

3260

10 58.6 -45 21

0.5

122223

~~750162~~

SR 1025d

440404

+0004 -025 / 847

+0007 -020

17

+0074

-45.33

+0009 -014

+10

-16

6

-0.5

19

62
1911



P/

4.000
-45.330
10.000
-16.000
6.000
158
-0.500

-0.722
-0.012
-0.691
-23.186
-3.329

-6

0.636
0.380
-0.671
-7.623
-0.873

-2

-0.271
-0.225

19

HPCT57

13 572-24 45

122066

307 172 243 2655



145 18 87.2 -3 18 815
0.5
40.0
2

122106 HR5258 6.39 + 0.45 1004 C F54

6618919 3.15 .317 .182 .484 2 506 2-6299 3

239.5 421.76
+7.11
-0199-0637
+38 P124
-0298

-028-060

-8.26

3.50 +2.3 -11.9 -12.2
3.3
-38 -279 -109

5253.000*

13.000*

57.200*

-3.000*

-13.000*

-0.028*

-0.060*

3.300*

45.709

-3.200

-0.033

-3.513

2.789

-0.292

-0.252

-11.287

-0.110

0.821

-11.760

37

325
-11.4

549

+2.4

14.0

20

125

10

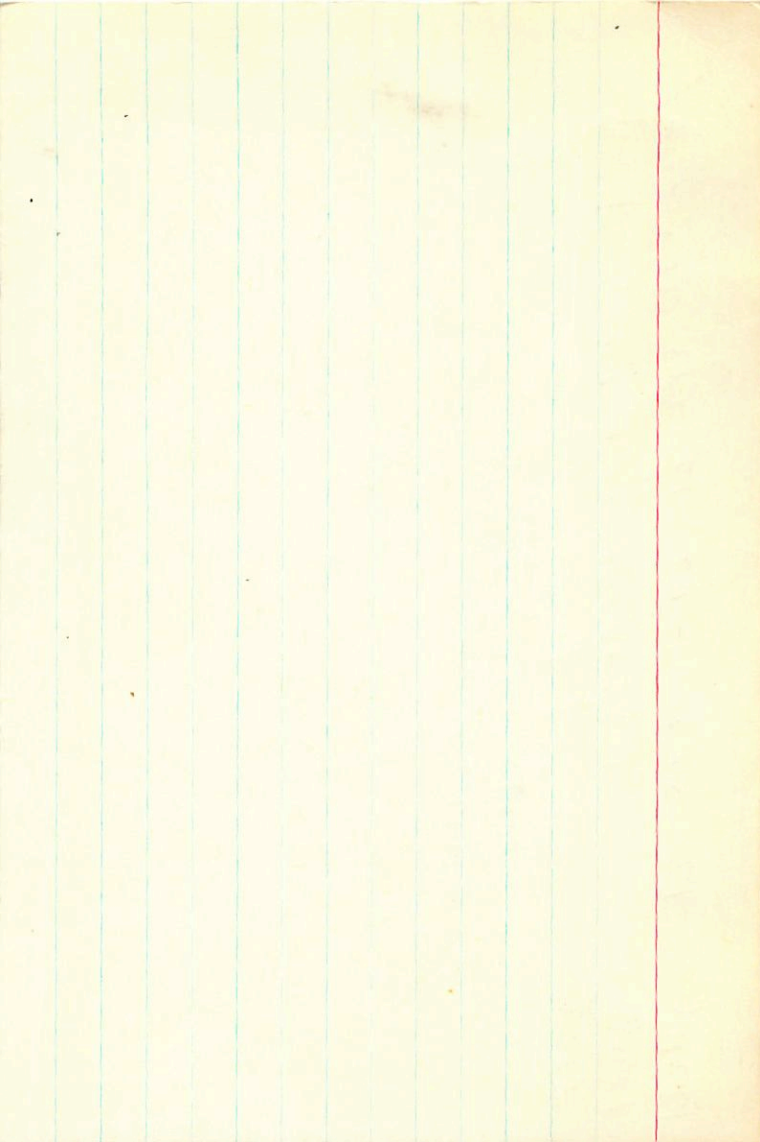
122106 13 57.2 -03 18 6.3 dFs -8.28

18919

6.39 + 0.49 + 04 1^m 18^m

8236

⁴⁴
-0019 -057 45 N30
-0019 ± 2.6 -066 ± 2.5 Ec → N30



-0026 ± 3.1 -016 ± 3.1
-0025 -010

122430 13 59.5 -27 11 5.7 91K3 0.008

18954

8247 31.755 1902.4 -27 11 21.73 1801.2

$$\begin{array}{r} 124 \\ \hline 1879 \end{array}$$

$$\begin{array}{r} 6.488 \\ 25.235 \\ \hline 31.723 \end{array}$$

$$\begin{array}{r} 794 \\ 179 \\ \hline 973 \end{array}$$

$$\begin{array}{r} 794 \\ \hline 973 \end{array}$$

$$\begin{array}{r} 31.788 \\ 123 \\ \hline 31.911 \end{array}$$

$$\begin{array}{r} 57174 \\ 31279 \\ \hline 88453 \end{array}$$

$$\begin{array}{r} 2000 \\ 31.958 \\ \hline 2177.958 \end{array}$$

34.4

$$\begin{array}{r} 794 \\ \hline 973 \end{array}$$

$$\begin{array}{r} +78 \\ \hline 20.95 \end{array}$$

$$\begin{array}{r} 6.37 \\ 46.024 \\ \hline 52.394 \end{array}$$

$$\begin{array}{r} 22.76 \\ \hline 21.65 \end{array}$$

$$\begin{array}{r} 21.65 \\ \hline 21.65 \end{array}$$

$$\begin{array}{r} 21.65 \\ \hline 20.95 \end{array}$$

$$\begin{array}{r} 20.95 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 21.65 \\ \hline 21.65 \end{array}$$

