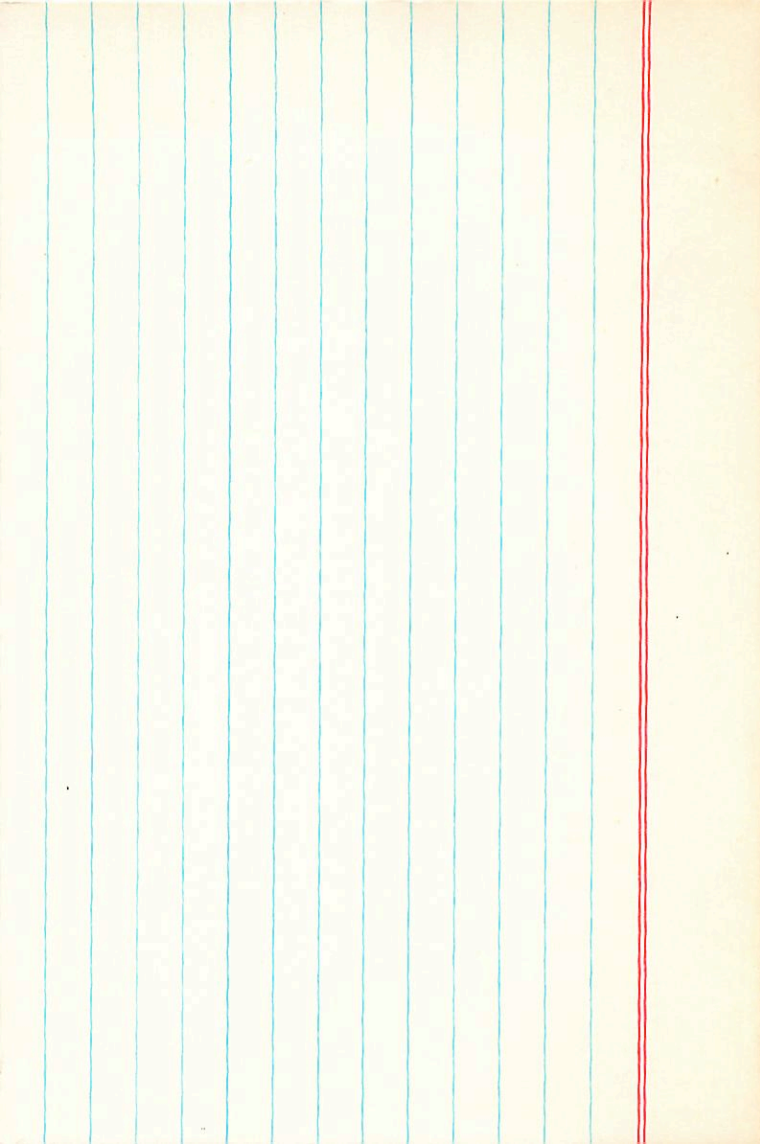
GL 16843 -0.014 ± 9.5 -0.38 ± 6.9

BR 5509 16.442 1500.1 54.21 18460

151 fgs |
-0.21
+0.1

-0.11
+9

5005
-0005



4059883

-0015 ± 4.4 - 043 ± 3.0

130256 14 44.5 t01 11" (6.8 A0 + 6.50136)

