

1228 0 14.1 +01 34 7.3 9M5 -6.36

140  
6521 M515  
0000 ± 2.4 +022 ± 2.1  
-0002 +016

0 14 5.495<sup>0</sup> 1902.6 +1 34 21.62 1897.8  
1495 -1.15  
20.54

1491  
5.465<sup>0</sup>  
1472

-0001 +019

6600 +0175 F14  
489 20.74  
20.89

6m, 50  
1933.70  
6.14

5.509  
-015  
1.494

+002

21.0543  
+27  
21.32

cuppl  
1939.44  
1933.8  
26

34.2

21.16  
+1.56

1928.01

1.489  
-006

5.506/500

00.55/20.95

417pm. +21 +14 +18

57

+53 +42 +32/1000m

7.03 +1.60 +1.75 (3) 15.49 5.54 +1.205 (2)  
7.02 +1.59 +1.74 (1) 15.40

5.39 +1.175 +2 +14 2.9

5.01 +1.

1.538

3.1

4.4

7.9



17.173

0.031  
-0.865

13.678

0.484  
0.044

14.394

0.134  
0.040

-6.300  
380.189  
7.900\*

0.014\*  
0.002\*  
34.000\*  
1.000\*  
14.100\*



A05221      0    14.1    +36    13                    +2.18

.0127                    +098    +0.052    H  
                                   0            + 2  
                                               
                                   +054

64.6M

+866	+318	+354	+4023	+0814	+4837	+31.2	+2.7	+33.9
-482	+331	+812	-2239	+0847	-1882	-8.9	+5.8	-3.1
-131	+886	+440	-0608	+2273	+1665	+10.8	-3.1	+7.7

14 + 14  
 18    17  
 24    1  
 5

77

062 558 . 591 807 +095 +052 +2.1031+4 199  
-006-002 098 031 -175 455 +6 +6 0 0127