36.8
35.6

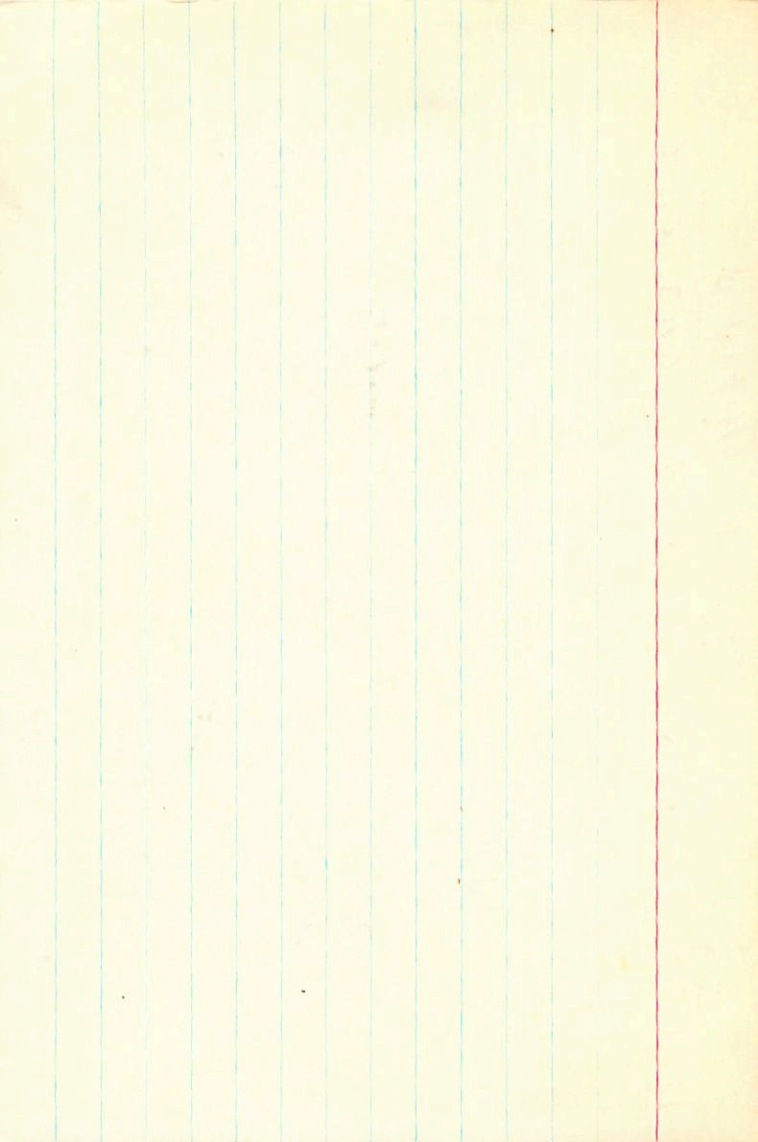
6.37 1932.45

$$\begin{array}{r} 21.29 \\ \hline 21.34 \end{array}$$

1939.57

1941.72

53.8
1933.10
1941.72



$\frac{4385}{43.5}$
 $\frac{15.42}{21.51}$
 $\frac{1426.21}{29.80}$

$\frac{4333}{1332.0}$
 $\frac{42.5}{5.27}$

~~555~~

$\frac{45.5}{44}$
 $\frac{41.39}{464}$
 $\frac{15509}{464}$
 $\frac{1845}{464}$
 $\frac{1577.54}{464}$

$6.17 + 0.48 (1.60)$

14 001 -31 27 FEB +5.3 4C

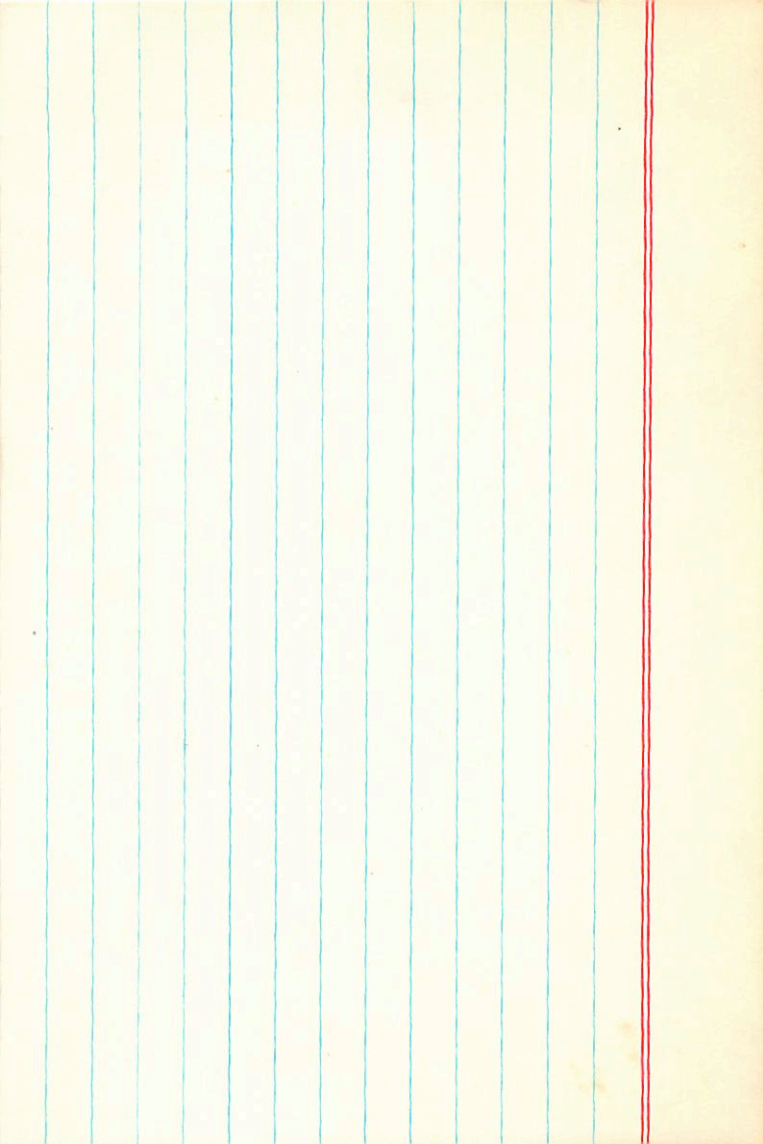
$\frac{6.956}{356}$
 $\frac{6.559}{288.78}$
 $\frac{40.072}{26.82}$
 $\frac{13991}{6.95}$