19900 3.5 (9.1 dF3 - 7.18

8689

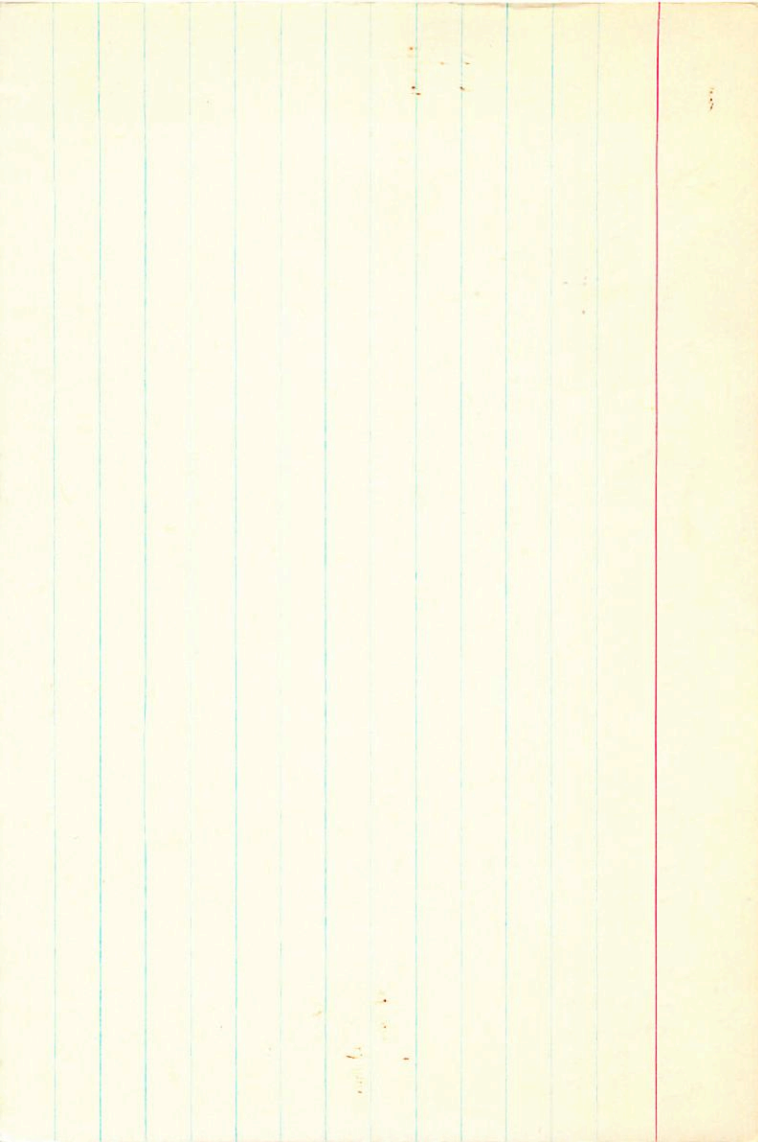
32.866 1596.4 t1 10 46.77 1888.2

$\frac{080}{.646}$

$\frac{2.66}{49.43}$

$\frac{32.528}{25}$
 $\frac{553}{693}$

47.79 1934.1
 $\frac{-16}{47.03}$



AD59394
Mild

-0044 ±1.9 -022 ±1.5
-0043 -028
-020 5.8
14 46.6 -13 57 2p
-0046 5.4
1/5 (6.3

-2.1 Book (7)
-4.1 6.
Am ~~1276~~

130554
14936

8600

34332 1501.7 -13 56 30.73 1898.6

$\frac{213}{1,545}$

3428
1144 3074

+1.13
 $\frac{29.60}{-}$

-994
-0350

5523

12.141
22.250
 $\frac{34.345}{436}$

2014

3087

15.19 162744
16.48

107.69
35.9

3422 3038
30.58

11.92
397

34.2

31.67
1.67
30.64
+14
30.52

50
30.63
-1.03

37.3

34390
 $\frac{37}{37}$

-148

30.40 1139.09
-16
30.40

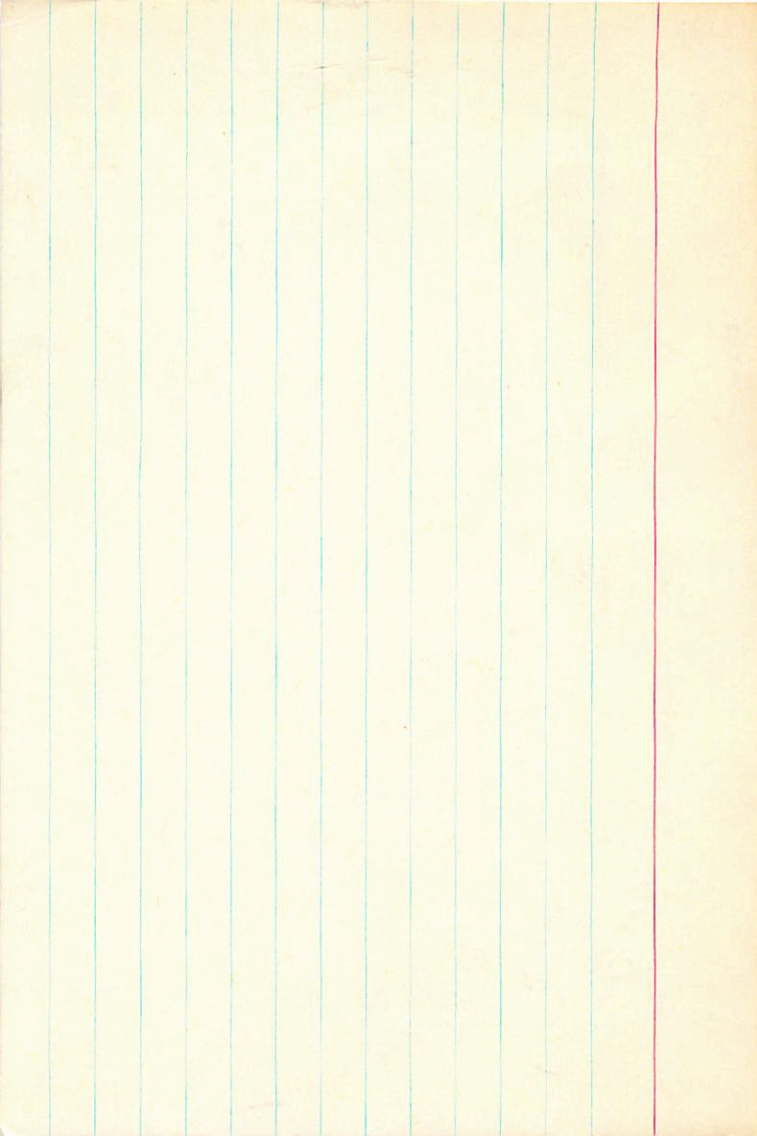
1451
1.522/93
32.52/127
31.2/512

-0024
-0183

0.64 -0.15