$$-8 +36 +20$$
$$\boxed{+22 -35 -8}$$



1255 0 14.2 +09 58 6.8 gm2 +11.26

144

GL +0002 ±6.4 +018 ±7.5  
+0004 +005

GL326

0 14 11.107 1905.0 +9 58 1.28 1901.6  
-9  
10.098

GM, 50  
1934.70

11.091  
+ 9  
11.100

12 53.909  
1 17.142  
14 11.054  
0.079  
0.12  
0.13

0.084  
0.112  
0.270

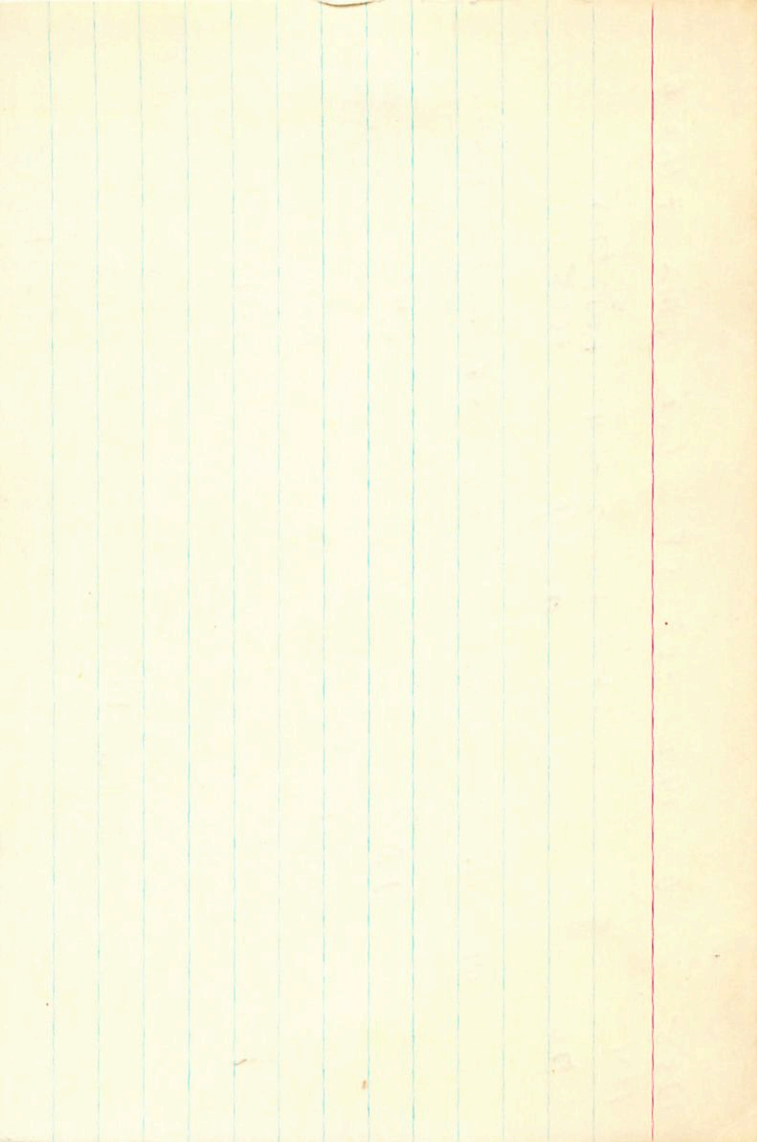
0.22  
0.09  
0.31

CapL  
1930.53

49 40.10  
9 20.92  
58 60.02  
0.98

32.6  
31.0

0.555  
+1.14





1239 0 14.3 +61 15 5.8 964 -3.66

145 12<sup>m</sup> GC -0002 ± 3.2 +003 ± 2.3

GC329 20<sup>m</sup> -0006 +003

A222

0 14 15,039 1889.9 +61 15 20.14 1850.5  
0.12  
0.051

5.72 x 43.25 = 247.18  
12.216 x 15.2 = 185.68

12 5-4.40  
1 20.230  
14 14.830  
15.020

6 59.7  
8 20.32  
15 20.11  
19.91  
2.4  
20.2

0.22  
-0.29  
36.4  
46.5

20.09 36.4  
+ 1.13 45.4

15,025<sup>0</sup>

Wash

20.01 1945.00

-0.3  
19.98

1324  
HR 64

0 17.4 -59 03 F5

GC337

4.76 + 0.46 + 0.06 C

283 245 444 2.649 (3) 1,3,7,6

263 215 605 2599

[ $Q_{11}$ ] 296

<sup>n</sup>  
4.74 +34 -16.8 +13

[ $G_{11}$ ] 387

+3 -3 +1 / 10 m.

<sup>n</sup>  
+086

<sup>n</sup>  
-081 -12.5

1324 00 14.6 -79 03 -013  
-021

60337 +0301+6.7 -038

37362 95.0+6205 28.38 89.5  
-4656  
35706 2.20  
26.08

37083 85.94 2745  
-24 0  
36859

980 9999 0865 36 957  
-0275  
-114

1186 -0164 -114  
0890  
0556 0563  
056-020 -0140  
-15. 900

40  
 1324 00 14.6 - 79 03 F2 ~~12.5~~ 4  
 Cays

06337 6.76 + 0.46 (1.62)

1086-030 " 10.059 - 0.017 CP (60)

$$\begin{array}{r} 10301 \pm 6.7 \\ + 10044 \pm 17.5 \\ + 0260 \\ + 0285 \\ \hline 10301 \end{array}$$

$$\begin{array}{r} 038 = 5.7 \\ - 027 \\ - 030 \\ \hline 28.38 \\ + 2.30 \\ \hline 26.08 \end{array}$$

$$\begin{array}{r} 1848.0 \\ - 027 \\ - 030 \\ \hline 1889.5 \end{array}$$

38.90

(64)

$$\begin{array}{r} 36.2 \\ 37.362 \\ - 1656 \\ \hline 35.706 \end{array}$$

~~1086 - 029~~

$$\begin{array}{r} 47.33 \\ 20.238 \\ 7.54 \\ \hline 1929.65779 \end{array}$$

$$\begin{array}{r} 30.387 \\ 65.09 \\ 36.8014 \\ + 1.236 \\ \hline 36.0542 \\ - 0.542 \\ \hline 35.512 \end{array}$$