~~7.030~~

$\frac{6.985}{883}$

$\frac{7.5}{6.4} \left\{ \begin{matrix} 2'' \\ 2'' \end{matrix} \right.$
 6718961
 $F=0953$

12251



122675

18969

8250

14 00.2

+46 00

6.5

182

-48.66

+0015 ± 3.5
+0022 -085

-079 ± 3.1

12.999

+45

49

41.49

1893.3

087

12.912

4.48

45.97

13.46

370

57.7

1926.4

59.555

14.82

42.88

507

28.8

35.5

13.022

42.56

43.44

593

42.90

3.01

12.994

995

+083

1930.3

12.58

43.00

42.66

43.00

1930.3

146

42.66

6693

8.06

+0.57

+0.07

F80

+1.0

122693

+25° 27' 22"

-1.022

- .123

-1.004

-1.003

-1.026

- .126

-1.001

4.004

-1.027

- .122

14° 0' 33.943

+1.014

33.957

14° 0' 33.950

.001

.951

+24° 48' 14.32

- .15

14.17

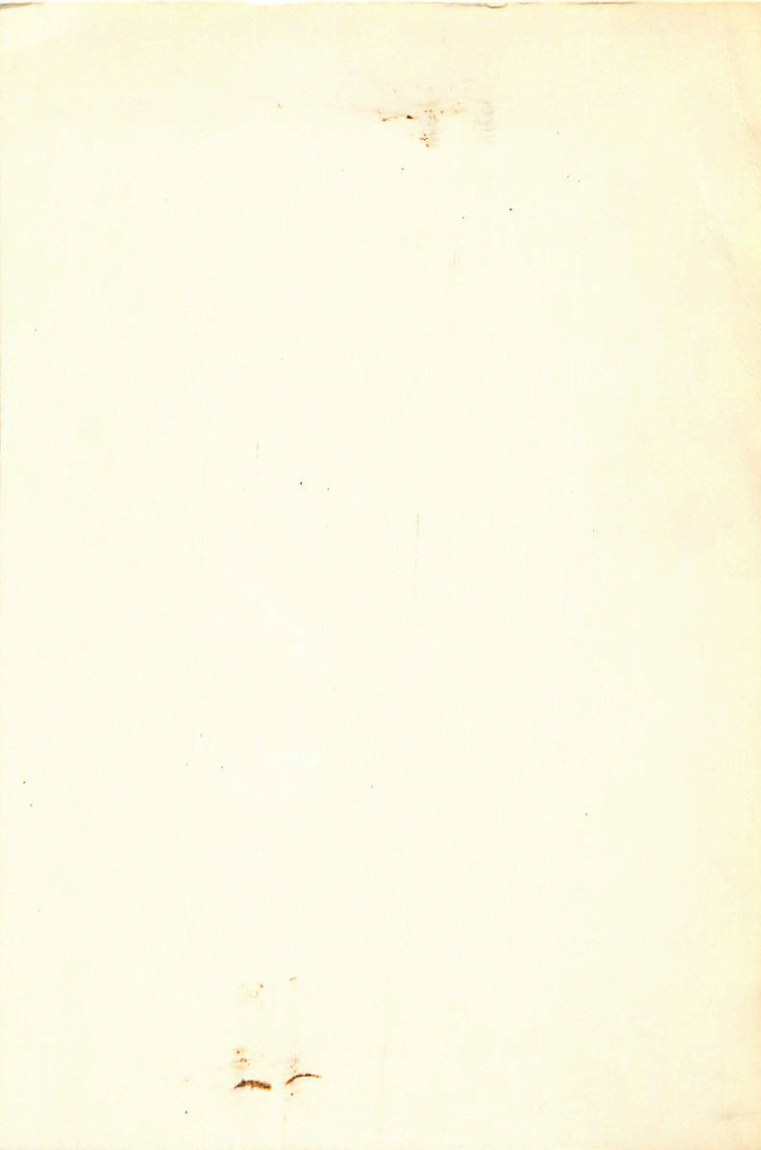
+24° 48' 14.110

- .28

13.82

1928.32

1930.2



-21.56

5282 14 0.7 + 68 56 6.26 N5

$$\begin{array}{r}
 -036-005 \text{ 66} \\
 -2 \text{ +1} \\
 \hline
 -038 \text{ -004}
 \end{array}$$