0.69
0.10
0.30
0.15
30.78

1941.1



56 Hugs

130259

19904

8592

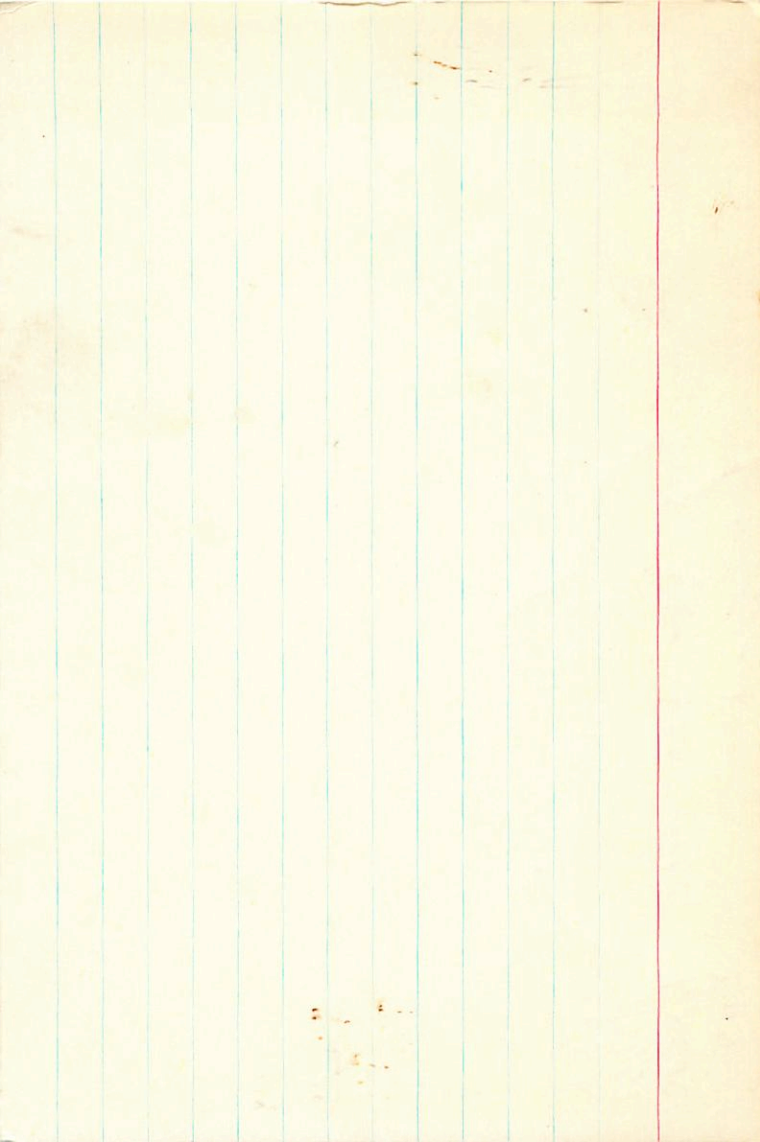
14 44.8 -25 53 5.4 g 25 -0.5 a

M D

43 44 N30

+0031 -010 2.4 66 7030

+0033 2.5 -007 2.4 66 7030



130265
19923

14 45.7 -58 55

+72.3 ± 0.6 C₂(14)

8.53 + 0.63 6.34

+76 +24 +4 . 019

Cur
-0.128 -0.17 mm

-662 -750 -856 517 -128 -047 -72.3 040+62 -114

-085 026 096 -030 -280 5-78 = 37.4 + 28 + 25

-0173±83 -044±6.7
-6168 -061

+2 +83 +51

010

44.299 1905.1

-5855 25.58

1500.4

+96 +2 +8

133
53

46,076
477

32.9

23,40

7.44 1424.44

7599

33
50

51.403

53.010

44.413

250

44.663
44.663
44.663
44.663

1045
44.522
53

-18.40

21.39

137

25.02

25.13

144.5

136

25.68

21.28

380
37.0

44.410
44.410

25.14
-61
20.21

ARS 9392 $\Delta m = 0$ -0010 ± 4.1 -092 ± 3.2
 130604 17 46.4 $+06$ 10 -0002 -086
 19934 6.7 dF5 -1.38

8597 24.220 1892.7 $+6$ 9 45.30 1888.2
 $\frac{057}{1277}$ $\frac{+5.69}{50.99}$
 24.248 $\frac{27}{1258}$ 47.04 1934.2
 $\frac{24.265}{270}$ $\frac{46.52}{46.84}$ 1938.4
 $\frac{270}{-007}$ $\frac{46.83}{-4.16}$ $\frac{36.8}{48.0}$

ADG 9394

130524

14

46.4

-24

03

5.8

9/11

-26.36

-0018 ± 3.9 -012 ± 4.0

-0011 -007

19936

8596

25.014

1504.7

-24

2

40.67

1403.4

$$\begin{array}{r} \text{HR 5521} \\ 25.014 \\ \hline 082 \\ \hline 096 \end{array}$$

$$\begin{array}{r} 58.401 \\ 26.598 \\ \hline 24.964 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 25.062 \\ \hline 005 \end{array}$$

$$\begin{array}{r} 25.066 \\ \hline 11 \\ \hline 657 \end{array}$$

$$\begin{array}{r} \overline{067} \\ \hline -035 \\ \hline \end{array} \quad \text{32.1}$$