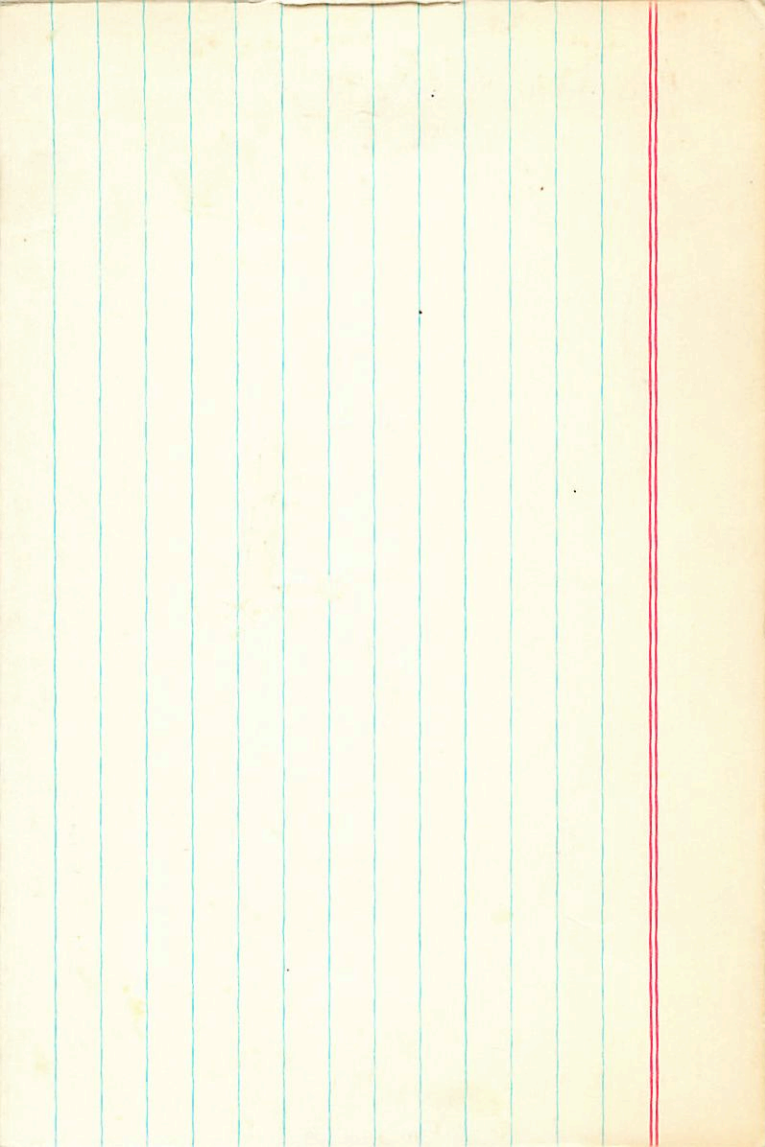
$$\begin{array}{r} 27.0 \\ + 0.2 \\ \hline 26.18 \\ 26.84 / 86 \end{array}$$

$$\begin{array}{r} 27.088 \\ - 0.03 \\ \hline 27.058 \\ - 0.97 \\ \hline -0.97 \end{array}$$

$$\begin{array}{r} 1.41 \\ - 0.68 \\ \hline 0.73 \end{array}$$

$$\begin{array}{r} 1.41 \\ - 0.68 \\ \hline 0.73 \end{array}$$

$$\begin{array}{r} 1.41 \\ - 0.68 \\ \hline 0.73 \end{array}$$



W 148/9 00 14.8 +16 14

-3.3

ABS 237

4.5035

$$+0.033 - 0.007 \text{ Yade}$$

$$-5 + 2$$

$$+2 + 5$$

$$+0.030 \pm 5 - 0.10 \pm 3.6$$

0

$$+2$$

$$-0.08$$

H0 1309

55 pA.

79.4 pA.

966	430	252	+1722	-0164	+1298	+1082	-0.8	+9.4
-482	588	650	-0820	-0250	-1070	8.5	-2.1	-9.0
-131	684	-717	-0222	-0292	-0514	4.4	-2.4	-0.7

$$+0.043 - 0.008 \text{ GC} \rightarrow N30$$

$$+0.033 - 0.009 \text{ MAN} \rightarrow$$

$$+0.036 - 0.009$$

$$+0.028 + 0.005 \text{ Y} \rightarrow N30$$

$$+0.043 - 0.008 \text{ GC} \rightarrow N30$$



+0030 55.1 -0.010 ± 3.6 6.20  
+0023 -0.011

14 47.085 96.4

$$\begin{array}{r} 14 \\ \hline 47.085 \\ \hline 96.4 \end{array}$$

+16 13 57.42 87.6  
6.2

$$\begin{array}{r} 58.04 \\ \hline \end{array}$$

47.022

1935.4

84

47.02

38.3

$$\begin{array}{r} 57.51 \\ \hline 57.56 \end{array}$$

1430.0

$$\begin{array}{r} 47.02 \\ -0.07 \\ \hline 46.95 \end{array}$$

$$\begin{array}{r} 57.47 \\ -2.0 \\ \hline 55.47 \end{array}$$

$$\begin{array}{r} 57.50 \\ \hline 57.53 \\ \hline 1.51 \end{array}$$

19347

990k

$$\begin{array}{r} 47.012 \\ \hline 46.988 \end{array}$$



A05235

1317

150/1

66340

38Pec

0 14.8 10F 36

+35.88  
+35.98

+37.8

2.6 } acc  
2.6 }

7.7 Fo

+0504052.60

6L

+0053 ± 2.1 +082E1.8

+0049 +082

0 14 49.820 1893.7 +8 35- 52.16 1885.8

-248  
1.522

5.26  
46.90

km, 50  
193460

49.715  
-726

51.09  
51.18

37.6

49.740  
-010  
1.750

.738  
216  
43.9

50.95  
+17  
51.12

1440.61

51.15  
4.25

57.8

0 1 0 1 4050 + 052 + 37.5 0 0 385  
0 0 050 0 0 379 + 325 + 35 0

+35 +35 +35

01

[+5-4 +30 -21]

