

$409 \frac{384}{792} - 470 \text{ way } 630 + 18$
 124850
 $14 \quad 13.4 \quad -5 \quad 46$
 $+140 \quad 70$
 $F7 \text{ H}$

HR5338

$409 + 51 + 635$
 $4.08 + 52 + 0.25$
 $408 + 515 + 0.25 + 5$
 $3.80 \quad 0.83$

644208
 $99(u) \text{ via}$
 $10059 - 4320$
 $114 + 42$
 1088
 $- 10017 - 428$

$160 \quad 449$
 $1341 \quad 450 \quad 450$
 $351 \quad 258 \quad 388$
 $127 \quad 846$
 $3 \text{ SRC } 2.65224$

[M] 224 + 24

$380 + \frac{98}{112}$
 $1.55 \quad -24 \quad -33 \quad -13$
 $-8 \quad -14 \quad -11$
 $-0006 \quad +11.5$
 -429

+2.7 (1.7)

33



5333.000*

14.000*

13.400*

-5.000*

-45.000*

-3.007*

-3.428*

1.400*

13.055

11.500

-3.844

-4.582

5006 ± 80 -011 ± 5.2

124929 14 13.5 +06 19 { 7.9 AS -17.78

5" { 100 d60 (-25 ± 50/20)

19254

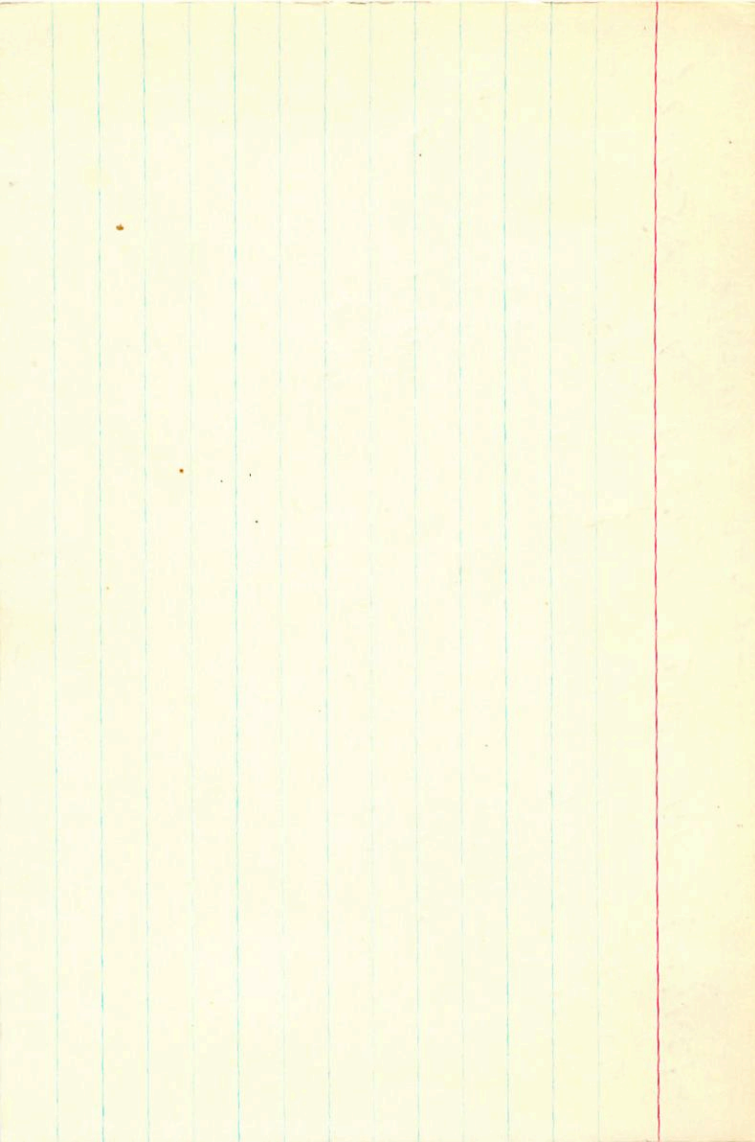
8345 50.556 1900.4 +6 18 43.92 1992.0

030
580

+1.64
44.56

50.540
27
567

44.71 1934.0
~~27~~
44.4



+590569

515

125139

14

14.0

854

55

+957

$-0021 + 0170$
 $+2$

76

$\Delta f m$

9.60 361 185 316

744

1146

$MV = +2.1$
²⁴

$-0024 + 019$
 -018

3/6 month.