$$\begin{array}{r} +.56 \\ \hline 40.11 \end{array}$$

$$\begin{array}{r} 24.52 \\ \hline 14.80 \\ \hline 41.30 \end{array}$$

$$\begin{array}{r} 41.30 \\ \hline 40.26 \\ \hline 1.04 \end{array}$$

$$\begin{array}{r} 40.33 \\ \hline 40.10 \end{array}$$

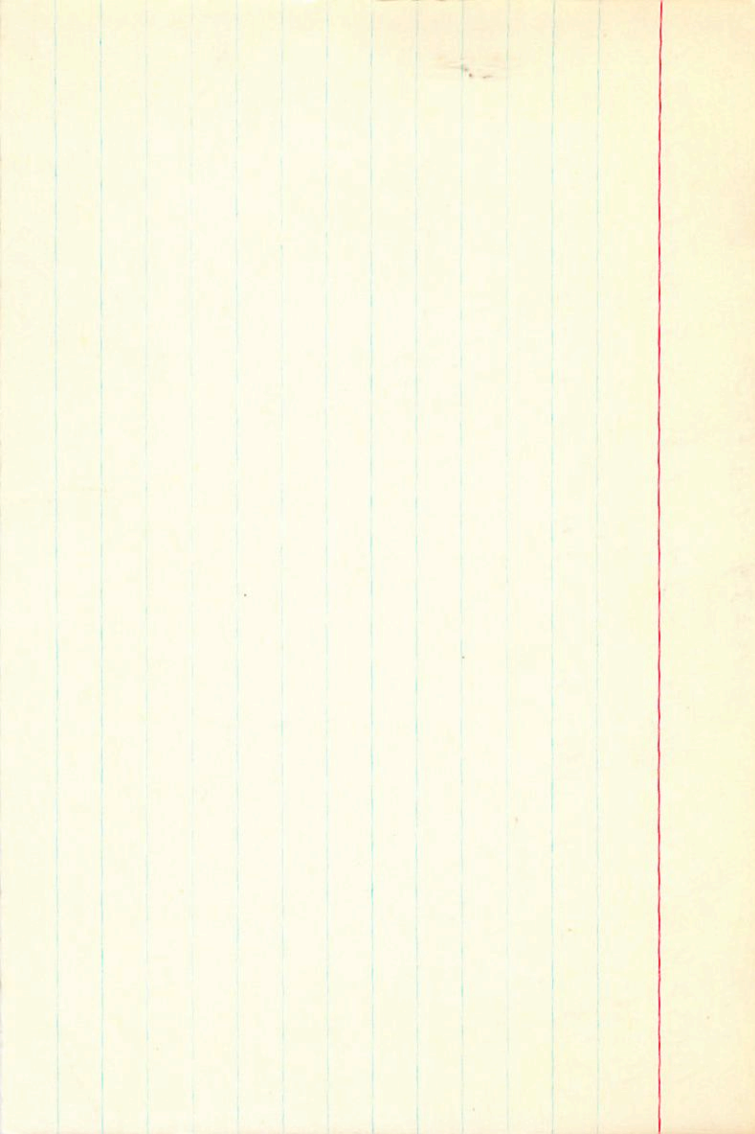
$$\begin{array}{r} 1938.70 \\ \hline 24 \\ \hline 4034 \end{array}$$

$$\begin{array}{r} 40.34 \\ \hline 1.23 \end{array}$$

1934.94

$$\begin{array}{r} 73.64 \\ \hline 36.8 \end{array}$$

33.4



5824
130603
14424
326 147 338 169 490
14 4/6 250 224 34
1576 573
357 505

10205 949
1081 449
1082 437 +085 229

10205 949
752
660
1081 449
1082 437
2303 80.3
2.27
21.46

10140 5335 2516
10140 5335
24
25
9804 -9214 1216
-4743
3889 10024
+085

16380 344
2350
2405 4317
-8
92
33.