+35 +19 +19

02

[+29 +24 -25]

ST 600  
1306

0 14.9

+0030 ± 10.2  
+0026  
+50 01  

---

+0030  
+2  
+016

344  
250 N = 436

W 152 52.758 19188

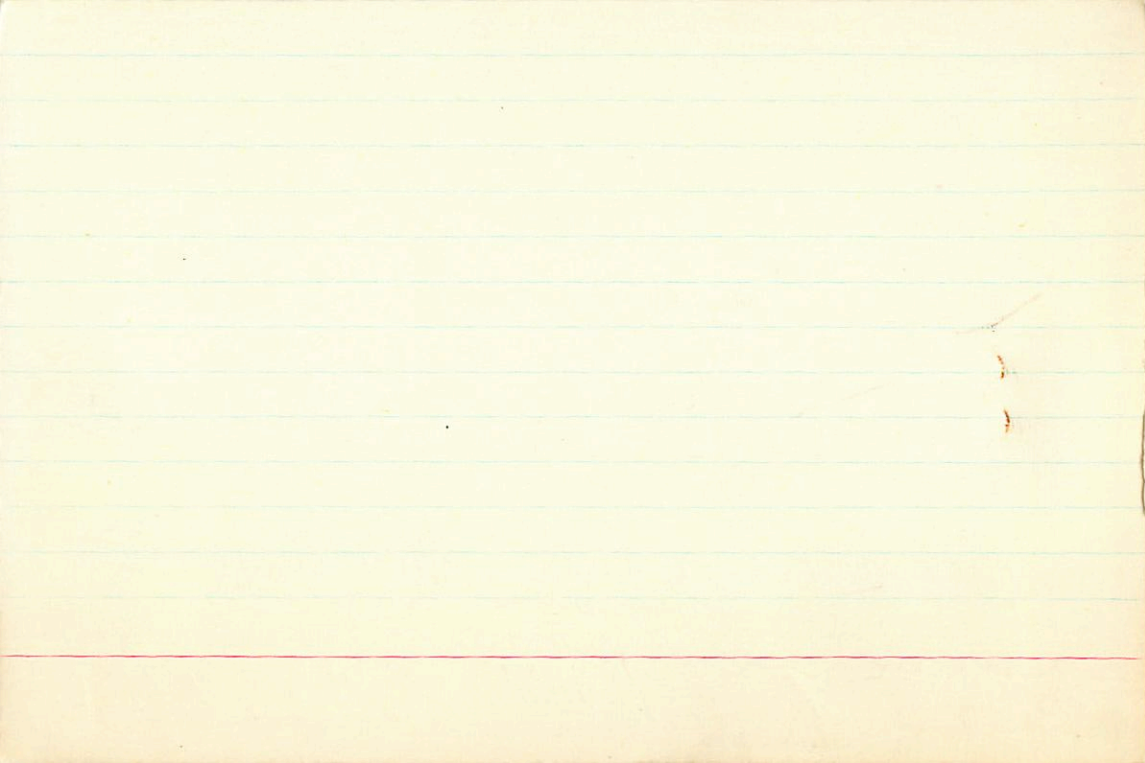
$\frac{-11.2}{.642}$

+50 0 35.06 1917.5  
 $\frac{-1.0}{34.96}$

69  
192  
19

5-2.09  
 $\frac{11}{.701}$

85.7 1940.50  
 $\frac{-1.5}{35.55}$





546 340 280 x

-21

22

-76-12 ③

DAD 2, 1

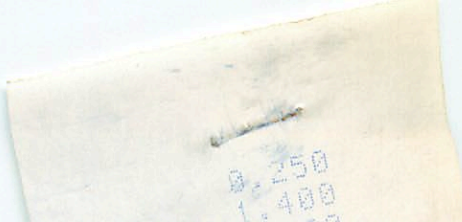
DAD 1, 9

A. J. J. J. 34

Sym -76-11 2







100  
100  
100  
100

+43.44

0

10.1

+43

12

85

Y 49

0

12.7  
15.1 4.5

+43  
+43

27  
43.67

+110 (7)  
~~110 (7)~~

HD 1326 GC 358

7.06 + 0.875 STJ

ADS 240 AB 5m = 3m Adm 2 (2) 8.09 + 1.56 + 1.24 5m MIT + 11C  
8.2, 10.6, 39: Kumpel B 1m 4 (2) 11.05 + 1.80 + 1.40 5m MLC + 20.76 5-w