21



5202.0000

0000

$$-0027 + 5.9 - 0.18 + 5.4 + 0.35 + 0.12$$

6.4

$$14 \quad 0.1.1 + 7 \quad 47 \quad 6-9 \quad \text{III} \quad -20.18$$

122744

18989

8256

$$7.719 \quad 1910.8 + 7 \quad 47 \quad 9.41 \quad 1908.2$$

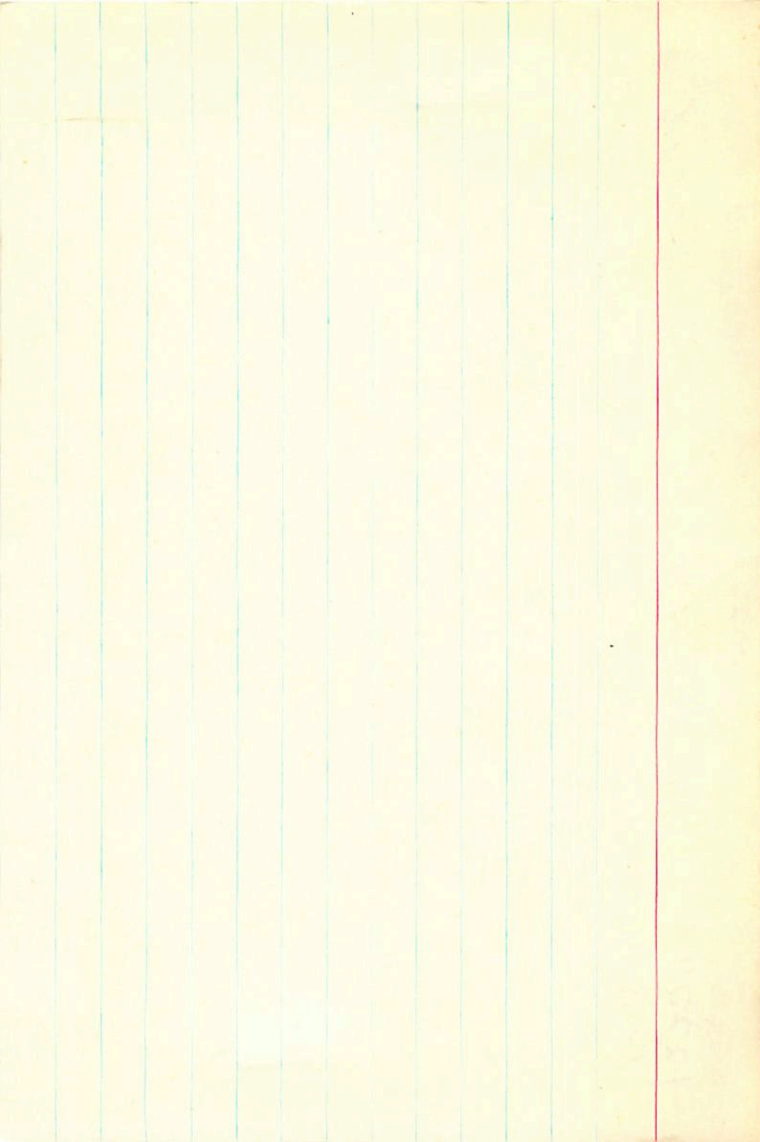
$$+106$$

$$\frac{825}{904}$$

$$+75$$

$$\frac{10,3}{6}$$

7.124



5275

14 01.8 75 08

-23.4③

122799

123154

14 01.6 +73

12

8.8 dG7 -146^{4W}c

+730615

8263

767

-115 ± 1 -012 ± 2 GR¹

437

-5

0

7.20 +37

-120

-012

794

8800

-120

-2 GAZ

73

07

-2768⁵ e

817

+38

→ 78
728

346

122837

18999