1108
225
113 75
110 42
113 45
1081 +0915
1104 1804
0124
424

Bud 51

33.17
+0.77
33.94
+1.9
35.84
+0.2
36.04
+3.11
39.15

49.1 19
46.8 +19 31

S
+5091 -100

+394
52.853

AB
0.60 4.66 +0.78 +0.26
4.65 +0.80

$\rho = 2.2326 \times 10^{-4}$
 $q_3 = 118.00$
 $\pi = 3.0484 \times 10^{-3}$

From P.E. Comp.

149.42 } strand

4.905 } Ann. Seals obs 18, 19, 14.37

From P.E. 3.36

A
Ann = 2.19

4.84 +76
4.50 +0.26

V-17 34

Working
2.14

6.93 +1.174

156
46
936

3.30

6.32 +0.44

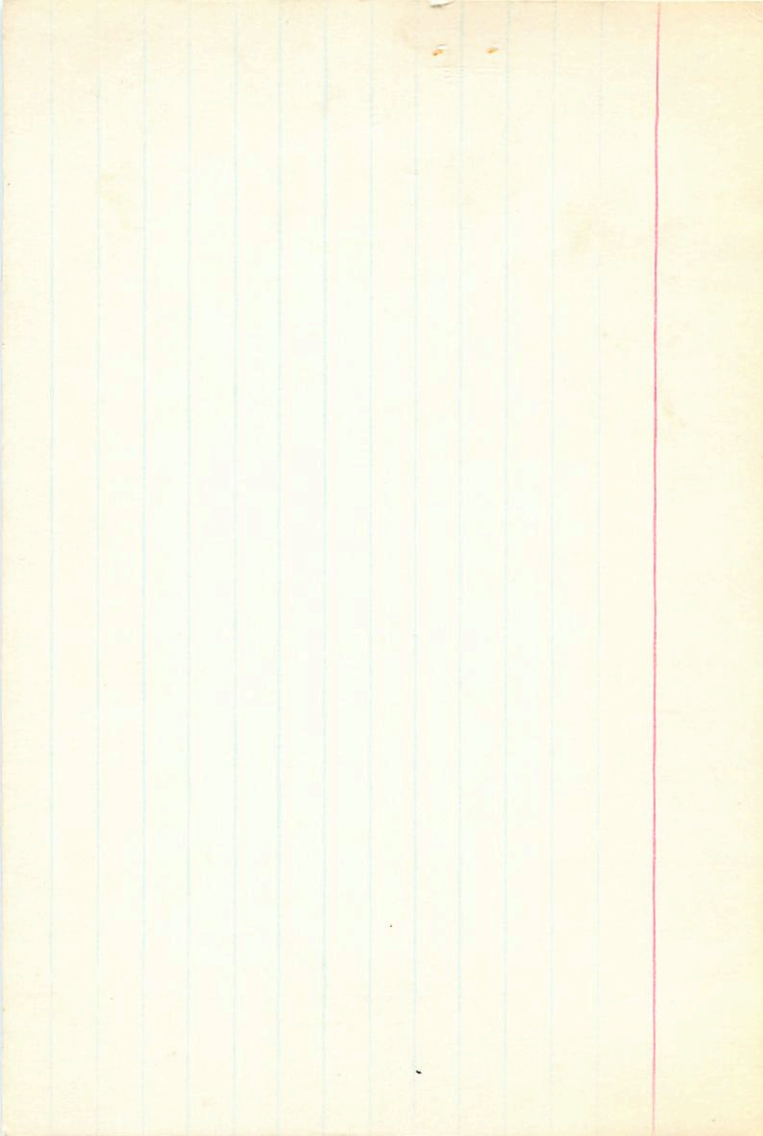
6124
7176

AB

MV m(I) m(B) log
+5.65 +5.05 0.93 -0.3
+7.75 +6.7 0.80 -1.0

N V W
-6 +1 +1

160 150
96 91
960
9400



-0083 ± 11.3 -194 ± 9.0
-0092 -210

ADS 9397 14 46.8 +10 26 -91.66

130669
19943
8604

9.0 } 30.2
9.0

.0209

-131 → 564

-125 -200 14

48.535 1408.9 +10 25 26.13 1406.9

341
1876

+8.36
3449

8.40
+

3

105 48.599

595
281

48.567 29

27.72 1939.4

27.85 1939.4

~~28~~
39.4

27.65
27.68

32.5

-6.81

-135.202

-133-199

3.57

07

-665 -717 151 984 -125-200 -516 -036 -17 -933

-083 -024 093 027 -521 327 -90.1 +67 +60.0-209⁰²⁰⁹

+42 +76 -62

+42 -61 -78

0425

+55 +68 -39

+47 -32 -76

130669 AB

not good

$\sigma_m = 0$

14 46.8

+10

26

dcg

62

$$8.45 + 0.865 + 0.575 \text{ (2)}$$

$$7.94 + 0.32 \text{ (2)}$$

