

BEV in (X)

7003102

13 46.3 -00 21

78

~~5000000000~~

5 labloger -025 -0089 →

5.0018

334

~~0 -025~~

+3

-3

+3

1829

-753 478 -450

622 742 -249

-215 468 857

+0892 -0207

+0787 -0317

+0255 -0200

+0658

+413

-633

+0055

+003

6000

+38

-65

+10

~~+003 -024~~

-0.6

-2.0

+6.9

N.02-24 +10

436

(-017) (-013)

41 28.11.94
2 50.39.04

45 18.08.04
199.60.00

42 44.92.00

2 33.63.88

45 18.08.04
199.60.00

13 43 46.41

45 10.05.00

45 10.05.00

1 148.16
2799.06

2050.98
45.34

5- 45.14

15- 3.54

48.04

45.14

-00 11' 45.5- 1920.0 2020

9 - .75

20 45.35

45.60

48.054 44.99 1899.4
48.620 48.00 1919.8
48.016 45.00 1920.0
48.609 45.41 1931.3
48.586 45.97 1936.4

18.600

809

609

595

-1056

45.1

-30

45.41

1931.3

45.59

77
3.8

-0 20 45.59

-18

1934.4

-1.00

18.558
28
586

45.974

-1.00

190

0010

119985

13 44.4 -45 49

+33.5 ± 0.8 C₂ (6)

(5784)

6018631

43139

-43 02701

8.54 + 0.63 6.3 12 - 2

041 (254) (410)

-19725

CR

6.60 347 155 491

2.624 150

3.86

+10 -47 +27 .02

-271

+37

-0.181 + 0.23

4.0

(05)

-1893

+335

-159 + 0.39

$$\begin{array}{r}
 -164 \\
 -192 \\
 \hline
 -175 \\
 \hline
 +03466 \\
 +035CP \\
 \hline
 +034
 \end{array}$$

25 ± 4 (19)

-0157 ± 150 +034 ± 150

-440 -898 -217 697 -178 +034 +33.5 -024 -24 114

-078 -011 140 022 -474 206 +233 -21 -10

-45 +25 -18

02

35.544 1904.6

-45 48 53.17 1904.6

$\boxed{+10 -47 +27}$

01

-1.54

-68 +61 -43

54.71

$\boxed{+43 -20 +43}$

713
36.257

112985
GC18631

X3139

13 44.6 -45 44

G-312 - $\sqrt{2}$

8.54 +0.63

$C_2 = +33.5 \pm 0.8 (6)$

+39-68 +43 .010
+9-46 +30 .020

^{G-2}
-164 +034
-192 - +035 ~~6~~
-176 7034

25±11 C(8)

-441 - 895 - 717 657 - 176 + 034 + 33.5 - 024 - 24 1/2
 -078 - 011 158 022 - 474 656 + 23.3 - 21 - 10

-68 + 60 - 13

-59 + 50 - 5

010

007

R.A.	:	13.750
DEC.	:	-45.800
PM. R.A.	:	-271.000
PM. DEC.	:	37.000
DISTANCE	:	4.000
MODULUS	:	60
RAD. VEL.	:	33.500
q1 (U)	:	-0.753
q2 (U)	:	0.017
q3 (U)	:	-0.658
np	:	677.486
U	:	20.715

0141
 1.20
 + 248

q1 (U)