A Sp. B<sub>1</sub>

29% = 11.44 9.60 + 1.22 STJ  
M + 293 (10)  
YK + 266 (6)

G.L. + 2.87M + 0.400

7.6 M2 + 10.7

+ 2.900 + 0.398

1960.18 5<sup>2</sup> 2.0 4205 10E  
1973.45 53.40 39.64 4 0E  
1882.67 54.57 39.41 2 0E  
1907.49 56.47 39.93 5B  
1958.65 60.3 37.09 2B

2.790 + 2.99 VVR

291A (10)

266Y (10)

278-7

8.07 7.03 + 0.88 R  
11.04 9.60 + 1.22 R

(NO)

1352 0 15.2 +16 03 7.4 dFS +7.96

156 +0155 → 220 landing  
GC347 -0155 -024 (H) GC  
23 Pac 223 025

+0449  
+0149 ± 2.1  
+0148

-023 ± 1.9  
-025

0 15 14.039 1898.6 +16 3 13.51 1893.0

1.31  
14.82

-01485 -0255  
24

6m, 50  
193 x 20

01511 -0226  
13.94  
14.04

PRY → 01511 -0226  
2179 -0247  
0016 -0270

6.65

Copy  
1940.89

850  
13,901 +577

13.02  
+06  
13.08

sub

845

13.56  
-1.26

37.5  
44.5

+220-027  
11.8

sub

+600

-1.26

9928  
1196



27

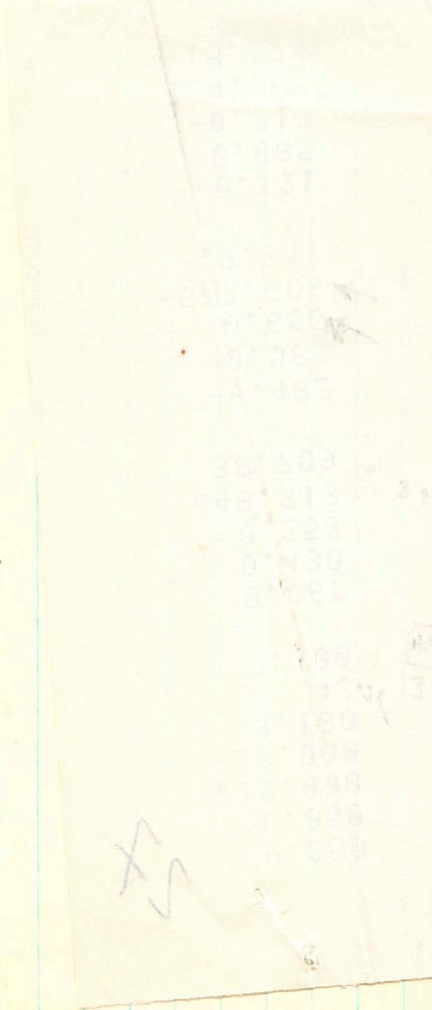
1375 0 15.4 +12 30 6.6 G.S. +2.68

158 23 24

N30 -0008 -018  
BLON #30 -001364 -018 ±5.1

-0010

SS



G And

1404

164

GC302

0 15.7 +36 30

4.5 Am - 8.01

N30 -0057 ~039

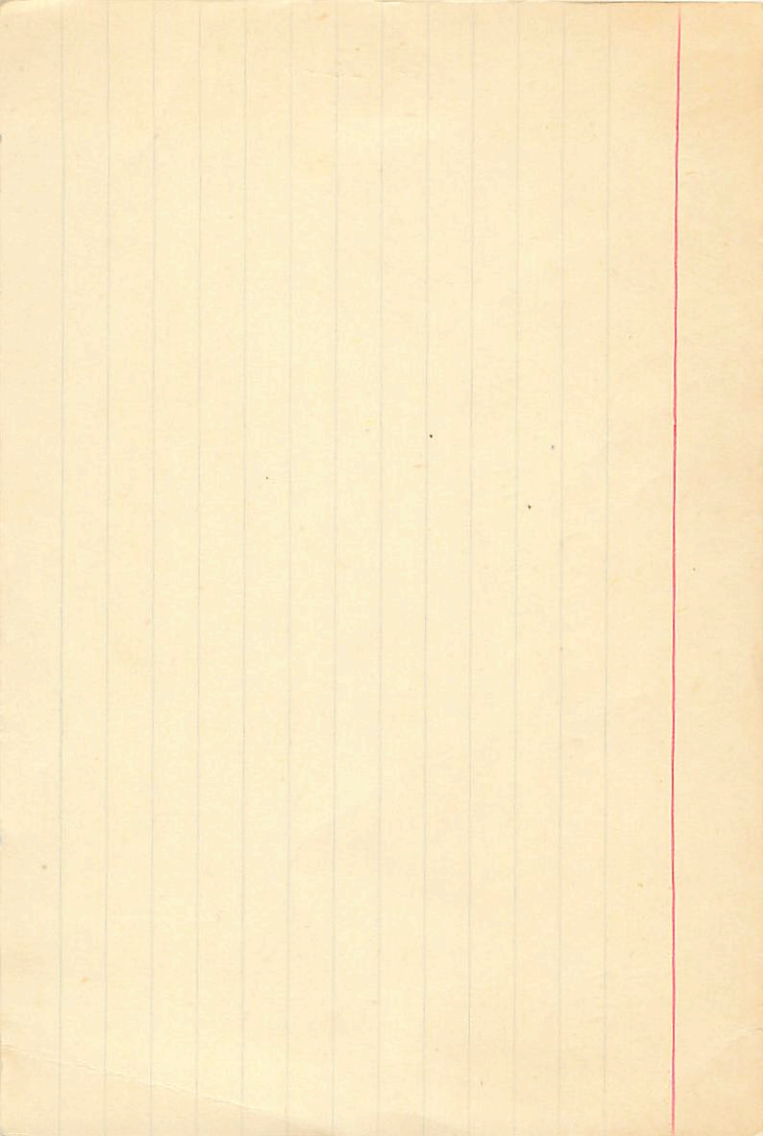
GC  
CONTINIO -0055 ± 1.9 -034 ± 1.6

1962  
1961

-6486

-7612







10/31

0 15.8 -21 25

7) +14.8 ± 2.6

1431

6.68 - 0.01 + 1.41 AVE

+23.7 (8)