↓

-688 +712 +136

+0587 +0641

+1228

+40.0

+1.2

+648 +520 +556

-0553 +0468

-0085

+2.3

+8.8

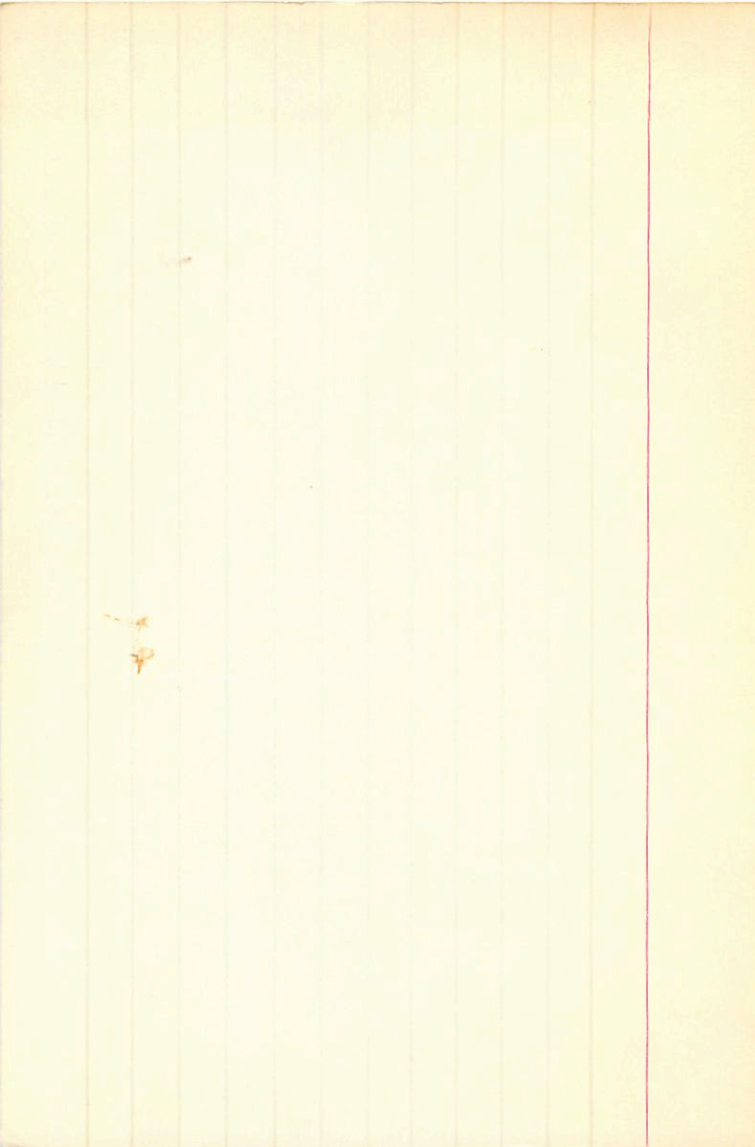
-325 -471 +828

+0277 -0424

+2.8

+74

—



-0106 ± 4.2 -110 ± 3.1

125040 14 14.2 +20 21 6.6 dF4 -8.48

19263

8350

13.266 1904.0 +20 21 14.52 1898.2

A06912

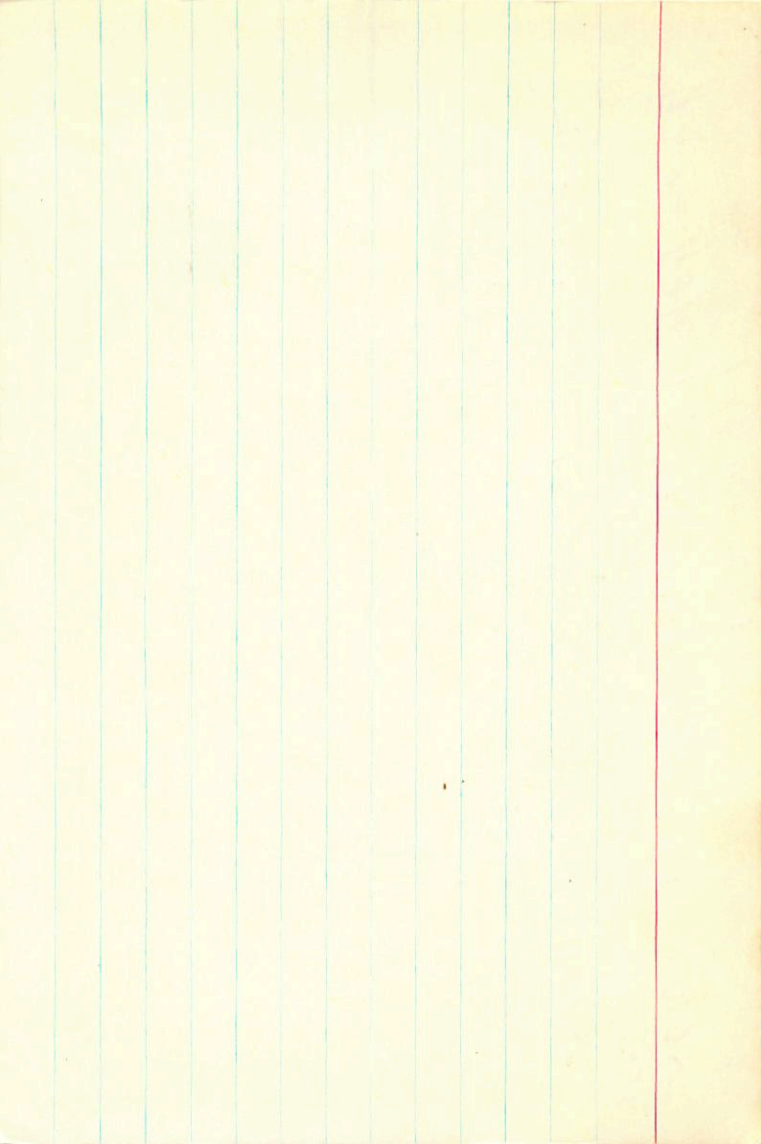
$\frac{488}{75}$

$\frac{+5.70}{20.2}$

1934.5

$\frac{13.449}{403}$

$\frac{16.52}{0}$



125193 14 14.4 +56 55 6.6 d62 -28.98

19267

8353

23 0000 -096²⁷ N30

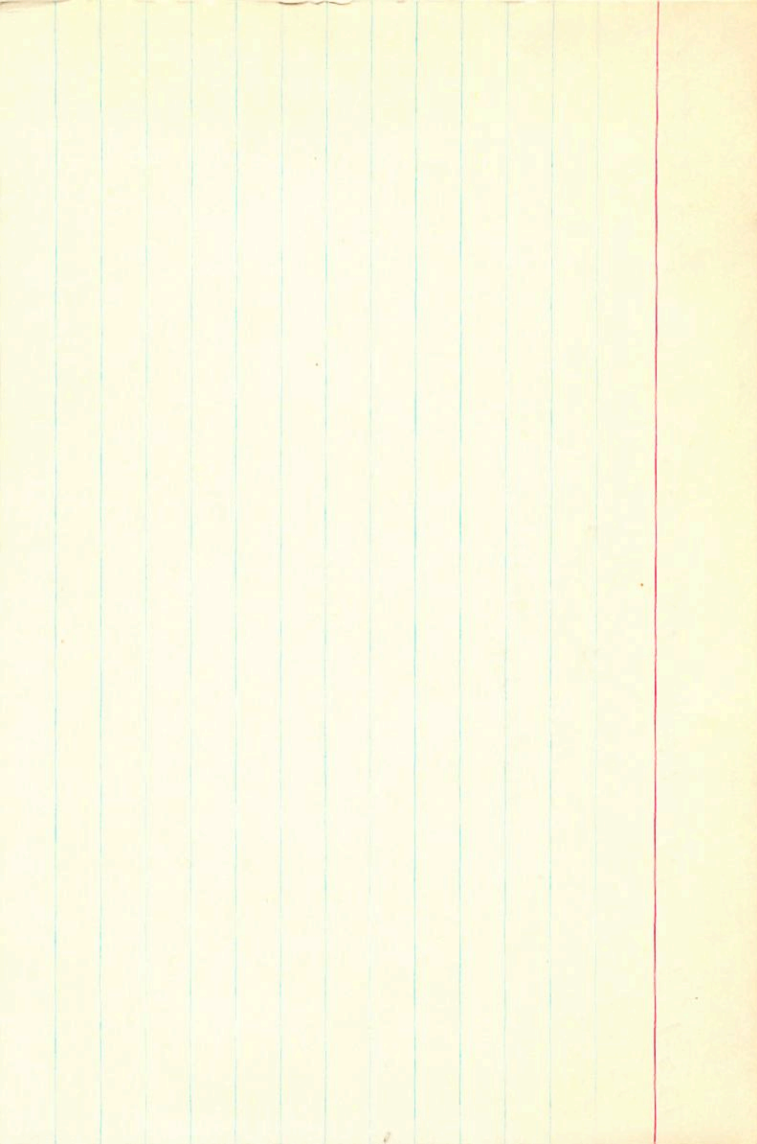
ADS 9197

+000523.4 -103 ± 3.0

$\Delta M = 2.73$

$q''_{mm} b'' d$

0.01 dA



TU Bow

14 14.4 +12 36

-85 \times $w(2)$

- $w(8)$

10.48 +0.17

11.30 +0.27

$\Delta S = 8$

-024455-022455

-554 -832 676 736 -024-022 -85 -015-57-076

~~6009~~

001

-681-62
-32-41-100
57-15-62

-66+92-133
+17-173-20

5084