— 13 44.8 -5 53 9.6 dir4 -46.18 W3

8138

73143

-35250 -559±2 CR



89Vi
120235
18645

-0027±2.5 -023±2.2
-0025 -023

13 45.7 -06 35 6.6 964 -0.98

8143 40.824 1900.5 -6 35 19.04 1898.1

133
957

22.342

18.485

40.827
32

879
+9

888
40.956

864

876
-081

32.4

+1.19
17.85

49.36 1926.8

30.45

19.41

165
18.96

+20
18.56

18.89 1939.64

+12
18.77

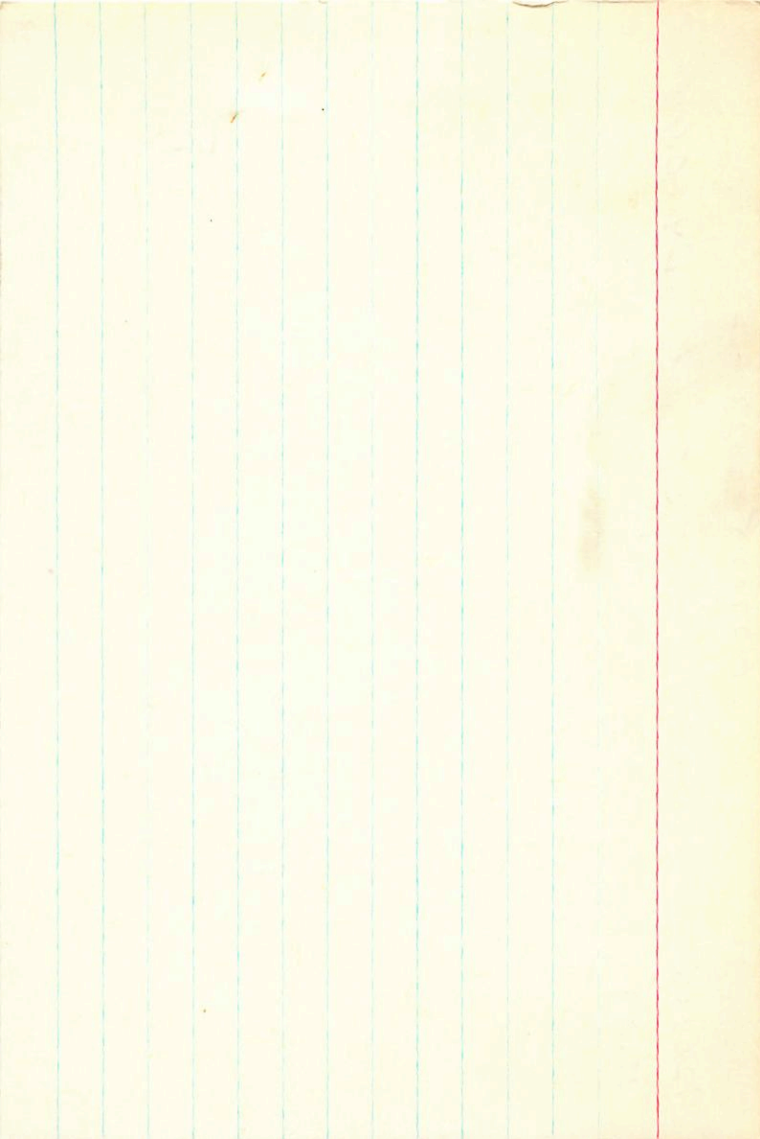
18.66

-0.81

6646

33.2

35.1



R B 00
120136

13 44.9 +17 42 4.5 dFC -15.6a-

15637

98⁸⁹
-0339 +034 N30

8140

-0339 ± 0.9 +034 ± 1.066 → 230

A055025

10.6 M2
open

56 ± 6

-j3387 +0369 W8 50

-484

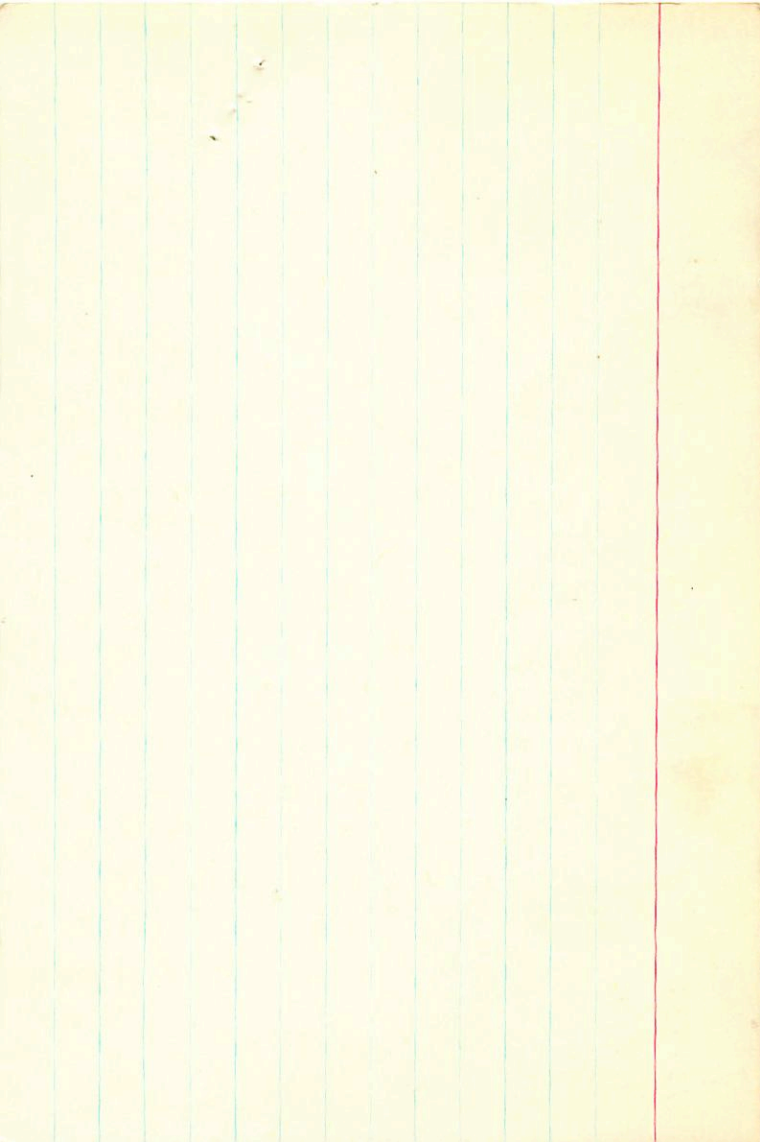
+0366

[-404 -285]

-505
+472

1.2

-15N



120126

13 44.9 +17 42

FYU

5185

4.50 + 48 + 05 J

6218107

315 .179 .439 5505C 2-6568
cut

5(2)B20

36 151 529
545

10 m⁴
202

237 -2

100 + 33.2 - 20.2 - 68

558 [37]

+ 1822 - 1282 + 520

9

4/2

28

DEC 1 1951
R. G. S.
DEC 1 1951
DEC 1 1951
DEC 1 1951

R.A.

DEC.

13.750

17.700

-506.000

000

-6047 ± 15.0 -18.07 -066 ± 15

C₃(15)