7.62

7.75

8.3

$$D(10-v) + 0.4.5$$

$$D(12-v) + 0.6.0$$

11.11

5.16

8.37

3.21

11.11

0.23

7.60

7.5.8

83

7.90

2.55

5.0

62

5814ya
 130694
 19954

-0182 ± 2.8
 -0191

14 47.3 -27 45 4.4 GA

8612 20.730 1903.7 -27 45 12.29

843
21.573
 +3.39
8.90

-01865 -0655
 -0186 -061
 -2456

52.487
 28.410
20.897
 973
973

56.56
 15.50
17.09
 10.90
1407

1534.75

-10.5

-245-058
938
635
 33.3

20.908
1902
 1959.28

11.33
 -20
11.53
11.30
 -2.40

1959.28
 1403
37.0
37.6

E+02

3.14
 3.14

63

1900
1901
1902
1903
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1998
1999
2000

130694.000*

14.000*

47.300*

-27.000*

-45.000*

-0.245*

-0.058*

5.000*

100.000

-9.900

0.758

-0.696

82.652

-0.944

-0.406

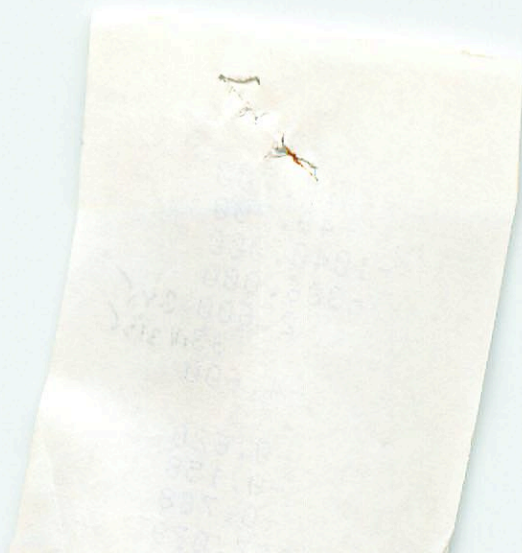
-90.372

63

0.298

0.469

25.162



14.700
-49.700
-1040.000
-386.000
2.600 2.45
33.11 31.25
-4.600

-0.620
-0.158
-0.768
0.079

-0182 AR.8
-0191 -06.4

5814ya
130694
19954
8612

14 47.3 -27 45 4.4 9.14 -5.58
-6030

20.730 1903.7 -27 45 12.29 1889.4

843
21.573
+3.39
8.90

-01865 -0655
-0156 -061

52.487
28.410

56.56
15.80

134.75

1

20.897
97.3
97.3

17.89
10.90
7.97

70.5

UCW

938
635
20.908
902

11.33
1939.28

140.3
37.0
37.6

33.3

37.6

11.30
-2.40

314
324

63