-7 114-66
-39 -58-167
70 21-66

-80+129-142
+41-202-17

F9E 24

8.0 d09-22c

18

758

14 14.9

125272

+5801491

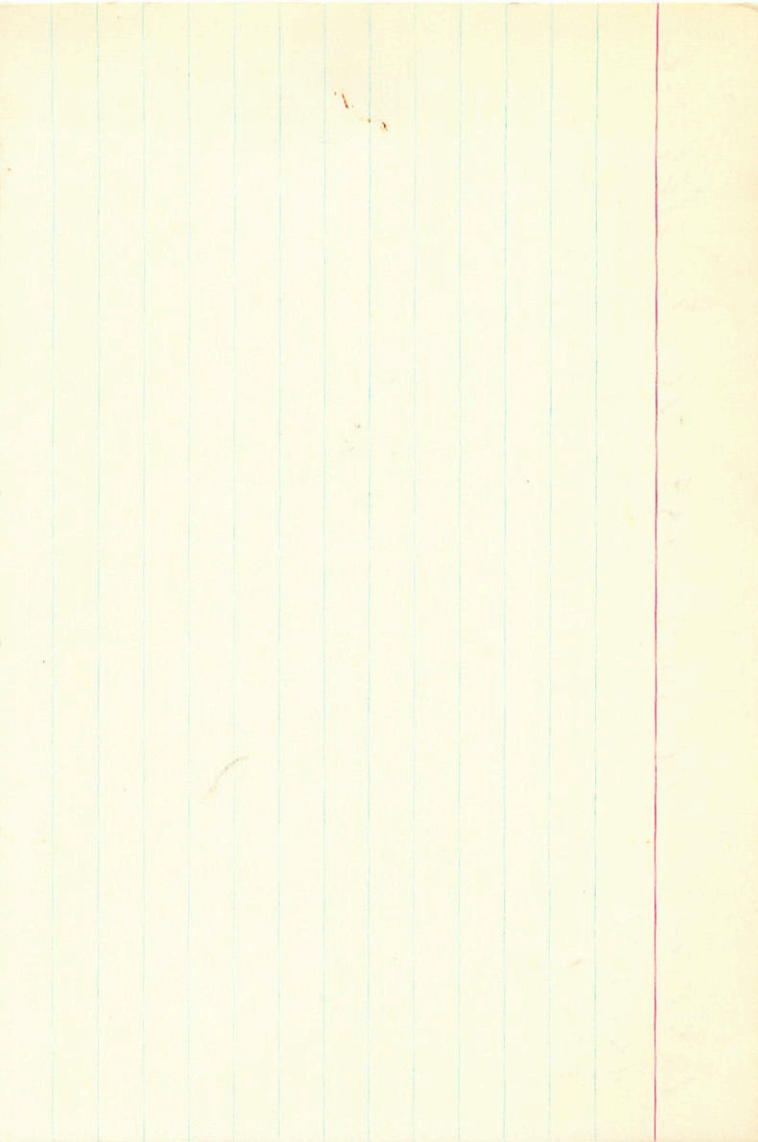
8357

-184 +115 Y

$\frac{+1}{-}$ 0

7166

$\frac{-185}{-}$



957

533
14 15.3 -07 19

N^w -14.1415

12584 121
 181521
 +01707 -2050 22
 +01693 -2021 22
 2519

647 44 554 22
 647 +72 (1.82) 682
 554 74
 93

+0179 -230 130

268-23

+0173 -207 130 +
 +0172 -235

+0168 -247 6-2
 0 +
 244

+2559 -141

+0173 -237

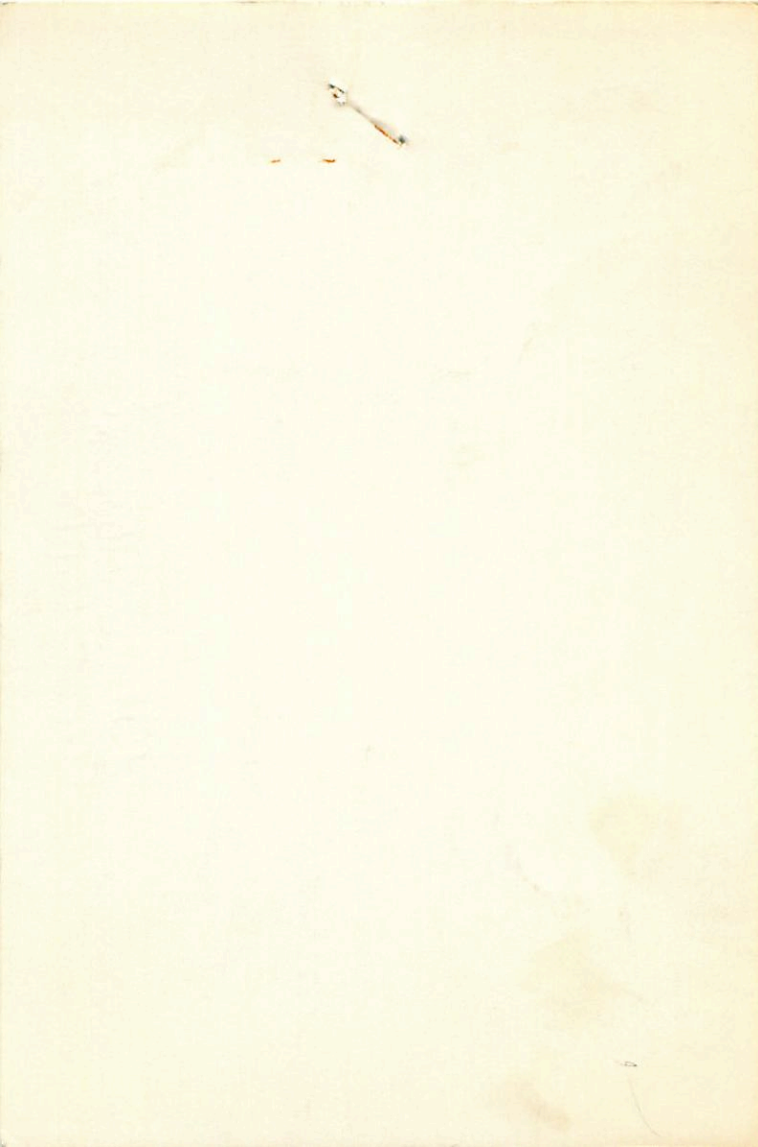
257-232

1257 209
 9486 7757 389
 -0586 2249 -14

1257 209
 3536
 -0151
 2249

253-232

0.24



125406

4108
108

14 16.0

+48 14

F5

4107
179218

HR5363

6.2

-35 41 GC*
-00135 -0485 25.5

GL19297

+12
+18

-00170 -0444
+20 +36
-017 -014 -041 -17.16

213 +18

4.0

1310

157.533 @ SPC 2.651

817

~~CR~~

471 $\frac{129}{+149}$

+2.2

57.5pp.