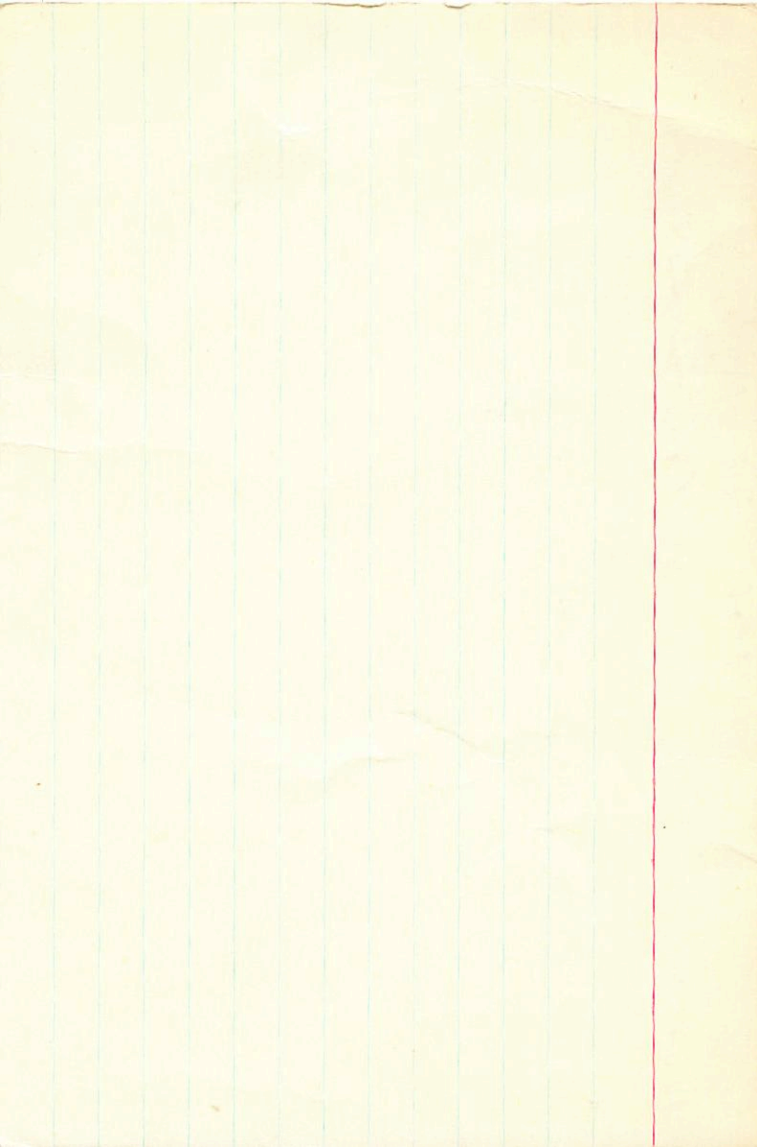
120223 13 46.1 -43 29 68.10 -24.1 ± 0.6

18655 8.97 + 97 1.96 -263 (B) *Nov*

3.754 1903.6 -43 29 7.52 1903.6

3.06
4.46

218
3.972



120223 13 46.1 -43 29 GP 2

Not used

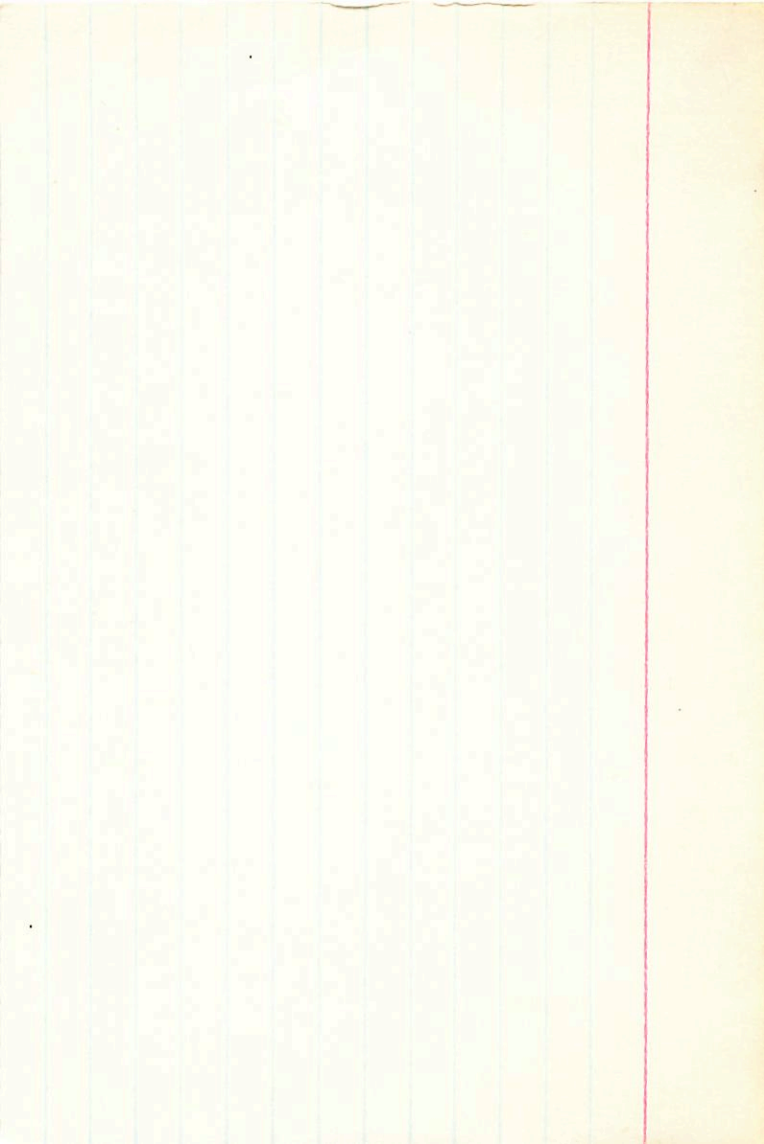
A(I)

$$8.94 + 0.59 + 0.57 \textcircled{2}$$

$$8.37 + 0.41 \textcircled{2}$$

$$\Delta(B-v) + 09$$

$$\Delta(n-o) + 405$$



723

$13^{\circ} 46' 1''$

$-43^{\circ} 29'$

HD 120223

+8.97

+0.97

+1.96 G8 IV-V

- 751 + 041 - 659

+ 623 + 375 - 686

- 219 + 926 + 308

UTTS662

4C

120253 13 46.1 -40 38 G-9 E-DI -64.3

FD1204

8.78 + 0.89 (1.50)

RA51471

$S = +0.13$

-236 + 062 CR

-224 + 46 CA

0.000 C(7)

-216 + 54

12

-225 + 60

→

x v w

$M_v = +6.8$

+6.3 + 2.9 = 10

-6224 + 048740

+3.8 + 12.4 + 1 + 2.6

-261

$\boxed{-261 \ 1952}$

8

120467 cont

-2103781

82.2
-56.5
-21.4

-1.751	- .495	Y
- 3	- 15	
<hr/>	<hr/>	
-1.754	- .500	
+ 1	+ 3	
<hr/>	<hr/>	
-1.753	- .507	←

1210

→ 749	+280	-600	+6.2236	-6.729	+5.5507	+66.6	+21.2	+87.8
+624	+603	-497	-5.1950	-1.4491	-6.6341	-79.6	+17.5	-62.1
→ 223	+747	+626	+1.8530	-1.7952	+1.0578	+0.7	-22.1	-29.4

13.750
-40.600
-344.000
48.000
1.300
18
-64.300

-0.753
0.077
-0.653
949.879
59.297

0.622
0.407
-0.669
-677.158
30.686

-0.215
0.910
0.355
472.950
-14.193

W

-102500

-714 (17)
704 (3)

CE Va 13 46.7 -01 41

13 46 42 -1 40 53
-102500 13 849 10 -1 38 44

-753 464 -460 +2356 +006 +2362
632 736 = 265 -1977 +007 -1970
-218 485 846 +0073 +025 +0678