Change

ADG 251 6.0 } 0.8  
8.0 } -0.06 ± 10.6 1005 ± 9.5

-0.43 -0.19 Y

62367

-0000 -009

0	15	45.069	1501.2	-21	24	57.52	1500.0
						-25	
						57.27	

026  
098

14	29.145
1	15.988
15	45.133

32	78.25	1533.13
8	20.12	
24	58.13	

15	45.0276	094
	1104	
	-0.92	
	1092	

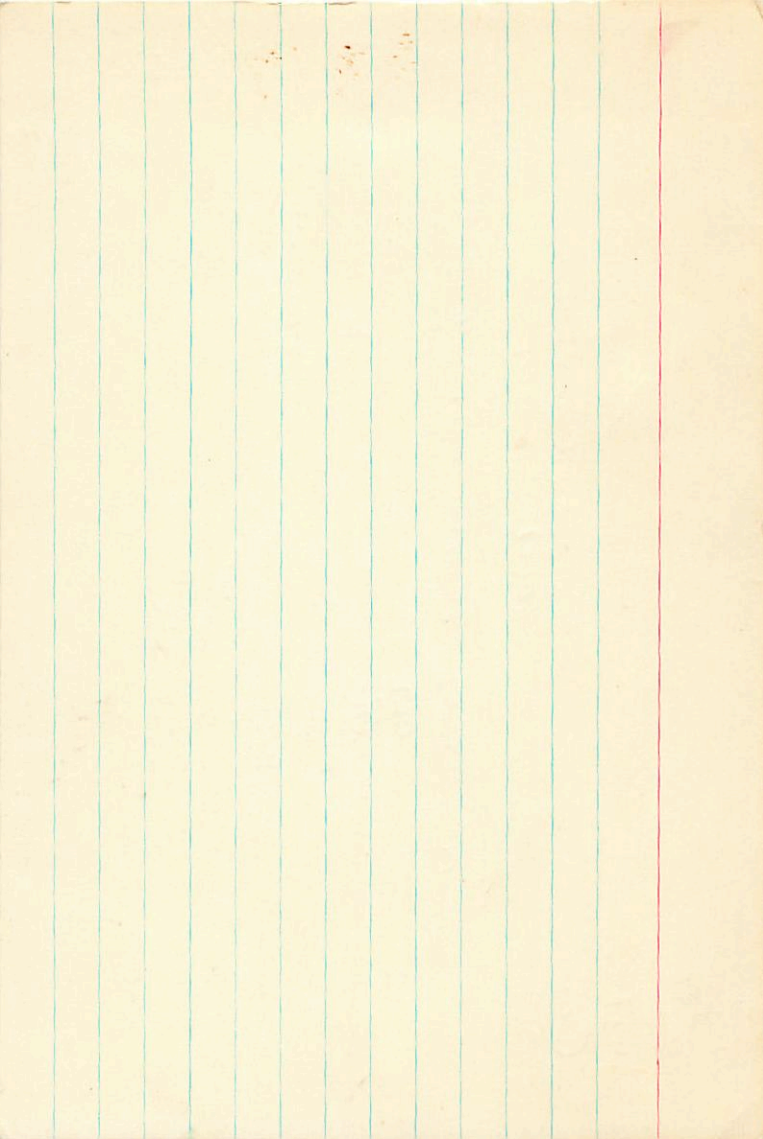
58.25	1533.4
+21	
59.04	

-1397 -1004

58.32 +24 1533.73

15	45.110
	-11
	45.099

58.08	58.06
	-1.2



+61032

1400

0 15.8

+61 56

7.1 dms

-30d 10

368

167

45.653

1918.8

+61 55

32.64

1907.2

$\frac{033}{1686}$

5 A

$\frac{-0.73}{21.91}$

6.96 + 1.54 + 167

45.637

31.86

1916.42

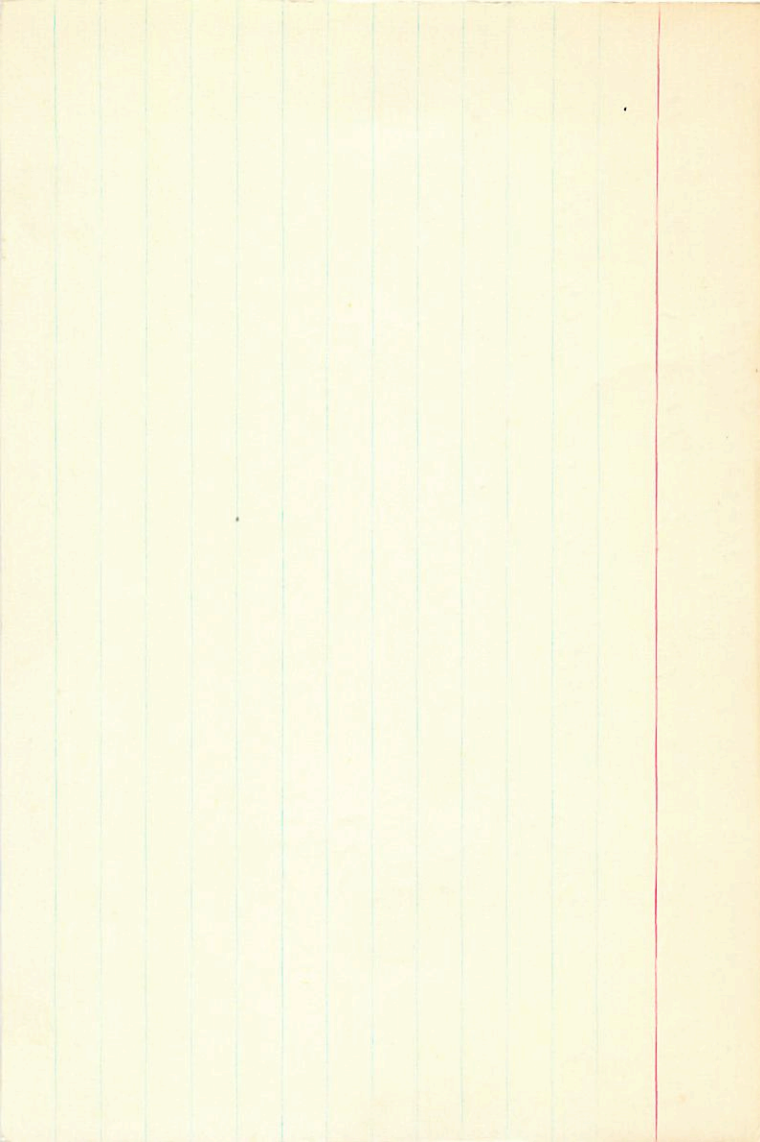
$\frac{001}{16234}$

$\frac{-33}{31.83}$

1915 1915

0880 0880

26.5  
20.2