-6.0 -17.8 -16.0

-0015 = -015

-106 -177 -42

-045 -17.1

24

5363.000*

14.000*

16.000*

43.000*

14.000*

-2.014*

-2.041*

4.000*

63.096

-17.100

-3.096

-2.001

-5.024

-0.162

3.451

-17.944

3.082

3.893

-13.102

4.05

34

14R5363

14 16.0 148 14

6.15 -17.10

~~0.12-0.54~~

-0012 ± 63
 -0014
 -043
 56.72
 1897.9

57.58
 57.412
 057
 $\frac{469}{2}$
 1801.9

-0015
 -045

57.377
 2
 $\frac{399}{2}$
 195.671

57.51
 -30
 $\frac{57.21}{-2.32}$
 1952.68

-688
 648
 -325
 725
 617
 -306

+0489
~~-0466~~
 +0231
 -1546
 -1316
 -0652

-10.57
 -17.97
 -0.421
 -6.0
 -17.8
 -2.4
 -16.0
 -6.0
 -17.8
 -16.0



-0031710.6-01679.5 Sp. B. P. 2
 -0048
 14 16.2 +10 44 71 A3-28.0a

19301
 8363

9.307 1501.6 +10 44 24.91 1898.8

150
457

9.250
 10
309

9.241
 25
266
 169 -

349

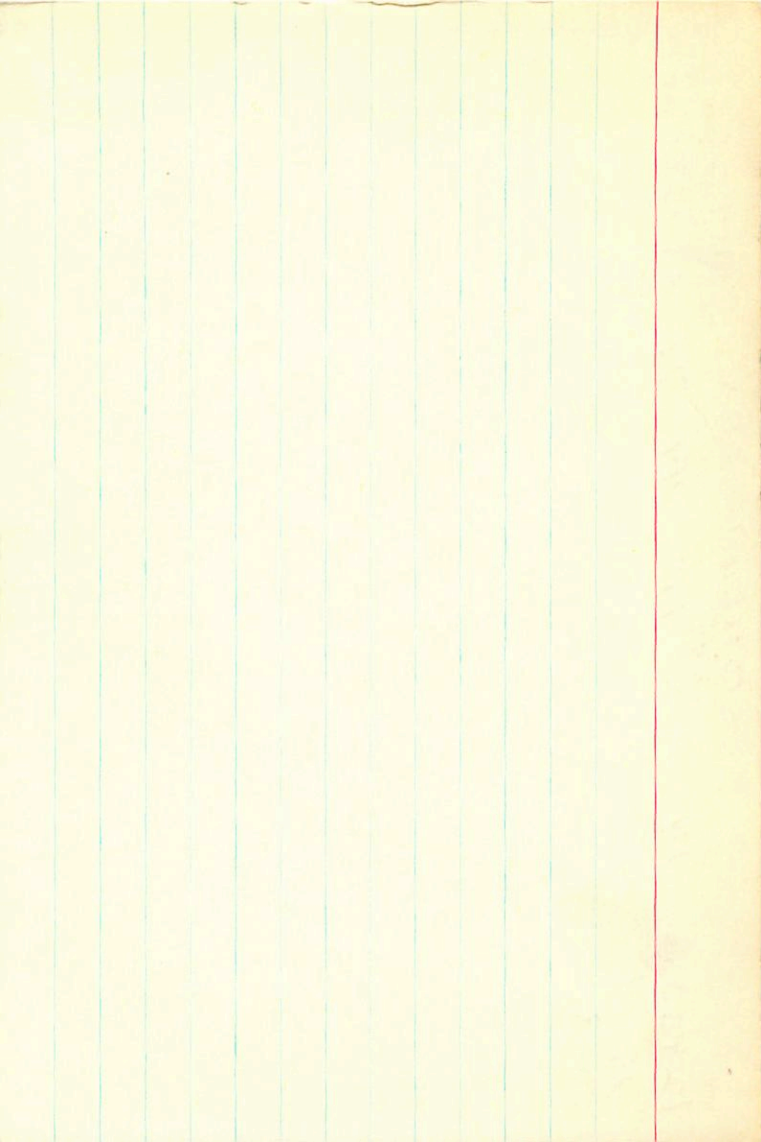
82
25.73

25.29 1433.6
 -15
25.14

25.41 1435.42

25.23
 -18
25.18
 -1.53

1302
36.5
 37.7



-0030 ± 2.2
 -0034
 125377

14

16.4

$+0.4$

07

8.7

965

-44.96

19308

9369

21.771

1894.6

$+4$

7

20.14

1889.7

166

937

95

2.34

22.50

0.5

$AD59215$

21.760

-152

21.21

1936.7

-16

21.05

25

795

1939.1

158

37.9

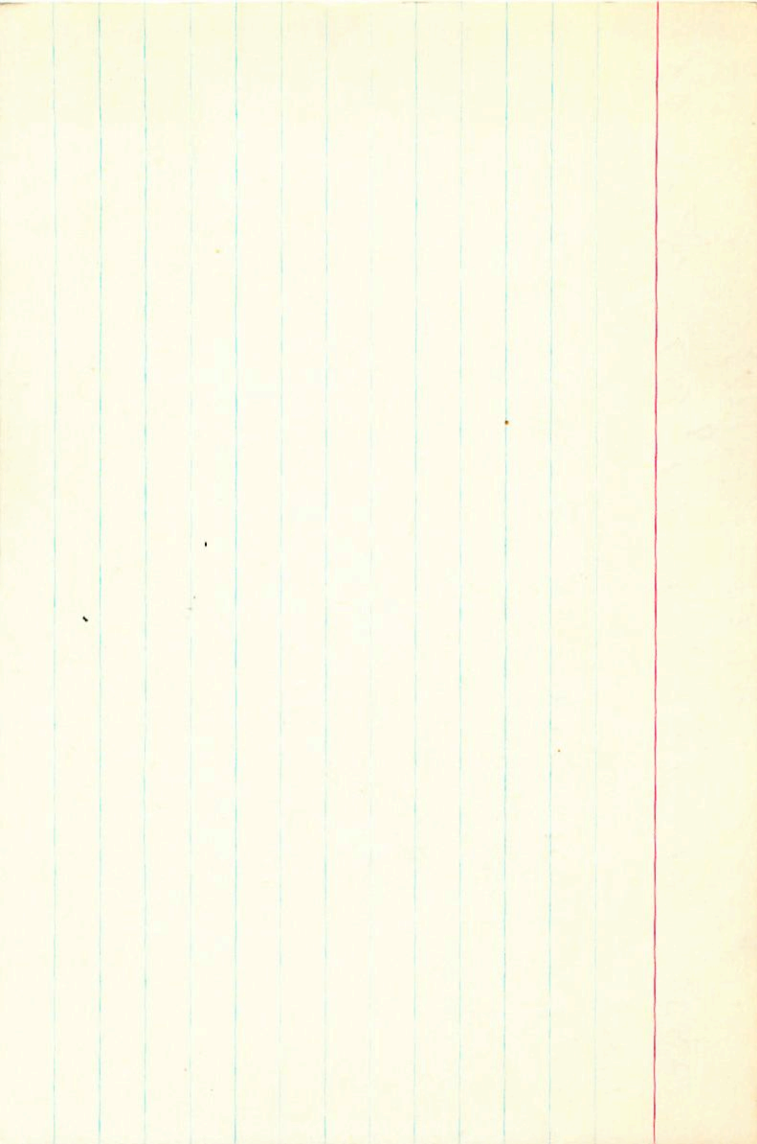
38.2

-1.38

43.3

787

-150



18800

12545/

19319

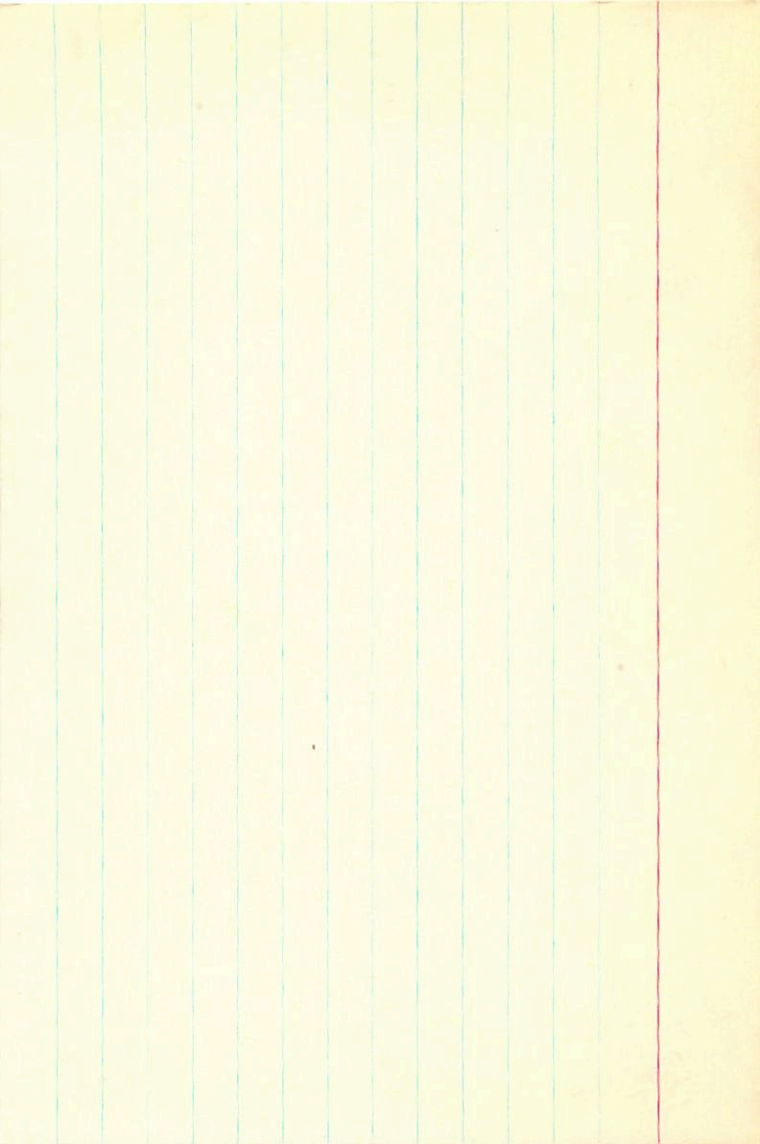
8373

14 16.8 +13 14 5.3 dF1 -1.92

+0072^{4F} -035^{4F} N30

+0070±2.2 -031±1.9

-0.3 (20)