-0045 +001
+ 1 +
-0074 +002
-066

-0068 -0014
-067 0007 +

755
757
154
181
102
-3

-0035 -10 A6142

11

0.000
0.000

-0.747

0.470

-0.470

107.000

42.001

0.625

0.737

-0.237

-121.642

-40.402

-0.226

0:485

0:845

~~2:805~~

0:999

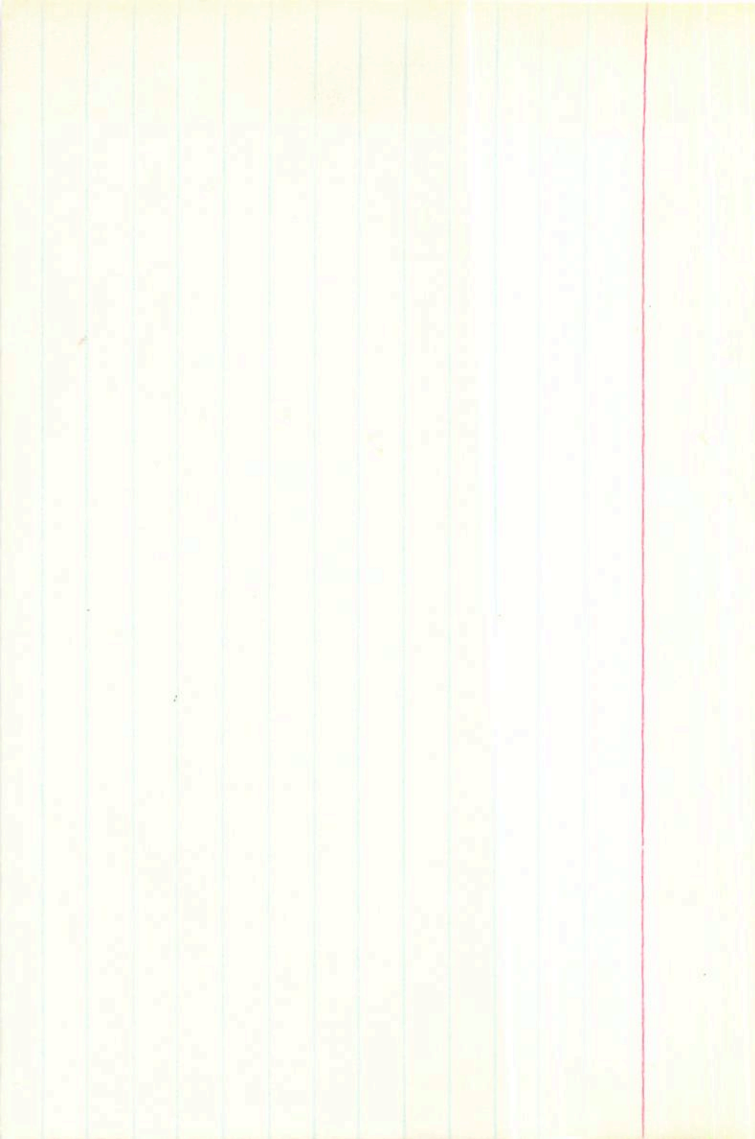
10 800

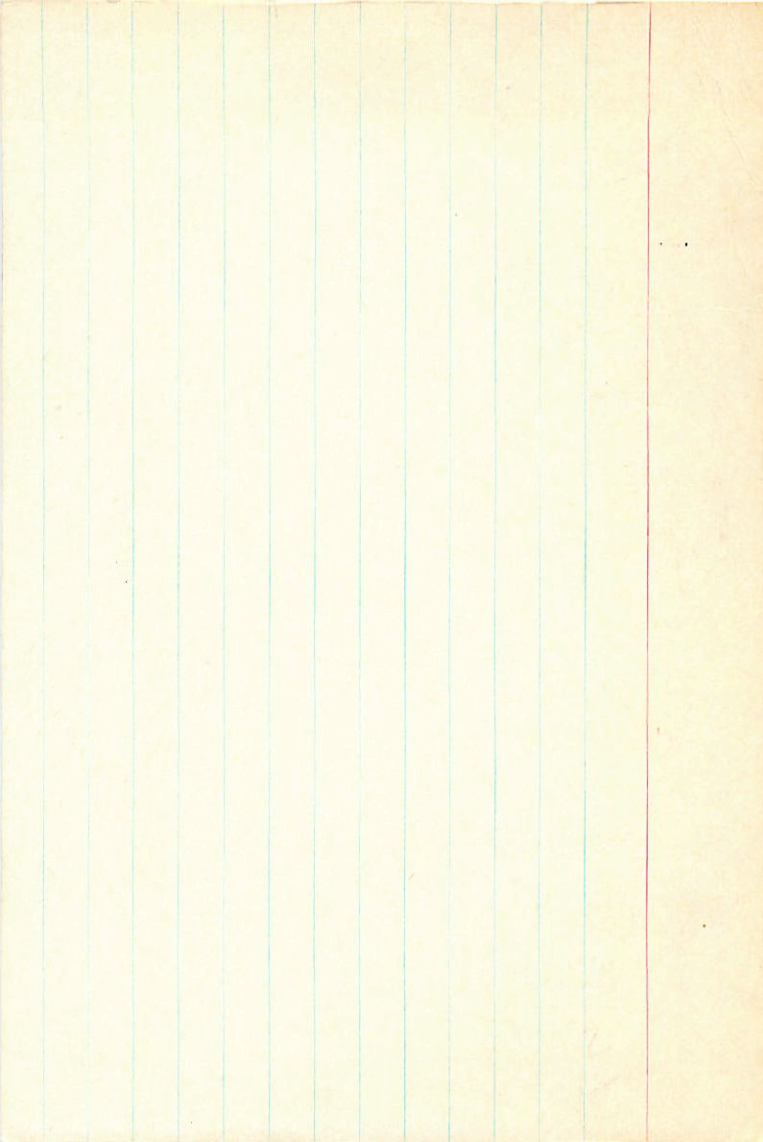
R 66m 13 428 +39 47 328d

-5.66
L 0007 -0.017

-014 +010 ML

263 284 5.72 +1.98
265 267 6.42 +1.52
286 6.66 4.58 +1.61
804 6.73 5.02 +1.59
324 2.74 5.69 +1.81
~~644 2.28 5.26 +1.58~~
659