8264

14 01.7

-14 44

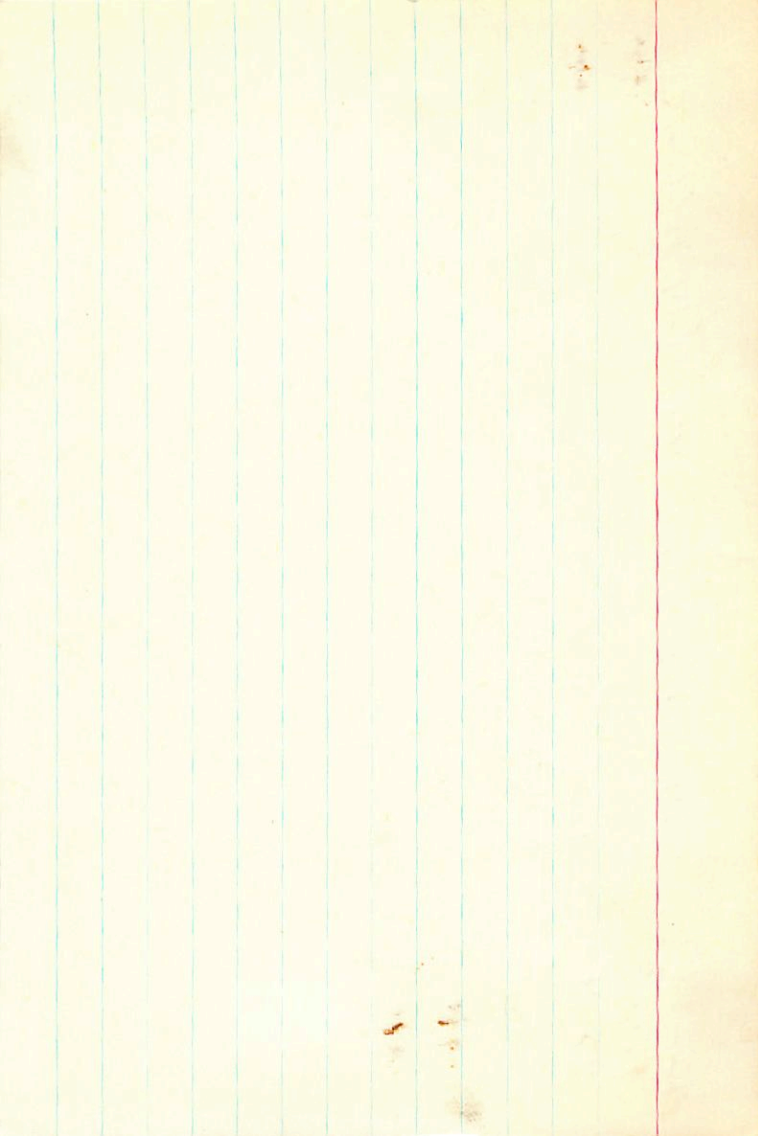
6.4 966-15.06

42

42

-026 N30

-026 ± 2.3 -024 ± 2.3 Gc → 1130



-28.56

5283

14 02.0 +2

33

6.22 NO

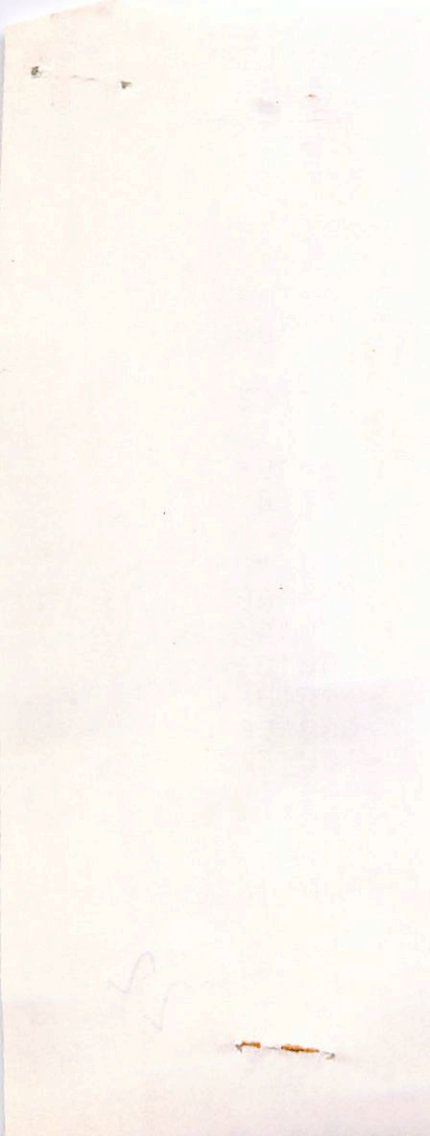
6.27 +1.02 +0.66 ✓

-033 -010 GG

-1 +4

-034 -006

22



-21:310

0.893

0.883

-7.788

-0.163

-0.124

23.776

-0.479

0.101

-28.500

100.000

5.000*

-0.006*

-0.034*

33.000*

2.000*

2.000*

14.000*

5283.000*

22

27





122796.000*

H14ya

123123

16029

8270

14 03.5 -26 27 3.5 GK3 +222a

3.26 +1.14

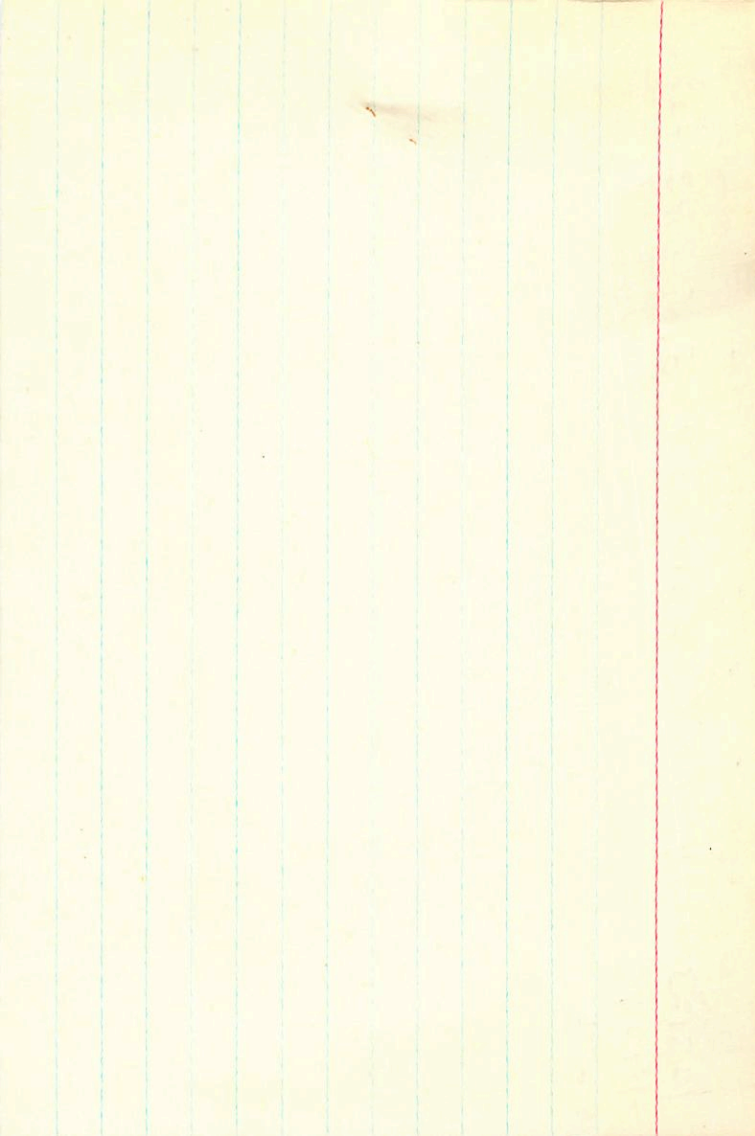
+27.2

354.