351

18B00 14 16.8 +13 14 -1.9a

AF1

HR5365

5K +104 -037 6c

5.41 +0.38 -0.03 F22 +104 -035 U

5.41 +0.38 -0.04 N +104 -034 F

~~FSP-6~~ ~~+104~~ ~~-035~~

+80729 10358 W 50

+80729 10373

1069 10N

+109-034

9791-2033 9972-6039 1074-0847

-3.6 2-827 228 974 +10.4-035 -1.9-008 -0.4 -161

058-004-086 007 242 -426 -1.9 +1.6 +1.1

03

+1.3 +5.9 -4.5 0.25

+9.7 -13.1 -5.8

-16.2 +2.5 -10.4

-13 +6 -9

04

+24 -9.7 -4.4

-14.9 +4.2 -2.0

02

+13.7 -20.2 -8.4

574
-0032 ± 4.2 +007 ± 3.4
-0023 -011

125632 14 17.3 +55 06 6.6 A2 -3.2 8

~~-0030 -026 000~~
~~-027~~
~~-064~~

19333

8379 16.25-1898.5 +55 5- 35.54 1895.0

$\frac{16.5}{4.16}$
 $\frac{-22}{2}$

-682 724 082 +0840 = +3.4 -0.3, 3 2
650 552 522 -0801 -3.3 +7829.4 1926.4
334 -410 848 -0410 -1.7 -2.784.90

+3.1
-5.0
-4.4

24.53
49855

34.50

16.318
377

2.14

961
 $\frac{320}{-096}$

35.03
-14
34.89

34.81

40.9

1944.60

16.272
272

35.08
-20
34.78

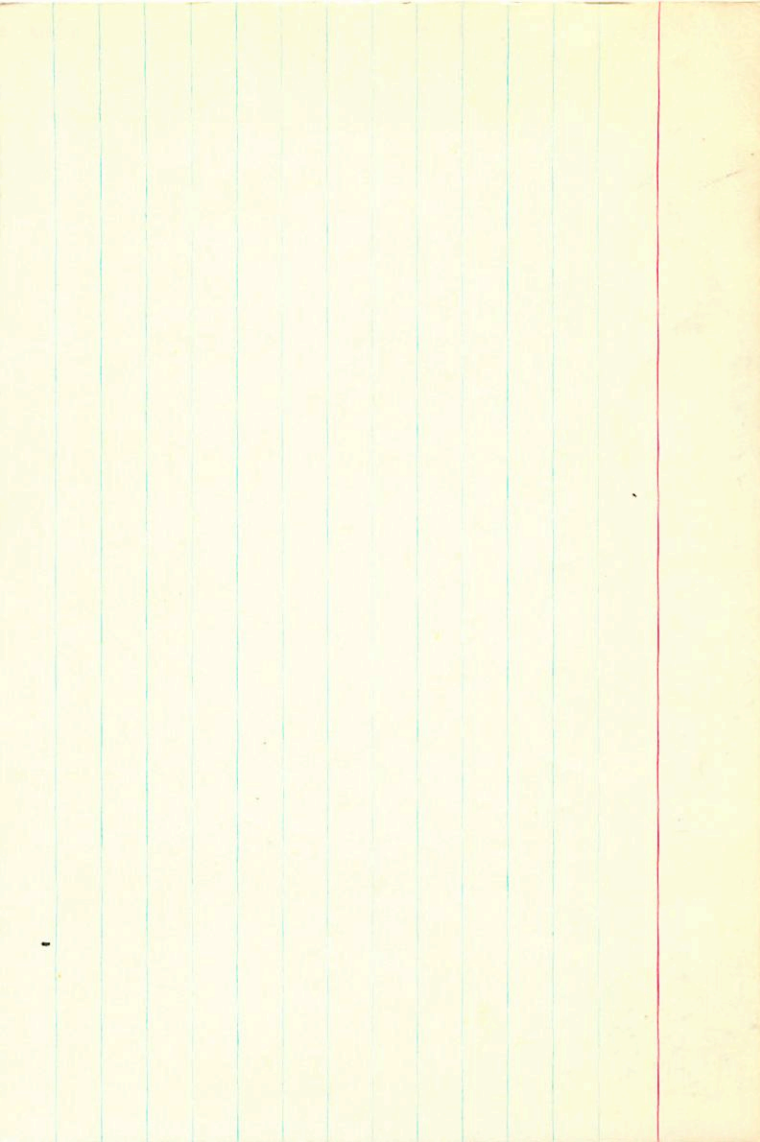
11829

16.289
 $\frac{14}{30}$

37.98
-21
34.77

1947.29

39.4
44.4



20300
125560
19334

-0101 ± 1.7
-0102

+052 ± 1.5
+052

14
17.4
+16
32
5.0
943
-8.0 a

9380

23.157
1898.8
+16
32
5.89
1896.4

$\frac{5174}{16}$

-2.79
3.10

23.307

$\frac{19}{326}$

4.99
1933.4

$\frac{6}{1040}$

4.93

37.6

23.245
 $\frac{14}{259}$

$\frac{585}{292}$
-3.82

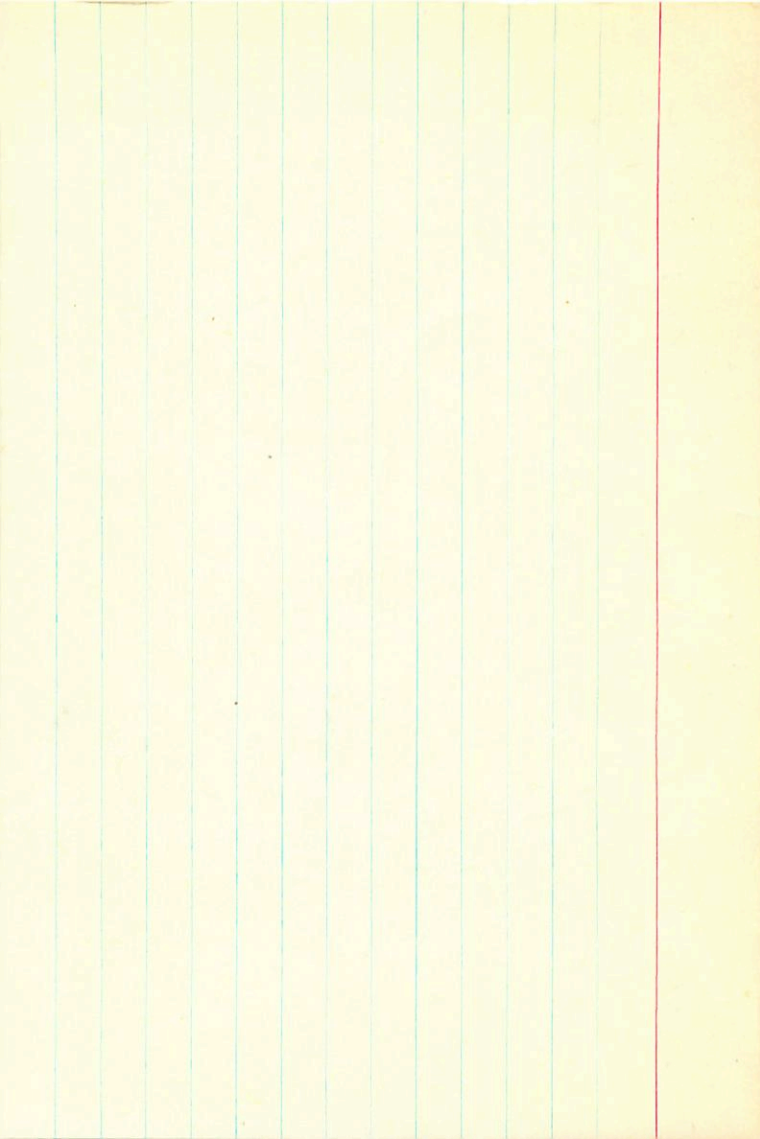
5.57
1940.38

-10
5.47

23.78
36.4

5.20
+2.10
5.2

40.0



HR5324 14 18.0 +30 39 Am +1.38

-0.61

~~6.30 +0.15 +0.10~~

125658

19345

8384

6.34 +0.15 +0.10 Am

-0.15 -0.07 GC

-0.15 -0.07 N30

~~0.12¹⁹ -0.07²¹ N30~~

-0.13 ± 3.7 -0.03 ± 3.9 GC → N30

A to R Am / Geo / Const / ... A 90.1 X Y Z
15 764 90 254 358 966 934 32.2 +8 +31 +92