-0066 ± 1.8
-0064

+034 ± 1.5
+034

-60
-625
-5.69
-5.4
-0.95 + 0.34 ± 0.6

Σ 2500 13 47.1 +14 0.3

HRS 200 12077
18674

8159

400 +1.60 K5 II

3.880 1901.0 +16 2 42.37 1896.1

$\frac{323}{4203}$

$\frac{-1.83}{401.54}$

4.3480

41.91 1834.2

$\frac{14}{994}$ 1436

$\frac{-2}{41.89}$

3.934

42.13 1939.95

$\frac{18}{942}$

$\frac{-14}{41.97}$

$\frac{968}{968}$

$\frac{41.93}{41.93}$

-2.35

$\frac{41.93}{41.93}$

$\frac{36.6}{36.6}$

$\frac{40.5}{40.5}$

+1.39

$\frac{40.5}{40.5}$

-450 -893 • 276 561 -095 +034 -5.6 a 009 -2 156

-043 004 085-008 -166 422 -814 75 +3 016

-5- +29 +8
+29 -5 +3

-12 +45 +14

+46 -14 +10

010

2

21

5195
Lshae1

13

4723

-39

89

-3.852

60300
120539

+0012+2.4
+0015

+010±2.0
+010

-48①

13 47.3 +21 31 5.1 gms -2.8ca

18683

8162 20.909 1896.4 +21 30 41.47 1897.6

-064
845

-52
4095

20.921 1820

932 910

42.0

41.44 1936.2

+2
41.46

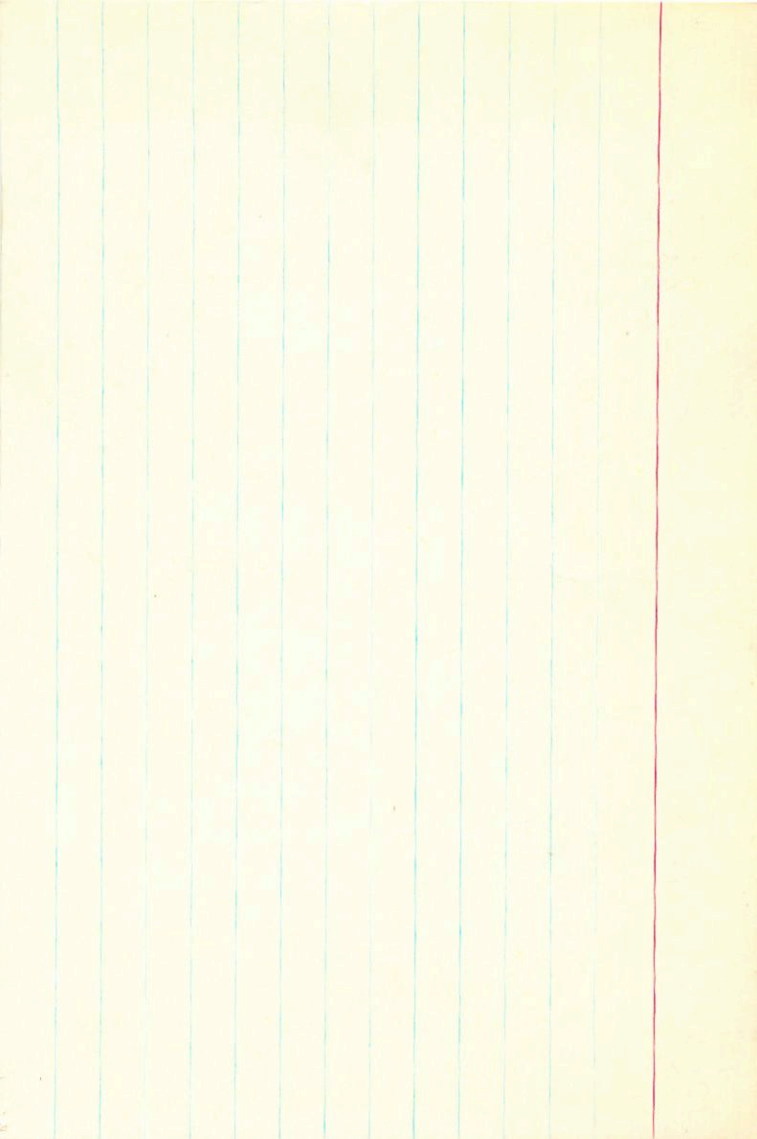
41.43 1940.58 7678

-16
41.27

38.4
40.8

20.881 7 +065
888

41.36
+0.41



12015-1 10 980 +21 31

025912 + 0026 + 1015 (circled) 0028010 + 9000 0027 0028 0029 0030 0031 0032 0033 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079 0080 0081 0082 0083 0084 0085 0086 0087 0088 0089 0090 0091 0092 0093 0094 0095 0096 0097 0098 0099 0100

0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079 0080 0081 0082 0083 0084 0085 0086 0087 0088 0089 0090 0091 0092 0093 0094 0095 0096 0097 0098 0099 0100

0034 0020

NO

0030 0031 0032 0033 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079 0080 0081 0082 0083 0084 0085 0086 0087 0088 0089 0090 0091 0092 0093 0094 0095 0096 0097 0098 0099 0100

0030 0031 0032 0033 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079 0080 0081 0082 0083 0084 0085 0086 0087 0088 0089 0090 0091 0092 0093 0094 0095 0096 0097 0098 0099 0100

120787 13 48.1 +61 44 6.0 dG3 -11.48

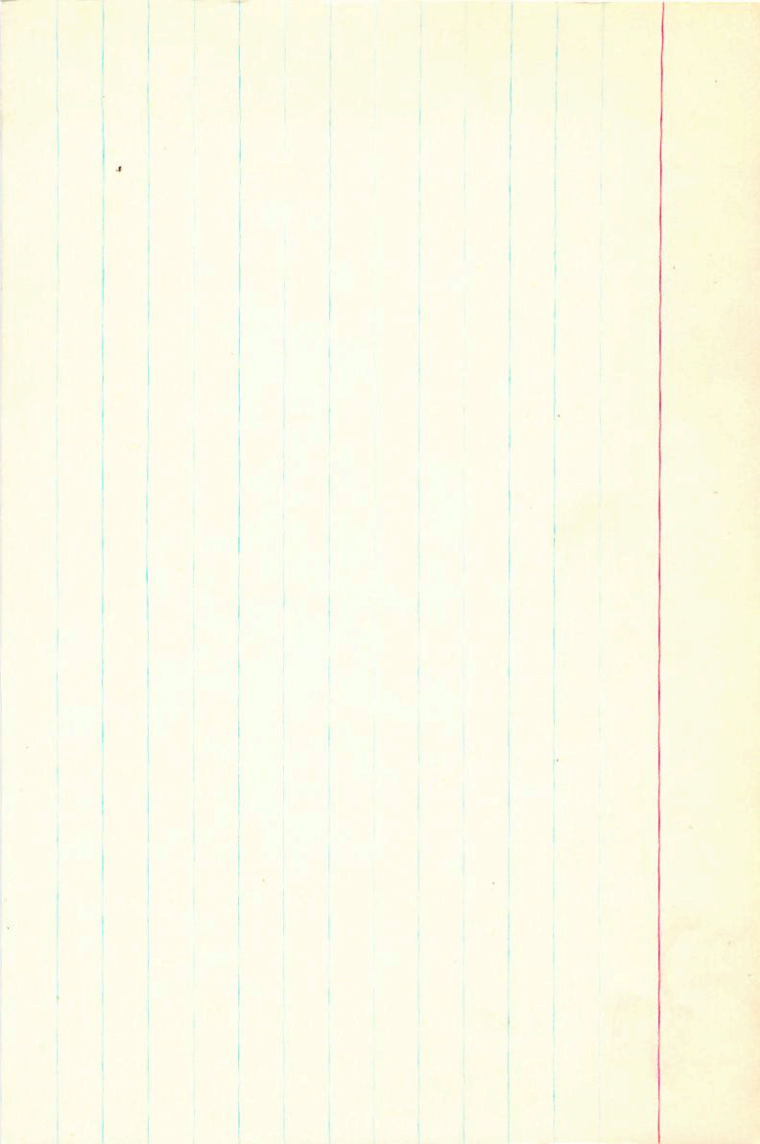
18704

8169

+0087³¹ -100³³ N30
+0092±22 -103±2.2 Q-C → N30

43.2 (16)
-13.1 (17) 23.0
-12.0 (8)
-12.4 (1)

(A)