⁵⁹
+0032 -145 591230

+0034 61.7 -145 ± 1.66 → 1120

+27.3 (2)



1.181 574 203 -520 1070 DM²
14 036 -34 08 120 11-15

5258
123134

2.07 +103 +0.85 L 195

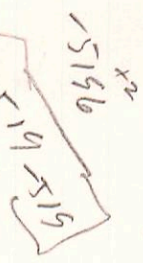
(158)

-131
+111

1.66 +0.375 55
1.88
1.11
1.3
0.6
8447 -864
0227 -4432

-0.04287 -0.5227
+ 31
F124 +1.36
F126

-0.4242
-5203 -5174
1.15700



-5203 -5174
0.354
Candian

-8648

1.181 574 203 MF

5288.000*

14.000*

3.800*

-36.000*

-8.000*

-0.519*

-0.519*

1.150*

16.982

1.300

0786

1.59

1.530

-0.694

30.6

25.086

-2.776

-0.593

579

-47.913

24

-1.434

0.408

181

-23.823

24

$p = 0.55$

W8277 14 044 +28 04 +26.58 (24)

W66M

05=7

-007590 -008 +9.0 " 044 -006
-0024 -021
+30

14 4 21.467 160.64 +38 3 58.10 1909.9

070
537
32
58.42

+0001 - 0036
- 4 + 36
0

~~21.467~~ 58.3 1530.2
-31

DNV

59.99

33/10000

713 +694 -102 +1290 -2.7 +1263
+640 +703 +310 -1535 -145.3
-287 -1556 +945 +0643 +25.0 +69.3

216 6978



$$-0359 \pm 3.7 \quad +0855 \pm 4.2$$

$$\begin{array}{r} 123210 \\ 19058 \\ +250526 \end{array}$$

$$14 \ 04.5 \quad +74 \ 49 \quad 1022 \quad +6.88$$

8.3

$$-141 \quad +0856$$

$$-135 \quad +090642$$

$$\begin{array}{r} 31.638 \quad 1899.0 \quad +74 \ 48 \ 36.85 \\ 1.831 \\ \hline 33.469 \end{array}$$

$$-4.02$$

$$\hline 32.83$$

-517-856 945 262 -128 +087 H.S. 084 +7

-071043118-072 004 265 +1.5 1.5-1 015

-1.5 +41 +13

123409

19061

8290

14 04.7

41.307

$\begin{array}{r} 252 \\ \hline 559 \end{array}$

$\begin{array}{r} 41.426 \\ 13 \\ \hline 439 \end{array}$

$\begin{array}{r} 41.41 \\ 15 \\ \hline 423 \\ \hline 432 \\ \hline -127 \end{array}$

$\begin{array}{r} -0058 \pm 50 \\ -6056 \end{array}$

+28 41

22.8

$\begin{array}{r} -009 \pm 3.4 \\ -015 \end{array}$

7.0 μ g G-6 -55.18

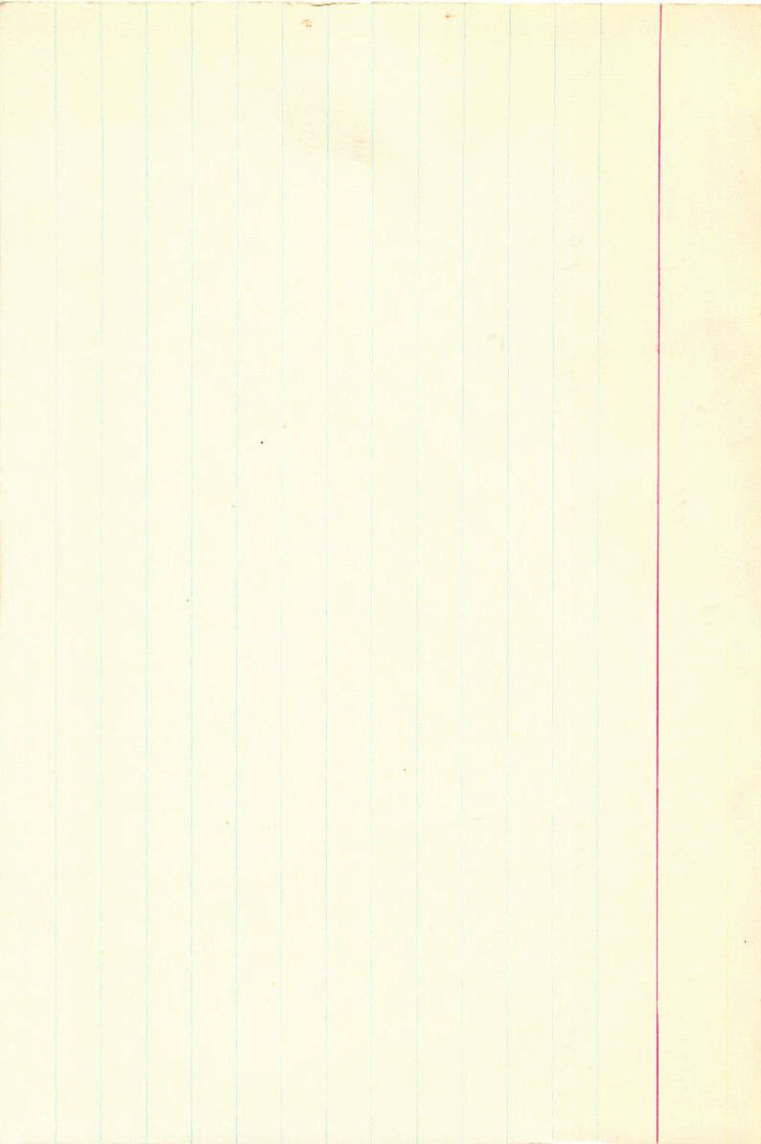
$\begin{array}{r} 46 \\ \hline 31.68 \end{array}$