-566-824 510 860 -015-007 +1.3 -004 +1-025

-008 -002 +012 +003 -052 047 +1 -1 0 011

-4 +3 -1

+3 -5 +3

G619401

G24736

$\Delta m = 00$

14 18.5 +08 54

B6 6.86 +0.43 -0.01 (4)

A 5.14 +0.01 -0.01 (2)

new orbit

$\frac{327}{3759} \quad 29$
39

Spencer.

Band 51

S
-0053 -0.058

-20.18

$\frac{327}{39}$

$\frac{6.15}{2.174} \quad 3$
39

+315

239

272

2.1.22

+410

+16

114

570.23

A055229

14 18.5

347 44

-1288

125796

0.0641

19347

-064 -014 H

8355

AKO
Van Nieu

-066 ± 3.0 = 011 ± 3.0 Van Nieu

-058 ± 5.7 = 017 ± 3.2 00 → 000

-0072 -022 ✓

720-160

400+

2 20

7.41 1.5 + 1.16

7.56

8.16

8.66

9.16

AKO

6720-9991 0715

7406-4488 0155

-568 -823 752 660 -064 -014 -128 -011 -13 -043
-036 -006 053 009 -213 223 -117 +10 +7 0141

-5 +23 -16

[+13 -24 -7]



126009 14 20.0 129 36 g m 4

6.6 Var
-15.4 (3) 111
-17.4 (8) 000
-14.8
-0032 -023 Sat 111
-0031 -0195 R 114

4.85 Var +140
175

447
111
2.65
5.11
7.80

-040⁴
-038-016 thru

2442225 6.56 +1.555 +1.84

26

5.85 +1.40

241 6.51 +1.595 +1.53

242

4.87 +1.385

245 6.47 +1.605 +1.47

248

4.85 +1.41

250 6.47 1.60 1.50

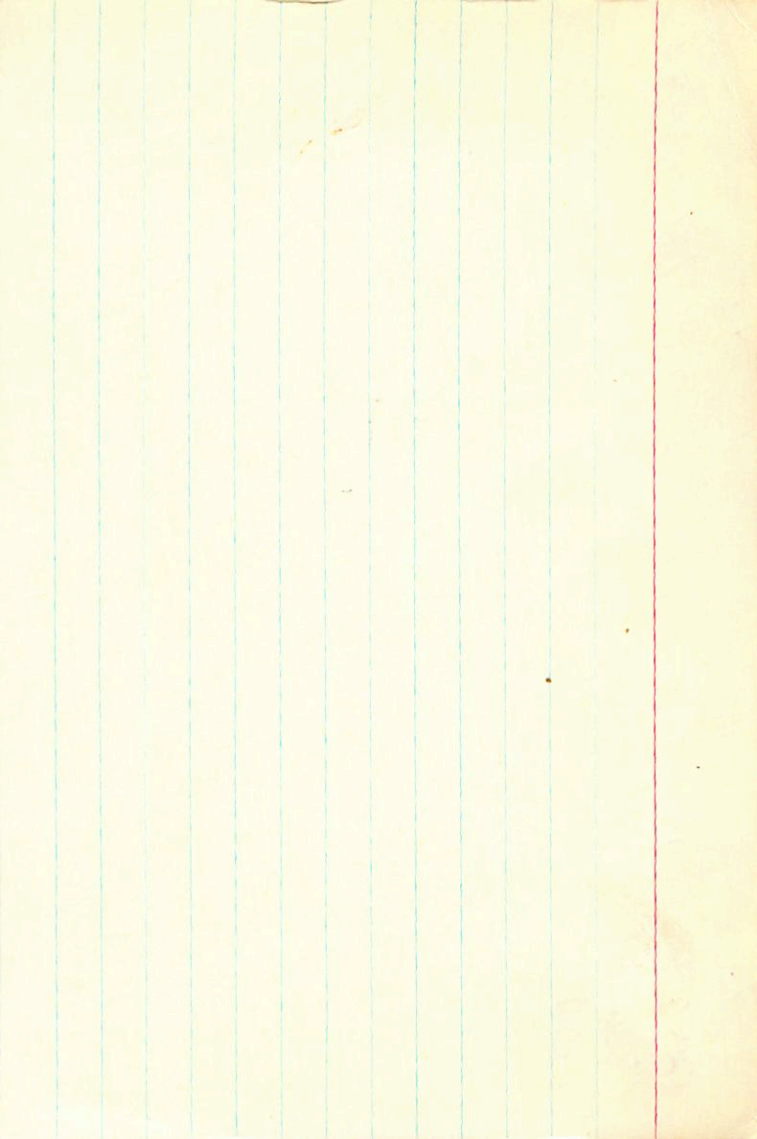
252 6.55 +1.59 +1.505

253 6.57 1.60 1.44

257 6.61 1.59 1.38

269 6.71 1.585 1.45

272 6.73 1.56 1.43



51470
125932
G-615389
W8389
Y3241

334
206
14
20.2
4.75
182
-27
32

4.80
+434
Cete
1275
1125
277
1231
1231

-2709803

W
1502
2010
1498

high
low
125 III Cete
+120.4
-154
-120
GC

+22 -22 +2 .015
+13 -57 +5 .02

484
79
184

1275
W8
277

high
low
125 III Cete
+120.4

1266103

117
-60
117

199-177
1435
-23.5
117

900
470

high
356
117

1.26
0.67
1003
0.67
0.50

(2218122)
23065

117
3
117

117
3
117

117
3
117

117
3
117

117
3
117

117
3
117

117
3
117

-01474 2.4 -12052.6 -105
-0158
-125
-114

12.514 1902.9
-015
-27 3 1 31.89 1500.0

13,206
692
45.944
26.626
2.626
692
692
12.055
23
33.5f
34.3
38.44 1533.71

36

12.654
692
692
692

674
33.6

30.06
30.99
30.15

509

532

20.59
1939.38

36.5

12.654
692
692

12.180
70.42
34.87
34.87

36.5

194
-31
34.87

30.44
-4.53

-01.51
-126

-01.502 -1215 -1206

-01.337
-01.344
-0013

-201-117 fhr

P.A. :
DEC. : 14.350
M. R.A. : -27.200
M. DEC. : -227.000
DISTANCE : -117.000
MODULES : 8.250
D. VEL. : 21

d1 (U) : 50.400
d2 (U) : -0.424
d3 (U) : 0.151
d4 : -0.710
d5 : 248.471
U : 12.450