120592/3

13 48.4 -48

QBH

7.36 + 0.79 + 0.50

6.5E + 6.9
RDE + 4.5

11.9

5.5

7.46 + 1.47 00

-0.124 ± 8.7 -0.26 ± 7.5
-0.109 -0.39

6618700/11

18709 24603

1899.6 -48 2 44.71 1895.3

+1.42
43.29

25.253

51.305

33.452

27.817

154

24.978

1590

1553

4/63

24.647

-21
626

A -0.109 ± 3 -0.34 ± 3

B -0.01 ± 3 -0.38 ± 3

116 - 620

43.29

17.69 1928.41

22.62

45.30

+ 80

49.14

44.53

45.32

-33

45.65

102.6

45.10

1955.80

84.21

42.1

46.8

46.8

1955.80

-0138 ± 9.5 -028 ± 8.0
-0101 -038

1974 26.824 1901.3 -48 3 5.10 1896.2

672
27.496

41.57
3.59

53.672
33.453
27.125
15.4
27.279
18
26.1

37.89
27.62
0537
+80
4.51
-14
4.55

1928.68

41.1

14160
27.080
-416

4.51
-14
4.55

10.70
5.35
1.76

26.930
-21
909

5.82
-33
6.15

1956.10

84.78
42.4

46.2

-455 -890 -743 669 109 -038 +5.7 028 -4.20 +120 ✓

-050 013 097 -025 -118 521 -3.4 -1.7

02

-0.8 21.4 -4.8
-4.5 -10.9 -7.7
8.1 -4.0 -4.8

-9.3 +24.3 -10.2

+15.8 -23.1 -0.7

-9.4 +25.7 -10.5 019

-0.8 22.6 -4.9
-4.7 -11.5 -7.9
8.4 -4.0 -4.9

+16.9 -24.1 -0.7

05

-0.5 7.4 -3.1
-2.8 -3.9 -5.0
5.0 -1.4 -3.1

-5.7 +9.7 -6.6

+4.0 -11.7 +1.5

4.0 2.0
4.0 2.0
4.0 2.0

3.60 +137 -20.5 +0.6 -0094
+331 -315 -13 -056 -5.4

2000 13 48.6 -24 08 +2.1 t

6029

38e -288

436 340 302

$\frac{38e - 345.2}{2}$

~~38e~~
-433

+2.1

5.28 -050 123 711 2.791
9.54 169 150 749 2.786

938

4R5207

13 48.8 -52 34 +272
46

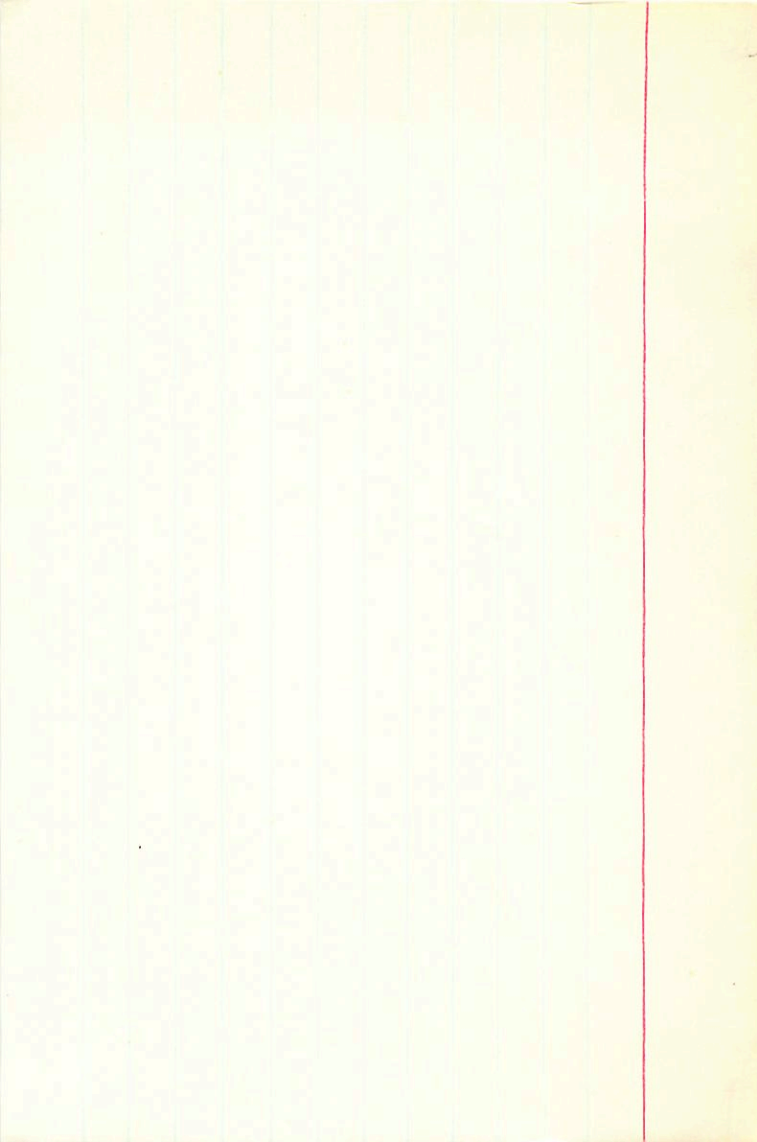
81.3 per.

-0630 -024 1230
-0037 -032 66

-0033 -027 -9
-30
-11

743 -078 -664
627 265 -732
-234 961 148

+1622 +0100 +1122 +9.1 -17.9
-0862 -0339 -1201 -9.8 -19.8
+0322 -1230 -0908 -7.3 -4.0



1.19323 165 449 (1)