$\begin{array}{r} 31.49 \\ -15 \\ \hline 31.34 \end{array}$ 1928.32

$\begin{array}{r} 31.4 \\ -28 \\ \hline 31.12 \end{array}$ 1930.2

$\begin{array}{r} 31.12 \\ \hline 31.23 \\ \hline -45 \end{array}$

$\begin{array}{r} 58.52 \\ 29.3 \\ \hline 30.7 \end{array}$



G-165-47

14 048 785 D

141 174 744

212

141 174

363-487

0375

7000

141

7887

141

2411

7000

141

25

+0073±5.5

-115±3.9

+0977

-117

-12

14

41

7.6

dF7 +14.18

123453

19072

8283

21.947

1903.0

-12

41

24.03

19498

AOS4115

-343

21.604

1.079

20.658

21.734

21.734

78.9

790

49.614

32.294

21.972

18.26

13.07

9.52

22.59

22.59

21.61

14.69

844

49.614

32.294

21.972

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22.59

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14.69

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22.59

21.61

14.69

844

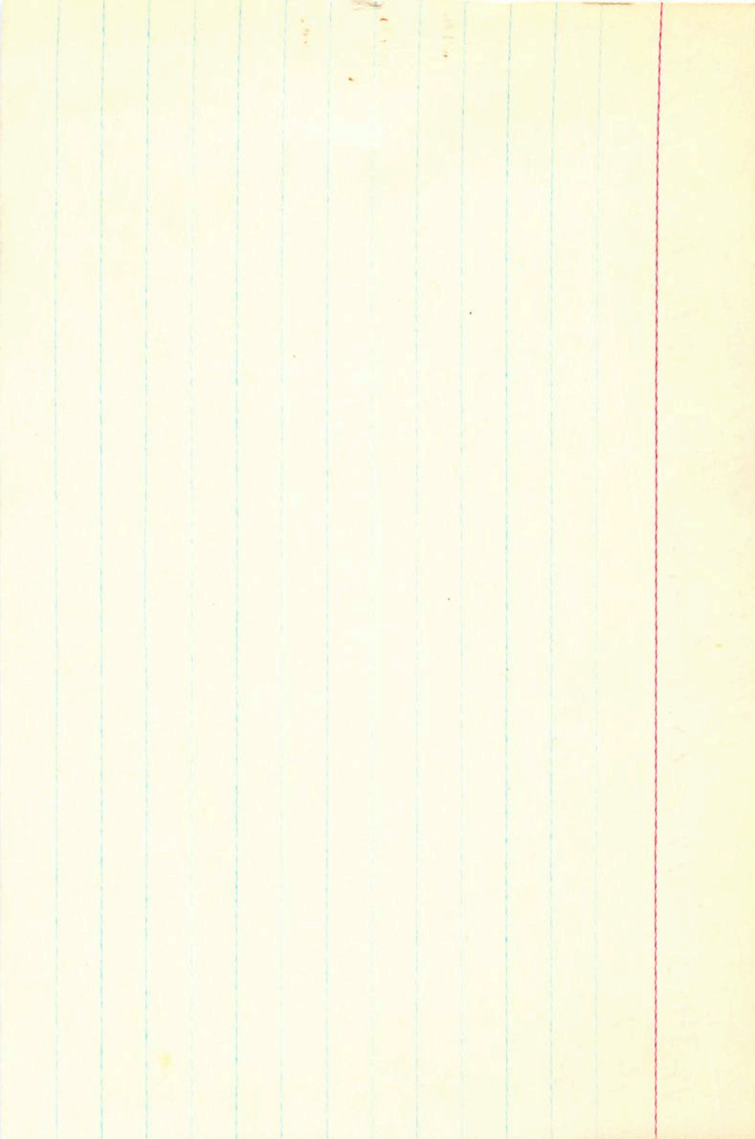
49.614

32.294

21.972

18.26

13.07



96Vn
-0006±2.2 +018±2.0
-0004 +012

123630 14 06.3 -10 06 6.5 967 -20.16

19092

8297 20.486 1900.5 -10 5 57.91 1899.1

$$\frac{030}{1.518}$$

$$0.584$$

$$\frac{19.870}{19.870}$$

$$\frac{20.459}{19.9}$$

$$\frac{502}{506} -012$$

$$\frac{20.507}{511}$$

$$\frac{-1.92}{55.83}$$

$$\frac{48.09}{8.40} 1927.28$$

$$\frac{56.78}{55.71}$$

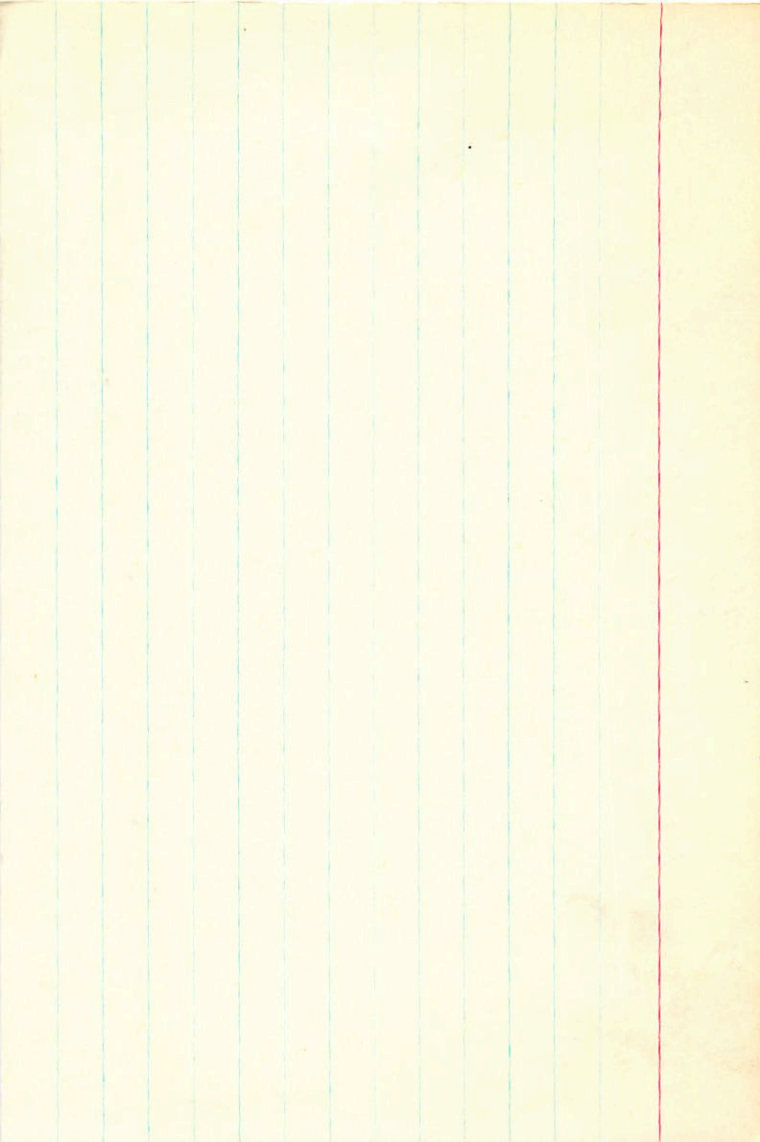
$$\frac{6596}{33.0}$$

$$\frac{1938.66}{55.51} \text{ (33.9)}$$

$$\frac{55.44}{55.36} \text{ (33.9)}$$

$$\text{ (32.5) }$$

$$\frac{55.44}{7.39}$$



20 6216 -0643 -641 Copying
-0647 -652 cc