d1 (U) : 0.933
d2 (U) : 0.298
d3 (U) : -0.450
d4 : -222.203
U : -29.427

d1 (M) : -0.347
d2 (M) : 0.780
d3 (M) : 0.219
d4 : 1.000

R.A. : 14.350
DEC. : -27.500
1. R.A. : -227.000
1. DEC. : -117.000
DISTANCE : 3.550
MODULUS : 51
D. VEL. : 20.400

q1 (U) : -0.674
q2 (U) : 0.171
q3 (U) : -0.719
dU : 548.471
U : 13.470

q1 (V) : 0.652
q2 (V) : 0.595
q3 (V) : -0.470
dV : -952.203
V : -58.427

q1 (W) : -0.347
q2 (W) : 0.786
q3 (W) : 36

14 20.4 -52 57

1080 ± 78 - 0.2 ± 8.3

23.871
852
757

2.3 58.89 0.4
1057 - 119
57.30

23.871 20.05 58.23
II - 60
58.63

872 70522 - 0.131

-0.981

0.499 - 0.10

1.1692

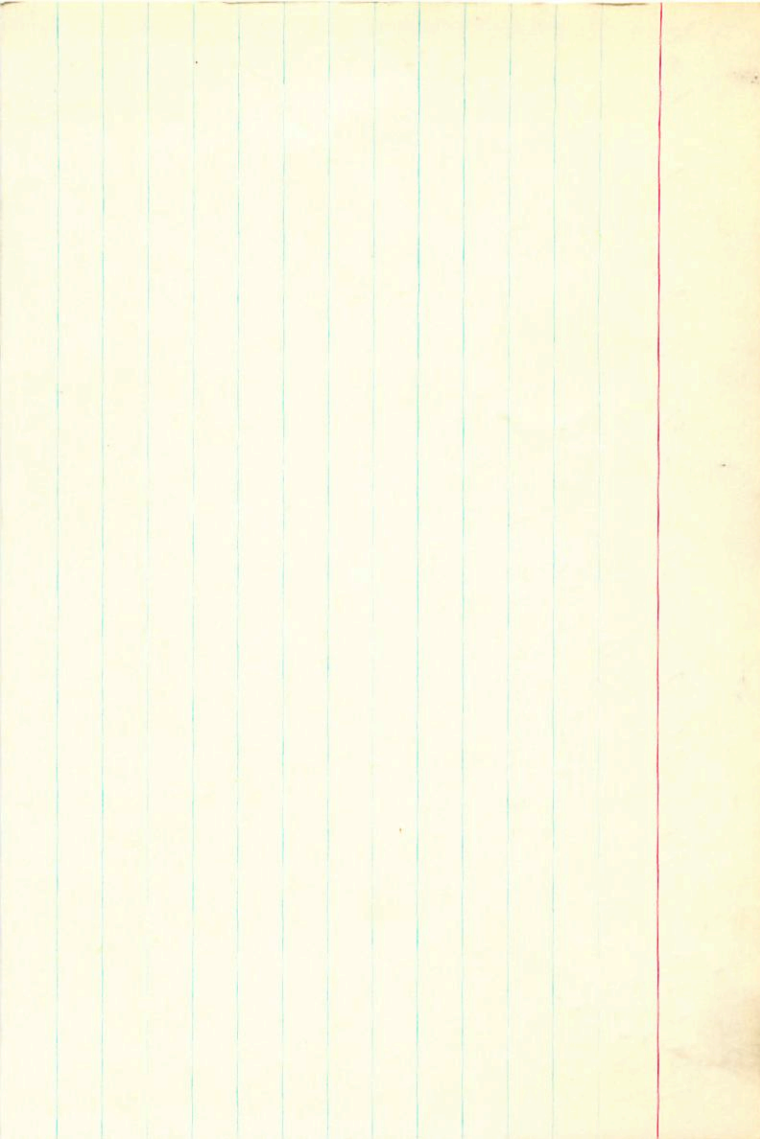
12585

2 dit
126035

14 20.7 -11 29 6.3 gG7 -1.28

19399
8402

-0007 ⁵⁰ -062 ⁵¹ N30
-0010 ±1.5 -063 ±1.3



126201

14 21.5 +06 03 d68 -4048w(13)

6C19416

7.18

+0.99 +2.06 ^{u.s.} - Alw(12)

W8418

-044 ^{±3}	+015 ^{±4}
-031 ^{±7}	+014 ^{±7}
<hr/> -040	<hr/> +015

+29 -1 -29 .02

-590 -8.5 105 555 -040 +0.5 -40.4 002 -4 071 ✓
-023 001 033 -002 -059 161 -40.2 +333 +23

+29 +31 -1

02

+29 -1 -29

$$-0030 \neq 3.3$$

$$-0032$$

$$31.186 \quad 1901.8$$

126201

Card II

$$+015 \neq 3.6$$

$$+012$$

$$+6 \quad 2$$

$$55.75 \quad 1901.9$$

$$\frac{145}{31,331}$$

$$31,331$$

$$31,207$$

$$\frac{27}{234}$$

$$31.189 \quad 221$$

$$+19$$

$$\frac{200}{200} - \frac{110}{110}$$

$$-72$$

$$\frac{55.03}{55.81}$$

$$55.81 \quad 1933.4$$

$$-24$$

$$1261$$

$$\frac{363}{34.4}$$

$$55.26 \quad 1939.29$$

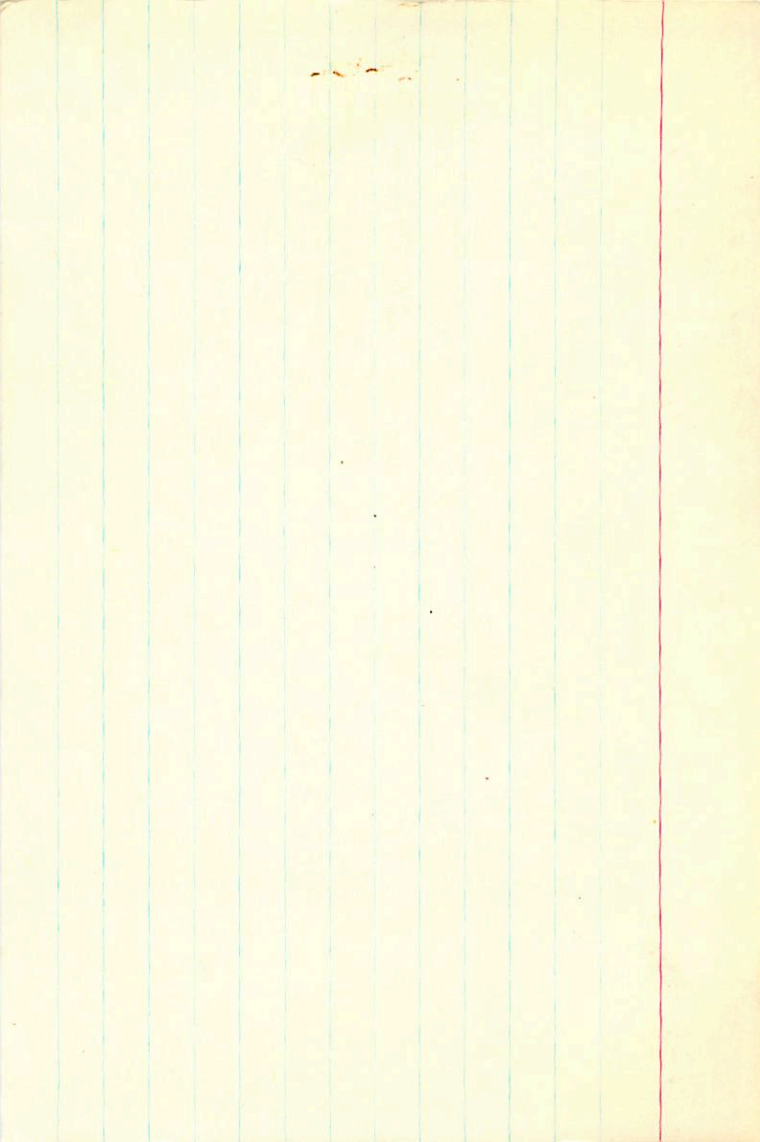
$$+5$$

$$\frac{55.31}{55.44}$$

$$\frac{55.44}{7.41}$$

$$7.41$$

34.1



5707

5392

1/2 21.7

1/4 02

A3

394

126218 -0841 10024 W2 50

19428 0842 10024 5.10 + 12 + 9 C + 1.20

slant

064 200 996 @ 5 P 6 2.864

46

558

118

422

983

206

093 = 6

1405

130

1.38

040 = 2

1003

130

B=1023

topk

+1.4

3.7

-0810

-074 + 0.11

89B -9726 0944

4534 2326 10077 0093

392

5.16



54



5392.000*

14.000*

21.700*

21.000*

126223

19488

8419

✓ (15)