250

120691

13 48.8 -31 04 FS -62.6

18717

7.16 +0.52 +0.02

2162

136(18) 47.353 1409.1 -0253 ± 6.9 -061 ± 5.7

17.56 1906.6

1.035

2.65

48.388

1491

59 184

21.480

1929.45

-0253 -061 GC 50.67

25.9625

-0265 - NW 27.12

844

-0241 -074 CR

47.949

17.75

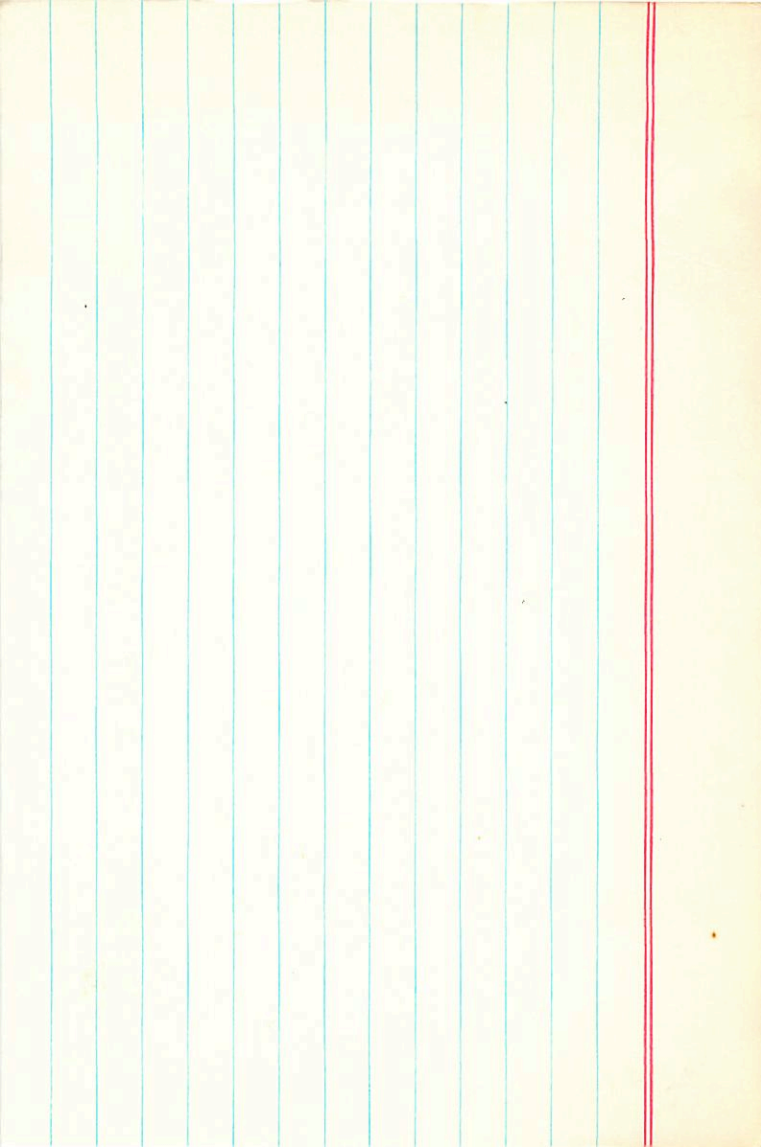
.0

-049 CR

-0253 -061

-0249 -057

..321



120754 13 49.1 -31 22 60± +8.7 4C

FD946

GC18733

6.7 } 0.7
7.7 }

6.10 +0.48 (1.60)

-0044 ± 6.0 -054 ± 4.4
8.323 1895.7 -0038 19.62 1889.9
239
8.562 3.55

-6041 -057

-6037 -052

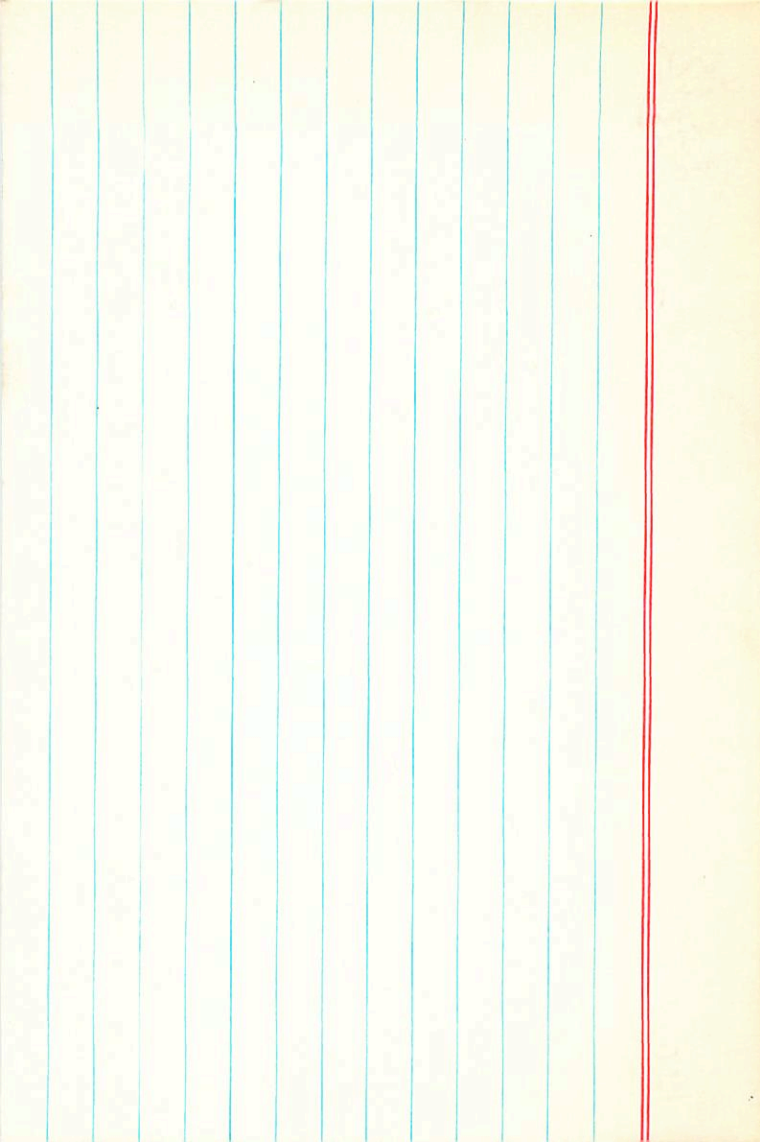
8.415

-2)
3

18.68 1939.69
-20

18.88

-0.48



120933

18741

8184

13 49.6

734

41

5.0 gm²

-43.6a

-0018±3.5
-0022
-043

35.182 19043 734 41 28.16 1903.0

$$\begin{array}{r} 082 \\ \hline 1,264 \end{array}$$

$$\begin{array}{r} 1.79 \\ \hline 29.95 \end{array}$$

54.6 1927.0

(29.0)