1438 0 16.1 +43 31 6.0 B9 +708

171

15 20

N30

+0018 -003

GC376

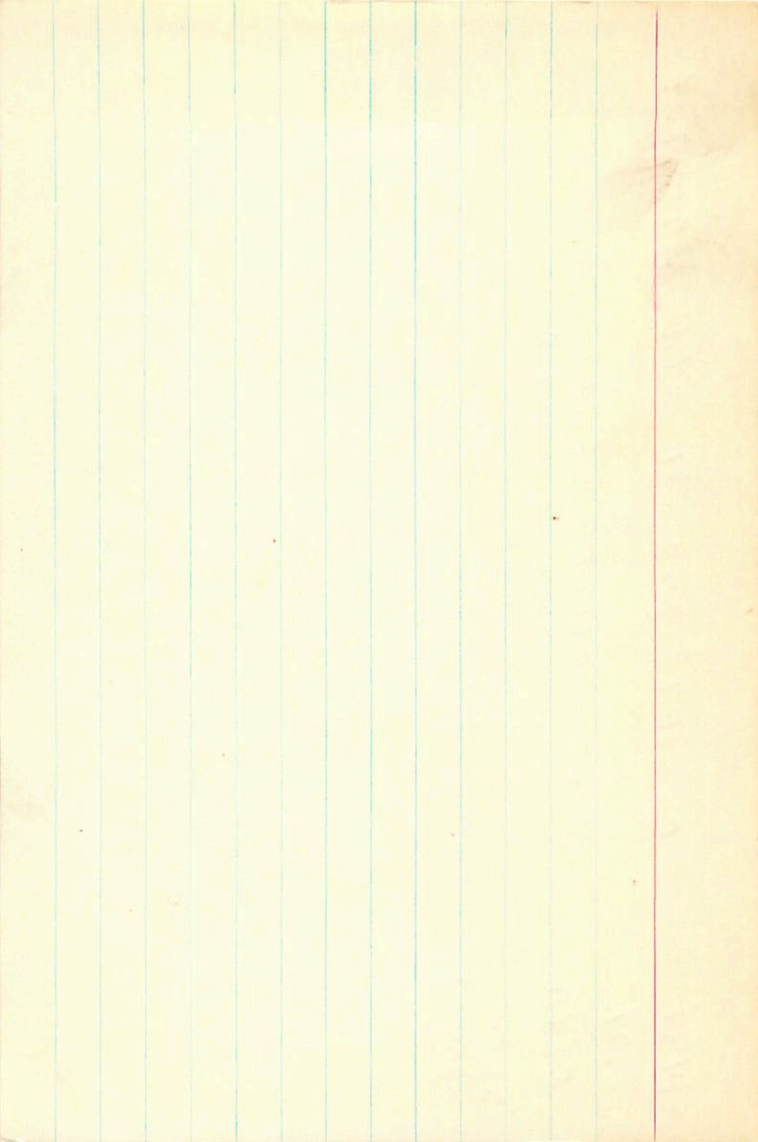
+0013 ± 23 000 ± 1.8

2 L And

10<sup>m</sup> 6"

A05254





1450 0 16.1 +25 43 8.8 dF4 +10.76

173 1.5  
G-C379 +0017±4.5 -035±2.9 9.0 dF4 +10.76  
+10.76

AOS257

0 16 7,476 1505.8 +15 42 47.24 1893.5-  
-075  
1401  
1.98  
49.22

1449

OV 16.0

+ 22

36

+ 11.7

66397

7.14 5.45 2.91 380 ① Plum

TUlas

0

16.6

+58

52

+1.58

+55030

+01484

$\rho = 1.813$

$\rightarrow +0.0021 + 0064 \rightarrow$   
 $+016$

$m - M = 6.5$

$L = 81$

$n_1 = 0.28$

$n_1 = +15$

$n_2 = 0.31$

$n_2 = -6$

$\Delta_m = 3.6$

$n_3 = +4$



+58030

TV 600

H01486

175

+0029 +005

+ 1

- 2

- 6

+0021

+016

+0045 ± 8.4

16.6

0

+58

52

+1.58

00000

36.134

+58 41 41.24

19193

+023 1005 Y1

-138

27 21.2

41.51

20

41.2

19.94

41.27

41.41

1946.87

42.17

-26

41.91

+40

1929.7

5.09

41.41

16 36.028

-016

.012

+086

+020

35.96

867

95997

023 997  
~~957-093~~

855 518 +023+005 +15 004 +1 012

-001 0 023 004 -024 109 +0.5 +1 0

-7 +36 +5 003

-9 +44 +6 0025

+41 -19 +4



(73)

46202 00 16.7 -22 37 12.8 099 102

$$11.48 + 0.745 + 0.22 \textcircled{1}$$

286

73.000\*

0.000\*

16.700\*

-22.000\*

-37.000\*

0.095\*

-0.020\*

5.400\*

120.226

0.000

0.343

-0.066

41.201

-0.300

0.137

-36.102

-0.064

-0.988

-7.741

68 III

1501 0 16.8 +26 11 7.7 G-0 -10.9 6

176

N30 -0009 -0007

G-6385 G-6400 ± 0.0 -0014 ± 7.8 -0008 ± 5.1

-0011 -0007