(19)

± 5 billion

-0024 -0006
-0026

-0360
-034 000

14 23 00

-2 07

13 77

-280

7.18 + 1.68 + 1.83 (2)

6.07 + 0.865 (1)

569

452

244

(28)

37
37

-12.728

0.134

868

2.035

750

126273.000*

14.000*

22.000*

-2.000*

-7.000*

-0.034*

0.000*

8.400*

478.630

-28.000

0.108

-0.579

68.014

-0.105

-0.167

-45.674

0.056

0.798

4.684

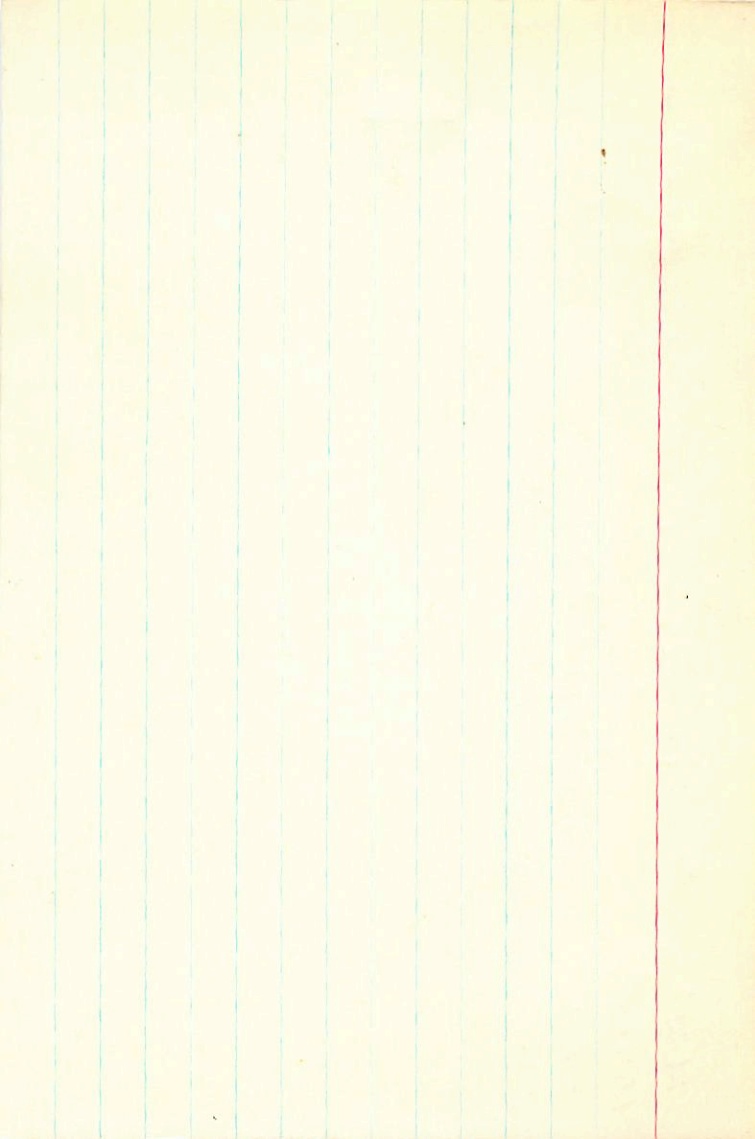
38

126218 14 22.0 -24 35 5.4 gP8 -22.1a

19435

8417 ⁴²-0041 ⁴²-017 ⁴²N30

⁴²-0042 ± 2.4 -021 ± 2.1 G1 → N30



12059254

126251 14 22.0 -11 27

19407

8418

440

6.51 +41 -0.03 1^m 18¹¹

6.40 +43 +0.02 C

12016 59.3331898.6

262

595

+2.01

3545

-11 26 37.46 18941

38.745

20.675

59.420

462

468

59.370

369

35.1

837

418

177

48.21

44.42

37.67

367.6

367.6

34.94

36.98

1527.03

367.6

1.33

1940.35

36.98

-005152.8 -036±2.0

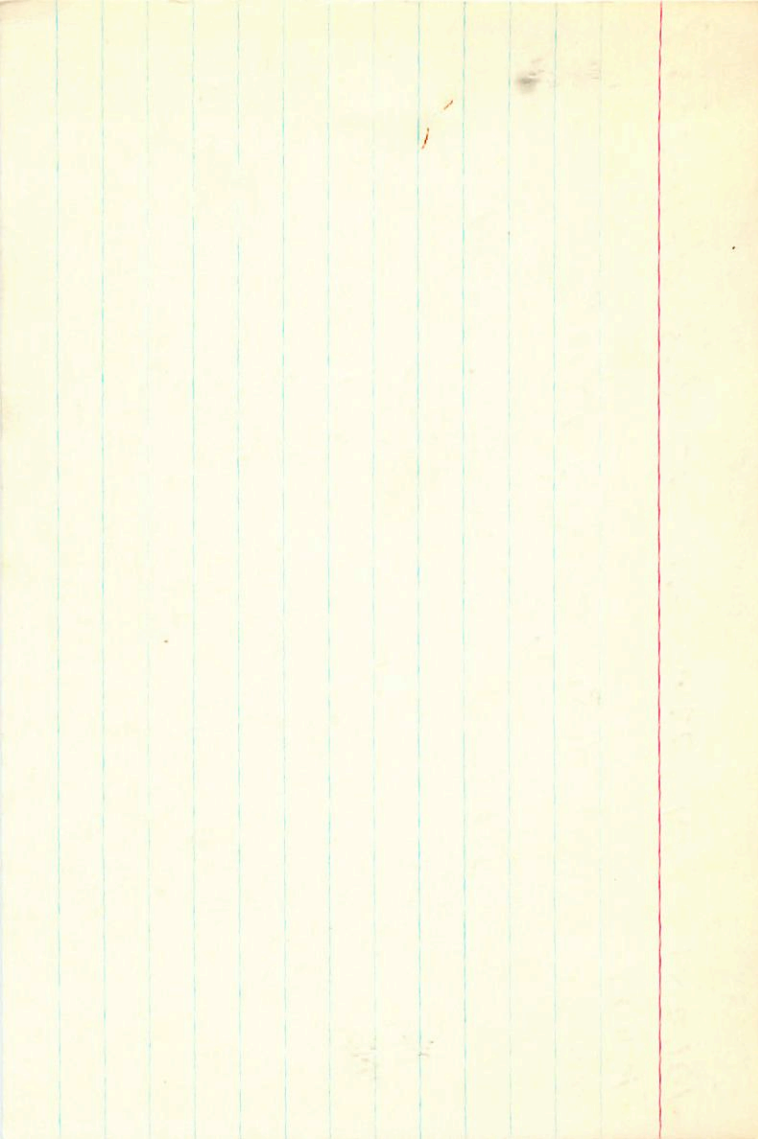
-0050 -034

6.5 dF1 -35.88

67.38

337

39.6



125864

14 20.4 -52 57

14342

-0080 ± 78 -0.2 ± 8.3

23.875
352
757

2.3

$-0057 -019$

58.89 0.4

1.54
57.30

23.371 20.05

58.33

□

-30
58.63

37✓

$-00532 -0131$

-0481

$-049 -010$

5380

22.0 -2 07 -28C

126223 14 23 00 -2 13 77 FM3

(B) (P)

15408
8419

7.18 + 1.63 + 1.83 (2)
6.07 + 0.885 (1)

+ 2V ± 5 kwhms
-0024 -0006
-0026

569
452
214
221

-036.0
034 000

250