$$\begin{array}{r} 29.008 \\ 6.22 \\ \hline 35.228 \\ 1905 \end{array}$$

$$\begin{array}{r} 20 \\ \hline 20 \\ \hline -064 \end{array}$$

$$\begin{array}{r} 26.02 \\ \hline 28.57 \end{array}$$

$$\begin{array}{r} 130 \\ \hline 28.65 \\ \hline -1.30 \end{array}$$

$$\begin{array}{r} 29.15 \\ \hline 29.23 \end{array}$$

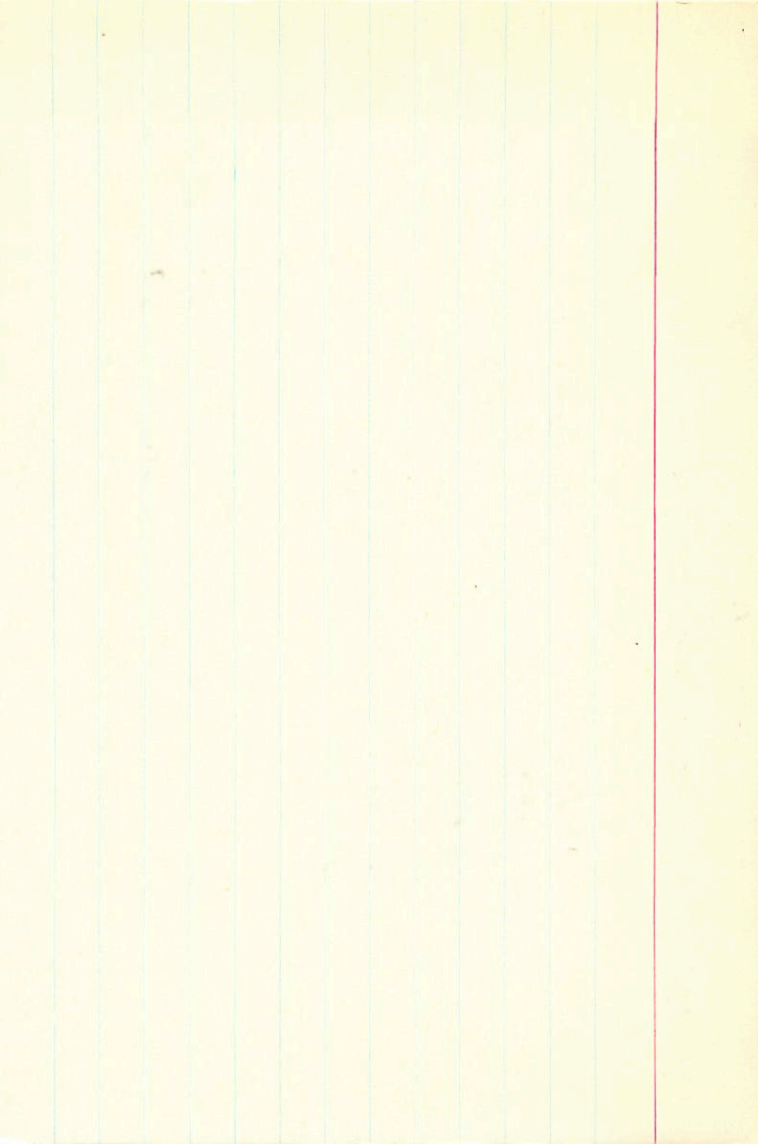
$$\begin{array}{r} 35.202 \\ \hline 196 \end{array}$$

$$\begin{array}{r} 28.92 \\ \hline 28.51 \end{array}$$

193964

4664
33.3
30.3

$$\begin{array}{r} 013 \\ \hline 28.38 \end{array}$$



120054

13 508 + 150 16

1003 2

95

93 2 100000

100-100
100

120933

13

49.6

+34 41

$\int m_2$ -43.64

HR5219

4.70

+1.56

-022 -03 F G₂
 -025 -038 F13

 -024 -035

+2 -28 -38 .011

.007

-450 -893 569 822 -022 -038 -436 -022 -25-117

-010 -010 020 020 -142 .047 -358 +32 +16 .011

+19 +20 -38

+2 -29 -35

+12 +23 -46 .007

0 -39 -36

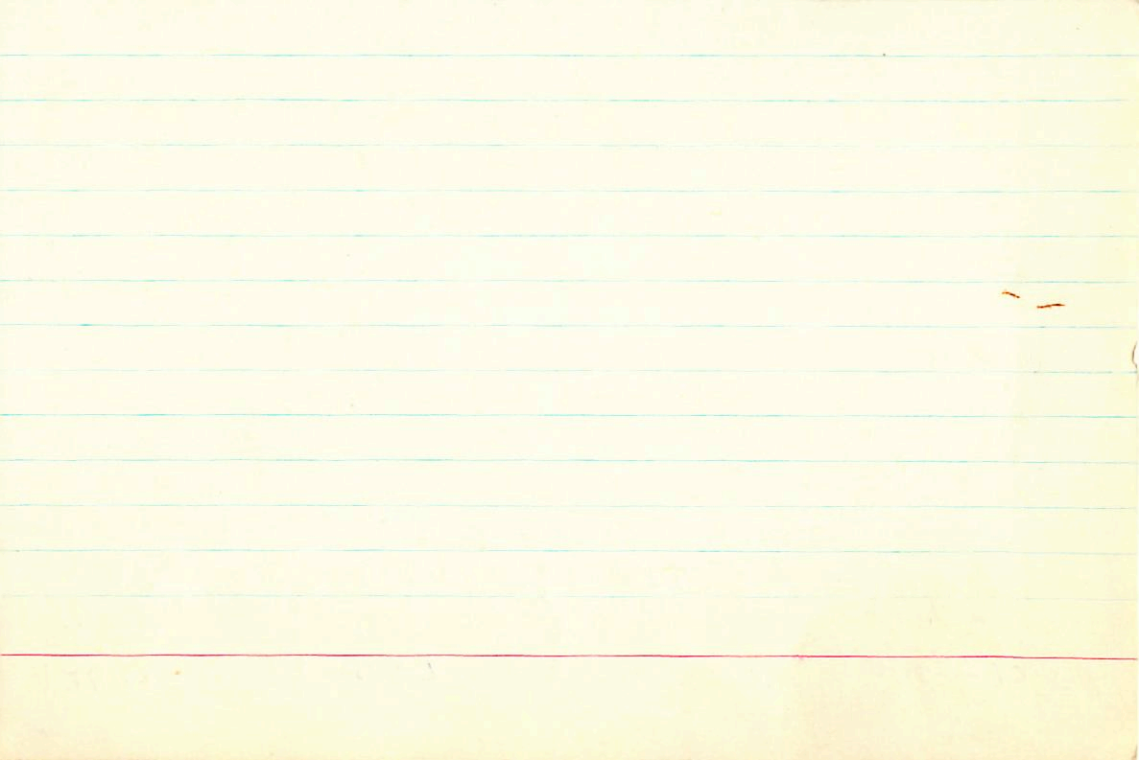
120950

13 49.7 +39 55 2.8 gm4 +32.58

18742

8185

+0010¹⁷ -027²¹ N30
-0004±4.5 -021±5.86-~~N30~~



112985
GC18631

13 44.6 -45 49

GC312 - $\sqrt{2}$

X3139

8.54 +0.63

$C_2 = +33.5 \pm 0.8 (6)$

+39-68 +43 .010
+9-46 +30 .020

GC
-164 +034
-192 - +035 GC
-176 7034

25711 (18)

-441 - 898 - 717 657 - 176 + 034 + 33.5 - 024 - 24 11^{1/2}
-078 - 011 158 022 - 47^{1/2} 65^{1/2} + 23.3 - 21 - 10

-59 + 50 - 5 007

-68 + 60 - 13 010

[+41 - 70 + 43]

-71 + 63 - 12 005

[+43 - 71 + 45]

8