cell

123505 14 06.5 -61 16 G9 U

73211 -06465 -646

9.72 + 0.78 + 0.235 (2)

21(I) 11(1st)

+5.82

1.022

307(12)

9.22 + 0.34 (2)

898

1.0195

352(16)

$\Delta(B-U) + 17$

356

536(8)

477 759 732
2390 8545 -066 6

$\Delta(U-D) + 495$

37 -4657

+10.7

9.72 + 0.78 + 0.235 0.037 2.14 + 32 - 84 - 61

9.22 + 0.34 2, 2 35 + 7.2 + 21 - 20 - 22

-467 -642

3.0

W V W

140.7 -0.454 -0.634

+71.9 -120.1 -102.1

-0648 -649

+22 -20 -23

9115
408
60 304

-468 -649

13973

9.66 478 263 231
967. 475 255 204

228

-649
3.15
+40.7

326 10915

390

-2615 1093

3604

262

0
425
59

26

647-8475
-644

R.A. :
DEC. :
-81.250 :
-873.000 :
-842.000 :
3.150 :
43 :
48.700 :

AD. VEL. :
MODULUS :
DISTANCE :
FM. DEC. :
FM. R.A. :
R.A. (U) :
D3 (U) :
D3 (U) :
D3 (U) :
QU :
U :
88.853 :

142.0 :
0.120 :
-0.742 :
X-3052.122 :
-112.212 :
D1 (W) :
D3 (W) :

D1 (W) :
D3 (W) :

R.A. : :
DEC. : :
SM. R.A. : :
SM. DEC. : :
DISTANCE : :
MODULUS : :
AD. VEL. : :
14.100
-61.250
-973.000
-849.000
3.150
43
40.700

q1 (U) : :
q2 (U) : :
q3 (U) : :
DU : :
U : :
-0.709
-0.217
-0.671
2241.599
68.323

q1 (V) : :
q2 (V) : :
q3 (V) : :
dV : :
V : :
0.641
0.196
-0.742
-2026.185
-116.619

q1 (W) : :
q2 (W) : :
-0.321

7264

19 6.5 44

3.02F2

41 π Sg₆

25 9

26386

19.1
-21.1
000
-34.3
6.0
-4.5

11611

324

-9.8a

-0004 -0357
+16 -8

+00012 -0359

0000 -0365 W₃ 50
-0006 -0332
-0087

0000-0345

3.7: 3.8, 0.1

6.0m, 0.4

ρ

-0267 +4.1
-1533 -2.6
-0687 +2.3

0.315 0.157 -0.936
0.342 0.901 0.266
-0.885 0.404 -0.231

→ 159m. +5.0
-20.0
-8.6